## GZA Geolanvironmental, inc

# FINAL IPEC QUARTERLY LONG-TERM GROUNDWATER MONITORING REPORT QUARTER FOUR 2009

(REPORT No. 8)

## INDIAN POINT ENERGY CENTER BUCHANAN, NEW YORK

#### PREPARED FOR:

### **ENTERGY NUCLEAR NORTHEAST, INC.**

Indian Point Energy Center 450 Broadway Buchanan, New York 10511



#### ON BEHALF OF:

ENTERGY SERVICES, INC.
INDIAN POINT ENERGY CENTER
295 BROADWAY, SUITE 3
P.O. BOX 308
BUCHANAN, NY 10511-0308

#### PREPARED BY:

#### GZA GEOENVIRONMENTAL OF NEW YORK

440 NINTH AVENUE, 18TH FLOOR NEW YORK, NEW YORK 10001

NOVEMBER 23, 2010 FILE NO. 01.0017869.92



Copyright C 2010 GZA GeoEnvironmental of New York

#### GZA GeoEnvironmental, Inc.

November 23, 2010 File No. 01.0017869.92 Engineers and Scientists

Mr. Patrick Donahue Indian Point Energy Center 295 Broadway, Suite 3 P.O. Box 308 Buchanan, NY 10511-0308

One Edgewater Drive Norwood Massachusetts 02062 781-278-3700 FAX 781-278-5701 http://www.gza.com Re: FINAL IPEC Quarterly Groundwater Monitoring Report Quarter Four 2009 (Report No. 8)

Indian Point Energy Center

450 Broadway

Buchanan, New York 11501

Dear Mr. Donahue:

GZA GeoEnvironmental of New York (GZA) is pleased to provide this Quarterly Groundwater Monitoring Report for Indian Point Energy Center located at 450 Broadway, Buchanan, NY.

We trust that this information satisfies your present needs. Should you need any additional information, please do not hesitate to call us at (781) 278-3805.

Very truly yours,

Very truly yours,

GZA GEOENVIRONMENTAL OF NEW YORK

Josh Simpson Engineer I

David Rusczýk, PE Senior Project Manager

Attachments: 3 Copies

Michael Powers, PE Consultant/Reviewer

Matthew J. Barvenik, LSP Senior Principal



#### **TABLE OF CONTENTS**

				Page
1.0	EXEC	UTIVE S	UMMARY	1-1
2.0	SCOP	E OF W	ORK	2-1
	2.1	Ground	water Elevation Measurement	2-1
	2.2	Ground	water Sampling	2-1
	2.3	Vapor C	Containment Building Foundation Drain Sampling	<b>2-</b> 2
	2.4		e Mid-Quarter and Confirmatory Sample Collection	
	2.5	Prevent	ative Maintenance	2-3
3.0	DATA	EVALUA	ATION	3-1
	3.1	Ground	water Mass Flux Computation	3-1
	3.2	Ground	water Sampling	3-3
		3.2.1	Groundwater Sampling Results	3-3
	3.3	Radionu	uclide Release Rates	3-3
	3.4	SSCs a	nd Property Boundary Monitoring	3-4
		3.4.1 I	Previous Q3-2009 Investigation Level Exceedances	3-6
			Q4-2009 Boundary Investigation Levels	
			Q4 2009 SSC Investigation Levels	
			Conclusions - Boundary and SSC Leak Detection Monitoring	
	3.5	Plume N	Natural Attenuation Monitoring	3-12
		3.5.1 l	Unit 2 Tritium Plume Attenuation	3-13
		3.5.2 l	Unit 1 Strontium Plume Attenuation	3-17
4.0	CONC	LUSION	IS AND PLANNED ACTIVITIES	4-1



## FINAL QUARTERLY LONG-TERM GROUNDWATER MONITORING REPORT Q4 2009 (REPORT NO. 8)

#### **TABLES**

Table 1 Groundwater Sampling Methods, Equipment, Frequency, and Depths
 Table 2 Historic Quarterly Low Tide Groundwater Elevations
 Table 3 2009 4th Groundwater Analytical Results and Averages
 Table 4 2009 4th Quarter Groundwater Analytical Results and I.L.s
 Table 5 Historic Groundwater Analytical Results

#### **FIGURES**

Figure 1 Site Location Plan Figure 2 Site Plan Figure 3 Lower Hudson Valley Geologic Map Figure 4 Current and Potential Future SSC Source Locations Figure 5A Long-Term Transducer Monitoring Evaluation Map 4th Quarter 2009 Average Tritium Activity Map Figure 6 Temporal Trends in Unit 2 Rolling Average Tritium Activity Maps Figure 6A Figure 7 4th Quarter 2009 Average Strontium-90 Activity Map Figure 7A Sr-90 Baseline Analysis - Unit 1 Defueling Evaluation Figure 8 4th Quarter 2009 Average Cesium, Cobalt, and Nickel Activity Map

#### **APPENDICES**

Appendix A: Limitations

Appendix B: Transducer Installation Logs

Appendix C: Chains of Custody

Appendix D: 4th Quarter 2009 Sampling Data Sheets

Appendix E: Post-Q4 2009 Mid-Quarter Sampling Data Sheets

Appendix F: Dose Calculations

Appendix G: Unit 2 Tritium Plume Trend Analyses

Appendix H: Southern Boundary Wells



## FINAL QUARTERLY LONG-TERM GROUNDWATER MONITORING REPORT Q4 2009 (REPORT NO. 8)

#### 1.0 EXECUTIVE SUMMARY

On behalf of Entergy Nuclear Northeast, Inc., GZA GeoEnvironmental of New York (GZA) has completed the Q4 2009 quarterly groundwater monitoring for the Indian Point Energy Center (IPEC), culminating in this report. Interpretations of the monitoring data have been made in the context of the current Conceptual Site Model. Development of this model began at the outset of the site investigations and has been iteratively enhanced as subsequent data has become available, in part through quarterly monitoring. The report has been written with a focus on the most recent quarterly data. Relationships to prior data and more in-depth technical explanations have typically been relegated to footnotes. This report format was chosen to allow efficient assimilation by those already familiar with the project. The footnotes contain important information and should be carefully read by all, but particularly by those less familiar with the technologies involved and the project history.

Based on the quarterly groundwater sampling data for Q4 2009, GZA concludes that groundwater contaminants continue to migrate toward the Hudson River to the West, and have not migrated off the Site to the North, East or South.

Radionuclide concentrations measured during Q4 2009 were combined with previous quarterly and post-quarterly data to compute rolling average concentrations reflective of groundwater contaminant levels over the past twelve months. These data were multiplied by the associated individual zone-specific groundwater flux values, derived from the recalibrated Precipitation Mass Balance Model<sup>1</sup>, to compute yearly average radionuclide release rates to the Discharge Canal and Hudson River. The Conceptual Site Model (CSM) continues to be validated through: (1) Precipitation Mass Balance Model calibration analyses, as based on groundwater elevation data collected in 2007, 2008, and 2009<sup>2</sup>; (2) the behavior of both the Unit 1 Strontium plume and the Unit 2 Tritium plume as evaluated each quarter; and (3) additional tracer data collected in 2008/2009. These data, in our opinion, continue to support the use of the current CSM as a basis for Long Term Monitoring Program design.

• From both qualitative and quantitative perspectives, the most recent quarterly data further support the conclusion that the overall Tritium activity in the Unit 2 plume is decreasing. These reductions are evident in this quarter, as shown on Figures 6 and 6A where the shaded plume<sup>3</sup> does not extend downgradient of MW-37 (and thus, no longer extends to the river), as first seen in the Q2 2009 quarterly report. It is further visually evident from Figure 6A that the core of the plume has also shown a marked decrease in concentration and extent over time; this Q4 data set is the first time since monitoring began where the 50,000

November 23, 2010 10-11-23 FINAL LTM 2009 Quarter Four Report.docx Page 1-1

File No. 01.0017869.92

<sup>&</sup>lt;sup>1</sup> Refer to Appendix H of the Quarter 2 2009 Quarterly Long-Term Groundwater Monitoring Report for discussion on the recalibration of the Precipitation Mass Balance Model. Precipitation and groundwater elevation data were collected onsite between 2007 and 2009 and used to compute groundwater fluxes across the site. The precipitation data from 2007-2009 sufficiently encompassed the historical variability of precipitation. Therefore, maximum onsite fluxes were calculated from the groundwater elevation data, and used to conservatively recalibrate the Precipitation Mass Balance Model, as discussed and employed in the Q2 2009 Quarterly LTM Report.

The formulation and basis for the Precipitation Mass Balance model, as well as the overall CSM, is presented in the Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc, on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value. This plume delineation boundary value equates to one-quarter of the drinking water standard for Tritium. Although GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site, the MCLs do provide a useful benchmark for comparisons of relative human risk. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

to 100,000 pCi/L shaded isopleth has retreated upgradient of MW-111. These findings are consistent with our CSM, which anticipates overall decreasing trends in Tritium activity. Consistent with one of the purposes of this Report, we also point out and explain data which, when first considered, may initially appear inconsistent with the assumptions used to develop the CSM. Such examples, where Tritium has increased in recent quarters, include: After a period of relatively low levels, a noticeable increase in Tritium activity was observed in MW-31-49 during the Q4 2009 sampling event. Similar variations in Tritium levels have been observed in MW-31 and MW-32 since Q1 2009, and to a lesser extent since monitoring began. The variability exhibited by the Tritium data from these wells is consistent with episodic releases of Tritium historically stored in the subsurface via natural and anthropogenic Retention Mechanisms<sup>4</sup>. This conclusion is further supported by the tracer data and other analyses discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report.

• A transient leak associated with the waste distillation tank valving within the Unit 1 FSB was identified and immediately repaired. Multiple monitoring installations proximate to, and downgradient of, the U1 FSB indicated temporal Tritium perturbations during the last few quarters, likely as a response to this transient leak<sup>5</sup>. These locations have all decreased below their I.L.s with Tritium levels at or approaching previous activities. Based on the observed data trends, it appears that the Tritium input into the groundwater flow regime from the waste distillation tank valving leak has generally dissipated through the system, at least down to the discharge canal.

The overall <u>Sr-90 activity within the Unit 1 plume</u> had generally been stable or decreasing in response to the West Pool demineralization activities conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs resulted in a noticeable increase in Strontium levels proximate to the SFPs, as well as indications of downgradient increases in Strontium plume activity (see **Figure 7** and **7A**). This is as was predicted given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing leakage rate from the SFPs<sup>6</sup>. As expected, the levels proximate to the pool have since decreased and it is expected that levels downgradient of the pool will also return to pre-defueling levels as this additional strontium contaminated water flushes through the groundwater flow system. It is anticipated that this flushing mechanism will be protracted given the impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also resume an overall downward trend once this transient perturbation has passed through the system.

Based on the data and analyses provided herein, our conclusion is that the Tritium and Strontium plumes are both undergoing overall long-term reductions in activity. Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP<sup>7</sup> and has decommissioned the Unit 1 SFPs, these plumes satisfy the requirements for

<sup>&</sup>lt;sup>4</sup> These Retentions Mechanisms are discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report.

<sup>&</sup>lt;sup>5</sup> While the I.L. exceedances proximate to the U1 FSB appear more clearly related to the valving leak, exceedances farther downgradient may also be associated with the peaks in MW-31 and MW-32.

<sup>&</sup>lt;sup>6</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

<sup>7</sup> Further institution of a contractive source of radionuclides to the subsurface.

Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the more recent behavior observed in the Unit 2 collection box data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms. In this regard, it is noted that these analyses cannot definitively and completely rule out

Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. However, it is also concluded that, while a portion of the leakage from the above cited localized events traveled directly to the saturated groundwater regime and resulted in the observed transient "peaks" in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events). These localized release events also interfere with the goal of resetting Site Investigation Levels (I.L.s); updating of Strontium I.L.s must therefore await return to the original Strontium baseline levels existing prior to Unit 1 defueling, and additional seasonal data is required to better assess Tritium response to precipitation-driven Retention Mechanism release variability. Therefore, the ultimate confirmation of the above conclusions will require monitoring over a number of years so as to allow ranges in seasonal variation to be adequately reflected in the monitoring data and thus demonstrate continued depletion of Tritium and Strontium from the Retention Mechanisms.

In summary, based on the data collected to date, the apparent strength of the CSM to evaluate that data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).

the possibility of a remaining small leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s). While it is not possible to quantify the size of the minimum detectable leak with any degree of certainty, we believe that the maximum leak rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time. This opinion is based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of more than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program; this amount of Tritium release to the river is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

November 23, 2010 10-11-23 FINAL LTM 2009 Quarter Four Report.docx Page 1-3



#### 2.0 SCOPE OF WORK

During Q4 2009, GZA performed groundwater monitoring activities at IPEC in Buchanan, New York (Site) as part of IPEC's overall Long Term Groundwater Monitoring Program (LTMP) at the Site<sup>8</sup>. The overall foundation for the development and execution of this LTMP is based on the CSM, a description of which is contained within GZA's Hydrogeologic Site Investigation Report<sup>9</sup>. The scope of work completed for this quarter's monitoring is described in the Sections below. Refer to **Figures 1 and 2** for a Site Location Plan and Site Plan. **Figure 3** provides a Lower Hudson Valley Geologic Map and **Figure 4** summarizes Current and Potential Future SSC Source Locations.

#### 2.1 Groundwater Elevation Measurement

GZA maintains a network of long-term monitoring transducers and dataloggers as part of the instrumentation located across the Site. These instruments record groundwater elevation and temperature measurements at regular time intervals<sup>10</sup>, which are then downloaded on a quarterly basis<sup>11</sup>. Transducer installation logs are presented in **Appendix B**.

During the quarterly sampling, GZA downloaded groundwater elevation data from the long-term monitoring transducers, which collected data over the entire duration of the quarter. The low-tide groundwater elevation data during Q4 2009 (11/28/2009) from these 22 transducers are presented in Table 2 and compared to historic minimum and maximum values on Figure 5A<sup>12</sup>. These data demonstrate that substantial variations to the observed flow field have <u>not</u> occurred. These data thus further validate the applicability of the Precipitation Mass Balance Model (PMBM) for use in subsequent radiological dose computations – see Section 3.1.

#### 2.2 Groundwater Sampling

During Q4 2009, GZA collected groundwater samples for radionuclide analysis from scheduled sampling intervals within select monitoring installations ("wells") as shown in **Table 3**. Chains of Custody for these samples are presented in **Appendix C**.

November 23, 2010 10-11-23 FINAL LTM 2009 Quarter Four Report.docx Page 2-1

<sup>&</sup>lt;sup>8</sup> Refer to the "Final Quarterly Long-Term Groundwater Monitoring Report Q2–Q4 2007 (Report No. 1)," dated May 2008 for Site background information and a description of the environmental setting.

Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc., on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

Currently, transducers record groundwater elevation and temperature readings on a 20 minute time interval so as to allow capture of tidal variability. An original, more extensive network of pressure transducers provided critical data inputs for the development of the CSM and the computation of yearly radiological dose to the Hudson River. Over the first nine quarters of the LTM program (Q2 2007 through Q2 2009) sufficient data was collected from this more extensive network of transducers to capture groundwater elevation response to seasonal and yearly precipitation variability. Therefore, starting with the Q3 2009 quarterly report, the transducer monitoring program was refocused on a select subset of locations to routinely monitor the on-Site groundwater conditions going forward. These locations were selected to provide the data required to document that groundwater flow conditions remain consistent with the CSM, thus demonstrating the veracity of the subsequent dose computations. The rational for the specific locations and depths included in the LTMP transducer redeployment are provided in Appendix K of the Q1 2009 Quarterly Monitoring Report (Report No.5), dated July 2, 2010 and Appendix J of the Q2 2009 Quarterly Monitoring Report (Report No.6).

With regard to these ongoing long term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data is collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

<sup>&</sup>lt;sup>12</sup> Figure 5, which previously presented shallow and deep groundwater contours, can be found in quarterly reports prior to, and including Q2 2009. This figure is no longer required given that sufficient quarterly contour data has already been obtained (See Q2 2009 for further analysis).

GZA used a number of different types of pumping equipment depending upon the sampling method and the characteristics of the individual monitoring installation<sup>13</sup>. **Table 1** lists the monitoring installations sampled, the sampling depths and elevations within sampling installations, and the sampling method and equipment used.

In general, GZA implemented two basic methods of sampling to collect representative groundwater samples: the Low Flow method and a modified well volume purge method. The Low Flow method allows collection of representative groundwater samples from discrete sampling zones within a monitoring installation, while limiting the accumulation of wastewater<sup>14</sup>. As agreed by Entergy Nuclear Northeast, the NRC, NYSDEC, and GZA, the modified traditional purge method<sup>15</sup> allows for the collection of a representative groundwater sample from a monitoring installation after purging 1.5 volumes of water<sup>16</sup>. We implemented this method in wells where low flow sampling was not practical. Sampling Data Sheets summarizing water quality data and sampling information are presented in **Appendix D**.

With all of the above sampling methods, GZA used dedicated sampling equipment, including polyethylene and/or nylon tubing and submersible electric pumps to the extent practical. The use of dedicated sampling equipment limits the possibility of cross-contamination between monitoring installations and/or individual multi-level samples within a single installation. Refer to **Table 1** for a summary of the sampling methods, equipment, frequency, and depths employed during this quarter's groundwater monitoring round.

#### 2.3 Vapor Containment Building Foundation Drain Sampling

GZA collected a water sample from manhole MH-5 on-Site to characterize discharge from foundation drains around and below the Unit 2 Vapor Containment Structure. These drains include both the foundation drain around the building periphery ("curtain drain") as well as that around the sump near the middle of the structure ("reactor sump footing drain"<sup>17</sup>). The Q4-2009 results for MH-5 indicate a decrease in Tritium levels by a factor of two when compared to the previous sampling results (Mid-Q2-2009 and Mid-Q3-2009); all other radionuclides were non-detect.

#### 2.4 Proactive Mid-Quarter and Confirmatory Sample Collection

No Proactive Mid-Quarter or confirmatory samples were collected Post Q4 2009.

<sup>&</sup>lt;sup>13</sup> Refer to Section 4.3 of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1, dated May 2008, for sampling method and equipment selection rationale.

<sup>&</sup>lt;sup>14</sup> As described in: Low-Flow Sample Collection, GZA, 7/18/2007

As described in: Modified Traditional Groundwater Sample Collection, GZA, 7/18/2007

<sup>&</sup>lt;sup>16</sup> When external factors (such as well-surface-flooding from storm water runoff or overland flow of plant component leaks) might have infiltrated the top of the well and impacted ambient groundwater conditions at a specific sampling location, GZA typically purged three to five volumes of water (using the modified traditional purge method) prior to collection of a sample to attempt to obtain a representative groundwater sample.

<sup>&</sup>lt;sup>17</sup> We could not verify that a foundation drain exists around the reactor sump in Unit 2. The assumption that it does exist is based on the plans for Unit 3 and the similarities in construction of both units.

<sup>&</sup>lt;sup>18</sup> These two Unit 2 drains which discharge into MH-5, along with similar drains for Unit 3 which discharge into Manholes B-1 and B-6, are being used as an integral part of the early leak detection monitoring network. However, sampling from these three manholes has generally been problematic for a number of reasons, but particularly due to conflicts with plant security measures which mandate that the manhole covers be permanently welded shut. Some limited access has been reestablished by modifying the manhole covers to allow for a small access opening. However, this modification still limits the ability to routinely collect samples representative of the foundation drain discharges rather than just the total flow through the storm drains. Further work is being undertaken on the manholes to facilitate representative sampling of these foundations drains.

#### 2.5 Preventative Maintenance

GZA performed general wellhead maintenance tasks, such as housekeeping of well vaults and roadboxes, and replacement of dedicated sampling equipment, tubing and transducers, as required.



#### 3.0 DATA EVALUATION

The Long Term Monitoring Program was designed to provide data to address four main objectives:

- Monitor radionuclide concentrations and evaluate groundwater flow rate to both detect and characterize current and potential future off-Site groundwater contaminant migration to the Hudson River, both via direct groundwater discharge to the river and through infiltration into the Discharge Canal, from abnormal radionuclide releases of liquid effluents, so as to allow computation of potential radiation dose to the public from these releases;
- Monitor groundwater proximate to Systems, Structures and Components (SSCs) which
  exhibit a credible probability of resulting in a visually undetected release of radionuclides
  to the subsurface carrying an activity level of significance;
- Monitor groundwater along the property boundary to confirm that contaminated groundwater is not migrating off of the property to locations other than the river; and
- Monitor the groundwater plumes identified on-Site to demonstrate overall reductions in total activity over time as is consistent with the requirements of Monitored Natural Attenuation (MNA)<sup>19</sup>, the selected remediation for the IPEC Site.

These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI). The following sections provide data analyses to address these four objectives.

#### 3.1 Groundwater Mass Flux Computation

As presented in the Hydrogeologic Site Investigation Report, the groundwater flow in both the upper and lower flow zones is toward the power block area from the North, East and South, with subsequent discharge to the Hudson River to the West. We estimate that groundwater flow associated with infiltration from the watershed may be as deep as 350 feet, but still ultimately discharges to the river. A corollary to this conclusion is that there is no groundwater flow, and thus no off-Site radionuclide migration from the power block area to the North, East or South.

To estimate groundwater flow (i.e., groundwater mass flux) beneath the Site, a groundwater flow model was constructed based on a precipitation mass balance analysis. This analysis is based on the precept that, on a long term average, the groundwater flowing through and discharging from the aquifer is equal to the watershed infiltration recharge; this conclusion was reached because the only substantial source of recharge to the aquifer is areal recharge derived from precipitation. The previous fifteen year average for precipitation measured at the Site is approximately 36 inches per year. Based on a USGS infiltration study<sup>20</sup> as well as the groundwater flux model calibration discussed below, approximately 25 percent of the precipitation falling on pervious surfaces over the Site watershed area results in infiltration recharge to the groundwater.

<sup>&</sup>lt;sup>19</sup> The selection of MNA as the remedial strategy for the Site is discussed further in the Hydrogeologic Site Investigation Report.

USGS. Water Use, Ground-Water Recharge and Availability, and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002.

The Precipitation Mass Balance Model (PMBM) was initially calibrated <sup>21</sup> to groundwater fluxes based on a Darcy's Law Model with groundwater gradients derived from Q2 2007 (June 1, 2007) groundwater elevation contours <sup>22</sup> (initial reference data set). This calibration not only verified the reasonableness of the overall groundwater flow rates predicted by the PMBM, but also allowed further discretization of the groundwater flow into upper and lower flow zones as well as flow volumes upgradient and downgradient of the Discharge Canal. The PMBM was also recalibrated <sup>23</sup> after collecting the final full set of transducer data in Q2 2009 <sup>24</sup>. Data analyses demonstrated that recalibration to the Q4 2008 data set yielded the most conservative (highest dose to the river) calibration of the nine quarterly data sets obtained during the LTMP, and thus was adopted for further dose computations. The analyses upon which this conclusion is based are provided in the Q2 2009 LTM report.

Since precipitation represents the driving variable for groundwater flux in the PMBM, the yearly precipitation just prior to Q4 2009 (approximately 31.7 inches) was calculated and input into the recalibrated model to compute the flows used in the estimation of Q4 2009 dose values. Based on the USGS study cited above, the aquifer recharge rate is therefore approximately 8 inches for the year prior to the Q4 2009 monitoring event. Applying this value to the pervious surfaces within the six individual groundwater flow zones shown on **Figure 4**, it is estimated that approximately 3.5 gpm of groundwater flowed into the Discharge Canal from the upper and lower zones in the previous year. In addition, approximately 7 gpm of groundwater flowed into the Hudson River from each of the upper and lower zones. Storm water discharging into the Discharge Canal and directly into the Hudson River was estimated to be approximately 36 and

<sup>&</sup>lt;sup>21</sup> The calibration compared the total groundwater flow values for each of the six on-Site flow zones computed independently using the PMBM and the Darcy's Law Model. The two models use different sets of input parameters which are not dependent or related to each other. The groundwater flow computed using the PMBM is based on yearly precipitation amounts and the proportion of this precipitation that results in infiltration recharge to the groundwater. The Darcy's Law Model, on the other hand, is based on the measured groundwater flow gradients (as computed from groundwater elevation contours) and estimates of the formation hydraulic conductivity.

Groundwater elevation snapshots from transducer data at low river tides were used to construct both upper groundwater flow zone (water table) and lower groundwater flow zone (potentiometric head) contours for each quarterly LTM report from Q2 2007 to Q2 2009. The deep zone groundwater contours illustrated a subdued reflection of the upper zone groundwater contours, demonstrating that the anthropogenic effects of the Site are generally shallow. Refer to the Q2 2009 LTM Report prepared by GZA and dated August 12, 2010 and the Hydrogeologic Site Investigation Report prepared by GZA and dated January 7, 2008 for further discussion.

After reviewing the groundwater elevation and precipitation data from the Indian Point meteorological station over the time period from Q2 2007 to Q2 2009, it was concluded that sufficient seasonal data had been collected to encompass the majority of the precipitation variability observed over the last fourteen years (fifty-six quarters); see analysis in Appendix H of the Q2 2009 Monitoring Report. As such, the PMBM was recalibrated. To be conservative, the model was recalibrated to the quarterly data set that yielded the largest total and/or Unit ½ Zone groundwater flows from the Darcy's Law Model (note that the Unit ½ Zone contains the vast majority of the radionuclide impacted groundwater). Based on these analyses, the PMBM was recalibrated to the groundwater fluxes from Q4 2008. While this quarter did not yield the highest total flow through the entire site, it did provide a high total flow and the highest flow through the Unit ½ Zone, and thus the highest computed dose. The recalibration of the model to the Q4 2008 data yielded Unit ½ Zone and total groundwater fluxes approximately 40% and 25% greater, respectively, than the original reference (Q2 2007) data set.

To continue to validate the appropriateness and applicability of the PMBM, a subset of the existing transducers are being maintained and monitored quarterly as part of the Long Term Monitoring Program, starting with the Q3 2009 quarterly report. The primary objective of maintaining these transducers is to provide ongoing confirmatory data that demonstrate substantial changes to the on-Site groundwater flow field have not taken place and thus verify that the basic assumptions inherent in the PMBM continue to remain valid. The transducer locations are provided on **Figure 5A** of this quarterly report, and the rational for the selection of these specific individual transducer locations is discussed in the Q1 and Q2 2009 quarterly reports. With regard to these ongoing long-term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data is collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

3.5 gpm, respectively. These flows can be further subdivided into flow zones with further detail as shown in the table in **Appendix F.** 

#### 3.2 Groundwater Sampling

The following sections describe the groundwater sampling results and associated QA/QC protocols.

#### 3.2.1 Groundwater Sampling Results

Groundwater samples collected on behalf of Entergy during Q4 2009 were analyzed at GEL Laboratories for Tritium, Sr-90, Cs-137, Co-60, and Ni-63<sup>25</sup>. **Table 3** presents the Q4 2009 analytical results for these radionuclides. The rolling yearly averages, which are calculated using all the valid data from the previous year [Q1 09 through Q4 09], including Mid-Quarter and confirmatory samples, are also presented in **Table 3**. **Table 4** presents minimum detection concentrations (MDC), standard deviation, and I.L.s assigned to each well for the Q4-2009 analytical results. **Table 5** presents historic Site groundwater analytical data. Isopleth maps of rolling averages for Tritium and Sr-90 are presented in **Figures 6** and **7**, respectively. **Figure 8** presents a data map of rolling averages for Cs-137, Co-60, and Ni-63<sup>26</sup>.

An overall evaluation of the sample handling, shipment and analytical procedures, indicate that the quality assurance quality control protocols have been met for Q4 2009, and the analytical results should be useable. This conclusion is further supported by a review of the Q4 2009 analytical data, as compared to previous historical trends. Refer to **Section 5.2.2** of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1 for further details pursuant to quality assurance quality control protocols.

#### 3.3 Radionuclide Release Rates

The recalibrated PMBM-derived groundwater flows within each of the six flow zones are multiplied by yearly rolling average radionuclide levels within each zone to compute groundwater radionuclide release rates to the Discharge Canal and Hudson River. These groundwater radionuclide release rates are computed separately for upper and lower flow zones as well as upgradient and downgradient of the Discharge Canal. The selection of specific monitoring locations for each of the six zones is described in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases.

Storm drain flows<sup>27</sup> computed based on yearly precipitation rates are multiplied by radionuclide concentrations measured in the storm drains to compute the associated storm drain radionuclide release rates<sup>28</sup> to the Discharge Canal and Hudson River.

lt should be noted that samples were also analyzed for gamma emitters via gamma spectroscopy. Although only Co-60 and Cs-137 are reported, gamma spectroscopy could detect and identify other gamma emitters if they became present in groundwater.

<sup>&</sup>lt;sup>26</sup> Isopleths were not drawn for Cs-137, Co-60, and Ni-63 because the few positive detections observed did not indicate the existence of a groundwater plume containing these radionuclides. This is likely a result of the high surface affinity (highly adsorptive nature) of these radionuclides for solid geological materials. They therefore tend to rapidly partition out of the groundwater.

<sup>27</sup> The storm drain flows also include groundwater discharges from the foundation drains for Unit 2 and Unit 3 VC Buildings, but not

The storm drain flows also include groundwater discharges from the foundation drains for Unit 2 and Unit 3 VC Buildings, but not from the Unit 1 NCD and SFDS, which are otherwise accounted for.

28 It is noted that otherwise accounted for.

<sup>&</sup>lt;sup>28</sup> It is noted that storm drain samples are not typically taken at times coincident with peak, or even average storm drain flow rates. By its very nature, the vast majority of the flow through the storm drain system tends to be episodic and of short duration due to storm events; sampling rounds are generally scheduled to avoid such events. Radionuclide concentrations are primarily due to groundwater infiltration into the drains and thus tend to be highest during periods of little rain when this infiltration is not diluted by the storm water flow. This incongruence therefore yields a high bias to the dose computation because the elevated concentrations associated with low flow rates are multiplied by the much higher flow rates based on total yearly rainfall.

The radionuclide release rates from the groundwater and storm drains to the Discharge Canal and Hudson River for Q4 2009 are shown in the table below.

	GROUNDWATER AND SURFACE WATER TO RIVER (CI/YR)	GROUNDWATER AND SURFACE WATER TO CANAL (CI/YR)
Northern Clean Zone*	3.10E-04	0.00E+00**
Unit 2 North Zone	0.00E+00***	3.30E-02
Unit ½ Zone	3.25E-03	2.88E-03
Unit 3 North Zone	1.87E-03	4.44E-04
Unit 3 South Zone	1.31E-03	3.88E-03
Southern Clean Zone*	3.29E-03	0.00E+00****

<sup>\*</sup> Activity in the Northern Clean Zone is attributable to an assumed Tritium background concentration of 150 pCi/L in the groundwater. The remaining radionuclides were assumed to not be present in this streamtube. Radionuclide release rate in the Southern Clean Zone is calculated from activity measured in monitoring wells MW-40 and MW-51.

Release rates are then used by Entergy to calculate the radiological dose to the environment via the Discharge Canal and the Hudson River using the procedure outlined in the Liquid Radioactive Effluents (0-CY-2740) document, prepared by Entergy and dated January 12, 2007.

#### 3.4 SSCs and Property Boundary Monitoring

In addition to providing the data for the dose computation discussed above, the Long Term Monitoring Program has been designed to also provide rapid detection of potential leaks from SSCs. This monitoring is specifically focused on those SSCs which exhibit a credible probability of resulting in a visually undetected release of radionuclides to the subsurface<sup>29</sup>. The monitored SSCs are shown on **Figure 4** and a description of the specific monitoring installations associated with each SSC are provided in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases. In addition to monitoring the SSCs, on-Site and off-Site wells are used to monitor the property boundaries for unanticipated radionuclide migration across these boundaries. Again, the rationale underpinning the selection of wells designated for this purpose is provided in the above cited Memorandum. These monitoring protocols are consistent with the NEI Groundwater Protection Initiative (GPI).

<sup>\*\*</sup> The radionuclide release rate to the Discharge Canal from the Northern Clean Zone is zero because the Discharge canal does not extend far enough to the north to be downgradient of the Northern Clean Zone.

<sup>\*\*\*</sup> The zero contribution to radionuclide dose to the river through the Unit 2 North Zone groundwater is due to a model-computed groundwater flow of zero through this zone. This simplified estimate results in an overall high bias to the dose computations, and is therefore conservative as explained further in **Appendix F**.

<sup>\*\*\*\*</sup> The radionuclide release rate to the Discharge Canal from the Southern Clean Zone has been computed to be zero because groundwater in this zone appears to flow under the Discharge Canal and directly to the river. This conclusion has been reached given that the surface water level in the Discharge Canal is, on average tidally, equal to the proximate groundwater elevation, both of which are above the water level elevation in the Hudson River. This approximation results in a conservatively high dose estimation

As discussed further in the following sections, reporting of visually identified spills/leaks within structures is included within Condition Reports under Entergy's Corrective Action Program. Additional emphasis has been placed on routine review of these reports as they potentially relate to GPI objectives.

Entergy is also in the planning process to add an additional multi-level monitoring installation located near the south west corner of the Unit 3 Transformer Yard, downgradient of MW-46<sup>30</sup>. The sampling of U1-NCD and U1-SFDS will also be continued as part of the Long Term Monitoring Program.

I.L.s were established for the associated monitoring wells to set quantitative radionuclide concentrations above which further action would be undertaken. As part of the ongoing groundwater monitoring program, the reported analytical concentrations are compared against I.L.s established based on the criteria shown in the table below. I.L.s are currently computed each year based on yearly averages of all the valid groundwater sampling analytical results of the previous year including Aliquot, Confirmatory, and Mid-Quarter sample results<sup>31</sup>. The monitoring well-specific I.L.s are presented in **Table 4** and are established for comparison with 2009 analytical results based on the quarterly samples collected and analyzed in 2008.

WELL ID	INVESTIGATION LEVELS (I.L.S)				
	TRITIUM PCI/L	SR-90 PCI/L	OTHER PLANT-RELATED RADIONUCLIDES		
Off-Site Boundary Wells (LAF-002)	any detection*	any detection*	any detection*		
On-Site Boundary Wells (MW-40, MW-51, MW-52, and MW-107)	1,000**	2**	any detection*		
Riverfront Boundary Wells (MW-60, MW-62, MW-63)	2,000**	2**	any detection*		
All Other Wells	>2x average***	>2x average***	>2x average***		

<sup>\*</sup> A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

In the event that the analytical results of a groundwater sample exceed the designated I.L., the following series of actions will be considered:

 Contact the laboratory to verify that all quality control checks were satisfactory, sufficient sample volume was used; required MDC's were met, etc.;

<sup>\*\*</sup> The values of 1000 and 2000 pCi/L for H-3 and 2 pCi/L for Sr-90 have been chosen to be low enough to result in timely detection of a new release or change to an existing release and still be outside the normal expected range of sample results at these locations, to the extent possible with the currently available data over time.

<sup>\*\*\*</sup> Any positively detected radionuclide that has a result greater than 2 times the average from the previous year. However, the IL is not reached until an H-3 result is also greater than 1000 pCi/L or a Sr-90 result is also greater than 2 pCi/L.

A cross section has also previously been developed through the Unit 3 area to supplement **Figure 4** and further demonstrate the relationship of site groundwater flow patterns and monitoring well placement relative to the individual Unit 3 SSCs (similar cross sections were previously developed for Units 1 and 2, as presented in the Hydrogeologic Site Investigation Report). This Unit 3 cross section C-C' is included in the Q1 2009 Quarterly Report as Figure 4A.

The calculation of ILs and yearly rolling averages prior to the Q1 2009 Report were based on the analytical results from the quarterly sampling rounds only, and therefore excluded aliquot, confirmatory and mid-quarter sample results. For the Q1 2009 Report and thereafter, if an aliquot analytical result confirms that the original quarterly analytical result was false, then only the aliquot result is utilized in the yearly IL calculation. If the aliquot result confirms the original quarterly result is valid, then both the original and the aliquot results are averaged together and then averaged into the yearly IL calculation as a single value. Confirmatory analytical results have the potential to impact the use of the original quarterly sample in the same manner as aliquots, however, unlike aliquots, these "independent samples" are averaged directly into the yearly rolling average without "pre-averaging" with the associated quarterly sample. Similar to confirmatory samples, mid-quarter samples are also averaged directly into the yearly rolling average calculation. However, mid-quarter sample results do not have any impact on the use of the initial quarterly samples as can either aliquot or confirmatory samples, as described above. In the case of both confirmatory and mid-quarter sample results, direct averaging into the yearly average of these additional results can somewhat bias the yearly average toward a particular quarter/season. However, given that confirmatory and mid-quarter samples are typically taken to confirm and/or prepare for uncharacteristically high radionuclide concentrations, this direct averaging provides a high bias to the subsequent yearly dose computations, and is thus conservative. In cases such as this where some bias inevitably will be created, establishing a conservative bias in the dose computations is considered more important than maintaining a seasonal non-bias.

- Re-analyze Aliquots of the original sample;
- Re-sample the location (Confirmatory sample) to verify the result;
- Increase the frequency of sampling (Mid-Quarter samples) for this location;
- Initiate an investigation utilizing Entergy's corrective action program and related resources as appropriate (e.g. site engineering / radiation protection); and
- Initiation of source/ground water remediation techniques commensurate with the potential dose impact analyses and good environmental stewardship.

#### 3.4.1 Previous Q3-2009 Investigation Level Exceedances

As indicated in the previous Q3 2009 Quarterly LTM Report, a comparison of the Q3 2009 analytical results to their respective I.L. values shows that the I.L.s were initially exceeded in six samples. Additionally, one sampling location (U1-CSS) exceeded the Tritium and Strontium I.L.s in Q2 2009 but was not sampled in Q3 2009. Four of these sampling locations (MW-31-49, MW-36-41, MW-37-40, and U1-CSS Strontium) still indicate radionuclide concentrations exceed their I.L.s in Q4 2009 samples; these results are therefore discussed in **Section 3.4.3** below. The remaining four I.L. exceedances (MW-32-59, MW-36-24, MW-50-42, and U1-CSS Tritium) were resolved during the Post Q3 2009 sampling and are discussed individually below.

MW-32-59. The Post Q3 2009 Mid-Quarter results at this location indicated an exceedance of the Tritium I.L. by a factor slightly under two. However, the Q4 2009 sample for this monitoring interval showed the Tritium activity had fallen to approximately one-half the I.L. Similar variability in Tritium levels have been observed at this monitoring location (as well as MW-31-49) during the past four quarters, with somewhat lower, but still significant variability observed dating back to the beginning of groundwater monitoring. The variable Tritium levels in MW-32-59 are likely related to the mobilization of stored Tritium within the shallow bedrock fractures near the Unit 2 SFP. This storage/Retention Mechanism was confirmed by the tracer test as initially described in the Hydrogeologic Site Investigation Report. More recently, it has been further supported by additional, new data (including additional tracer data) and analyses as discussed in Section 3.6.2 of the Q1 2009 Long Term Monitoring Report. However, it is also recognized that this Tritium increase may be related to the Unit 2 ISFSI work. GZA will continue to collect Mid-Quarter samples to monitor the Tritium levels in MW-32.

**MW-36-24.** The Q3 2009 results indicated Tritium levels were slightly above the I.L at this location. This exceedance was followed by the Q4 2009 result, which indicates a decrease in Tritium levels to an activity below the I.L. The Q2 through Q4 2008 tritium activities at the deeper levels at this location also show a generally stable to decreasing trend. While the exact cause of the elevated Q3 Tritium activity is unclear, it could possibly be related to the increased Tritium levels observed in MW-31 and 32 during previous quarters<sup>32</sup>. It is also recognized that this Tritium increase may be related to the Unit 2 ISFSI work or possibly the transient U1 FSB distillation tank valve leak (see Section 3.4.4).

**MW-50-42**. The Q3 2009 results at this location indicated Tritium levels were slightly above the I.L.; followed by a decrease below the I.L. during the Q4 2009 sampling round. The elevated Tritium levels at MW-50-42 are possibly related to the transient U1 FSB distillation tank valve leak (see Section 3.4.4) As reported in the Q3 2009 LTM Report, it was anticipated that these Tritium levels would return to previous levels with time because the leaking valves were

<sup>&</sup>lt;sup>32</sup> MW-36 is downgradient of MW-31 and MW-32. The elevated Tritium levels in MW-31 and 32 are likely related to the mobilization of stored Tritium within the shallow bedrock fractures near the Unit 2 SFP.

repaired. This hypothesis was confirmed by the Q4 2009 data. However, it is also noted that, given the downgradient location of MW-50, the prior I.L. exceedance could also be associated with the increased Tritium levels observed in MW-31 and 32 during previous quarters<sup>33</sup>.

**U1-CSS (Tritium).** The Q2 2009 results<sup>34</sup> indicated Tritium levels were slightly above the I.L. at this location. The Tritium increase in U1-CSS was likely related to the transient U1 FSB distillation valve leak (see Section 3.4.4). Given that these valves were immediately repaired, it was anticipated that the Tritium levels would decrease toward previous levels at U1-CSS. The Q4 2009 Tritium results agree with this initial conclusion, as the Tritium levels have decreased below the I.L.

#### 3.4.2 Q4-2009 Boundary Investigation Levels

A comparison of the Q4 2009 analytical results for the On and Off-Site Boundary Wells to their respective I.L. values shows that the I.L.s were not met for any of the monitoring locations. Therefore, there was no requirement to further investigate radionuclide activity in these wells. However, monitoring installation MW-40 and MW-51 are being further evaluated on a routine basis, as discussed below.

MW-40 and MW-51. While there have been no historic I.L. exceedances at these two southern boundary locations, and the data from this quarter (Q4 2009) falls at the lower end of previous ranges, these monitoring locations continue to be closely scrutinized on a routine basis given the sensitivity associated with the southern power block boundary. Even though it is recognized that the peak Tritium levels detected are low (less that 350 pCi/L) and near the lower limit of detection, there appears to be a general correlation in Tritium peaks at multiple depth intervals in both of these monitoring installations (see Figure H1 in Appendix H). An appropriate metric to evaluate whether or not these peaks are due to groundwater migration of Tritium from the power block area is the relative groundwater elevations between these locations and the power block areas where Tritium contamination exists. As discussed at length in the CSM sections of the Site Investigation Report, southern boundary groundwater elevations are well above those in the power block area. As such, groundwater, and thus Tritium in the groundwater, cannot migrate from the power block to the south; in fact, groundwater is migrating in the opposite direction. This conclusion was previously validated for nine guarters (between Q2 2007 and Q2 2009) through analyses of groundwater elevation contours (see Figure 5 in the quarterly reports prior to Q3 2009). In addition, starting with the Q1 2009 Quarterly Report, Figure 5A is being generated to specifically compare high importance transducer readings to historic maximum and minimum readings. The objective of this analysis is to demonstrate that substantial changes to the on-site groundwater flow field have not taken place and that the CSM remains valid. Multiple sampling zones from both the MW-40 and MW-51 monitoring installations are included in this analysis. Based on these analyses, as well as the substantial body of data developed over the last 5 years of investigation which underpin our CSM, we state, with a high degree of confidence that the low level peaks in the Tritium activities observed in these two monitoring installations are not due to groundwater migration from the power block area. This conclusion has continued to be validated each quarter. However, we do not have a definitive explanation for the observed peaks. Further investigation into other potential mechanisms, such as atmospheric Tritium washout and seasonal laboratory biases are ongoing.

MW-50 is downgradient of MW-31 and MW-32. The elevated Tritium levels in MW-31 and 32 are likely related to the mobilization of stored Tritium within the shallow bedrock fractures near the Unit 2 SFP.

<sup>&</sup>lt;sup>34</sup> Samples were not scheduled to be collected from this sampling location in Q3 2009.

#### 3.4.3 Q4 2009 SSC Investigation Levels

For the SSC monitoring wells, a comparison of the Q4 2009 analytical results to their respective I.L. values shows that the I.L.s were met in seven samples. The following table summarizes the cases where the I.L.s were met, and the exceedances are individually discussed below.

WELL ID	RADIONUCLIDE	RESULT (PCI/L)***	REANALYZED RESULT (PCI/L)	INVESTIGATION LEVEL (PCI/L)
MW-31-49	H3	45,800	NA*	15,470
MW-36-41	Sr-90	5.14	NA*	4.36
MW-37-40	Sr-90	16.9	NA*	2.26
MW-55-24	Cs-137	10.3	NA*	Any Detection***
MW-60-154	Cs-137	13.4	NA*	Any Detection***
MW-62-138	Sr-90	2.83	NA*	2.0
U1-CSS	Sr-90	17.5	NA*	14.83

<sup>\*</sup> NA indicates that the sample was not reanalyzed.

MW-31-49. The Q4 2009 results at this location indicate Tritium levels exceeded the I.L. by a factor slightly under three. The second of two Post-Q3 2009 Mid-Quarter samples also indicated that Tritium levels were approximately double the I.L.; additionally, in Q2 2009 this sampling location recorded its highest Tritium concentrations since the initiation of the LTMP (48,400 pCi/L). However, the Post-Q2, the Q3 2009 and the first Post-Q3 2009 Mid-Quarter samples all indicated Tritium levels were well below the I.L. at this location. A similar degree of variability has also been noted in the other sampling zones at this location (31-63 and 31-85) since the Q1 2009 sampling event, with somewhat less, but still noticeable variability going all the way back to the beginning of monitoring. While the complete root cause explanation for the elevated Tritium detection at this location is not fully known, we believe it is likely related to the mobilization of stored Tritium within the shallow bedrock fractures near the Unit 2 SFP. This storage/Retention Mechanism was confirmed by the tracer test as described in the Hydrogeologic Site Investigation Report prepared by GZA and dated January 7, 2008. However, it is also recognized that this Tritium increase may be related, in part, to the Unit 2 ISFSI work (see Section 3.6.4 of the Q1 2009 report). This location will therefore be subject to added scrutiny during the upcoming quarterly monitoring rounds to evaluate potential increasing trends in Tritium levels.

MW-36-41: Similar to Q3 2009, the Q4 2009 results at this location indicate Strontium continued to exceeded the I.L.; however, because no samples were collected from this sampling location. In 2008, the I.L. was calculated from a single Strontium result collected in 2007. Therefore, while the complete root cause for this I.L. exceedance is unclear, it may be nothing more than the result of an upswing in activity due to local variations in flow paths or other in-situ processes (natural geohydrologic variability), when compared to an I.L. based on a single value measured during a downswing. However, it is also noted that this sampling installation is located within the delineated Unit 1 Strontium plume (downgradient of Unit 1 SFPs), and this Q4 result comes just after the highest Strontium activity recorded in this well (Q3 2009) since monitoring began. Therefore, the Strontium increase could possibly represent a delayed response to the Unit 1 defueling activities, particularly in light of discussion for MW-37-40 below. This location will therefore be subject to added scrutiny during the upcoming quarterly monitoring round and has been added to Figure 7A.

<sup>\*\*</sup> ND indicates that the radionuclide was not detected greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

<sup>\*\*\*</sup> A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

MW-37-40: The Q4 2009 results at this location indicate Strontium was measured at approximately seven times the I.L., with levels at five times the I.L. during the Q3 2009 sampling round. The remaining three zones at this location (37-22, 37-32, and 37-57) also indicated an increase in Strontium levels during the Q3 2009 sampling event with continued elevated Strontium levels in Q4 2009. Given that this sampling location is downgradient of the Unit 1 SFPs, these Strontium increases are likely a delayed response to the increase in water levels during defueling activities in the Unit 1 SFPs. The behavior associated with the movement of Strontium through the system with temporal increases after the water level was raised and then the pool emptied after defueling of Unit 1, was expected. It is anticipated that Strontium levels at this monitoring location will return to lower levels with time because the likely source of these radionuclides has been terminated. This location will therefore be subject to added scrutiny during the upcoming quarterly monitoring round and has been added to Figure 7A.

MW-55-24: The Q4 2009 results indicate Cesium was detected for the first time at this location since January 2008. Both of these detections are just barely above the 3 times 1 sigma uncertainty limit. Therefore, it might be assumed that these detections are nothing more than laboratory anomalies, particularly given previous laboratory issues with false Cesium detections. This conclusion would be supported by the lack of Cesium detection in the other two depth intervals at this location. However, MW-55-24 and the deeper zones at this location (MW-55-35 and 55-54) indicated elevated Strontium levels during the Q2 and/or Q3 2009 sampling rounds. In addition, MW-53, located upgradient of MW-55, also detected a small Cesium activity in Q2 2009. Given these factors and the location of MW-55 directly downgradient of the Unit 1 SFPs, the elevated Cesium levels are more likely a delayed response to the previous increase in water levels in the Unit 1 SFPs during defueling. As such, it is anticipated that Cesium levels at this monitoring location will return to non-detectable levels with time because the source of these radionuclides has been terminated. This location will be subject to added scrutiny during the upcoming quarterly monitoring round.

MW-60-154: The Q4 2009 results at this location indicate Cesium was detected at a low level for the first time since the LTMP was initiated (fall 2007). In addition, Cesium has never been detected in the other depth intervals at this location (MW-60-35, 60-53, 60-72, 60-135, and 60-176). It is also noted that Strontium, a strong indicator of contamination from the Unit 1 SFPs (most likely source of Cesium on-site), has also never been detected in any depth interval at this location. These non-detections are as would be expected because MW-60 is located well outside the plume track for the Unit 1 SFPs release. Given the above lines of evidence, it is GZAs opinion that the Q4 2009 Cesium detection is likely related to a false laboratory detection. However, this location will be subject to added scrutiny during the upcoming quarterly monitoring round.

MW-62-138: The Q4 2009 results indicate Strontium levels were slightly above the I.L. at this location. Because the Strontium levels at MW-62-138 are low, a small increase in Strontium (~1.5 pCi/L) above more typical levels results in an I.L. exceedance. As such, this Strontium I.L. exceedance could be related to natural geohydrologic variability. However, MW-62 is located at the downgradient perimeter of the Strontium plume and therefore, this Strontium increase could also be a limited, delayed response to the Unit 1 SFPs defueling. Based on the magnitude of this detection in relation to previous Strontium activities measured in this well, as well as the shape of the Strontium vs time curve (see Figure 7A), it is GZA's opinion that the later hypothesis is the more probable. This location will therefore be subject to added scrutiny during the upcoming quarterly monitoring round.

**U1-CSS:** The Q4 2009 results at this location indicate Strontium was detected slightly above the I.L. at U1-CSS. The previous sample collected at this location (Q2 2009) also indicated Strontium levels were above the I.L. by a factor of two. U1-CSS is downgradient of the Unit 1

SFPs, and appears to be situated along an anthropogenic preferential flow path<sup>35</sup>. This Strontium increase is likely associated with a response to the raising of the water levels and increased leakage in the Unit 1 SFPs during the previous defueling. Similar to the near-pool Unit 1 monitoring locations, it is anticipated that the Strontium levels at this location will eventually decrease since the remaining fuel has been removed and the water drained from the Unit 1 SFPs. This location will be subject to added scrutiny during the upcoming quarterly monitoring round.

#### U1-NCD and U1-SFDS

Sampling of the Unit 1 North Curtain Drain (U1-NCD) and the Unit 1 Sphere Foundation Drain Sump (U1-SFDS) are currently included as part of the Long Term Monitoring Program. These drains have been documented to capture a large proportion of the Strontium leakage from the Unit 1 SFPs, and continue to collect groundwater containing Strontium and Cesium and direct it to treatment. These drains have also historically been assumed to collect some groundwater contaminated with Tritium from the Unit 2 SFP. This conclusion was validated by the tracer test conducted as part of the hydrogeologic site investigation (see the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008). The limited amount of quarterly sampling data as well as the impact of the Unit 1 defueling activities renders the setting of I.L.s for these monitoring points currently premature. However, visual inspection of the existing data was performed and general decreases in Tritium levels were observed in samples from both drains during Q4 2009. Strontium data from these drains also show continued decreases, as summarized on Figure 7A.

#### 3.4.4 Conclusions - Boundary and SSC Leak Detection Monitoring

Recognizing that measured activities in the Off-Site and On-Site Boundary Wells have remained below I.L. levels, this overall data set continues to demonstrate that radionuclides are migrating toward the Hudson River to the West, and are not migrating off of the property to the North, East or South, as expected given groundwater flow directions from the property periphery toward the power block area.

Given the analyses discussed above, there is also no compelling reason to believe that any new unidentified leaks have developed in the SSCs monitored relative to Unit 2 or 3. With the exception of location MW-31-49, Tritium levels within the U2 plume<sup>36</sup> are below their I.L.s and the plume is continuing to exhibit overall, long-term reductions in Tritium activity. While recent increases in Tritium levels have been observed in MW-31 and MW-32, these data are consistent with episodic releases of Tritium historically stored in the subsurface via natural and anthropogenic Retention Mechanisms<sup>37</sup>, which is further supported by the tracer data and other analyses<sup>38</sup> discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report.

Relative to the Unit 1 data, increased leakage was anticipated during final fuel removal from Unit 1 SFPs. This leakage was readily detected as increased Strontium in the groundwater by the Long Term Monitoring Program. The initial near-pool and more recent downgradient

<sup>&</sup>lt;sup>35</sup> The U1-CSS monitoring well was installed through the East wall of the Containment Spray Sump. It is therefore located directly below the utility trench associated with this system as well as that associated with the historical discharge pipe for the Unit 1 NCD.

<sup>&</sup>lt;sup>36</sup> It is noted that there is no Tritium plume associated with Unit 3.

These Retention Mechanisms are discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report.

These data and analyses further support a conclusion that the Unit 2 SFP had ceased leaking after the transfer canal "pin hole leak" was repaired in late 2007. However, given the more recent behavior observed in the Unit 2 collection box data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms.

Strontium increases are being routinely monitored as summarized on Figure 7A, and are expected to continue to show further decreases with time.

The recent increases in Tritium levels at MW-42-49, MW-53-82, U1-CSS and MW-50-42 exhibited a general trend of I.L. exceedances occurring progressively farther downgradient with time (from the Post-Q1 to the Q3 2009 sampling rounds). This trend is consistent with that anticipated given the independently <sup>39</sup> identified Q1 09 transient leak in the waste distillation tank valving within the Unit 1 FSB, rather than from a potential new release from the SSCs associated with Unit 2 and 3. This leakage episode was rapidly identified and immediately terminated. These four locations are now (Q4 2009) all below their I.L.s with Tritium levels at or approaching previous activities. Based on the observed data trends, it appears that the Tritium input into the groundwater flow regime from the waste distillation tank valving leak has generally dissipated through the system, at least as far downgradient as the discharge canal <sup>40</sup>.

Overall, GZA believes that continued monitoring will further demonstrate decreasing long term trends in groundwater contaminant activities over time for both the Unit 1 and Unit 2 plumes given the source interdictions completed by Entergy. However, ultimate confirmation of these conclusions will require monitoring over a number of years to demonstrate continued depletion of Tritium and Strontium from the Retention Mechanisms originally sourced by: (1) historic Unit 2 SFP Tritium leakage; and (2) the historic and more recent Strontium leakage due to Unit 1 defueling. It is further noted that quantification of these overall radionuclide reductions will require that ranges in seasonal variation be adequately reflected in the monitoring data and any further additions of radionuclides to the Retention Mechanisms, such as through the transient releases discussed above, be dissipated from the geohydrologic flow regime.

Given the above cited constraints, it is premature to begin recalibrating the I.L.s that were originally established at the beginning of the LTMP in 2007. Since inception of this program, it has been observed that I.L.s have been routinely exceeded in a number of cases where subsequent data have demonstrated that no new leaks have occurred. The majority of these cases occur where the radionuclide levels are generally low and/or near their detection limits. It appears that data variability, likely due to seasonal precipitation influences and local variations in flow paths and/or other in-situ processes, is the primary cause of these false positives<sup>41</sup>, particularly pursuant to Tritium. Therefore, the basis upon which the I.L.s are computed needs to be re-evaluated in light of the long-term natural transient variability of the groundwater system in response to precipitation events, etc. Furthermore, while re-evaluation/re-setting of I.L.s is a clear goal, it is still premature given the lack of sufficient data. This is particularly true given the recent behavior in Strontium levels due to the Unit 1 defueling (see Figure 7A) and the transient Tritium releases discussed above and in the Q1 2009 Quarterly LTM Report. As such, the

<sup>&</sup>lt;sup>39</sup> The valve leakage was initially identified during routine visual inspection rounds and immediately terminated. Given that the leak was within the Unit 1 FSB structure, it was documented in a Condition Report under Entergy's Corrective Action Program. This valve leak and repair subsequently came to light within the GPI program during investigations into the cause of the abrupt increase in Tritium levels in MW-42. Additional emphasis has therefore been placed on routine review of these reports as they potentially relate to GPI objectives.

<sup>&</sup>lt;sup>40</sup> As discussed above, additional portions of these releases likely remain above the water table in the release area as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

<sup>&</sup>lt;sup>41</sup> In this context, "false positive" does not refer to an error in the actual data value. Rather, it means that the I.L exceedance in question did not result from a new release. While I.L.s are meant to be set at conservatively low values, and thus "false positives" should be expected, a corollary objective is to set I.L values which keep the number of false positives low enough to eliminate development of complacency.

current I.Ls will remain in effect while a sufficient data base is acquired to allow better quantification of the natural (non-leak related) variability in the data.

Three critical conclusions can be drawn from the above summarized data and analyses: 1) the current CSM for the IPEC site provides a good basis for the design of the Long Term Monitoring Program; 2) the procedures and rational used for selecting monitoring locations for leak detection have been further validated given the clear detection of the confirmed Unit 1 SFPs increased leakage during fuel removal, the transient U1 FSB distillation valve leak (see Section 3.4.4), and the surficial release of Tritium to Manhole A2 in Q2 2009; and 3) increases in Strontium levels following a documented leak take longer to materialize in the groundwater than might otherwise be expected.

#### 3.5 Plume Natural Attenuation Monitoring

The fourth and final objective of the Long Term Monitoring Program is to evaluate if the groundwater plumes identified on-Site demonstrate overall reductions in total activity over time, as is consistent with the requirements of Monitored Natural Attenuation (MNA), the selected remediation for the IPEC Site <sup>43</sup>.

Given the likely ages of the leaks identified and characterized during the hydrogeologic investigation, it is probable that the Unit 2 (Tritium) and Unit 1 (Strontium) plumes had reached steady state conditions prior to the beginning of the LTMP. Given that: (1) the identified leaks in the Unit 2 SFP have all been previously repaired (the last leak repaired in 2007) and; (2) the water in the Unit 1 West Pool underwent intensified demineralization (beginning in April 2006 with a reduction in Strontium levels of over 95 percent), one might expect that the plumes should have started to markedly attenuate toward zero with time. Both plumes have in fact generally shown significant levels of attenuation, when they are viewed in their entirety and past release events and expected seasonal variability in the sampling data are accounted for. However, the attenuation has not been as rapid as we originally anticipated during time frames subsequent to the source interdictions implemented by Entergy.

In the case of the <u>Unit 2 Tritium plume</u>, levels have dropped markedly from the highest levels measured during the two-year hydrogeologic investigation. However, the rate of Tritium decrease with time has decreased. This rate of reduction has been difficult to predict due to the impact of natural geologic and anthropogenic Retention Mechanisms. These subsurface features have trapped and stored Tritium released during historic Unit 2 SFP leaks, and are now likely releasing this Tritium to the groundwater flow regime in an episodic manner after the physical leaks have beenteminated. This conclusion is consistent with the original CSM presented in the Hydrogeologic Site Investigation Report, as further supported by the tracer test data in that report as well as subsequent tracer data, as described in Section 3.6 of the Q1 2009 Quarterly Monitoring Report, dated July 2, 2010. In addition, trend identification is further complicated by impacts associated with localized transient releases, as described above. Further discussion of this quarter's data pursuant to evaluation of the Unit 2 Tritium plume MNA is provided in **Section 3.5.1** below.

Relative to the <u>Unit 1 Strontium plume</u>, Strontium levels should drop much more slowly than Tritium levels. This is because, in addition to the Retention Mechanisms discussed above for Tritium (which also apply to Strontium), Strontium also undergoes partitioning whereby this radionuclide is adsorbed from the groundwater onto solid surfaces (both geologic and

<sup>&</sup>lt;sup>42</sup> Given the proximity of monitoring installations to documented release events, the delay in release arrival is likely due primarily to Strontium partitioning and the time required for leakage to traverse anthropogenic features.

<sup>&</sup>lt;sup>43</sup> The selection of MNA as the remediation for the Site is more fully discussed in the Hydrogeologic Site Investigation Report.

anthropogenic). When the input of Strontium to the groundwater is reduced (such as via the initial fuel pool demineralization and subsequent decommissioning) the solid surfaces desorb Strontium back into the groundwater, thus maintaining Strontium levels. Strontium partitioning is therefore expected to substantially slow plume attenuation. Despite partitioning effects, some plume attenuation was observed in response to pool demineralization prior to defueling, particularly proximate to the pool. However, defueling of Unit 1 resulted in a temporarily increase in the leakage rate of West Pool water into the formation. This was expected based on previous work on the Unit 1 SFPs, but was unavoidable given the requirement to raise the pool level for fuel rod removal<sup>44</sup>. The increased leakage rate has resulted in a noticeable increase in Strontium levels in the immediate vicinity, and downgradient of, the fuel pool as discussed further in **Section 3.5.2** below.

#### 3.5.1 Unit 2 Tritium Plume Attenuation

#### **Qualitative Evaluation**

From a qualitative perspective, a reduction in overall Tritium activity in the Unit 2 plume can be seen through a comparison of the Q4 2009 delineated plume boundary (**Figure 6**) to those in prior reports. Not only have Tritium levels within the plume generally shown an overall, long-term decreasing trend, but the reductions over the past few quarters have become particularly evident in the delineated, shaded bounds of the plume. This quarter continues the trend where the shaded plume and longer extends to the river as it did in previous quarters through 2008. The shaded boundary now terminates upgradient of MW-37, over two hundred feet from the river. Additionally, the rolling average Tritium activity in MW-111 this quarter (Q4 2009) is also now less than the 50,000 pCi/L plume isopleth for the first time since the start of the LTMP. This trend over time has been summarized on **Figure 6A**, which is a compilation of the quarterly Tritium plume maps as well as that from the Investigation Report.

#### **Mann-Kendall Quantitative Analysis**

To more quantitatively evaluate MNA progress, a Mann-Kendall analysis, as referenced in USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis, <sup>46</sup> was performed on the Tritium levels measured through Q4 2009 at monitoring locations associated with the IP2-SFP and downgradient Unit 2 Tritium plume. This statistical technique was chosen because it is particularly well suited for data sets with a limited number of points. Each of the vertical monitoring intervals at each monitoring installation location was analyzed separately. In general, only data collected after final completion of the multi-level installation <sup>47</sup> was used.

<sup>&</sup>lt;sup>44</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

<sup>&</sup>lt;sup>45</sup> The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value. This plume delineation boundary value equates to one-quarter of the drinking water standard for Tritium. Although GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site, the MCLs do provide a useful benchmark for comparisons of relative human risk. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

<sup>&</sup>lt;sup>46</sup> USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis, EPA QA/G9, QA00 UDATE; EPA/600/R-96/084, July, 2000.

<sup>&</sup>lt;sup>47</sup> Each borehole was completed as a multi-level installation. These multi-level completions were designed to segregate the borehole length into individual sampling zones with depth. The sampling zones were generally established to coincide with the more productive zones of the fractured bedrock and overburden (both natural soils and backfill). These sampling zones were then isolated from each other with various types of seals placed in the open borehole. The objective of the seals is to prevent vertical flow through the borehole and thus establish the same conditions in the formation which existed prior to the drilling of the borehole.

However, there were a number of exceptions to this generalization where open borehole and/or borehole packer testing data were also used. These data were incorporated where possible given the importance of early time data (proximate to when documented leaks were still active). Additional, more detailed discussion relative to the basis for these analyses is provided in Section 3.6 of the Q1 2009 Quarterly LTM Report.

Graphs showing the variation in Tritium concentration over time in the immediate vicinity of the Unit 2 SFP are presented as **Figures G-1**, **G-2** and **G-3** in **Appendix G**, for MW-30, 31 and 32, respectively. Additional graphs are also presented in the appendix for the other monitoring locations downgradient of the Unit 2 SFP (see **Figures G-4** through **G-14** for MW-33 through 37, 42<sup>48</sup>, 49, 50, 53<sup>49</sup> 55 and 111)<sup>50</sup>.

The Mann–Kendall analyses for the individual monitoring points are summarized on **Table G-1** in **Appendix G**. The table includes the results of the analysis for each depth interval ("well") at each of the multi-level monitoring locations enumerated above. The table is color coded, with green shading designating wells showing a decreasing trend, yellow for no trend, and red for an increasing trend.

Comparison of **Table G-1** for Q4 2009 to that from Q3 2009 demonstrates that there have been no major changes. Of the 32 intervals included on the table for Q4 2009, approximately two-thirds (19) show a decreasing trend, as compared to 20 intervals last quarter. It is important to note that this group of "decreasing wells" includes all those located within the core of the plume with the highest Tritium concentrations (MW-30-69, MW-33 and MW-111, with historic yearly average Tritium concentrations > 40,000 pCi/L). These high-concentration wells better represent overall plume behavior because they encompass a great percentage of the Tritium activity in the plume.

Of the 12 wells shaded in yellow (exhibiting "no trend"), only 7 provide valid representations (as shaded) of Unit 2 plume behavior. The shading designation for the others cannot be used to infer conclusions relative to plume trends for Unit 2 based on this analysis, as follows:

Three wells (MW-42-49, MW-42-78, and MW-53-82) are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP, and therefore are not yet expected to show a decreasing trend due to Unit 1 defueling<sup>51</sup> and the previously discussed U1 FSB valve leak.

As such, the Tritium data is considered depth-discrete. It is noted that the multi-level installations at some monitoring locations were removed and replaced with upgraded systems, such as for the monitoring installation at MW-32.

November 23, 2010 10-11-23 FINAL LTM 2009 Quarter Four Report.docx Page 3-14

<sup>&</sup>lt;sup>48</sup> MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP could be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above.

<sup>&</sup>lt;sup>49</sup> MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP could be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above.

Monitoring locations MW-66 and MW-67, also located downgradient of the Unit 2 SFP, could not be included in the analyses because the data sets for these two wells do not yet include the recommended minimum number of data points (>ten) for the Mann–Kendall analysis method. These two locations will be added to the analyses starting in Q1 2010.

MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow

- Inspection of the graph for MW-36-24 (Figure G-7) shows a rapid and large decrease in Tritium concentrations at early times in this overburden (discharge canal backfill) well (from > 30,000 pCi/L to <3,000 pCi/L). This large decrease is followed by a number of small perturbations around a relatively flat trend. While it is visually clear that this well has shown a major decrease in Tritium levels since containment of the 2005 shrinkage crack leak, the Mann–Kendall analysis only evaluates the number of increases relative to decreases and does not weight the analysis relative to the magnitude of each change. As such, visual inspection demonstrates that this location actually exhibits an overall decreasing trend, even though the analysis results in a no trend designation (yellow shading on table). However, it is also noted that the last few quarters have shown what appears to be a short-term, small peak in the Tritium activity in this well, as likely associated with the transient release from the U1 FSB distillation valves (see Section 3.4.4), and/or the recent increases noted in MW-31 and MW-32.
- Inspection of the graph for MW-50-42 (**Figure G-11**) also shows a large, rapid decrease in Tritium concentrations during the first three data points collected at this sampling location (>9,000 to <MDC pCi/L). Following the third sample, the Tritium levels have shown a stable trend with small perturbations throughout the last three years. A distinct, overall decrease in Tritium levels is observed in the time series data; however, the Mann-Kendall analysis only evaluates the number of increases versus decreases in the time series. A visual inspection of the total Tritium dataset in MW-50-42 clearly indicates an overall decreasing trend. However, it is also noted that the last few quarters have shown what appears to be a short-term, small peak in the Tritium activity in this well, as likely associated with the transient release from the U1 FSB distillation tank valving (see Section 3.4.4), and/or the recent increases noted in MW-31 and MW-32.

It is noted that five of the seven remaining "no trend" wells are all associated with the shallow sampling ports of two monitoring locations: MW-31, and MW-32. These two locations are actually not located downgradient of the Unit 2 SFP from a saturated groundwater flow standpoint. Rather, they are generally located up- and cross-gradient<sup>52</sup>. MW-31-85, is also part of this group of upgradient wells. This is the only well for which the Mann-Kendall analysis indicates an "increasing" trend. The upper-most interval in both MW-31 and MW-32 have shown substantial variations in Tritium levels over the last four quarters (Q1 through Q4 2009) with somewhat less, but still noticeable variability going all the way back to the beginning of monitoring. The current and historic variability in these data can be explained by either: 1) an ongoing small episodic (< 10L/day) leak in the Unit 2 SFP; 2) a "Retention Mechanism" in the saturated and unsaturated zones under the SFP that can retain substantial volumes of highly Tritiated water (e.g., historic SFP leakage) for substantial amounts of time<sup>53</sup>; and/or 3) a

regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP could be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above.

52 While not downgradient of the SFP from a groundwater flow perspective, Tritium leakage from the SFP can still migrate to these

<sup>52</sup> While not downgradient of the SFP from a groundwater flow perspective, Tritium leakage from the SFP can still migrate to these locations via vadose zone transport above the water table along dipping bedrock fractures. During the site investigation work, a tracer test was performed which clearly demonstrated that water released proximate to the SFP foundations (adjacent to MW-30) does migrate to the east and south past MW-31 and MW-32 prior to entering the water table, and then flows with the groundwater through these wells and then to the river to the west. This vadose zone migration mechanism is discussed more fully in the Hydrogeologic Site Investigation Report.

<sup>53</sup> This hypothesized "Retention Mechanism" is supported by our understanding of the construction methods used for the IP2-SFP and adjacent structures, evaluations of contaminant concentration variability trends over short timeframes and precipitation events, as well as the original and subsequent tracer test results, as further described in Sections 7.0 and 8.0 of the Hydrologic Site Investigation Report and the Q1 2009 monitoring report.

November 23, 2010 10-11-23 FINAL LTM 2009 Quarter Four Report.docx Page 3-15

combination of the above<sup>54</sup>. While Tritium concentrations in the groundwater plume could be impacted by both an ongoing leak and the Retention Mechanisms cited above, tracer concentrations in the groundwater cannot be replenished by SFP leakage. As discussed in further detail in Section 3.6 of the Q1 2009 Quarterly Monitoring Report, the original and updated tracer data strongly support a Retention Mechanism explanation. In addition, it would be expected that Tritium release from the Retention Mechanisms would be episodic, for example as associated with periods of increased infiltration from precipitation. Such episodic releases would be expected to result in the peaks in Tritium concentrations observed.

The sixth remaining interval reported as "no trend", MW-30-84, is located immediately next to the SFP and generally downgradient of MW-31-85 (interval with increasing trend). While the Mann Kendall analysis yields no trend for this interval over the full monitoring time frame, the interval actually appears to exhibit a slightly increasing trend beginning in the late fall of 2008. The specific reason for this increase is not known, but it is worth noting that the Tritium activity in this interval is over an order of magnitude below that of the interval immediately above (MW-30-69), which shows a decreasing trend. The trend in MW-30-84 may be reflective of that in MW-31-85, both of which are being subjected to added scrutiny through more frequent monitoring.

The seventh and final remaining well, MW-55-35 (**Figure G-13**), shows a distinctly decreasing trend in Tritium concentrations at early times, followed by relatively stable to decreasing Tritium levels through Q1 2009. The data (and a visual inspection of **Figure G-13**) demonstrate that Tritium levels had decreased from >9,000 pCi/L to relatively stable concentrations of < 1000 pCi/L over that period. However, an increase in Tritium activity was detected beginning in Q2 2009, with relatively stable levels thereafter. While small perturbations during this relatively stable portion of the time series have resulted in a no trend designation, it is also noted that the increased Tritium levels after Q2 2009 may be associated with the transient U1 FSB distillation valve leak (see Section 3.4.4), and/or the recent increases noted in MW-31 and MW-32. As such, this well may provide an accurate representation of the behavior of this portion of the Unit 2 Tritium plume. However, this lack of a decreasing trend does not necessarily imply a continuing leak in the Unit 2 SFP given the expected impact of the release from the distillation tank valving, and/or the recent increases noted in MW-31 and MW-32 (Retention Mechanism based), as discussed above.

Based on the evaluation summarized above, the Mann-Kendall analyses of the individual depth intervals within the groundwater monitoring installations located proximate to and downgradient of the Unit 2 SFP overwhelmingly support a conclusion that the Tritium plume has exhibited an overall decreasing trend with time since monitoring began. However, it is noted that as the rapidly decreasing trends in Tritium activity give way to much more slowly decreasing trends as an asymptote is approached, the variability of the Tritium sampling results due to hydrogeologic and laboratory variability are likely to result in more "no trend" classifications based on the Mann-Kendall analysis. Therefore, identification of another, more appropriate method is being investigated, particularly as the total LTMP data set becomes more robust with time.

#### **Tritium Plume Total Activity Analysis**

As discussed above, the individual well trend data, when viewed collectively, support a conclusion that the Tritium plume concentrations have been decreasing with time since

<sup>&</sup>lt;sup>54</sup> It is also recognized that the potential exists for a fourth potential source of Tritium; that is any other leak or spill above the upgradient portions of the Unit 2 Tritium plume (such as the distillate tank valve leak discussed in **Section 3.4** above).

monitoring began. Another method to analyze plume behavior is to compute the total Tritium activity in the plume at multiple snapshots over time. This procedure<sup>55</sup> was implemented for each quarterly LTMP sampling round from Q2 2007 to Q4 2009. In addition, the bounding Tritium concentrations from Figure 8.1 of the Hydrogeologc Site Investigation Report<sup>56</sup> have also been included as a starting point for the graph. These data are summarized as a histogram on **Figure G-15** in **Appendix G**.

As can be seen from the figure, the total Tritium activity in the plume downgradient of the Unit 2 SFP has shown a distinctly decreasing trend over time. The total Tritium activity in the plume has decreased 45 percent since Q2 2007, and has decreased by 89 percent when compared to the bounding level Tritium concentrations. However, it is also noted that these time/activity data to appear to be approaching a non-zero horizontal asymptote<sup>57</sup>. While the general "first order" plume decay is what would be expected for a plume undergoing Monitored Natural Attenuation after source termination, a non-zero asymptote suggests a continued input of Tritium into the groundwater flow regime. The data currently available lead us to believe this continuing Tritium input is likely associated with the Retention Mechanism(s) and/or localized transient releases, as described in this and earlier reports.

#### Conclusion- Unit 2 Tritium Plume MNA

Based on the data and analyses provided above, our conclusion is that the Tritium plume is undergoing overall, long-term reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP, the Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation.

Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report.

#### 3.5.2 Unit 1 Strontium Plume Attenuation

Despite the effects of partitioning, as discussed above, the overall Strontium activity within the Unit 1 plume had generally shown some attenuation in response to the West Pool demineralization activities conducted by Entergy in preparation for defueling. This work began in 2006 and resulted in an approximately 98% reduction in Strontium in the West Pool (see Figure 7A: U1-NCD, U1-SFDS, MW-42, U1-CSS). However, the final defueling of the Unit 1 SFPs had resulted in a noticeable increase in Strontium levels proximate to the SFPs (U1-NCD, U1-SFDS, MW-42, and U1-CSS; all of which have shown large sustained decreases since mid 2009), as well as generally more recent increases in the Strontium plume levels downgradient (MW-53, MW-55 MW-54, MW-57, MW-50, and MW-37) over the past few quarters. This is as

<sup>&</sup>lt;sup>55</sup> The individual sampling point Tritium concentrations were multiplied by the groundwater volumes in representative zones (discretized over area and depth), as computed using soil and bedrock effective porosities developed from the pumping and tracer tests (see the Hydrogeologic Site Investigation Report for further information).

Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc. on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

One physical cause for a horizontal asymptote would include a persistent, unidentified leak still remaining in the Unit 2 SFP. With Tritium at approximately 30,000,000 pCi/L in the SFP, a leak directly from the pool of only approximately 10 L/day would be sufficient to provide the required Tritium input to the groundwater. However, the available data do not appear to support the existence of such a leak. The rational underlying this conclusion is discussed more fully in Section 3.6 of the Q1 2009 Quarterly Monitoring Report. This conclusion will continue to be reassessed as new data becomes available, particularly that associated with the collection box.

was predicted given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing the leakage rate from the SFPs<sup>58</sup>.

The data for Q4 2009 indicate that the overall Strontium levels continued to exhibit a general decrease and have now reached pre-defueling levels in the immediate vicinity of the pool (U1-NCD, MW-42 and potentially U1-CSS and MW-53). These monitoring locations would be expected to be the first to reflect the complete decommissioning of the SFPs given their location/function. The U1-SFDS, which is located further from the West Pool, has also begun to show a decreasing trend from Q2 2009 to Q4 2009.

Somewhat farther downgradient, the Q4 2009 data are consistent with the "tail" portion of the perturbation as the previous increase in U1-SFPs leakage works its way towards the river. This behavior is most evident at monitoring locations MW-37, MW-55 and MW-57<sup>59</sup> where the increases appear to be generally leveling off with anticipated future decreasing trends. MW-54 and MW-50-66, however, appear to have already exhibited a decrease back to previous levels, even though they are progressively farther downgradient than the wells cited above. This behavior serves to again emphasize that the IPEC Site is located in a bedrock fracture controlled hydrologic regime <sup>60</sup>. As such, this type of localized "distance-based inconsistency" is to be expected and likely indicates that these wells are closer to (or within) the more pervious preferential flow pathway that is hypothesized to be responsible for the convergence and narrowing of the Tritium and Strontium plumes as they move toward the river from sources centered at widely spaced locations upgradient <sup>61</sup>.

Farther downgradient, in the vicinity of the river, there are no peaks in Strontium activity that can be clearly attributed to the Unit 1 defueling, perhaps with the exception of a mid-depth monitoring interval in MW-62 (MW-62-138). This depth interval in particular (along with, but to a lesser extent the shallower intervals in overburden) appears to show distinctly increasing trends in Q1 2009 and Q4 2009<sup>62</sup>. However, it is believed that this location is less likely to be responding to Unit 1 defueling given that it does not appear to be proximate to (or within) the preferential flow path cited above.

From an overall, long-term perspective, it is expected that the levels somewhat more distant from the pool than MW-42 (e.g., U1-SFDS, U1-CSS) will continue to decrease to pre-defueling levels similar to U1-NCD and MW-42. Strontium levels closer to the river may still show increases as this additional Strontium-contaminated water flushes through the groundwater flow system. It is expected that this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also continue their overall downward trend once this perturbation has passed through the system; decreasing trends are expected and predicted

As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

Based on Q2 2009 data; this installation is sampled annually

While groundwater flow through the fractured bedrock at the IPEC Site is highly preferential at small areal scales, it is characterized by sufficiently interconnected small bedrock fractures to allow the hydrogeologic system to function and be modeled as a non-homogeneous, anisotropic, porous media at Site-wide scales.

By way of contrast, in a porous media flow regime, the centerlines of plumes that start at widely spaced locations (spaced perpendicular to the groundwater flow path) will typically remain widely spaced (although the edges of the plumes will likely move closer as the plumes get wider through dispersion). In the case of fracture flow at IPEC however, not only do the Strontium and Tritium plume centerlines converge, but the plumes also get narrower as they move downgradient. In addition, MW-50 displays high relative Strontium concentrations and fault gouge was encountered during the drilling of this well. These behaviors/data are hallmark signatures of a more highly fractured zone preferentially controlling groundwater flow and thus the migration of the contaminants therein (see the Site Hydrologic Investigation Report for further CSM-focused discussion of this issue).

 $<sup>^{\</sup>circ}$  The increase in Q1 2009 in MW-62-138 was followed by a steady decrease over the next two quarterly monitoring events.

#### **Section 3.0 Data Evaluation**

given that Entergy has terminated all leaks in the Unit 1 SFPs through decommissioning and the Unit 1 Strontium plume continues to decreases in accord with Monitored Natural Attenuation. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation.



## FINAL QUARTERLY LONG-TERM GROUNDWATER MONITORING REPORT Q4 2009 (REPORT NO. 8)

#### 4.0 CONCLUSIONS AND PLANNED ACTIVITIES

In summary, based on the data collected to date, the apparent strength of the CSM to evaluate that data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).

Based on the specific results and evaluation of the Q4 2009 groundwater monitoring within the context of the Long Term Monitoring Program, IPEC plans to continue routine groundwater sampling and related maintenance. This work will be conducted in accordance with the IPEC Radiological Groundwater Monitoring Program IP-SMM-CY-110, and will incorporate the enhancements described herein.

More specifically, evaluation of data collected during Q4 2009 has shown the following:

- While I.L.s have been met at a number of locations this quarter, there is no definitive
  evidence of new leaks from the Systems, Structures, or Components monitored, with the
  exception of the prior, anticipated additional leakage from the Unit 1 SFPs during the 2008
  activities, the transient leakage from the distillation tank valves in Q1 2009, and the transient
  surficial Tritium release to Unit 3 Manhole A2 in Q2 2009.
  - Based on past work, additional leakage was expected during the raising of water levels in the Unit 1 SFPs for final fuel removal to ISFSI storage. Unit 1 SFPs leakage was terminated with the drainage and sealing of the pools. This previous, transient leakage was initially verified as pronounced increases in Strontium and Cesium in the monitoring locations closest to Unit 1, and continues to be monitored.
  - The Q1 2009 leakage from the waste distillation tank valves was independently identified based on an increase in Tritium levels in monitoring installation MW-42 proximate to the tanks. These valves were immediately repaired. Additional I.L. exceedances occurred in downgradient wells (MW-53-82, U1-CSS, and MW-50-42) during subsequent quarters. These downgradient locations are now (Q4 2009) all below their I.L.s with Tritium activities at or approaching previous levels. Based on the observed data trends, it appears that the Tritium input into the groundwater flow regime from the waste distillation tank valving leak has generally dissipated through the system, at least as far downgradient as the discharge canal 64. However, the potential impact of this release further downgradient will be specifically scrutinized during subsequent monitoring rounds.
  - Elevated Tritium activity was detected in Unit 3 Manhole A2 during routine 80-10 Effluents Program sampling during Q2 2009. This manhole is located proximate to the Unit 3 FSB. Subsequent re-sampling of this manhole showed rapidly decreasing Tritium activity, indicating that this was a one-time transient event. This elevated Tritium was also detected in a proximate groundwater monitoring installation (MW-45), likely due to

<sup>&</sup>lt;sup>63</sup> The valve leakage was initially identified during routine visual inspection rounds and immediately terminated. Given that the leak was within the Unit 1 FSB structure, it was documented in a Condition Report under Entergy's Corrective Action Program. This valve leak and repair subsequently came to light within the GPI program during investigations into the cause of the abrupt increase in Tritium levels in MW-42. Additional emphasis has therefore been placed on routine review of these reports as they potentially relate to GPI objectives.

<sup>&</sup>lt;sup>64</sup> As discussed above, additional portions of these releases likely remain above the water table in the release area as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

exfiltration of Tritium from the manhole. As of this quarter (Q4 2009) the Tritium levels in this well have returned to previous levels for two consecutive quarters. While the specific root source of the elevated Tritium is still unclear at this time, Entergy has formulated a plan to investigate a suspected SFP seasonal airborne vapor depositional source.

As such, these data support the validity of the current CSM for use as a basis for Long Term Monitoring Program design. It is further noted that, while a portion of these three documented localized leakage events traveled directly to the saturated groundwater regime and resulted in the observed transient "peaks" in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

- Based on the Q4 2009 data, as well as that collected during previous quarters, it currently appears that the <u>Tritium</u> I.L.s originally established are somewhat too sensitive relative to natural seasonal/precipitation-driven transient variations in radionuclide activities, as well as the variability inherent in the laboratory analyses. Relative to <u>Strontium</u> from the Unit 1 SFPs, the previous increases in activity in a number of monitoring points, due to the previous Unit 1 defueling activities, limit our ability to establish Strontium baseline levels for assessment of new I.L.s pursuant to the Monitored Natural Attenuation (MNA) of this plume. It is anticipated that this additional Strontium activity will take a number of quarters to flush through the onsite groundwater flow system and attenuate to reasonably stable levels. As such, the originally established I.L.s will continue to be used until sufficient data is collected to allow re-evaluation of I.L. levels for the radionuclides of interest.
- As discussed in the Q2 2009 report, GZA believes that sufficient seasonal/yearly data had been collected through Q2 2009 (nine quarters of data<sup>65</sup>) to allow recalibration of the Precipitation Mass Balance Model. This Model, as used to compute groundwater flux through the Site as part of the radionuclide dose computation, was therefore recalibrated during Q2 2009. To be conservative, the model was recalibrated to the quarter yielding the highest, rather than average, computed dose (Q4 2008 Darcy calculations). This will result in a high, conservative bias to the dose computation for this quarter (Q4 2009), as well as all subsequent quarters going forward.
- From both qualitative and quantitative perspectives, the most recent quarterly data (Q4 2009) provides further support to the conclusion that the overall <u>Tritium activity in the Unit 2 plume</u> is decreasing. These reductions have become particularly evident on the more recent quarterly report **Figures 6** and **6A** where the shaded plume <sup>66</sup> no longer extends to the river as it did prior to Q2 2009. It is further visually evident from **Figure 6A** that the core of the plume (with quarterly rolling average activities greater than 100,000 pCi/L and 2007

\_

IPEC00224864

<sup>&</sup>lt;sup>65</sup> After reviewing the groundwater elevation and precipitation data from the Indian Point meteorological station over the time period from Q2 2007 to Q2 2009, it was concluded that sufficient seasonal data had been collected to encompass the majority of the precipitation variability observed over the last fourteen years (fifty-six quarters); see analysis in Appendix H of the Q2 2009 LTM Report.

The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value. This plume delineation boundary value equates to one-quarter of the drinking water standard for Tritium. Although GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site, the MCLs do provide a useful benchmark for comparisons of relative human risk. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

bounding core activities greater than 250,000 pCi/L) has also shown a marked decrease in concentration and extent. Additionally, the 50,000 pCi/L isopleth no longer encompasses MW-111 in Q4 2009 (first time since the initiation of the LTMP). Based on the data and analyses provided above, our conclusion is that the Tritium plume is undergoing long-term, overall reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP<sup>67</sup>, the Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation.

The overall Strontium activity within the Unit 1 plume had generally been stable or decreasing in response to the West Pool demineralization activities conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs resulted in an initial, noticeable increase, followed by a subsequent and commensurate decrease, in Strontium levels proximate to the SFPs, with later indications of increases in the downgradient Strontium levels (see Figure 7 and 7A). This is as was predicted given the requirement to temporarily raise the pool levels for rod removal, thus increasing leakage rate from the SFPs<sup>68</sup>. As anticipated, the levels proximate to the pool have decreased to pre-defueling Strontium levels, and levels downgradient of the pool are also beginning to decrease as this additional Strontium-contaminated water flushes through the groundwater flow system. It is expected that this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also resume an overall downward trend once this perturbation is finished passing through the system. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation. However, as indicated above, the establishment of updated I.L.s for the Unit 1 Strontium plume must await return to the original Strontium baseline levels existing prior to Unit 1 defueling.

<sup>-</sup>

Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologo Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the more recent behavior observed in the Unit 2 collection box data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms. In this regard, it is noted that these analyses cannot definitively and completely rule out the possibility of a remaining small leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s). While it is not possible to quantify the size the minimum detectable leak with any degree of certainty, we believe that the maximum leak rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time, as based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of greater than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program, this amount of Tritium release to the river is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

<sup>&</sup>lt;sup>68</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

#### **TABLES**

Table 1	Groundwater Sampling Methods, Equipment, Frequency, and Depths
Table 2	Historic Quarterly Low Tide Groundwater Elevations
Table 3	2009 4th Groundwater Analytical Results and Averages
Table 4	2009 4th Quarter Groundwater Analytical Results and I.L.s
Table 5	Historic Groundwater Analytical Results

## TABLE I GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS INDIAN POINT ENGERGY CENTER BUCHANAN, NY

			Projected 2010 Sampling Frequency <sup>2</sup>	SAMPLING INTERVAL <sup>3</sup>				SAMPLING DEPTH	
Well ID <sup>1</sup>	Sampling Method	Sampling Equipment Used		Ft Below Top of Casing		Elevation in Feet msl		SAMPLING	3 DEPTH.
Well ID	Sampling Method			Тор	Bottom	Тор	Bottom	Feet Below TOC	Elevation in Feet msl
MW-30-69	Waterloo Low I low	Waterloo Multilevel System	Quarterly	67.3	71.3	8.4	4.4	(6) 3	6
MW-30-84	Waterloo Low I low	Waterloo Multilevel System	Quarterly	77.3	85.4	-16	-9.5	83.8	-8
MW-31-49	Waterloo Low I low	Waterloo Multilevel System	Quarterly	34.8	49.3	40.8	26.3	48.8	26
MW-31-63	Waterloo Low I low	Waterloo Multilevel System	Quarterly	55.3	63.8	20.3	11.8	63.3	12
MW-31-85	Waterloo Low I low	Waterloo Multilevel System	Quarterly	69.8	85.4	5.8	-96	84.8	-9
MW-32-59	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	28.3	61.3	48.8	15.8	58.8	18
MW-32-85	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	79.3	92.8	-2.2	-157	85.3	85
MW-32-131	Waterloo Low 1 low	Waterloo Multilevel System	Inactive	125.8	1383	-48 7	-612	130.8	-53
MW-32-149	Waterloo Low I low	Waterloo Multilevel System	Quarterly	125.8	156.8	-70.2	-79.7	149.3	-72
MW-32-173	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	165.8	174.3	-88 7	-97.2	172.8	-95
MW-32-190	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	180.3	193.9	-103.2	-116-8	190.3	-113
MW-33	Low Flow	Peristalue Pump	Annually	8.0	30.0	10.6	-117	16	2
MW-31	Low Flow	Peristalue Pump	Inactive	5.0	30.0	13.5	-11.5		2
MW-35	Low Flow	Peristalue Pump	Annually	6.5	30.0	12.1	-11.4	15.0	3
MW-36-24 <sup>5</sup>	Low Flow	Peristaltic Pump	Quarterly	11.0	210	0.8	-12.2	17.0	-5
MW-36-11	Low Flow	Penstaltic Pump	Inactive	36.0	11.0	-212	-29.2	37.0	-25
MW-36-52	Low Flow	Peristalue Pump	Quarterly	18.0	53.0	-36.2	-112	50.0	-38
MW-37-22	Low Flow	Peristalue Pump	Quarterly	12.0	22.0	3.0	-7 ()	17.0	-2
MW-37-32	Low Flow	Peristalue Pump	Quarterly	28.0	32.5	-13.0	-17.5	29.0	-11
MW-37-40				38.5	10.5	-23.5	-17.3		-21
MW-37-57	Low Flow	Peristaltie Pump Peristaltie Pump	Quarterly Quarterly	52.0	57.0	-23 3	-213 -42()	55.0	-40
MW-38	Low Flow		Inactive	5.0	40.0	93	-25 7	25.4	-11
MW-39-67	Waterloo Low I low	Penstaltic Pump		65.0	70.5	150		670	-11
		Waterloo Multilevel System	Semi-Annually			3.5	9.5 -5.0	83.5	
MW-39-84 MW-39-102	Waterloo Low How	Waterloo Multilevel System	Serm-Annually	76.5 93.0	85 ()				-3
	Waterloo Low I low	Waterloo Multilevel System	Sem-Annually		103 0	-13 ()	-23 ()	101.5	-21
MW-39-124	Waterloo Low 1 low	Waterloo Multilevel System	Serm-Annually	115 0	126-5	-35 ()	-46.5	124 0	-44
MW-39-183	Waterloo Low I low	Waterloo Vultilevel System	Semi-Annually	169 5	186.0	-89.5	-106.0		-102
MW-39-195	Waterloo Low Flow	Waterloo Vlultilevel System	Semi-Annually	193.0	198 6	-113.0	-1184	195.0	-115
MW-10-27	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	18.2	35.2	55 ()	38.0	26.7	16
MW-10-16	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	112	53 7	29.0	19.5	16.2	27
MW-10-81	Waterloo Low Flow	Waterloo Viultileyel System	Quarterly	617	812	8.5	-110	80.7	-7
MW-40-100	Waterloo Low I low	Waterloo Multilevel System	Quarterly	93.2	106.7	-20 0	-33.5	100.2	-27
MW-40-127	Waterloo Low I low	Waterloo Multilevel System	Quarterly	125.2	136.7	-52 ()	-63.5	127 2	-541
MW-10-162	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	158 7	190.3	-R5 5	-116.9	161.7	-88
MW-11-40	Low Flow	Peristalue Pump	Quarterly	22.0	12.0	32.9	12.9	36.0	18
MW-11-63	Modified Well Vol. Purge	Waterra Pump	Quarterly	59.0	64.0	-11	-91	61.0	-6
MW-42-49	Modified Well Vol. Purge	Submersible Pump	Quarterly	31 ()	51.0	38.7	18.7	41.0	28
MW-42-78	Modified Well Vol. Purge	Waterra Pump	Quarterly	69 ()	79.0	0.7	-9.3	74 ()	-4
MW-43-28	Low Flow	Submersible Pump	Quarterly	8 ()	28 0	40.8	20.7	23 ()	25
MW-43-62	Low How	Sulmnersible Pump	Quarterly	42 ()	62 ()	6.8	-13.2	54 ()	-5
MW-44-66	Modified Well Vol. Purge	Submersible Pump	Quarterly	52 ()	67.0	41.5	26.5	63.0	30
MW-11-102	Modified Well Vol. Purge	Waterra Pump	Quarterly	79.0	104.0	14.5	-10.5		13
MW-15-12	Modified Well Vol. Purge	Peristaltie Pump	Quarterly	27 5	12.5	26.2	11.2	37.0	16
MW-15-61	Modified Well Vol. Purge	Peristalue Pump	Quarterly	51.5	61.5	2.2	-7 R	58.0	- 1
MW-16	Modified Well Vol. Purge	Submersible Pump	Quarterly	6.0	30.0	12.1	-119		7
MW-47-56	Low Flow	Submersible Pump	Inactive	36.0	56.0	34.3	14.3	52.0	18
MW-17-80	Modified Well Vol Purge	Waterra Pump	Inactive	70.0	80.0	0.3	-9.7	72.0	-1

<sup>1 17.000-18.999 17869 17869-91</sup> NG 2009 - Quarter 4 Fables , Fablet - Q4-09 Multooks, Frequency, Depths x1sx, Methods , Frequency, Depths

Page 1 of 3 See Page 3 for Notes

## TABLE I GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS INDIAN POINT ENGERGY CENTER BUCHANAN, NY

Well ID <sup>1</sup> MW-18-23  MW-48-37  MW-49-26  MW-49-42	Sampling Method  Low Flow Low Flow	Sampling Equipment Used	Projected 2010 Sampling Frequency <sup>2</sup>	Ft Below To	p of Casing	Elevation in	Feet msl	SAMPLING	DEPTH.
MW-18-23 MW-48-37 MW-49-26	Low Flow Low Flow		Sampling Frequency <sup>2</sup>		F				
MW-48-37 MW-49-26	Low Flow			Тор	Bottom	Тор	Bottom	Feet Below TOC	Elevation in Feet msl
MW-49-26		Peristalue Pump	Inactive	8.0	23.0	7	-76	15 8	-()
		Peristalite Pump	Inactive	33 ()	38.0	-17.6	22.6	35.8	-20
MW-49-42	Low Flow	Peristalite Pump	Quarterly	15.0	25.0	-0.3	-10.4	20.0	_6
	Low Flow	Peristalite Pump	Quarterly	32 ()	42.0	-174	-27 4	37 ()	-23
MW-49-65	Low Flow	Peristalite Pump	Quarterly	60.0	65.0	-454	-50.4	61.0	-40
MW-50-12	Low Flow	Peristalue Pump	Quarterly	22.0	12.0	-7 [	-27 [	27.0	-13
VIW-50-66	Low Flow	Peristaltie Pump	Quarterly	62.0	67.0	-17 ]	-52 1	60.0	-1
MW-51-40	Waterloo Low I low	Waterloo Multilevel System	Quarterly	29.7	44.2	38 ()	23.5	39.7	2
MW-51-79	Waterloo I ow I low	Waterloo Multilevel System	Quarterly	63.2	81.2	4.5	-13.5	78 7	-1
MW-51-104	Waterloo Low I low	Waterloo Multilevel System	Quarterly	101.2	1112	-33.5	-43.5	103.7	-3
MW-51-135	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	130.2	143.7	-62.5	-76.0	135.2	-6
VIW-51-163	Waterloo Low Flow	Waterloo Viultilevel System	Quarterly	1517	166.2	-87.0	-98.5	162.7	-9
VIW-51-189	Waterloo Low Flow	Waterloo Viultilevel System	Quarterly	1812	197.8	-116.5	-129 9	189.2	-12
VIW-52-11	Modified Well Vol Purge	Peristalue Pump	Annually	2.0	12 0	118	18	10.0	
MW-52-18	Waterloo Low Flow	Waterloo Viultilevel System	Annually	10.0	30.0	19	-15 1	17.5	
VIW-52-16	Waterloo Low Flow	Waterloo Viuliilevel System	Annually	48.0	56.0	-33 1	-411	48.0	-3
MW-52-64	Waterloo Low How	Waterloo Multilevel System	Annualls	59.0	71.5	-44.1	-56.6	64.0	-4
MW-52-122	Waterloo Low Llow	Waterloo Multilevel System	Annually	110.5	123.5	-956	-1086	122 0	-10
MW-52-162	Waterloo Low How	Waterloo Vultilevel System	Annually	154.5	164.0	-1396	-149 J	161.5	-14
MW-52-181	Waterloo Low How	Waterloo Vultilevel System	Annually	171.0	198 1	-156 J	-183 ()	181.0	-16
VIW-53-82	Low Flow	Submersible Pump	Quarterly	62.0	82.0	83	-11.7	75.0	-10
MW-53-120	Modified Well Vol Purge	Waterra Pump	Quarterly	100.0	120.0	-29.7	-49.7	105.0	_3
MW-54-37	Waterloo Low I low	Waterloo Multilevel System	Quarterly	29.0	42.0	-159	-28 9	36.5	
MW-54-58	Waterloo Low I low	Waterloo Multilevel System	Quarterly	51.5	64.0	-38.4	-50.9	57.5	
MW-54-123	Waterloo Low Llow	Waterloo Multilevel System	Quarterly	116.0	126.0	-102.9	-112 9	123.0	-10
MW-54-144	Waterloo Low I low	Waterloo Multilevel System	Quarterly	135.0	155.5	-1219	-142 4	144 0	-13
VIW-51-173	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	170.5	182 0	-157 4	-168.9	172.5	-1.5
VIW-51-173	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	185 0	203.6	-171 9	-106.5	190.0	-17
VIW-55-24	Low Flow	Peristalue Pump	Quarterly	110	210	13	-1703 -5 R	16.0	-17
VIW-55-35	Low Flow	Peristalue Pump	Quarterly	30.0	350	-11.8	-16 R	32.0	-1
VIW-55-54	Low Flow	Peristalue Pump	Quarterly Quarterly	11.0	510	-11 h	-10 h	17.0	-1
VIW-56-53	Modified Well Vol. Purge	Submersible Pump	Semi-Annually	49.2	54.2	-23 h 21 0	-35 6	52.0	
MW-56-83	Modified Well Vol. Purge		Semi-Annually	69.9	84.9	0.4	-14.6	74.0	
MW-57-11	Modified Well Vol. Purge	Waterra Pump Peristaltic Pump	Armuelly	60	U 0	9 ()	4 ()	10.0	
vIW-57-20			Annually	15.5	20.5	-0.5	-5.5	19.0	
vIW-57-20 vIW-57-15	Modified Well Vol Purge	Peristalue Pump	Annually	30.5	15.5	-155	-30 5	190	-1
MW-58-26	Modified Well Vol. Purge Low Flow	Peristaltie Pump	Semi-Annually	16.0	26.0	-13 3	-114	20.0	
		Peristaltic Pump		50.0	65.0	-1 +	-11 +	54.0	
MW-58-65 MW-59-32	Low Flow	Peristaltic Pump	Serm-Annually	21.0	31.0			27.0	_3 -1
	Low Flow	Peristaltic Pump	Inachve			-6.5	-16.5		
MW-59-45	Low Flow	Peristaltic Pump	Inactive	35 ()	45.0	-20.5	-30.5	42.0	-2
MW-59-68	Low Flow	Peristaltic Pump	Inactive	53.0	68.0	-38 5	-53.5	58.0	-4
vIW-60-35	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	24.9	39.4	-12 4	-26.9	349	-2
vIW-60-53	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	15 1	59 1	-32.9	-16.9	53 4	-
vIW-60-72	Waterloo Low Flow	Waterloo Vultilevel System	Quarterly	66 1	78.9	-53 9	-66 4	72.4	-5
vIW-60-135	Waterloo Low Flow	Waterloo Viultilevel System	Quarterly	1219	1414	-112 4	-128 9	134.9	-12
VIW-60-154 VIW-60-176	Waterloo Low Flow Waterloo Low Flow	Waterloo Viultilevel System Waterloo Viultilevel System	Quarterly Quarterly	117 1	1619 2004	-1319 -1584	-152 ·1 -187 8	154 4 175 9	-1: -10

<sup>1-17,000-18,999-17869-17869-91-</sup>XG-2009--Quarter 4-Fublus ; Fublul - Q4-09-Xelbuds, Frequency, Depths xlxx, Methods ; Frequency, Depths

Page 2 of 3 See Page 3 for Notes

#### IPEC00224868

## TABLE I GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS INDIAN POINT ENGERGY CENTER BUCHANAN, NY

					SAMPLING	INTERVAL <sup>3</sup>		SAMPLING	DEBLIH
Well ID <sup>1</sup>	Sampling Method	Sampling Equipment Used	Projected 2010 Sampling Frequency <sup>2</sup>	Ft Below Top of Casing		Elevation in Feet msl		SAMPLING BEFTI	
***************************************				Тор	Bottom	Тор	Bottom	Feet Below TOC	Elevation in Feet msl
MW-62-18	Low Flow	Peristalue Pump	Quarterly	1.7	117	10.0	0.0	13.5	1.2
MW-62-37	Low Flow	Peristalite Pump	Quarterly	33.3	38.3	-186	-23 6	34.5	-198
MW-62-53	Waterloo Low I low	Waterloo Multilevel System	Quarterly	49.6	54.1	-36.8	-413	53 J	-40.3
MW-62-71	Waterloo Low I low	Waterloo Multilevel System	Quarterly	61.1	82.6	-48.3	-69.8	71.1	-58.3
MW-62-92	Waterloo Low I low	Waterloo Multilevel System	Quarterly	88.6	99 [	-75 8	-86.3	91.6	-78 8
MW-62-138	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	126 1	113.6	-113.3	-130.8	138.1	-125 3
MW-62-182	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	177.6	1987	-1618	-1857	182 1	-169.3
MW-63-18	Low Flow	Penstaltie Pump	Quarterly	8.0	18.0	-3.8	-13.8	14.9	0.7
MW-63-34	Low Flow	Peristaltic Pump	Quarterly	30.0	35.0	-158	-20.8	31.5	-17.3
MW-63-50	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	415	58.0	-29.2	-457	49.5	-37.2
MW-63-93	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	81.5	100.5	-(4) 2	-88.2	93 ()	-80.7
MW-63-112	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	106.5	112.0	-94.2	-99.7	111.5	-99 2
MW-63-121	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	118.0	127.5	-1057	-115 2	121.0	-108.7
MW-63-163	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	150.5	165.0	-138.2	-152 7	162.5	-150 2
MW-63-174	Waterloo Low Flow	Waterloo Vlultilevel System	Quarterly	168.0	191.1	-1557	-178 6	174.0	-161.7
MW-66-21	Modified Well Vol. Purge	Portstalne Pump	Quarterly	7.0	27.0	6.0	-7 (1	14 1	0
MW-66-36	Modified Well Vol. Purge	Pensialtie Pump	Quarterly	31.0	36.0	-17 ()	-22 ()	33.6	-19.5
MW-67-39	Waterloo Low I low	Waterloo Multilevel System	Quarterly	28.8	54.3	-15.8	-413	38.3	-25 8
MW-67-105	Waterloo Low I low	Waterloo Multilevel System	Quarterly	90.3	110.8	-77.3	-97.8	104.8	-92.3
MW-67-173	Waterloo Low I low	Waterloo Multilevel System	Quarterly	164.8	188.3	-151.8	-175.3	172.3	-159.8
MW-67-219	Waterloo Low Flow	Waterloo Viultileyel System	Quarterly	209 3	229 8	-1963	-216.8	218 8	-206.3
MW-67-276	Waterloo Low I low	Waterloo Multilevel System	Quarterly	250.8	281.3	-237.8	-268.3	275.3	-262 8
MW-67-323	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	317.8	328.3	-304.8	-315.3	322.3	-309.8
MW-67-340	Waterloo Low 1 low	Waterloo Multilevel System	Quarterly	3353	347.9	-322.3	-334.9	339.8	-327.3
MW-107	Low I low	Submersible Pump	Annually	105.1	126.1	34.9	13.9	32.7	1.10.1
MW-111	Low Flow	Peristaltie Pump	Serm-Annually	11.6	17.4	7.0	1.5	16.5	2.4
U3-41)	Modified Well Vol. Purge	Pensulue Pump	Quarterly	25 0	27.6	-10.2	-12 8	25.6	-10 <b>8</b>
U3-11	Low Flow	Peristalue Pump	Quarterly	0.2	1.2	3.1	2.1	5.7	2.8
U3-12	Low Flow	Peristalue Pump	Quarterly	0.6	1.6	2.7	1.7	5.7	2.6
U1-CSS	Low Flow	Peristalue Pump	Semi-Annually	NA	10.2	NΑ	19	110	6.1
LAF-002	Low Flow	NA	Semi-Annually	NA	NΛ	NΑ	NA	NA	-22 3
UI-NCD	Grab	NA.	Quarterly	NA.	NΑ	NΑ	NΑ	NΛ	NA.
U1-SFDS	Grab	NA.	Quarterly	NΛ	NA.	NΑ	NΑ	NΛ	NΑ
MH-56	Cirab	NA	Quarterly	NA	NΛ	NΛ	NΛ	NΛ	NΑ
13-1 <sup>6</sup>	Grab	NA	Quarterly	NA	NΑ	NΛ	NΑ	NΑ	NΑ
B-6 <sup>6</sup>	Grab	NA	Quarterly	NA	NΑ	NΑ	NΑ	NΛ	NΑ

- Note:

  1 For nested multi-level monitoring wells, suffix of well IID indicates depth (nounded to nearest foot) from reference point on casing to bottom of well screen For Waterloo multi-level systems, suffix indicates depth (nounded to nearest foot) from reference point on casing to bottom of well screen suffix are open bedrock wellbores.

  2 Projected sampling frequencies presented for 2010 are subject to change.

  3 For nested multi-level monotomic wells, interval includes well screen and sand pack. For Waterloo multi-level systems, interval includes open wellbore between holotion of 15 packer above, and top of 15 packer below sampling port. For open bedrock wellbores, interval extends from bottom of casing to bottom of hole.

  4 Sampling depths within sampling intervals (i.e. location of pump intake) have been located adjacent to a transmissive zone where possible.

  5 Dat pattern denotes sampling interval is positioned within overburden. Open box indicates sampling mierval is in bedrock.

  6 These locations are storm drains.

T. 17.000-18.999 17869 17869-91 MG 2009 - Quarter 4. Fables ; Fablet - Q4-09 Methods, Fraquency, Depths xlxx, Methods, Fraquency, Depths

Page 3 of 3 See Page 3 for Notes

#### IPEC00224869

#### TABLE 2 HISTORIC QUARTIFICA LOW THE GROEN NOW VIEW ELFVATIONS INDIAN POINT EAGERGY CENTER BUCHANAN, NY

Well ID	II .										
	Ouarter 21, 2007	Ouarter 32, 2007	Ouarter 4 <sup>3</sup> , 2007	Ouarter 12, 2008	Ouarter 25, 2008	(Feet msl) Ouarter 3 <sup>6</sup> , 2008	Quarter 4, 2008	Quarter 18, 2009	Quarter 29, 2009	Ouarter 310 11, 2009	Quarter 4 <sup>13</sup> . 2009
IR-I	NA.	-1) 86	-1 57	-2 15	-1 13	-1 (15	-1 69	-128	-1 52	-i) 27	-3 59
-2	50.23	48 62	51.87	53 73	52 11	52 90	50.75	NΑ	NΛ	NΑ	51.69
MW-30-69	11.83	11.53	12 00	NΛ	12.28	11.77	11.71	12.33	. 11.84	13.76	NΑ
MW-30-81	12 77	12 17	12.83	NA	13.06	12 68	12.36	13.13	12.82	12.18	12.27
MW-11-19	44 09	NA	45.10	17.50	46.1.1	15.39	44.13	16.11	45 10	-	-
MW-31-63	11.56	NA	12.71	15.52	13.96	12.17	11.21	11.12	13.20	-	-
MW-11-85	.49.59	NA	40.81	13.19	41.89	Ji) 58	.49.64	12 10	40.61	-	-
MW-32-48	NΛ	42.12	46.73	48.81	47.77	46.98	45.79	48 08	47.31		
MW-32-59	NΛ	41.44	45.00	47 99	46.75	45 72	44.48	46.83	45.62		
MW-12-85 (MW-12-92)	10.27	12 15	12.78	13.30	13.17	12 30	12 16	12 (0)	. 11.61		
MW-32-131 (MW-32-140)1-	13.11	11.96	13 21	25 01	15 67	11.34	11.53	11.86	11 06		
	1						9 77				
MW-32-149 (MW-32-165) <sup>1-</sup> MW-32-173	8 18	9 87	. 10 06 9 86	10 20 9 92	9 70	971 945	977	9 68	. 9 18 8 81		
	NΛ									-	-
MW-32-190 (MW-32-196)1-	6.74	8 05	7.88	7 88	7 52	7.16	7 05	7.24	. 6.26		
MW-33	10.08	0.80	10.38	11.49	11 66	10.55	10.60	11.23	10 52		
MW-34	9.87	9 82	10 44	11.63	12 03	10.54	10.54	11 25	6.71	-	-
MW-35	10 03	9.67	10.37	11 65	12 06	10 68	10.68	11.36	. NA		
MW-36-24	8 89	7.31	7.67	6.85	6.86	7.58	9 05	NΛ	. 7.25	-	-
MW-36-11	8 22	NA	NA	NA.	NA	NA	NA.	NA	NA	-	-
MW-16-52	7.43	6.43	6.45	6 12	6.29	6 99	7.45	8 1 2	6.62	-	-
MW-37-22	5.51	5 15	4 83	1 66	418	5.36	5 55	4 45	. 5 24		
MW-37-32	5.51	5 07	4 82	4 63	4 05	5.36	5 (4	4 55	5.32	-	-
MW-37-11)	5.40	6.83	6.19	6 17	5.95	6.18	6.03	5.46	6 19		-
MW-37-57	7 07	6 23	6.39	6.28	6 07	6 64	7 20	6.50	6 56		
MW-38	3.01	2 19	1.46	2 22	1.53	2 12	1 22	NΛ	. 2 24	-	-
MW-19-67	NA.	NA	26.81	32.20	31.69	25 96	25 21	28 7 1	NA	-	-
MW-19-81	NA.	NA	26.61	31.94	31.48	25.78	25 12	28 62	. NA		-
MW-39-100	NΛ	NA.	26 38	30 99	31.34	25.52	2179	28 32	NA		-
MW-49-102	NA	NA	26 31	31.56	NA_	NA	NA.	NA	, NA	-	
MW-39-121	NA NA	NA NA	26 05	28.37	30.67	25 07	2143	27.71	. NA	-	-
MW-39-183	NΛ	NA	25 28	29 74	29 83	22 33	23 79	26.78	. NA		
MW-39-195	NΛ	NA	24.36	28 80	28 89	23 35	22 70	25 63	. NA		
MW-10-27	NA NA	NA 12.22	55 16	60.39	59 99	54.70	5122	59 53	57 25	58.75	55.71
MW-40-46	NΛ	47.27	53 19	59.35	59 (19	52 57	52.35	59 13	56 56	-	
MW-10-81	NA.	41 65	47.15	56 06 54 10	55.78 53.75	17 28	46 83	55 67	53.13	-	-
MW-10-100 MW-10-127	NA NA	18 89	45 18 44 60	5110	53.75 53.39	11.83	44.32	53 59 53 29	. 51.21	-	-
										10.15	12.00
MW-40-162	NΛ	36 67	41.09	50 49	50 26	41.32	40 66	49 76	. 46 80	. 48 42	42.85
MW-41-40	29 87	NA	32 48	36 57 33 31	33 81 32 76	31 28	30.71	33 62	32 05	-	-
MW-41-63	25 04	NA NA	. 27 77 34 55	33.31 34.96		. 27 53	26 % 34 43	30.38	. 28 39 34 47		
MW-42-49 MW-12-78	NA NA	NA NA	34 33 35 71	36 63	34.81 36.28	34 52 55 38	35 117	34.78	. 34.47		-
MW-12-78 MW-13-28	32.75	31.08	31 98	10 0.5	33 95	32.51	32.15	53 13	32.51	32 66	NA.
MW-43-62	30 83	NA NA	31 98 NA	NA.	33 93 32 16	30 48	32 15	34.13	30 88	32 00 NA	30.28
MW-44-67	33 36	NA NA	34 36	NA 37 99	32 10 35 47	30 48 35 29	31 76 34 00	54 1.5 34 96	. 30 88	NΛ	30.28
MW-11-102	23 10	NA NA	24.81	NA	30.88	25.86	25 16	28 09	27 11	-	
MW-45-42		24 82	28 47	34 19	37 16	28 63	25 45	32 02	29 03		
MW-45-61	NA NA	24 33	27.57	32.91	32 46	27 16	25 45	. 29 99	23 25		
MW-46	12.80	24 33 11 95	12.57	32 91 15 05	32 46 14 97	12 62	26 68 12 81	29 99 14 29	. 23.25	12.83	NΛ

2. 2006. \$560. [800] 2800 (AP) 2006. Qualet 1, tible 1. Tools 2. Qualet CW to attend the action of contrasts.)

Page Lock See Page New Yorks

#### TABLE 2 HISTORIC QUARTIFICA LOW THE GROEN NOW VIEW ELFVATIONS INDIAN POINT EAGERGY CENTER BUCHANAN, NY

					LOW RIVER		VIER ELEV VIIO	NS.			
Well ID	Ouarter 2', 2007	Ouarter 32, 2007	Ouarter 4 <sup>3</sup> , 2007	Ouarter 12, 2008	Ouarter 2*. 2008	(Feet msl) Ouarter 3 <sup>6</sup> , 2008	Ouarter 4 . 2008	Ouarter 18, 2009	Ouarter 2°, 2009	Ouarter 310 11, 2009	Ouarter 4 <sup>13</sup> , 2009
MW - 17-56	21.83	20.77	23 05	27.76	31.53	22 84	22 17	26.51	23 13		
MW-17-80	22 29	21 11	21 82	26 53	28 35	21 52	21 08	26 37	24.18		
MW-48-23	-0.08	-0.27	-0.39	-1.14	-0.23	-0.18	-0.48	-0.91	-0.10		
MW-48-37	0.64	0.20	-0.06	-0.18	0.32	0.06	-0.15	-0.50	0.04		
MW-19-26	1.04	NA.	-0.37	-0.62	0.51	0.37	0.19	-0.25	0.51		
MW-49-42	0.31	0.90	0.40	-0.44	0.92	1 02	0.68	-0.06	0.51		
MW-19-65	0.89	1.01	0.34	0.07	0.70	0.68	0.17	-0.08	0.57		
MW-50-12	7 24	NA.	NA.	NA.	521	6.40	7.06	5 66	6 09	-	
MW-50-66	3.71	NA NA	NA.	1.97	221	2.83	2 34	1.95	2 82		-
MW-51-40	NA.	48 60	50.07	51.95	52.35	49 44	49.24	49.32	45 15	40.45	42.45
MW-51-79	NA NA	39 92	41.07	42 91	44 17	+0.71	40.36	42.75	42 15	. 40.45	42.45
MW-51-102	NA NA	35 98	38 07	38 40	39 04	36 56	36 17	38 18	37.78	=	-
MW-51-102 MW-51-104	NA NA	NA NA	37.93	38 41	39 02	36 49	36 03	37 99	37 49		
MW-51-135	NA NA	17 12	39 17	39 99	40.71	38 10	37.68	89.75	. 37.49	-	-
MW-51-163	NA NA	13.79	34.83	36 15	36 77	3130	33.90	35.71	35.11		
MW-51-169	NA NA	29 33	30.16	31.34	30 77 31 79			30.81		32.18	29.93
	6.04			8.47		29 65 8 65	29.36 8.44		10.48	.92 18	29.93
MW-52-11		5.61	8 12		8.85			8 19	9 20	-	-
MW-52-18	6.64	NA	8 6.1	6.01	6.07	5.89	6.02	5.78	5 87	-	-
MW-52-48	7.08	NA	6.55	6.53	5 95	6.20	6 14	6.05	5 75		
MW-52-64	5 96	NΛ	5 90	5.25	5 03	5.21	5 16	5 20	4 89	-	-
MW-52-118	5.34	NA	141	4.11	1.32	4.36	1.68	4.23	1 23	-	-
MW-52-122	5.25	NA	1.26	4 32	118	4.21	1.55	4.11	. 120	-	-
MW-52-162	0.67	NA	-0.80	-1.31	-0.80	-0.98	-1.30	-2 07	-1.18		-
MW-52-181	0.41	NA	-1 08	-1.56	-1 ()()	-1.30	-1 fel	-2.38	-1.51		-
MW-53-82	N/A	9 59	10.03	11 99	12 60	10.35	NA	11 11	. NA	11.11	9.87
MW-53-120	991	9.18	9.59	10.87	11.49	9 76	NΛ	10.55	. 978	10.43	9 43
MW-54-35	NΛ	NΛ	6.40	6.27	6.36	6.16	6.41	5.75	5.87		
MW-51-37	7 52	NA	6.58	6.15	6.53	6.30	6.58	5.90	6 (14)		-
MW-54-58	6.86	NA	5 82	5.60	5 55	5.53	5 76	5 49	5 1 7	-	-
MW-51-123	5 69	NA	116	3 65	3 52	4.01	F06	2 99	3.56		
MW-51-111	8.85	NA.	7.13	6.60	6.48	6 92	6.97	5.89	6.53	-	-
MW-51-173	5.17	NA	3.52	2 99	2.85	3 27	3 29	2 19	2 72	-	-
MW-54-190	5 08	NA	3.46	2 1) [	2.76	3.16	3 13	2 00	2 49	-	-
MW-55-24	8.56	7 82	7.97	8.17	816	818	9.02	8.35	8 06	8.39	7.80
MW-55-35	8.10	7.29	7.52	7 60	7.59	7.69	8.30	7.63	0.49	-	-
MW-55-54	8.47	7.65	7.75	8.08	8.32	8 22	8 82	NA	7.89	814	7.66
MW-56-53	21.01	20.16	NA	NA.	29 93	NA	21.90	27 33	22 (16		-
MW-56-83	21 10	20.10	22.18	26.41	29.16	NA.	21.51	25 13	22 60		-
MW-57-11	9.57	8.83	9.36	10 99	NA	](11)3	10.27	11.11	10 (19		-
MW-57-20	9.38	NA	NΛ	NA	12 07	10.02	9 92	10.63	9.84		-
MW-57-15	9.08	NA.	NA.	NA.	10.59	NA.	NA	10.71	NA		-
MW-58-26	8.03	6.49	6.58	8 32	NΛ	7 29	7 19	7.56	7 40		-
MW-58-65	6 03	6.83	6.22	NA.	7.36	7 13	6.46	6.68	6 70		
MW-59-32	1.06	NA.	0.67	0.12	0.77	0.81	0.47	0.31	1.37		_
MW-59-15	1.06	1 27	0.42	NA.	9.21	NA	2.52	0.44	NA.		
MW-59-68	2.91	2.51	1 97	0.90	-0 11	NA.	-1 79	-5 06	7.93	-	

 $_{\rm C}$  2000, (8000) (8000) (8000). At 2000 (Quality 1) ables . Table 2 Quality Quality CW) to alress size on this

Page Notes

#### TABLE 2 HISTORIC QUARTIFICA LOW THE GROEN NOW VIEW ELFVATIONS INDIAN POINT EAGERGY CENTER BUCHANAN, NY

					LOW RIVER		VIER ELEVATIO	NS.			
Well ID	0					(Feet msl)	Quarter 1, 2008	Ouarter 18, 2009	Ouarter 2°, 2009	o	9 Quarter 4 <sup>13</sup> , 2009
			•	,	•	•	•		•	Quarter 3 , 200	9 Quarter 4", 2009
MW-60-35	2.19	1.28	1.32	1.58	1 6.4	0.82	2 (1)	1 99	1.07	-	-
MW-60-53	-0 6.3	-1 24	-1 67	-2 0 1	-1.37	-1.76	-2 11.3	-2.70	. NA		
MW-60-55	NΛ	-0 28	-0 73	-1 10	-0.47	-0.90	-121	-191	, NA		
MW-60-72	0.74	-0.09	-0.45	-0.68	-0.14	-0 64	NΛ	-1 43	0.28		
MW-60-135	0.94	0.11	-1) 44	-(191)	-I) 27	-0.71	-1 02	-1 72	0.11	-	-
MW-60-154	0.08	-0.96	-1.61	-2 07	-1 49	-1 91	-2 25	-2 99	. NA	-	-
MW-60-176	-i) 48	-1.38	-2 (13	-2 17	-1 82	-2.16	-2 59	-141	NA		
MW-62-18	0.25	1) 25	-i) <u>,</u> §7	-(179)	0.13	1) (16	-(±12	-i) 82	NA		
MW-62-37	1) 59	0.61	-I) (I,3	-(1.16	1) 49	1) 59	-(115	-1.13	0.11	-	
MW-62-52	NΛ	0.48	-0.30	-1.13	-0.19	-0.29	-0 93	-1 (14	-0.42	-	-
MW-62-53	0.95	0.54	-0.25	-1.01	-0.10	-0.16	-0.84	-2 03	-0 44		
MW-62-71	0.89	0.22	-0.56	-1 26	-0.55	-0.56	-1.24	-2 15	-1.03	-	-
MW-62-92	1 07	0.58	-0 09	-0.76	-0.11	-0.10	-0.85	-1 68	-0.70		
MW-62-138	1.40	0.77	0 (8)	-(1 19)	0.13	0.26	-(1.17	-1.33	-(i  li)	-	
MW-62-181	1.33	1) 38	-1) 33	-(199)	-0.32	-1) 36	-(192	NA	-0.88		-
MW-62-182	NA.	-1) 3.3	-1.83	-0.78	-1 29	-1.25	-1.85	-2 66	-1.82	-	
MW-63-18	0.14	0.09	-0.10	-0.37	0.09	0.32	-0.08	-0 (14	0.02	-	
MW-63-31	0.51	0.19	-1) (19)	-(1.31)	0.13	1) (15	-0.13	-0.74	0.18	-	-
MW-63-50	0.86	0.29	-0.38	-1.03	-0.47	-0.55	-1.24	-2 08	-0.45	-	
MW-63-91	1.16	0.48	-0 19	-0.87	-0.25	-0 [6	-0.89	NΛ	-0.01		100
MW-63-93	NA.	1) 55	-1) 2(1	-0.87	-(1-31)	-0.24	-(198	-1 68	-0.13	_	_
MW-63-112	0.03	-1) 82	-1.46	-2.05	-1.69	-1.60	-2.26	-114	-1.15		
MW-63-121	1.41	0.60	-0.18	-0.78	-0.21	-0.05	-0.86	-1.49	0.11	_	_
MW-63-163	0.70	-1) (19	-0.83	-1 18	-0.86	-i) 9(i	-1.54	-2 46	-0.98		
MW-63-171	0.88	1) (15	-1) (55	-1 29	-0.62	-0.61	-1 19	-1 97	-(i 59		
MW-65-48	NΛ	NΛ	NΛ	NΛ	38 60	43.22	NA	48 19	36.98	40.08	38.06
MW-65-80	NA NA	NΛ	NΛ	NA.	34.97	32 95	32.72	33.71	33.30	33.79	32.81
MW-66-21	0.26	0.17	-0 22	-(17)	0.05	0.17	0.29	-0.33	(1.50)	0.52	(1 [1)
MW-66-36	0.81	0.48	-0 04	-0.51	0.35	0.15	0.10	-0.86	0.51		-0.25
MW-67-39	NA.	1 02	0.34	-(133	0.36	0.41	-(1112	al) (17	-0.56	0.81	-1.25
MW-67-105	NA NA	1.39	0.61	-(11)}	0.57	0.65	0.16	-i) 67	-0.13		-1 6.7
MW-67-173	NA NA	0.75	-0.14	-(183	-0.28	-0.26	-0.82	-1 62	-1.55		
MW-67-219	NA	0.74	-0 19	-0.91	-0.32	-0.32	-0.86	-1 87	-1 59	-	-
MW-67-276	NA NA	161	0.60	-0.13	0.44	. 041	-0.14	-1 03	-0.91		
MW-67-323	NA NA	0.18	-0.96	-1 75	-1.13	-1.35	-1 93	-1 03	-2 73		-
MW-67-340	NA NA	063	-0.52	-131	-0.87	-0.96	-1.56	-2 42	-2 40	-0.76	-3 27
MW-107	116.85	113.87	117.48	121 79	118.94	115 00	115.76	120.28	117.52	-0 /(1	-321
MW-108	9.58	861	8.77	9.98	1(1)7	NA NA	9 02	9 6 5	9 26	-	
MW-108 MW-109	9.58	6.80	7 22	9.50	10.07	7 82	7.88		9 26	-	-
	9 52		9.74					NA MA	. 947	-	-
MW-111	JJ 9.56	9 66	974	10.74	11.21	9.71	10.48	10.87	9.47	-	-

Lorent, Need (1869) (ASS) - AP-2000. Quarte Lothes Lorent Quarter CWT to access stores on the

Program 4 See Type 4 for Noves

# TABLE 2 HISTORIC QUARTERIA LOW TIPE GROUNDWATER ELFAATIONS INDIAN POINT ENERGY CENTER BUCHANAN, NY

					LOW RIVER	TIDF GROUNDW (Feet msl)	VIER ELEV VIIO	NS.			
Well ID	Quarter 21, 2007	Quarter 32. 2007	Quarter 43, 2007	Quarter 1 <sup>2</sup> . 2008	Quarter 2°. 2008			Quarter 18, 2009	Quarter 29. 2009	Quarter 31011, 2009	Quarter 4 <sup>13</sup> . 20
DUI-1	NA.	1.31	1.16	0.76	0.81	NA	NA	NA	1.08	-	-(±77
W-1	NA.	NA	30.15	NA	31) (1-1	29.52	29 05	29 10	NA		
J1-CSS	NΛ	8 98	NΛ	NΛ	19.11	15.39	NA	20.46	13.89		
J3-1	4 20	NΛ	NΛ	NA.	NA.	NΛ	NA	NΛ	, NV		
13-2	5.34	NA	NA	NA.	NA	NA	NA	NA	NA		
J.33	7.53	6.52	6.63	8 67	9.25	8 25	8.94	913	7.29		
R-11)	1.25	NA	1.35	3 22	271	1.49	2 69	3.41	3.75		
13-18	3.91	113	4 B(1	3.71	.1 97	1.31	3.81	4.01	4.23		
13-C1	NA NA	1.64	1.58	3 16	(1.99	2.36	0.81	0.64	1 92	2.43	0.12
J3- l' i	4.51	4 12	3 67	3 99	3.86	4.33	3 69	3.83	4 12		
13-12	1.33	1.02	1.79	4.20	3.91	1.28	3.76	4 (15	4 20		
5 Quarter 2, 2008 groundwar Quarter 3, 2008 groundwar Quarter 4, 2008 groundwar 8 Quarter 1, 2009 groundwar 10 Quarter 2, 2009 groundwar 11 Quarter 3, 2009 groundwar 11 Subsequent to Quarter 2, The rationale for this rediction	ner elevations were me ner elevations were me ner elevations were me ner elevations were me ner elevations were me arer elevations were me 2009, as described in need transducer redepto	asured on 7 10 08 at asured on 11 11 08 asured on 1 9 09 at, asured on 5 22 09 at leasured on 8 9 09 at our June 14, 2010 m whent is included in	11 35 am at 2 54 am 2 42 am 2 41 pm 8 18 am emorandum which to the June 14, 2010	nemorandum							
are listed in parentheses 3. Quarter 1, 2009 grounds	The current configura	tion intervals MW-3	2-48 and MW-32-1					The state of the s	ar serverprining it.	eon galaton	

 $_{\rm C}$  , 7000 , 8000 , 860 ),  $M^2$  , 2000 . Quarter 11, this situated - Q-200 Quarterly CW. The attended to the constraint and

Piese 4 or 4 San Ago 4 for Noves

#### TABLE 3 FOURTH QUARTER 2019 GROUNDWATTER AND THEAT HEAT HY TAP AVERAGES INDIAN POWER FOR GUARTER BY LIMAN AS A STAFF

													INDIAN POINT	ZIZ ZI	i.K												
			SAMPLE ZONE	SAMPLE ZON			T						v	VIASIS RESI I	TS								YEARI.	V ROLLING W	DR AGES!		
wen m'	SAMPLING OLARTER <sup>2</sup>	SAMPLE ID	CENTER Depth ELBelow	CENTER	SAMPLEC	OFFECTION		гатим фо	)		Se 90 (pC) E)			C+13° (pC+1)			Co 65 (pt +15)			N 63 grC+14		DOLL (PCC)	5i 5% (pt i 1.)	CV 137 (pto L)	Co 6º (pt) 11	% 63 (p() 1.)	WHID
			lop of Cavoz	Flevarian Pt out	Date	lime	Result	Nid Des	ALDI	Result	Std Des	ADI	Result	Still Des	ADC.	Result	Std Des	NUK	Result	Std Dm	ADC	Assuage	Average	Annage	Annage	Average	1
X39530-69	Q1-2909	024	61	51	1140 2009	21.00	14,116	2,591503	1.881.72	4 104	2885401	9.135/38	-, 130° (6	2.646, 91	2,641 - 24	. 165 16	3 16 (6)	1,046.66	5.8	1.0	71	100.9	(4)	V)	NO	4.5	3477-39-09
VW # 10	Q2211 Q1316374	64	45.1	1.1	11217	15.0	826 (1	3 -01, 12	f 1.	3 5 11	4331.11	1.35	* 6" 10	587 11	6431 #	420.01	4.50	- Pr. 11	N.A.	7.1	5.4						
100 mm.	Q5-21 6 Vac	1.5. C	961	6.1	512.0.6	0.0	9.5, 64	. "T (1	27 . 1.	4.791 /2 -2.15.45	5 C r	2.111.	2.60 o 655.00	\$ 321 m	6.1. 11	119 =	7.75 11	251.0	7.1	11	27						<del></del>
VW 9/81	9.211	013	51.5	51	1. 12.1.1	1121	1 (90 - 15	2.58 FT	1 M C 1 /90 - /2	9.18E-02	5.501 ± 1 5.931- (c)	8 . L + C	-1314. 897F-90	1965-001	107F-94	8.38.00	5 01 H	5 to 11	N.	NA NA	71	5 17:05	100	4977.10	- 25	NA.	A197 30 88
1201-1-24	02-24 F	1.15	7.7	- 61	12 24 4	.10	2.68 6	y 0.1 1.	TLT C	-, 151 × 1	1.5 - 5	C.91-C.	1.5.3	CS4 11	1.94	1.791 #	2 2 11	151.6	- 11	1.1	7.1	4.1.10	W	.,,,	1,7	ici	1111 10 30
VW 5-81	0.0011	1.5	81.8	8.1	80.1%	15.75	5 (0.11	200 0	191.0	5000	110111	8 *** 1	1801 #	(E (I	A 751 H	4791.0	512 0	1597 11	7.1	11	N.1	_					
VW 9-81	Chat & Vac	1.8	57.5	-S.	912.7.6	12.2	627 6	183, C	751.7	484.77	281 # 1	8910.	1.5, 0	50 S 11	1 (E) (F) 2 (E) (F)	3 7 11	5.2% T.T	1981 #	N.	11	N.						
7,21,15,110	0.000	333	16.6	70.3	74,500	1.04	1 1000000000000000000000000000000000000		1.9WF 12	1.180 9	to a	\$ 47F-95	167 18	* 916 6	3.341.00	- 511-01	18	30.011.00	NA NA	3.1	80.	211.56	Stori	NO.	3.5	- X.	365, 24, 6
Appropriate	Q2-2 F Vix.	105	15.8	208	1.124.5	1.12	18/II 0 9/5, 17	121 C	184 C	1.89 a t 5. 21 a t	2.501.2.1 2.31.2.1	79.100 Calad	28.1 a . 36 0	5.91 #	6 17. 11	. 14 O	70, 0	17.1 *	- 11	NI.	- 51						
VW 1	Q12 (A)	117	.45 18.5	36.5	51247	11.33	214 0	241.0	1111	12171	3 (1 (1	1950 c	3/1 0	1381 11	191 #	1.1 m	10" 11	169 #	NA NA	- 73	3.1						-
VW 1	Q15 6 V v	1.7	18.4	200	91.5.6	1.18	317.01	2.85 C	770.77	4.45.14	1 291 × 1	5351	1.71 0	331, 11	141 1	5.731 #	170 0	51" 11	7.4	11	5.4						
VW 1	01/282	98	-45	12.5	19,100	81.57	1.280-1.6	8,94-0.2	150 0	6.436-03	5.00.40	5 ST +1 C82k-35	1.72650	3.524 - 6.1	481° a 3641-01	10111	5.862 + 6.1	117(-0)	NA	NI.	N.1 N1	156.55	3.1% (60	NO	100	N/	ADV-31-6
AAA 3 43	01:200 01:100 01	115	63.3 (3.1 (4.1	12.3	1 1240	103.	1.28+1.6 3.51 c. 3.167 c.1	101 of 2	1 181	5436-0 1,91,11 557,11	531+1	( 826-35	174 m 177 m	177 11	119 #	7 14 11	137 H	1701 #	3.4	NI	5.1	1772	711	-			
Vacobe:	35211	- 6	611		21.2 % 1	12.94	1.195-64	5 .b. of	2311 %	. 59m/ L	52Ec.1.	9.1.05	5 -5, - 5,	191, 411	121.0	1,366,011	188, at-	1. ([21.1	7.1	111	N.1						
720.3.73	050 5 Ca 015 6 V c	1,8	55.1		91247	10.15	11.01	511, 0	2.1.1.	81.171	199 41	529 cl	4 % 0	7.5, 11	611 *	5.0171	58" 11	5201.0	N.	11	5.1						-
V337, 31, 773	0.211	121	73.5	12.3	. (23.2 # 7	.321	21.1.6	5 951 + 2	1571 C	. 101 0	7.45 %	1371 %	. 920 %	5 /21 + +	679 #	2.271 +	5 -21 + 1		N 1	7.1	- 5.1	2312.36	1		<u> </u>	<b></b>	400.44.00
7,27, 3, 84 7,27, 3, 84	Q:2389	111	81 h 51 h	9.1	1.1111	1.1	189 1	5 PH	3.10F.10	1807-9	7 (1 (1	7 (10)	5 151 +	\$ 948.40 \$ 5 1 1 1 1	1.00	1760000	141	1.1 (	NA NA	N.E	7.7	7311.55	3.00	8.9	3.2	- 564	NEC 16 85
100 - 1,455 100 - 1,455	Q2-21 6 NGC	1,6	2-12	-0.2	21.24.5	12.9	5.85, 1.1 - 361 G	105.0	4 S. L.	2.81.41 -2.8141	8 (d × 1 8 (d × 0	5.61+C	823.40 -234.0	2.0L. 0	6.791 #	5 1 1 4 1 2 30 H	55, 11	15.00	71	11	7.1						_
7.42. x 84	C1 5 6 V c	1.3	4.4	75	91217	11.00	5.65 (1)	31.0.0	- M C	2.50	419.1	0.8101	8 -8 0	- 1/1 = -	187 11	< 1/1 / 1	4 20 11	4.89 =	3.4	11	- 5.4						
AR 1 81	Q131.63% to	10	3-13	J**	91.5.6	15.15	121.0	1.6 0	151 0	5.54 (4)	99141	814 (1	72.4	. 81 =	1 Not 11	- 121.01	51,1 11	4.79	7.1	11	N4 N3						
7,27, 52, 63 7,27, 52, 63	9.78	16	482	18.7	1,500	414	1.765.06	30 12	1 980F 10	1.521.11	5151.11	7 NOT CI	617 S	157	2 1 15 mm	3.7011-00	191.0	350 re	N.a.	3.5	80.	1.717.56			3.7	- 88	385, 35 4
146.84.1)	C146Vc	1.1	48.4	4.5	1221	15.46	1.497 (1	100 0	f / .	3.96" (1	1731 +	129 (1	*** H	5.521 #	6.41 11	280.0	577 11	5131 #	NA NA	11	5.3						
(Alt 85.4)	Q524 6 KG	11	5.52	15.7	81.15	15	354 C	1971 C	2.5. 1.	181.6	1,51 4 1	-26 t.	- 11° 1	311 m	6°3 a	225, 11	15.0	190.11	7.1	N1	5.1						<del></del>
	05-21 5 Vac	10.7	25.5	.5.5	51521.6	1.15	5 (g. 10) 3 (H. 10)	17 to 0	155, 14	-1(1 3 121 )	679 21	591.11	1.65, 00	53(1.6	1 (F)	3.01.0	1,011	15, 11	7.1	N.	27						
ANY-32-85	Q1 2569	(1) (d)	55.1	15:3 35:3	24100	31.29	559000	6.380/107	14/1 C 1785 C	3.26Ler3	2 W 03	5 5 L L L	187.01	1835 00	11,1,-60	2272-00	17560	135L O	NA NA	54	2/3	8 50 15	& Oak of	ND ND	8.0	NA.	406.3.8
100 - 1245 100 - 1245	Q2-2 6 Vis.	112	2	80.0	6.247	25.61	851.6	101.0	151.0	1.334	51121 51121	60.0	2 11 0	7131.00	869 *	5 51 4 1	118, 11	191 *	77	N1	71						-
1731 33 67	02.11	11.	51.	46.3	8371.0	4.51	196	5.371 (*	157 0	3 (1 (1	7.131 (1)	2.25	211 0	677 1.1	< 751 ==	15' 11	5.781 ()	5 31 11	NA.	- 51	3.4						
/JL 50 84	01 5 6 V v	1.5	66.3	803	81 N 6 915 N 6	1-1	5.00 13	1 0	2 1 1 1 2	18.11	5 (61 ) (1	500 1	8 C 1	512 11	161 4	.9" 11	4.81" #	6.167 1.1	NA NA	\ \1	NJ NJ		_				_
120 (24)	01/2569	106	249.7	4, .	2.62.69	1836	81.0	5.550 + 61 2.550 + 61	1.94 C	I ULC BOSESS	6.756-0	11444 0964	. 'V. '	2.68.00	1.51. # 1.55p-mi	-2 Ct +	751. #	5.28 cs	11	34	\$1	100,00				NA.	M59-23-54
Adh. Sc. 10	(227)	1.10	15.3	71,2	10000	15.3	3 2 2 4 2	27.15	471 A	* of a	8 -4" 1	57(1)(1	24. 1	. NI =	181" #	1831 (*	250 00	1.571 #	N.4	1.1	5.3						
Vitr 10 - 16	312 F	1.1	. 15 i	***	81241	12.15	1.96,41	1 50 0	. 501 04	286' (1 5944-0	591 (1 58E-5	50-0	*481 O	(0, 0)	6.7SI = 51 + 9	2  2  a 22  2  a	7 ( 1' m 8 (a. a)	9167 1 1	7.1	11	N.1						-
133 - 12 - 15	20-21 6 May 20-21 6 May	- 27	. B.s. 16.3	1.11	51.316	1>	90.15	1.6. 0	2.5. to 30. to	- ALAH 1177 (*)	5 (9) 2 (1	780-0 981 1	4.191.0	3511 11	6.69 #	231 8	181. *	510, 10 530, 10	N1	NI.	2.1						
3,537-72-15	04211	1.3	. 15.*	-72.2	0.2220.6	14.35	2 (5) 12	136.0	. 971.10	45,562.4.2	100241	5.522 - 1.	-9**9 0	5 - 0 - 1 1	. 141	-1.981 -11	8.15 =	\$ 100 + 1	5.1	53	53						
A000 00 00 00		1.6	-7.0	68	21210	13.90	152.00	199,00	-31 C	2,676,66	4,040,04	4 74EHA4 5 181 + 1	1.59.(e) 3.5 (-1)	5 6 9; cs; - 121 =	117 4	2.943. pt	5470.04	1.100 (0.1	Au N	244	N	1 25 0 01	3.2	53		NA .	20001242
	32-21 6 M.C.	4.1	. 23	157	83247	1. %	125.13	c	19.0	205,001	* 81 # 1	(0,0,	4 14 0 320 i	9.20, 11 53.1 m	614 *	200, 10	5.21. #	530, 11	177	- 11	- 11						
1,11, 50 -2	25 % 6 Mic	- 11	~8	91-	81 7 6	13	135 17	207.0	9 3, 1,2	7.60 PC	5.87 (	5131 (1	1811	.46" 11	5.50 a 1.50 a	^ (SI =	6077 11	2.10, 11	NA NA	11	NJ NJ						
100-12-1	2002 6 std.	- 1-	. 23	.92	915.0.6	121.	10 to	16. 0	551.1	29/04/	5 31 41	821 0.	. 6, 0	15 11	1801 #	68171	1/2 1	551 11	- 11	NI.	- 71						-
MWW	21.2589	nac.	3903	13.	200200	1945	7.698, 119	1280.00	1,8811,0	2.66668	33300	# # E G	3.6666	2610.00	2.990.00	199.50	3.000.00	3.600.00	NA.	NA.		210018	N.	N.	363	5.4	30003539
100 32 A	Q2 2 x 3 Q2 31 6 M u	11:	1 1 1	13.7	127217	15.2	252 (3 )F (3	5 750 12 5 750 10	1.70 1.7	2,510 (2 8) 10 (2	4 61 +1	190 1	5 8.0 m.	2 E O	2.671 a 6.771 a	51.1 ct	23 C n	5.60 11	NA.	7.1	7.1						
Village A	(0.0 to the	115	3.7	-,15	81.35	1.1.	215, 03	. rt. e	51.0	1301.1	501° 1	7.20 (C)	549.11	629 a 621, 10	1811 4	2.61	194° 11	1591 0	7.4	1 1	- 34	_	1				-
300 - 12-1 4	20-21 to May	4,8	. 2.5	-,11	5152.5	12.13	155 13	28. C	180, 0	4 5 41	.21 + 1	8 . 5 1.	1.5, 0	484, 11	1861 *	1.61-1	155.0	845, 111	- 51	N	- 53						
1350.51 fulli sv. *	C1200	128	19.2	11-	1, 20 16 6	15.12	1 1-93-68	135.0	671 17 5 56-85	2 146/80	10001	2 F 596-15	157 0	\$300.00	4 151 a 26-519 5	1.840-46	195° a	6.67 mm	N.4	N.	N.1	1 (1) - 15	100	NY.	10	3.4	3.00-2
VSS-35 VSV-30-21	000KH	- 33	19		1000	1.1"	1.16,-10	10.72	3.98 ard 1.986.00	-2 NG44 6 MH44	1000	7 (1815.0)	4.505-76	9 ( 1 × ) 81 ( )	6 186,-44 3 3 31 - 56	0.895-01 1 31 PHO	11000	585.6-0 x	NA NA	1	- 3	1.965-19	- 3		(7)	111	100
V20.31 51	00000	11.	1	-1	1 1/16	3 51	150 0	.61	1321 0	781 (1	- 411	8 (8) 1	126.1	1731 11	1   5   11	81111	17.00	157 #	N.1	1 11	5.1	1			100		
735.31.31	0.20	118	4		175713	41.3	7 17 18	2.41.12	141.0	191 ct	37171	5787 1	770.0	1,47 11	1.61 =	30110	187 ()	5 (1 a) 5 (3 a)	NA NA	11	7.1	_	1		<del> </del>		
X200-261	Q2-2009 Q3-2-1-1	006	10	-25.2	VI 2606	21.40	1.30-6	7 3 0 1 1 4 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1	151 0	025.+06	1.196.36	7 MD+33 L++1	.2 597-0.	6140 01	Libsf ar	1 155-61	3000 (de	3,391 (O	5.4	VI.	71	1.050.04	< \$72,400	ND.	NO.	7.1	MW-35-0
VW # 11	0.217	1.0	17	141	126217	5.1	1011.0	29	157 C	514.4	1191 +	1961	* 94* II	- 19 00	151.4	1.791 =	1.60, 1.1	5.571 (c.	NA.	7.1	34						
A117-36-52 A199-36-51	Q1 2569 35-3569	- 617	- 0	1" 9	127/2009	32.59	5.191108	6.08F107	2 JHBs JC , 63e, C	3.37E/00	8.955 (c) 82L-1.	6075-08	SOCIAL Child	7.963; (3)	1.241.400	1 651, 01,	1.00.11	1-65- LJ	NA NA	24	N1	7 \$20 16	3,500 +1.0	ND ND	5.3	NA.	400.39 C
Christian.	0.247	115	- 4.	11.6	100017	331	87H 6	5.79 (2	1521 C	341.0	1.61 4	19 (11)	19.5 - 5	9/1 · · ·	9 81 4	1.631 (4)	25, 11	(A) (A)	- 71	NI.	- 11						
47141 2" AE	0.790	935		1	8.78.2509	11.27	4.5%(0.08)	4.400 s.4	2.150.10	\$ 81E 90000	1396.90	27 G 79E-03	3 .25 (600)	74 ×	SSSS CTRANS	2.0H2.00	100000	3 2 82F-U1	NA NA	i i i	32	4 616-36	670.93	N0	NJ.	53	360.57.5
VIII. 12. VI	0.211	115		-	21211	1.0	154 6	199.71	1791 A	5371 x	1371 4	-81 i	107.0	183 11	1.91 *	8 (1 (1	1.30 mm	120 m	7.1	N1	N.1	_	1				
VW 15 D	9.2311	117	-		. 1282 # 1	.152	129.6	2.81 %	1.521 C	d . b	15.1 4	-261 - C	S 80 C	5.641.1.1	6 9 1	2.29.21	5 m 11	5 (1 1 )	7.1	N.C	2.1	105.35	560.03				NO. 52.32
Alterate	Q****	11.	79	1.	179.7369	100	150 6	5.67	175F V2	17(9)	101 4	0.011	1,557 - 96	114	139 #	15000	116711	11" ()	NA NA	11	NA NA	105.37	0.0000000000000000000000000000000000000	50	N	- NA	
Charles.	0.211	115	27	- 1-	. (28.2 )	351	190 6	2.80 %	151 0	2.54 %	2.61 5	7. No.	-67 C - II	4.19 11	. 641 **	2 121 0 1	151.0	1,21 11	71	- 11	71						-
V.M. 3, 70	Q: 2009	135	19.7	313		11.3	4586000	\$190.00	2.846-10	5.47540000	3.8	7 5695 11	7.84E+40000	100	2007 2 Torot	2.675-9.	1 1	EE -17		3.2	NA.	15[:-15	835000	500	0	3.3	A60.37.6
Alle st. 11	05047	115	1/2 1/2	-2-2	7,216	1.5	1381 ()	8.7M 12	179 C	191 1	1391 4	3.80	-2.8.C - H	5.00 11	151 4	5 901 +1	1 20 11	138 #	3.1	11	33						_
Marie and	9.211	116	6.2	1.12	. 1282 111	8	+521 - 6	2.881 1.	1521 C	. 91 11	1.5. 4	121 / 1	26%	6 0 1 0	65, 11	101 *	f #	\$ .2. 11	- 17	- 11	- 51		I		5	- 51	
VAL 8- 8-	Q1-2-65* Q2-2-67	11.	13.2	-582 18.1	12(250)	11.22	148 B	5.23Fet 2	141 C	5 29E+01	191 - 191	6.685-35 57.7 i	47 2002 287 P	3 13L/50 7 5/1 1 1	5 SFE - 64	1 (01 - 0) 4 791 + 1	3 le (6) 187 ()	1.531 - 06 5 or 1 m	NA NA	11	N1 N3	4 812 - 39	2,632,461	N0	50	- 21	MW-3 -0
VAN. 8. 4.	05.24.7	1   5	63.4	18.7	******	2 *	11/51 15	1.51.0	2.24	5171 1	* 1d *	7.7	5030	3 (1 ) )	1/81 #	33,[1]	1 7	3 551 #	N 1	1 51	N.5				1		

| 1.17 (\* 1869年17年2 - 1872年17日) (2012年1月日日: 1994年3月2日 - 1994日 | 1747年3月1日日: 1994年3月1日日: 1994年3月1日: 1994日 | 1

to di

#### TABLE 3 FOURTH QUARTER 2009 GROUNDWATHRANALI HEALT IN AND AVERAGES FOURTH QUARTER 2009 GROUND STREET OF A STREET

		T												VIA SIS RESI	1.79								11.01	A ROLLING AV	n.orv!		
	SAMPLING		SAMPLE ZONE CENTER	SAMPLE ZONE	SAMPLE C	OLUECTION																TRILLI M					
meato,	OLARTER:	SAMPLE ID	Depth F1 Below Inp of Cavog <sup>2</sup>	CENTER Elevation Proof				гити м про г			5e 30 (p€) E)			C+130 (pC+1	,		Cost ptola			N 63 (pC+14		ip('\.()	Si 5% (pt i 1.)	Cv 13** (pt ) L)	Co 6º (pt) 11	≥ 63 (b() 1.)	WHID
7.07. 3. E.	0.217	1 11	Injust aveg	16.7	Date	lime	Reall	Sid Des	AUDIC LISTEL C	Result 1	Std Des	VIDI	Result	Still Des	ADC:	Result 1.791 c.1	Std Des	AUX	Result	Std Dm	ADC	Average	Average	Annage	Annage	Average	
¥\$15 - 385	Q2-1979	101	15.1	-211	1 1276.69	11.45	2.500	1.6 2.102	3 8.4%	3 241 -02	. 256.70	8 151-13	23.53	1418-00	, 01E+44	52120	218460	2.985-1.3	3.5	23	277	2.44e-12	363	No.	v	44	250x - 18
X3V-35-67 X3V-70-6	Q2/2989 Q-/24 F	106	6"	- 13	19700	34.55	1.386100	187/107	15% JC 784 S	5.33E/30	3.68 (6)	6.5 Lot 3 Cl. (	-8 (30+3) -6 34, +4	5 125 80	14.1.400	7.7.98	1.605 60	170-0	8.4	N4	NA NA	15.0 /C	7.867-1.0	ND ND	N.)	24	407.394
X37-75-84	Q2-2-981	506	132	-6.5	15/70/9	32.22	13594 C	3 88-412	150-12	2.156400	95.40	CNUK-JS	-3 5.21L	1.191./6/1	. SL+8f	1.631 - 01	76 s - 51	3.321 - 00	5/4	N.	N1	2.432	3.586,-0.0	500	10	N/I	3.DV-39-8
V/V: 35 81	gn 2,49	176	g1 c	914	1979.9	15.36	2.29 0	1500,000	157 (	2 ME100	6.70° i	(3.11)	8 75 22	89 cl	1/1 /	1 30Feat	3 / 25 - 400	3.80F-160	NA NA	11	NA NA	2.65 12	1875-4.9	ND	(V)		AUX 39 0
VW % P	C1240	117	154	21.5	1 (***)	16.14	176.92	15, 1,	5 35E + 1 50E - /2	*41.11	11.00	2 C0615-03	2.70	7411 #	189 =	-1 53E-01	707 11	4.70° a	5.1	N.L	1.1	2.895-32	2,332,939	NO.		- 27	X-0-26-
120 - Sec	3424	1.1		-1-	1, 12 1 1	12.46	2.540.93	.11.11	91.1	5 161592 3 14019	6.83.26 8.64.2.1	F6 1.	-9.355Q	530E-90	( v V ) ii	- [1] =	01.0	8 951 m	7.1	- 7.1	7.1						
1.11, 30, 41 141, 30, 41	21247	1000	180 4	10.74	1 1247	1 15	2.549.93	7-5- 11 98-93	506-150 5-871 1	2 14019	665.3	9 54 ECT 8 6E CT	3.921.75	6 19 ×	6117 #	1771 0	. 11	100 m	3.4	No.	53	NB	N.	8.0		5.6	All Di
339-39-135	22.30KB	106	505	40.5	0249	12.6	460003	A.2. 1.2	. 4Ma (C.	6.85L-3	666.7	File.	-2 ABSSS	2.536.40	31.14L	4.04L U/ 5	495.63	200 E L JL	- 51		- C.	10.30	500	55	70	100	A110 - 200 - 2
VW-9-2"	0.289	111	24.2	41.5	1.520	14.39	1.790 000	3.55, 11	5 8/4 4 1 486C	1.02E-08	6 to 1.	5 5 1 - U. 27 6 8 2 E 13	5.245 YES	5.40.00	751 H	465-C) S	X 1. *	6805-ac	. 859-01	100100	2000-11	1 58: 10:	3.2	8.2	0	300	X60
7.10 P. v.	Q**+)	1.0	-4.	j. 4	1.1017	151	150 0	18 12	13/1 0	217171	1.901	5 69 1	1.11.0	8 (7 ) 1	147 4		1.50 (1)	181 s	537 () 53	161.1	7171.01						
VW 8 **	0.217	1.6	*4.*	10.5	1.7517	140	7.0	533 (1	7.79 1	231.1	7.00	87111	15.1	. (9) #	1.000	^ (i) a	5 (3" 1.1	5 (1 )	5.4	NI.	83		Vn.	V0		ATI	
X22+8-46 X24+8-46	01/2889	1.6	46.2 -6.2	2	13 (250)	11.28	150 C	2.59-912	148-10 144-0	2.09E-03	2012/05	5 6 E-35	EF85-31 -, 141 0	2 88L/50 5 8.3, 1 1	2.35E+86 1.55E #	0.15E-03	7 86 (8)	7.84-61	25 Cheerland	1 891 + 03	2.721 - 61	1322-02	- 27	V)	V)	AD.	349/45/4
VW 8 35	05217	1.6	42 32		11.124.1	4 1	1.8 0	29 12 5 821 11	2181 P	5 871 V	581° ) 5151 # 1	1 (SE) 1944 - 14	1.61.0	241.0	1.11 4	381 (1	154 0	5.69 #	7.1	11	N.3						
X357-61-81	Q1-2069	36	872		1119.2009	10%	1.523,142	1 45, 72	3 1881 - 12	2 921 -33	5 (65-0)	6.405.3	477539	1,622 (0)	tatt at	-, 817 (1)	1,442,100	1925, 73	2.46.17	1 "(6.00)	2,191, [1]	1 966 c 'Q	(7)	AD:	727	40	200-19-1
VW ≥ 81 VW ≥ 81	0,411	1.6	81"		1 3047	115	2.11.0	31 12	139 6	2747	135 1	5 151 1	1.80 0	. 81 11	1781 +	1.281 #	137 0	5 60 mm	126.1	211.1	2.121 (1						
775 E ST	9.317	111	3.1		1 117	151	1.11	284 (1	7 151 1	Setsiet	661 I	81111	1-1 0	6 (5) 11	2890.00	54 m	E (\$10.00)	15.1 4	5800 00	- 51	2290.00	2627-62		No.			A757 40 S
Vitralia, 6	21.0003	1.0		- 4	1 124 1	1.1	. 52. 1.	. 14. 1.	. 19 1	C 501 4.2	5.521.61	( b., -1,	2191 0	(6), 11	101 *	4,15,11	10.11	1.01 #	48 FM - 1,	1.996-30	.1111	150					
VW b +	01017	11.	1.5	1.	1.175.6	1.3.	1.6% (L)	518 11	218F C	7. N. F.	577, ct.	24-0. 241-01	1000	5.79 0	6 721 - 0	I N A I	3.50 (1)	1901 #	7.1	11	34			_	-		
455 W 34	03.0969	136	***		115543	1.85	4.500.443	5.597.00	158 > ,0	7.9(1) (7	2.60	900800	120640	4.74(.6)	1910-04	6817-59	10000	1350.00	3.00	1896-31	2107-71	1.585-12	8.5	10	8,5	- 50	VW B
Although and	(3.21)	- 17	11.1	4,	1 1241	12.6	122 /4	98' 11	2 181 C	5.381 cl	51,1 × 1 53(1 × 1	* 1" 1	13(1)	117 11	751 4	19 0	441 #	5.187 + 1	Na.	199 %	NA NA						
AUV 8 63	21/263	112		4.	1 1176 6	1.35	1 1/2 1/2	5.53" (1	5 (9)	12363	1.95" 1	* 31 + 1 	358.04	5 *S1 # 5 *24 ***	6.7 4	425-6	256-13	5-69 m	N.4	1896.0	N.1	1 42 - 12			223	- 20	20 00-10-0
VW 8 62	5441	1.6	4 -	1.58	1.1017	15.55	115 15	f 1-	151 C	1.781 1	-5f" i	5 Ict ct	. 81. ()	13.1 =	187 =	419 11	381" ++	10/1 #	*97 11	1 (9)	-11-11-1						
305 -8 -162 305 -8 -162	34247	1.5	.4.	-55 *	1,1 2.5	12.8	.8.11	8511	214 C 981 H	121 - 0	5 -8, ±1	\$1.101 \$2.50	22 C + 0 9 C + C	5 5 11	611 4	154 #	5.64, 1.1	950 F	71	11	71			_			
VW 4 - 64	Q0263 Q121	115	31 ·	203	4/13056 Thinks	23.56	5 T C	2,000,400	1566-22	5.385156 . 71	140 90	5,851,6	139.70	57111	1500.00	1301.01	139,000	3 %( +0) 1 %(	200	338	222	5 (8), (0	156.00	ND.		NA.	\$300.41
300 (4,)	0.000	115	e  -		31,3233	.718	1.N C	111 14	189 1	1.01.11	1.5	8 40 4 1	1.5.7	. 94   10	1.8. 4	2.04 9	16	1	11	- 11	177						
V20-4-4-1	02.289	112	505	- 4	427090	1 1	1.1.0	2.850.000	184-C	2.671	\$5600E	42° 648	81396-01 1 37.5	54111	1 (5) 4	5 °S1 + 1	1 1 1	111	N.1	NA 11	N.1	4 12 02	3.542.720	- 0	(7)		AW-915
746.32.23 746.1.13	() di 2009	013 30	5,5	. 4	E06043 1	711	.51 C	5,098,000	430.0	1 (SI ) 1	5.40° i	C21 (1	100000000	5.431 m 5.400.403	29000000	1451 (1	6.585,40	5.980.50	s sidilar	E965-55	130000000	1880.01	3.00000	6.780-65	538 S	The atting	MW J S
100 (200) 100 (200)	Chall & Vac	1,6	12.5	2 .	116.05	1.9	-2. 14	10, 0	. 61, 1. 184 C	'35. C	\$51 F	144.	1 - C 15 861 I-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 41 4	101 H	19, 10	.1.0	5.1610	- 71 1.	2 (4 ) (1			W.040.00			2000 00 22
7.45. L. "A	Q3-2 ( ) Q3-2 ( )	118	- 31		8 (217)	200	1.71 6	4.44 1.	1791 C	2.88 C	161 4	550.1	4.55 (3)	211.0	0.42] 11	21.11	180 0	Tell a	1101.1	1171 1	*19 11						
7.11. L. ")	Q. *+7 Q. 4989	115			107017	4.11	74 K	2186.60	1571 C	171 (1	8.450.30	* 1/1 / I	1.F 1.	931 IA	1 P 1	1.57.11	277.0	41-11	81" ("	5 (4) 1	211.1	42 - 2	100	- 53		- 80	Mercica
335-42- 8	35-3(49)	1	1	-11	1 247	11.15	5 J. C	1.88, 10	, NM 1/2	-,6-19-0	5 41 44	4 4 4 5	161, 90	355, 011	1.4114	85191	160, 90	11000	(199-11	. 911 01	2160-91						
/dt. la .6 /dt. la .6	0.217	(1)	1	.1	(0.00)	114	< 511 0	79 17	150 C	2 M (2	537 i 901 i i	1.73(-1)	1.151	\$ 101 mm	1.61 0	870.01	130 11	154 m	8 191 + 1	1.81 1	11911						
\$190,8475 \$100,1515	0,50,60	181	23.5	25.3	10 bis	13.0	151.0	590-90	151.0	2.151.17	17.	795E46	5.38 (0)	3.936.30	5 9 9 pp	4.500.00	5.050-00	3.79.90 5.50° + 1	5.0	266		2.840-07	No.	80	- X-	XA.	MH-3-3
325 -43-28	0.211	115	215		J. 1283	1949	9 C	> 21 11	154 5	15 L C	5.500	(29131)	15 a. 15	194 =	125, 0	.11.5	100	1 % 11	7.1	- 11	17						
7.21, 15.1. F-50, 46.92	QC TAN	112	- 1	- 11	1003698	28.00	1.886.0 1.4.7	1/1 / *	1.659.e-00 1.551 / C	2.09E/G	1"/ 1	5 mate no.	1.086-65 3.7 d	6 136-60 5 61 m	* 107 oc	2.7/1 (1	199000	4.871 #	- Ku	No.	7.1	1.967-77	9.765(4.1	5 5 Mill word	NO.	NA.	M00 (13)
XXV-11-66	Q1-2009	Cli	62.1	-2 . 25 I	23 2606	100	2 091 · · G	19201-04	1751 0	13217-00	986-00	8 6956	1965.406	3.546 D1	1150 (8)	-18 1 × 1	102 (0)	1120 (0	54	17	71	1510.70	753	V()	50	9.1	300-11-00
VW 1778	0.21	112	74.	11	128217	117	2 1 0	351 1	2.61.0	2.201.01	139 (1	557.1	21717	1.35, 1.1	1.41 0	411.1	1.151 #	175 11	3.4	2.1	- 53	100.0	- "	- "	- 1.67	-,,	101111111111111111111111111111111111111
VW 1-75	9.147	113	2.	1	1 1112	- 66	7.11 0	201.0	1 881 C	1311	5.41.41	818 1	- 28 C	8.69 1.1	(3) (	91.11	181 ()	575E E	1.1	N1	N4 N4						
VW I-132	0.211	113	81	188	1282 * *	12:04	257098	96.05	950-10 . 91 C	\$.60°3	1.1	2 (TE) 5 (Mar.)	9.81° 0'	1.865.50	promise.	9,597,61	1.57	3.31 m	1.0	- 11	- 54	13/7.70	S.,		N)	- 55	VW I
Vitalia, C		115	81	165	2/24/	12.6	186.1.	. 5/4	. SH C	114.0	992.10	41-15	47	C 1st ++	6 61 #	0.281.0.1	515, 11	2.51 8	5.1	1.0	- 51						
VW 1. C	Q10000	115	81	18.5	7.7.508	39.60	1.18000600	5.850.43	1705.0	3000	HERM	8 121 ( ) "salb. !!	1.17	\$ ***  11	14 1 m	275.50	2.590.00	1731 e	N.a. N.a.	\ \ \ \	N.1 N.3	2.95; - 15	. 8.0	82	83		160.33
ASSESS.	01211	117	1-	10.5	121247	3.21	23ol 0	5 M L L	1 % C	. 501 - 1. 1 61 C	1 112-12	6171	-1680	1.1 #	. 14 1	121 0	107.11	1.81.11	7.1	N1	11	-	-	-			-
AM. 18 %	0.20	+ 18	i-	1. 4	1 (0)	1.7	24   12.5	44.11.	1.61.0	4117	844.4	200	187	P . 0 t	4171 +	8 **1 +1	449 0	4.64	7.1	7.1	5.3		X-9	- X-V	V2)		
VW-4581	Q****	1.16	44	- 1	121217	121	1.4 6	\$ [5] 1°	1.84.10	2.41.48 \$7.11	5171 + I	815 1	1771	339.40	1781 0	2 Marca 1	**4.1.0	71   1	77	\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \	7.3	183 6			(2)		4855.080
V35-45-61 V35-45-61	0.211	118	19		31247	.136	1.11 6	2.04 %	2 R	1.0140	\$64, - 0, 3.21, - 1	9.521 - C 51 - C	0.23, of el Cs of	124 0	6 11 4	518,71	124, 11	594 #	71	11	- 11						
500-16	\$15e0	103	les	-	2552959	13.40	1 8(71)	288767	1,562'-02	1 325.48	4.0	521.43	1.680, 60	2.768-63	273096	1,10	3.827.444	3.38E-03	101	100	33	9220.00	8,668.61	567	v	NA .	3,055,446
VW 6	31016	1.4	D 5		11.0.6	14.5	8/2/17	c	2.8% ()	525,71	51.41	6.831 ( ) 8.88, ( )	587 d	5 (g) ii	1 70 4	271.0	1700 11	130, 13	7.1	11	27						
V:0 -10 V:2 -00 -10	31-349 Q: 5999	1.8		-	235,7420	15	1 (10)-1 (1 3 (25)-23	15.72	, to   10 1,090e-00	5,640-04 2,689-6	* 154 A1	6 . L . L 8 59 6 60	. 8°. or	725, 411	1:0-st	14/6, 11	511, m	1.00-03	2.1	2238-4	2196-01	125.00	1667.11		NO.	20	NEW 197
1231-45-26 1232 #6-26	Q2-2 f F	- 17	- ::-	!	27.19	.1.6	121 6	2.01	191 C		. 172.	15 ( - ).	, 14 m	51. 11	3.1.1	- 1121	167	201.0	-,1-11	151 5	. 51 11						
333 -45-26	0.211	118	1		. 12/12/4 1	25.1	1.1.6	2.61.75	I SM C	. 191 %	1.1.4	824-4	Mark	7.191.11	6.51 #	111 1	5 58, 111	3 301 F	26. 11	111	. 40.11						
7.27. N. 1.	01.2909 ()* * + 7	794	- 33		1, 1, 6	1	250.00	38.46	139.0	* 00 0 -01 1	- 11	3 38-3	15111	7.5	1.551 #	238 (3	1 - 11	1 1 1	2.8.03	151.1	188.01		1800	(0)	10		A08-0-0
AM. R. S.	05217	115	14	14.	875 6	1.64	5 PS 5	2.691.11	179 0	-q ,	171 +	1951	1, 0 ()	5 181 ++	1791 4	715[1]	130 11	1 (5)   1	187111	1 191 1	179 (1						
Vitaliana Kitaliana	0.000	115	65	45	36309	254	2.511 /5	21969	1.89 C	1 4 11	2302-00	9141	(1-1-1) 31%ac	2592-63	190.00	20121 A	26.0036	523 6	2.36.00	3 3 2 6 3 6	250000	172.0	135.49	NO	N3	525	3850 + 9-0
7.00 R 1.4	05217	110	- 71	15.	5, 7, 6, 6, 7, 6	- 3	1311 6	2 (40 m) 2 (41 m)	191 0	**************************************	791 + 671 +	7 17 1	1.6.1	2592-03	351 0	5017	7.640 W	1/9/11	105, 11	1791 1	**************************************						
AM Port	0.217	+18		15.	107017	1 2	1 (41) 6	2.897.17	1.04 0	1.47.3	1.481. *	N I/T /	111 1	5 19110	8.81" #	1.491. #	454 11	SNIE	115 11	17.17	20101						
MW 5002	Quarter (/2-2 f	986		200	8.07.2949	1229	2.00 se	3,350,67	3.000 52 1.21 C	3,5687 64	\$200000 \$701.4.1	\$382938 7.56 L	1.500 MH	2.085/60 5.23, 13	0.370 mc	255.11	2.750.060	2.308196	35300 03 3754 11	170000	2.0563.00	3.00.03	\$ 18699b	NO.	, NO	763	\$100,000.0
VW 4 .	01217	118	-		8771.6	1.1	1101 6	2.61	179 0	5.13"	70 4	- 21: 1	23.1.12	5.61.11	1111.0	3 (8) (1	127 0	1 1 31	1245 (1	61.1	11.1						

 $\begin{array}{ll} 1.17 & (a.636) 179(0.789) 6187 (79) & \text{Comp. Lithlighter of constant NM Ass.} \\ 1.0893 & \text{Lithlighter of constant NM Ass.} \\ 0.5 & \text{finites.} \end{array}$ 

Fire\* 4.5 No. 2 Proc. 5 Arr. No.

## LABLE 3 FOLKETI QUAKTER 2019 GROUNDING LEKANALE HEALREST LEVAN AVERAGES FOLKNYDAN PROGRESSELEN ELEVANDE AVERAGES FOLKNYDAN PROGRESSELEN ELEVANDEN ELEVANDEN

			SAMPLE ZONE										v	VUASIS RESI	r TS								13 (8)	V ROLLING AVI	RACES!		
mento,	SAMPLING	SAMPLE ID	CENTER	SAMPLE ZONE CENTER	SAMPLE C	OLIECTION		гити м по г			Selfa (pO f)			Cs 13° (pCs I)			Cash prists			N (3 g/C) L(		DOLLIU M	Se 5% facults	CV 132 (0/C) 13	Co 91 (pt) [1	N 63 (00 L)	Well to
weiiii	OI ARTER		Joseph El Below Jones Cayon	Flevarian Plans							,											ip('t.f.)		-			-
CW 55 46	0.00	150		100	Date 1010as	1 mr	Result 100 A	Not the	ADC LBS-C	Result 5755-00	Still Des	ADI 14.77.38	Result 168F-sct	Stil Des	VIDC:	Result 1970 H	Std Des	NUC Tockets	Result 937-13	VM Um	1286-KJ	Verrage 1856-13	Average	Annage	Annage	Average	\$650.50
(A - 24 - 45 f)	Clast & Cas	C)	9	-01	115,179	15.16	1.9 6		US.		2.891 4	2151-7	. 22 5	5 9 11	1891 #	-21141	100, 11	269 11	35 1.1	. 11 %	. 74 %	0.000.1					4.00
W 51.75	0.00	1.50	- 61	15	65 N W	4.51	1.9 6	. 10 17	174 0	251	^ 15  a ^ 5   a	4 F 1	1 (3) (i	895' 11	571 #	2016	14   11	1 1 1 1	136 11	1 851 +	2181-01						
21.74.66	05017	1.4	61	-05.	. 1262 11	3.0	- MI 0	2 821 1	139 C	1.01 1.	. 31 .	5.010	1,1,11	1991 11	3 821 m	. 261 #	515, 11	A	( d, 11	190 1	-11111						-
20,24,250	Q1-2009	146	. b.	35	1.28/200y	\$156	237, 61	5 665, (0)	192F 'C	1926-05	990 70	\$ "r[.r)	9.892-11	2.8(1) (6)	1.25[1.01]	164,00	2 16/160	3.97110	89C-10	1671-0	1871 01	27% 12	40	40	45	ND	30053
All Sand	0.21	112	0	-3	8 787	100	-C1 C	. 11.14	131.0	5 51 - C	27.5-5	( S) ( )	295.45	129 0	114 4	131.5	201, 10	230 11	25 (5)	1.69 5	2 - 1 11	_	_			_	_
71. 8 TP.	0.217	115	().	15	1 (**)	126	Led U	371 1.	THE	21/1/11	5.5890	8 61 1	119 0	5 GT 1 1	A #1 #	F 10	4.4" #	47" 11	4797	Al I	23(1-)1		2.0	20	73	- 20	4600
Character 1	Q1/2/4/7 Q2/2/4/7	11.	1 3	-1.	1 2 2 2 2 3 2 3 2 3	.5.0	1.08688	. 50 1.	1.486 JC 1.8.1 C	-0.1240800 5.1140	18 1.	8 .51 4 .	4 93, -38000 5 1	94 H	1121 4	-2960.	5321-69	551 H	1.591 5.	1 ab 3.	2 41 41	1502, 12			N.3		0.28600
(di. e)	05.247	1.12	-4.	- 1	9 1247	1.1	15st C	671.17	141.0	71.0	150.0	5.441.1	1.50.0	. 921 1.1	12.1 0	71.00	127 11	121 4	25, 11	1.831 (	2191.11						
(04/35/34	(1-24	656	100		129289	151	19.0	971 1	1.00 %	57756	5 SE-61	8 1-1 1	3780 cm	5 791 i i	# PLA	2.781 #	4 46. 11	2.05	* 741 1	481 i	2-1 1	2.52					
31.05.0.10	35.2 k r (3 h s )	1.79	. 5	- 16		1, 15	111.	71. 12	91.7	5, 291.0.1	faste et	26.15	48 (5, 4.9)	5.51.11	1901 #	15.1.4.1	2.54, 0	1.9, 1.1	4.65, 5	2.994 %	2 3 9						
77.4 . t.	31211	11	9.7	- 12	1, 18 2/ 6	1.15	116 (1	377 (1	. 19 0	171 (I	149 (1	1.347 n 1.771 n l	- 61 C 1	. 171 1.	3.89 a	- 61 cl	1.38 mm	191 #	3.01.11	1.99 (	184.0	_	_	_		_	+
N 0 24	Q1 (9e9)	168	1919	613	1.7000000	1 65	1.435.65	4 (6.64)	189 × 30	\$ 64F 25	3.515.4	3 State 434	6 2 T S	4 28 E- Se.	4 4 (31- GE)		480000	1397-46	I Cheeci I	1.336.64	2.189(4.4)	SB	SS	Sis	563	325	A/W 5
700 2 10	2524.7	1.6	16.	7.5	8 747	1 4	217 (1	31.71	*1 c	85.1.0	200 a	5.791 (1	4 0	1.01 0	177 +	*131 (1	221 11	101 #	450.0	181.1	*40.01						+
Al. 4 18	\$1207	(1	15."	177.4	1.187-6	1 15	136.15	12" (*	191.11	57711	515 (1	8 7 1	135 0	. 69"   1	111 0	2 dl =	417 0	41" 11	18.11	5.1 (	181						
38033034	21.2569 31.2549	108	362	- 95	125000	12.9	1,980,94	136.40	5.000 (G	981101	19750f 1601-01	6.586.08 (1.1.1.1	- 55, - II	338.00	124.9	. 1461 144	\$780.69 165, 40	3.52, 60	- , 50-11	1.900 of . 591 of	2330.00	50	3.0	50	303	50	25855
25 - 5 60	25247	1.0	.42	-,35	8 . 24 *	15	116.75	20.11	. 91 5	14.40	5.0141	7.92 5.	5.6 - 6	1 1, 11	1.61 *	4,25,10	1.4 0	1.6, 1.1	17 5 8	. 91 1.	2.61.0						
7)V < 43	CITAL	198	259.2	)* -121.5	1 187/ 6	1.3%	18.11		151 C 0.898.402	5.81 C	1.15.1	* 3/1 i l	2650-66	5.951 m 3.852-400	ATT II	37.E+80	132000	45.1 a 1702-03	2.430.59	1.796+35	2.155-01	NB	8.9	NO	- 23	No	* ACW
dh. c . 80	Q1/2/63 (11/1)	1.6	46.7	1214	\$ 20 2000 5 ~ ^ # J	1 44	2.67 (1)	2,800,2402	81.0	1.151.0	2 (3. 1 3 (600)63	0.1104	20.0	5 701 #	5.096400 6.047 a		\$ \$25,404 5 ° / 1 1	5 1 #	5 547 1 1	1.69.1	21.1.01						
AL 4 60	Q1/17 Q1/24 F	- 11	.50	1014 -1215	1.18.00	1 11 -	958, 11	19.11	41.0	191-0	887 i	611.01	5 75 11	5.821 #	6.61 *	2,817.1	5811 ()	515 C	98. 11	2.1 d. c.	2.01.01						+-
XX-52-11	63.00	101	DOS 2000000000000000000000000000000000000	68	4-94/21K9	100	5.00.02	160.0	20.72	4,52194G 6,53143	2.64564		2.685-70	42.7	10,000	4,5+46	9.49 ad			N.A		5.5-C			N. 1	- 84	\$100.0
**: -: :: :	01 184 07 184	554			4 400000	161	14%	940.00	1.00	0.02163	5.671.0	100 pt	1 - 6 - 4	398 43	741	3.835.63	1 29 30	136 CV	**	1.4		1 14 G			N.3	9.4	\$600
N. N. 2364	92-263	504	- 64	-12.1	\$1.09	2.52	4.52.91	\$2,000	1900-0	4.235.01	114494	20.00	1825.06	6.342+1.3	\$ 56£, 66.	d. 63	4.3345-35	484.00	5.3	3.4	8.4	82	\$5	\$5	85	t	3532
AN CO. IS	2.74	1245		. i ge e	159243	1555	119740	198 H	98.50 74.57	4 4 E 1 1 1 E	1,735,01	187	7,040 GH 7,237 GH	8.500 CO	1750.00	710.00	1.681, 56 5.650.00	147.13	۸.,	No.	N.	1677-0	10	- 33	N.I	NA NA	3/3//
08.00000	02/2009	124	Tig:	120	4.550,000	12,61	119.9	9.933,113	1,861.0	18,951,00	7 300	2 (4)(6)	-2.5"8:90	5.831, 40	1 951 . 64	- 511 + 5	6.700	1,71 (6)	83	74.1	133	1000			- 33		3585
VW 13-81	0.247	136	-	4.7	1.26.2909	13+4	6260-06	3.950.40	3.7% or	0.98794	57E 96	9760.00	110,00	3960-65 (61, 11	101 *	2.2959	3 (9) (10)	186 1	801000	18/6/9	2161.11	1.985.36	2.596, 459	1168 (19)	v	No	\$100.0
Charles.	00011	112	+ ;		21247	.526	183 C	251.1.	1 M C	15 175	351 # I	55.10.	1 1 1	181 11	181 *	1.8121	138.11	184 11	4995.00	181 1	2 (1 (1						-
W 45 8"	0.211	115	*4		120000	211	5+II C	751.12	187 0	20111	130 1	- ×1+1	1311 +	2.81 #	191 *	, lol =	1 7 11	1801 #	5.5 11	1.791 (	2.166-61		2.75.48				
	02 6 81.0	14	1988	.97	110.00	1938 5 P	5.95 (4)	5 No. 1 .	1,000,00	2.5	2.11	34.0	3,650 pt	4 536 - 64 2 - 8, 11	. 61	2.89 sec	186. "	115.11	. 31. 11	2.299-4	2 1000-031	257-13		. 590			NW 5
(State of the	35-2 k r (31-2 k r	115	. 2.5	323	1.124.1	1 + 9.	265, 17	5000	. 14 C	2.89.11	4.15	5.901-0.1	26, 0	C19 #	1.5	-614121	126, 11	121.5	8.961.1.1	1.881 %	2.11.11						
Calle at 12	21212	116	64	101	1010a) 1010a6	13.18	4 (61 ) 3	1.01	201.0	3 6 1	2.101.0	1010	173, 0	5 121 #	137 a	3 [2] #	565 0	5.00 (0.00)	. 101 11	141 (	2101.1						+
VW 4147	0.767	108	34.5	25.0	23,506	(4.5)	1.46006	50.17	150 92	4.020-080	1165 ×	2.685.1	1.785-100	4.13E-y	1.021 - 05.	1191015	1000	90 ST NC	31 F (0)	2008-0	236F (1	135. Uz	5,907,90	587	N	3.2	1000
Village of	Q0-2 8 F	1.5	45	1,31	8-15	.131	1.01.6	3 31 1	15.1 C	2.50 4	134 4	C88, +1;	-181, -5	1.74 1.1	1.51 *	\$ 5,141	15.0	150 0	19111	2.74 G	2101 0						-
1777 4 . 5-	0.217	- 1	24.5	14.	1.1017	134	71.6	2.98.12	7.01 0	6.00 1.1	117 4	- 91 (1	-1 5, -1 -2 5, -1	5.63 #	1.51 *	221.4		431 m	371 (1	191 (	1.291 (1						1
VW-SerV	9 2969 3 3 489	- 0.6	57.6	-611	26200	1214	5.800+10	233,46	1.565-30	27 10 1	\$164.01	Cyl. O.	95% oi _[v, m	2786-69	1560-00	120 8	7.947 co	1 505 D	1511	2 (SE OL	2.50(-0)	150.00	18800	10	N.3	89	Mee 5
C21-5-58	992333	- ()		-1	1 1047	,150	8H C	2.08063	2 3-42-1°C	. 1.1 *	804.00	41.75 6.61.01	0 1, 15	9,2%, 1.1 9,6% iii	2.2.1 0	9.89.01	17	191, 11	8.14 - 6	2.70 %	291.5						
AULT C. ES	01.289	0/6	t- t	-b933	23269	1.55	559 0	2 151	1949.0	2.908344	119.00	3.295.95	5 Y Y Y	3,090,000	7.87 H	3/1 4	\$600.00	5.32(x.0)	9.00(-9)	2008-02	236600	9.510-10	4.558.000				3000
77. 1. 17.	(22.21)	1.6		1022	34017	12.16	432.15	2,687,69	*81 7	5.7.1 +	1-1 -	8.14" 1	1"4 0	351" 11	1,61 =	2.61 0	1 4 4	100 00	247 1	9.1 1	2141.1						1
CW 4. *L	2020	1.0		100	81247	1.10	4 200 12	2/2017	2.181 7	.49	174	5 Stat	1201	141.0	1 61 4	5.971 cl	555 11	1.79 a	191 11	21.1 (	211.11						
eu:	(15.6)	156	100	1800	2.1 2.49	12.9	1112.13	2.68(3.6)	176.3	3.348-5	1.56.90	6.81 . 31	3.385.48	3386.6	3.663.556	2,945,62	2,935,143	3 2 5 (9)	2.316.004	2.374.110	2.560.00	1.525.113	1 462.93	3.0	· ·	N/a	W. 1
avs. L	35247	1.6	- 1-	1517	81241	1, 9	1.9. 11	10%-9-	2.396 - 3.	101 (	1.69	Spenial Second	1.81.0	2.74 1.1	111 0	27T (I	130 a	136 11	< 81° a	2.4 %	280.0						-
Christia, In	34247	11.	.11	4511	1, 15 2 5	12.14	1.16, 1.1		2.94 C	18,100	181. *	21 (1)	41.6%, 0	- 151 #	154, 4	5 3 4	No. 11	. 31 *	266, 11	1.01 %	4 (1						_
00 s	S1.767	158	19	4571	15.349 15217	12.15	1,665.443	235	+ 4 9 + 17	3,05493	1.17196	5.98E.01	1525.eG	+ 646 - 66	11097-14	11350	17 F 172	941 - 66	3 5 1 5 5	2176-0	2.08/01	1.817-03	835518	30	N2	20	2.85
(4), 1, 4,	03/2 × 7 (3.5 × 7	1.0		101	81217	1 15	181 13	5737 12	23.60	5 151 +	1.60 *	2017 1	1.7 1	2 [5] =	1.79 4	1.01 +	198	1,4 *	3.001 1.1	7 191 (	2.2(1.4.1						_
(Nr 4 , ")	\$1247	- 1	290	1571	23/2/09	12.1	148, 13	3 11 12	3.50F+3C	1,96810	1291 +	7347 (	737.1	134" 11	7.0000	45, 11		4.90" 1.1	177.4	2378002	2.7(1.1		1.965-171		100	505	32000
330,000,000	01/2009	176		-1.51	15211	12.0	149749	1,086,145	. 91 C	. 91 1.	1389 0	909000	-1.18E+00	3.452 (0)	18.1 "		166. 0	3.90-03	- 31. 1	. 74 %	2.50 (0	111	1,940,113				10000000
qrs. x	\$12.0	1.0		150	81217	1.5	102.0	807 67	2.3/85-12	.61 (	2.41	1.70	7.7.4	331.0	144 #	7781 (1 1181 #	157 #	196.11	1311 +	214.1	2.171 (1						
	24-24-7	100	-	1.7	1, 11,1.5	121	1.0400.0	12	2 (A C	. 51 11 1:akib.	154. 4	- [1] - [1] 4369-05	1 558, 46	2.894 - 1.3	184		200	13] II 160:13	12800	2.456.96	299.00	1.541.0	-		353	- 33	990
(di. et al.	02217	1.0	- 4	- 1	127217	1.46	1.11.6	2.995.42	1 3UE- JC	44 (	1.00	1.50(1)	1811 0	61.11	677 #	281.11	1911 11	5 4 11	11.78-	1.79 (	220 1						
(direcol	0.217	112	4 4	-1	1 1017	311	150 6	5.391 17	139 0	3 (1) (	1.79 4	2.001 1	79.0 1	55111	161 #	1 (7) 0	577 11	187 11	187	2.181 +1	87						_
AM: 44'74	01.240	156	42	43.8	3/430/0	13.16	9.500 (2	250.47	3306.02	3.7(8+6)	87K (M)	1390.00	193096	3 (45) 400	3.690 194	1.586.01	3.786.154	3 50 000	5.886.01	2.50(.++0	2.556.+3	2 20 66	5 692, 653	NO	10	049	5330.7
State State	Q2Q 8 1 Q3Q 8 1	1.5	1	435	12/2000 85 July	-1.26	2.8.0 0	- 181 F.	191 C	42.1 to	288	28.70	-144 0	7 21 11	1 (4) *	250171	128, 10	2.54 0.0	- 11 O	2.61 %	250.01	_	_			_	-
All. 44.24	0.21	- 11	1,0	15.6	1.2243	*31	2.571 15	263.12	1381 0	*56" 1	2.10	,	4.21 0 4.31° i	.49" 11	1.61 =	2.71 1.1	151 =	4.79 11	2.6.00	1.731 (	2.01.11						
2200000	0.799	169		28.8 -28.8	12.12.4	11.55	Filher R	2.6, 72	8,878+00 , bill 0 <sub>4</sub>	2318-61 CLL-1	20.000	( -8, -1,	197 1.	(51.11	1.021 + 2	1888	1.3. (6)	1 mil - ac	2.5641.1	2 8 8 4 4	2366.01	x 11 - 1 k	7600 444	344	NO	70	460
grossá.	416-73-7	d.		-,6.6	85.00	1/25	5 - 1 - 6	5.19.75	. PI C	235	2.18	9.5.1.	4.09 a.	3.6.11	1.01 0	. 25, 11	1181 11	27.1	8.99 1.1	1.54 %	- 69 11						
200 80 28 201 44 41	0.717	112		78.8 18.3	415099	1 1 2 2	1 1/2 >	1.49 r*	190 0	30.45(16)	52008	1767	1 "U m 5 6 3 " 5 U	6740.00	199, 0	7.971 11	4.51 m 3.850, 50	130.0	3.4	171.1	22(1.1)	5.980.01			×3		3000
$dk \in \Omega$	0.217	1.7	£*	15:2	1.1217	107	534 C	251	1.61.0	* 741-1	51.7.1	+311	9.55	4.74.00	151 1	1.77	6201.00	7/31 (1)	1.4	- 11	N.I			T			
K100 HEAR	02/24/3	126	- 1		116290	23.79	28600	161 161	1.01.0	2.16/00	99093 813 a 1	221 × 15	6634.0	3392-83	7.998.96 ( 1 st	100.00	4 TSE 36	5.01.11	53		N/4	3.25203	275, 300	905	N3	- 53	3897.0
VW-22-11	00 0 x 3	138	<del>                                     </del>	1	121.299	17.68	. 236 (80)		100010	1 "21, 40	5.97E-36	F 6 67 13	3.956~,46	477.00	11,6-0	1 118-01	259000	3355-0.1	4 ( 5-6)	58E+03	5500-7	4.55E-35	1250.03	No	(2)	5.7	5890.5
CB. 5. 50	07 0 mg	1.5	1 8	- 25	121249	22 C	1.40.6	264.1	1.865.0 1.985.0	2.2%	1.01 × 8.61×1	8.51E-0	2 J88 - G1 1 8°C - 12	178 (0	2.8(L/-)t. 3.66-/a	2,331,48	1 0 cs	8.86 - 0.3 8.26-0.1	1.441 - c.1 8.263 - c.i	2.666.4	2.06-01	1.521.16	3.2543	- 50	53	- 22	3800
NO1-18-26	90,200	3290	2.0	84	2,6306	12.19	4 . WOODS	2.895+1	1.988F-10	8.15.363	*3.494	F 895-15	1405-96	2.6. 40	9 2515-m	1.195-38	5.84.00	888 B-r (1	8.4	V.,	300	152.10	225, 13	- 55	75	- 37	3885-2
1777 48 24	02211	1.6	1 3	- 51	101047	2.41	131.0	181 (**	1.171 C	3 ° p ' p '	1431 x 1 9 360 x 5	19 <sup>-1</sup> (	1 M1 m	1.1 90.1	1 10 1	2.151	1000 11	954 11	N.4	- 11	3.1						+
N. 20 CR (0)	0.797	160	4 6	- 303	2547000	l ini	7.756 C	7.00047	1.690-07	8,808.0	866.0	8.706.70	2057.00	4778900	111111	2.151 #	10000	1957-03	Ki	864	No.	1,000-00	0.140.61	300	- 60	NA.	1000
621-28-05	02:24.1	1.0	Ч.	-19 -	131247	.15	, k8 C	.511.	I M C	2 91 41 5 91 41	16,	C 581+1.	975	1901 11	1 121 4	-, \$4-41	3.11.11	. 3 *	71	11	- 11		_				+
2000	0 369	136	1		40000	100	100	1 10 11	1997-10	1, 141 -41	91/12	9.271.08	200.00	100000	Tigoro	128 8	T. 240 (1)4	170000	100000	2.196.133	7 805-01	7.4690-07	N2	80	- 50	100	3000
V31-61-02	02-211	1.5	515	2 -	11.19	.115	TSIL C	. 54 1.	1 .1 C	. 612.1	5 (8) ≥ 1	10.0	11.1 **	8 % 11	184 #	5121	191 0	5 %1 #	7.1	- 11	27			T			

 $\label{eq:controlled} \begin{array}{ll} 1.17 + 1.85 \times 1.78 \times 1.89 \times 1.87 \times 1.09 \times$ 

final dis

#### LARLE 3 DOLKULQUARDR 2005 GROUNDWALLKANALD TICAL RISH UTS AND ANDRAGES INDIANDRISE SARIGE CENTER IN CHANGE

													INDIAN POINT BLCIL	SAS M	.K												
			SAMPLE ZONE	SAMPLE ZONE									1	VUASIS RESI I	TS								A FARL	V ROLLING 33	PRACES!		
wento'	OLARTER <sup>2</sup>	SAMPLE ID	CENTER Supply ET Reform	CENTER	SAMPLEO	DITECTION		гатим дест	)		Se 90 (pCi f)			Cs 13° (pC) F <sub>3</sub>			Cn 6h ppf+1a			N (3 g) C+1.4		DOLLAR CLOSE	Si 50 Ept (1.13)	CY 132 (p.C) L)	Co 6º (pt) [1	% 63 (p(11)	#WHI ID
			Inp of Cavog <sup>2</sup>	Flevarium Pt rost	Date	lime	Result	Sid Des	MDC	Result	Still Des	MDI	Result	Stil Dei	ADC.	Result	Sld Des	MUK	Result	Std Dm	ADC	Verrage	Average	Annage	Average	Average	
VW 4-14	95017	111	315	**.	8 1247	1.4	271.0	191 (**	151.0	310.0	111111	2.12.1	2.171 00	\$1.00 p.s.	7.631 a	3 ICL + +	5 (8) ++	7 381 #	5 1 1	1.791 +	2.61.01						
255.60.32	Q1.2963	rise		10.9	39309	2138	100.0	2.397.02	1.88.12	18.7.61	\$391703	2262.00	1287 (0	3.860.00	1892.00	xx45.00	3 2 6	3.526.000	2200	3.196.02	35%003	3.512.01	80	X9	N3	- 80	43.782
170 6 51	05011	1.6	9.	10.5	11716	125	15st C	50.0	179 6	5 (c) c2	5.731 + 1	807.1	1111 0	35 (1	1431 #	1621.0	1981 11	* 851 m	1.01.0	1191	231.01						
325-9-51	9-211	11.		-0.5	.1512111		-1 0	.11.5	15.1 C	1.4 %	-5% - 1,	C 121 o 1	-256 0	7 SST 11	9, 4	2004.00	756.11	691 #	- 21	- 11	21						
\$289-60-13 \$311-0-1	QC2993	1177		-555	23309	31.25	151.0	200,000	139% 92 1 Y C	44.165-01 5.121-4.1	5501 × 1	580603	4.54±-09	9.00E-08	13000460	80,000	5 Cl 11	2006.402	-02000 	2,248+99	2560-73	1.90-70			N9	30	\$89,600
A40.00	0.11	11		19.6	151017	1.1	1731 0	(c) 1.	149L C	1.01.0	587 1	- 87 i	, (81 m	11 7887	160 4	1.3/1 mm	619 11	4 80 m	2.55	1.50	2.61.01						
Sec.	11.2069	156	271.0	122.1	23/249	1251	389.44	(6.3.44)	1997 C	2600	696000	6,563.3	1.3546	2.68 -6	1.55,75	126-3	\$65, 61	3.500-96	3. 10.51	221.8	286.01	1.41, 12	N.	V.	(5)	- 90	X 5 4 3
VW 40 15	03/24 /	1.5	3.7	42.1	9.124.4	11 55 11 55	216.15	. 85. F.	. J C	1.551.7	5880 1	1950	75.0	3.70 to	8 5, a	156 1	5311.11	5-1 # 3.951 #	77	127.1	200		-		-		
1717 % 15	\$1500	1.1	1, )	107 [	10 30 30 60	11.45	31" 13	1 50. 14	41.0		1911	50100	150.7	1.82. 1.1	181 #	455, 11	4.500 a	5 CF 11	Na.	N1	8.1	120.00	(3)		N23	- 20	
35 60 LS	\$1/24.9 \$2-2.4 **	106	254	447	20209	13.38	119, 1	2/1. 1.	. a c	4368635 761 C	585.05	( %) + 1	7.148.68 -2.51 0	3.02E+06 ( %) =	157, 10	200,250,00	3342.13	4 C4E / 0G	1 1 N 1 N 1 N 1 N 1 N 1 N 1 N 1 N 1 N 1	3.995.95	3.126+03	1445052	× × × × × × × × × × × × × × × × × × ×	1.345,500	- 20		30,00000
MINISTRAL ST	05-2 k r	10	.5-1	447	8 12 4 7	1, 1-	5132.12	120.0	. 481 C	3 521 - 0. - 181 - 0.	1.40 - 1. No. 1 - 2.1	5.981.4.1	-5970 - H	5 (4) (6	6/6L #	2.81 4	9102 8	410 11	.97.11	. 91 1.	2 68 1.						
X89:36:36	01.260	154	3.88	1614	2/92/99	1296	ing as	1965.05	1000	455000	68.600	5/81/03	2.435.08	3216.06	\$600.00	4.56.00	332000	1.50.00	32.11	2/66/1/0	21,000	100.0	307	36,3		AID	ACK 56 1
VIV.6 5	22.24.7	1.6	-4)	1011	8 1247	1 1k	100.00	34, 1	. WI C	2.101.7	9 - L - C - L	- 501-01	1.7.0	5 151 =	5.1, 0	1731 0	- SC / 11	4.9)1 m	- NA	1.1.5	- 54						
VAL 6 2	Ç1217	1.1	-4)	[21]	10 30 30 6	1.5	100.13	1.83, 1,	61.0	2.90 - 0	1787-11	1971	8.50	4 444, 111	1.751 a	*11 #	4.57	Cer. 11	3.1	N1	N.i.						
N/55 (63 (68) 3234 (62) (8	Q2 (2.4.4.	103		· .	1.73.568	11.55	153.96 191.0	. 571 1.	3,00000 1,94 G	1 (1-1)	192-5	140.	5.834.70	19.1 =	* 957 - 95 * 5 1 #	\$ 126.61 1 5.1 0	122, 11	121 *	1, 58, 11	194 ).	-1111	3.99:70	1 (967-10)	No.	N2		NOC 62
VIV-62-18	992333	10		1.	2,247	.131	2.60 C	2 161 1 .	H C	1.01-0	5 (1) (1)	24 c). 80 ft (c)	8 (2. ) 0	274 11	. 61	2 (1.0)	266, 40	1.58 #	7.1	- 11	71						
577.623	0.289	116	813	193	121200	1130	48 97+ C	2.00	1 68-C	1.386488	1115/0	900000	781.4%	3.00	2000	600	10000	3.910.00	- Ni	344	- 11	150.00	V.	V)	V)	- 40	MW-43
7.41. 45. fc.	Q1217	1.6	111	198	1401)	512	150 C	441.	139 0	V61 (1	578	8 191 +	1.25 0	300 0	1,61 =	4 (C) (C)	135 11	181 +	78 (I	151.0	21.1.01		_		_		1
323-62-6	9-21-7	11.	615	-15.5	31 24 *	.53	2.1 0	. 11 1.	1.91.0	0.13 - 5	15, -1,	8 (61 -) 1	-S s1, 1)	. 11 5	201. %	. 61 =	25, 11	21 4	- 11	- 1	7.1						
X151-62-53 1717-67-53	01.543	1.0	11	- dica	1.50000	17)	153 0	2.169/042	13/1 0	4.53698 5.951 i I	5, 41	5 61 1	19" (	5.3(2.00)	144 #	* 57° 11	7 Seds 36	111 0	5 F 11	1751 1	2121.11	3.2%G		, N	- 83	- 20	3502-61-
7271-62-71	00011	1.5	81,	-0.5	2,247	.01	2-1-0	2.3 %	1 to 0	51-41 13-4 A	29 41	8,91, +1,	28,194	1,5,11	189 4	4 SECT - 5 CT - 1	1,4 11	1.51 #	- 71	- 11	- 11						
7.55	0.041	0.8		-11 3	10100	- 18	25H C	. 51	2.342.07	3.625.01	1140	835000	1.270.000	281 *	129000		100	121-03		i i	- 1	1900			3.3		\$100.62
V3V-625-1	03.247	1.5	1-	195.5	1 1241	15	1.91 0	2311	1.5E C	. 8141	5/81 #1	807.1	60 0	3.6.0	11 *	87111	149 #	131 *	0.8, 11 Na	181 .	20.0						
7,05,45,11	0.217	- 11	-i	48.5	1 1111	*	0.00	24.72	1.01.0	3.01.1	115.1	1,641.11	934" 1	5.781 #	634" #	471 4	1.34" 1.1	5"1 #	N.t	Ni.	5.1						
\$220,62.60 \$250,62.50	Q2-2009 Q2-2 F F	1.75	\$1.6 51.6	- 5.5	127/296	12.25	5.296/02 51N C	2.991.1	3.886.30 1.51 C		5 (2) × (	67M598	2.690,00	4288560	10.00	9.887 ac	1.161 #	156, 11	- 5/A -1 28, -1,	. Sal 1.	2.21.0	4 510 02	100	- 50		- 100	M96.62.5
7.00, 45, 65	0121	1.10	51 -	"8.8 "8.8	1 1147	13"	*81 C	24 12	100.0	371.73	617.71	8 70 1	131.11	\$ \$ 57 mm	1.61 =	9.5	1 h 1 m	14" 11	3.4	31	3.4						
A644 (621 (102)	0.000	126	336.1	-1953	127,000	12.80	1.39.110	259,00	2.642.0	2.004.110	100000	6.336.53	420.41	2.001.00	16.30	200.00	236	2.640.00	50	200	- 1	\$210.02	216, 19	101	100	535	3235-62-6
100 -62-15	20/24 1	1.5	. % 1	425.1	2,247	12.%	2.1.	2.8, 1,	. 121 0	. 31 11	8 U+C	791 # T	1, - 11 - 36- 1	7 151 #	150.0	155 5	105, 11	1.51 #		1861 %	-121-11						
1777 42 78	\$1247	+ 1	78.1	[01]	1 123 6	151	176 15	150.15	77.7	^57° +	798.11	-8** 1	11.5 m	7.77 11	83/1 =	22,172	2977 11	871.6	N.4	N1	3.1						
5886 80 - 80 V0 (-62) - 82	01.503	126	.50	3693	101000	10.00	1965.45	2.21. 1.	0.998.00	998.98 4 .41 - 1.	- 180 H	6.886.63 5.161.4.1	2.61743	0.838-08 0.121 m	14% - 00	989.96	2.010.00	2.600 -000	617, 11	1.891.75	-1111	0.000-00	83	X.)	- 53	No	N 20 30 3
V3V-625-32	35211	101	127.	402	1 12 2 6	1515	156. 12	2.1.1.	214 0	- 41 to	8.2+0. 5(1)	5 .141	3 (E) (E)	2.81 #	8.01	-2121 A T	2.5.11	2.41 .5	- 11	- 11	3.1						
X33,63-13	21040	16.8	19	177	\$ 09 09 kg	19.80	150.00	1.6% (10)	3000 157	1000	6.585.00	8.5000	8*3-4	268 10	89 0 96	30°F 90	\$20.00	3.877.00	N.A	Sú	N2.	196. G	Su		N.J		NW 60
VW-60-3	Q2-2 4 1 Q3-2 4 1	1.5	.15		11247	1.20	151 C	. 521 1 .	154 C	1.6170	51 C-C	f 281-15	- 2 T D	736, 11	151 0	87440	1.61 #	1541 C	71	71	71						
V2V-63-18	0.024.1	11.	.15		1,1241		1241 0	. 10 13	Total C	275.42	19421	145.00	-9 291 A .	12.0 11	4 "81 #	.74 ()	724 43	\$101 #	5.1	53	53						
\$223-68-88 \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\	91.3009	1.6	31.5	173	1.20/2003	8020	1366.00 171 C	3.336-85	190.0	1.006/e8 1.1/1.1/1	5.61+1	8.32,00	4,437,40	2340-60	197.00	+3.64ER1	1 (*) 11	1521 #	3.5	- Au	NA NA	1987-12	100	103	75	SA	M96-62-2
Vitrotoral	0.011	1 D	4.5	4.5	11291	,100	141 0	. 91 1.	I SM C	25 1741	115.75	CS.1+1.	57	874.00	× 651 ==	20110	3 55 11	5 (1 =	77	11	- 11						
2707.63.56	9-24	116	0.5	3.0	179790	33.06	987	107.00	153 C 199 C	6670.03	500000	8 8 8	1807.00	112-40	9 (6) # 1 5 (6-9)	3.540	110000	1 ab eth	NA.		33	1315-00		N.	80	NA.	\$65.01
770 665 F	0221	1.6	.75	17.5	4124	131	151 0	91.7	149 0	1.981 (1	2.84.41	381.0	100 0	(2.11	1181 *	761.11	1.8L ++	133 #	N.	11	N.1	_					
120,600	9.211	11.	- 25	1	1, 12 1 1		16 L C	- 10	15.1 C	25 1 1 2 2	231.05	( /s  - ).	2.1.1.	(8.1.1.1	1.1	4, 91, 11	21.11	2881-0	- 11	- 11	- 51				1		
MW-65-97 V31-63-97	4/2-2 4 1	1.0	7.	-9	109200	1000	3.940 · @ 1.641 · C	. 11 14	154 C	1.080.00 1.1-1-1.	060 ATROOPS	5590.	21101	7 21 11	1 151 *	- fol 11	1775, 111	164 11	7.1	- 11	7.1	266000	***************************************		76.8	NA.	NEC-093
VAL 45 91	0.217	112	91	0.	1.1017	151	2011 0	79.7	1-981 C	1817	2121.01	. 191 .	2.10.0	57 J 11	441.4	375 H	101.0	550 n	NA NA	N1	N.I.	_		_		_	
Not -68- 12	(1.58)	100	51.9	903	150.240	14.96	435.00	2.26 - 65	23.63.0	146-35	830-30	5.045403	44 Sile, 98	28899	9000	2.04490	#40×40	4.38-90	NA	- Ni	- N	4 6.5 0 7	V3	V)	505	V.	A' 57 48 1
VW 44 12	(30.24.)	1.5	1.5	572	51247	15.5	162.15	54. 1	. 54 C	150.0	5000	181 (1	-, s1, 1)	7.5.1 #	136 4	1781 #	198 11	1.1 =	27	11	3.1		_				_
VIV-64-12	34211	11.	-1. `	5/2	1, 124.1	1.1	1 %, 1,		. 5.1 C	5.01.0	5.81. c 5.	9.3001	- 21 - 1	(19 # 3.5 G	636. *	S21 #	61, 11	5.21 *	11	1.0	11	532.02				5.4	
7.11. 42 7.11. 42	C1/2/K9 C1/1/4/7	1.6	220	10.87	\$39290 5 [ ^ # J	1.35	929:46 - 3K + 1	2109.60	49 C	111	6 4 21 + 1	5.5°E-06	19,35,69 4,49 (2)	8 5 11	5,930 m	2351 11	1701 =	110.11	N4 N4	N-4	N.1	332.0	2121				X35-463
VIV.68	01047	11		-0.8	1 3247	1.0	196. 1.	. 25.	. 951 C	5.000	5 151 A I	576 1.	1 PJ 10 5 TU 0	587 11	5.54 H	266, 11	96.11	8.771 #	7.1	7.1	3.1		_		_		1
MAN ST. ST.	11.00	116	362.5	1417	179790	1.00	100	100 10	99.10	2.805-33	40000	190.03	1822.400	111111	1.125.000	1736.01	1800160	\$100ketic	8.4	, ii	83	5.500-10	X.	X3	V)	NA.	X/W /44
\$255-60-264 \$255-60-264	31211	1.5	.42 \	450.	51200	1 - 15	5 % 1.	. 54. 1.	. 561 C	4, 101 x 0 4, 101 x 0	70 to to	5.614.1	-258 0	511.0	7 L O	-1.191 -1.1	180 0	9 (c. 1.)	71	11	21				<del>                                     </del>		-
1717 41 41 1859 63 171	Q1200	103	42.4	151*	1292989	13.15	000000	3.28367	300000	13(1) 4270-98	875.1	5 181 + 1	5 TO 1 1	3.919 (C)	1,171 (	491 m	11 70.	3.026.000	N.C	24	N.)	4.676.00	350	NO.	N		N. W. 45.1
V33 -6 to	31.24 · ·	1.5		-171	51243	1 - 2	18 . 1 .	. 5d. 1.	. 581 5	-2.19(3.1	57	\$ 1 - 1.	. 58 1.	- 351 1.1	. 101 m	2.90 (1)	1,4, 11	. fall #	7.1	1.1	7.1	25.00.0E	200				
VIVAS T.	2562.63	11.	-	40	11111	14.54	18.1.	60 1°	.5J C	74.41	507.7	9.614	100.0	C fol 1.1	61SI = 91 =	1 701 0	504 11	5 831 m	7.1	11	N.1						
VIII ACT	0.2969	6547			127743	18.55	1800.0	5.5 (5.00)	1 *98-30	29,698	*53.01	8737.00	8,990-54	3 (57 (6))	# 1 19 St	875-05	2340.56	2.1003	200.01	370898	1907.0	5.657.07	5,5	3.96510	- V3	100	3690.66
170 6 21 100 6621	Q1 % 6 V c	1.5	1.1.	-	12/24/	10.0	9.251 G	187 0	581° (*	3 191 cT 1 251 cT	519 (1	750.0	127.0	25, 11	1521 #	201.11	11.1 =	181, 11	1.81 +	74.0	22. 1		_				_
139 66-21 139 6-21	0.211	- 10	-1-	1	282 0 0	-1.7	8231 C	25211.	1 U C	13,171	5 1121	9111	41 121 A . 1 101 H	35L 0	15.1 a 650 a	2 (91 × 1	1.04 11	581.0	8-8-11	1.61 (	2 50 11						
	9.500	600	33.4	193	101090	1961	3.0%p.cs	630 (1)	600.00	1491	10000	5 171 1	1040.00	784 13	A TOTAL OF	633640	\$270.00	3.77.63	355.00	1,799136	1379.0	1 290 20	9.587.50	- 566	3.2	202	\$100.66
XXX-66-36 XXX-66-36	Q22 K F	1.6	57	-192 -192	28244	.5.26	1 tel - 6	- 19 G	181 C	3.01 % SJ 10	1.01 +	17931	55L+L	614 0	1.51 *	-520141	105, 0	1.00 1.1	655, 11	. 71 S	210 5						
127-16-10	100211	110	324	-192	1.124.1	1	1 32 6	111 0	2.64 6	2/8/1 1.1	120 11	1 50141	1 1747 1	6 29 8	N 11 1	-517121	1 55 0	7 951 8	2 NE 11	1 721 1	2.00 (1						-

1171 + 1856 1787 1876 1876 7 Come Hibbs 1964 Come - Lemma Miles A Qualities

This, 45 No. 7 No.

#### TABLE 3 FOURTH QUARTER 2005 GROUNDWATER AND A TREE TO TAKE A GENERAL TRADE AND THE AN

													381 C FEA	11111													
			SAMPLE ZONE										i.	VIA SIS REST I	TS								11-181	A' ROLLING AT	FR YOFS!		
men to,	SAMPLING OF ARTER	SAMPLE ID	ONTER Depth H Relos	SAMPLE ZONE CENTER Elevation Florid	SAMPLE CO	DITECTION		гити м дест	1		Se Se (pC) fy			Cs 135 (pC) L <sub>1</sub>			Cost ptila			Vi 63 gi€ i 1.j		IRILIUM ipC(1)	Si 50 fpCi L)	CA 135, (0/O 15)	Co 6º (pC+11	% 63 (p(11)	Well to
			Inp of Caveg		Date	lime	Result	Sid Des	MDC	Result	Still Des	MDI	Result	Stil Des	ADC.	Result	Std Des	MUK	Result	Yid Dm	ADC	Astrage	Average	Aurage	Annagr	Average	
A700 61 30	02.2 F	1.6	15.1	75.8	12,24		1631.0	11111	1308-10 1 11 C	JUSEIN	154.4	2027.08	21.78 d	*/dE-05	1966	1.116.01	706000	4.406.640	176.63	2.86.00	2.91 %	109011	118693	NO	, V)	ND	702.0.30
V34-6 -02	00011	1.0	12.1	-7.9	28.2 * *	254	- fel 19	131.1	1 M C	(1)	11.1	198. 11.	. 96 1	11111	1 21 4	12/2/	131, 11	141.0	- 16. 11	1 91 %	2.91 (						_
738.45.45	0.21	- 11	141	*58	1.1547	107	281 6	* 181 + *	149 0	35[ 1]	187 *	1.64.01	157.0	8 (1 =	881" =	7.1 *	17.11	1071.0	587	1 191 +	1781-01						
388060003	QL 2967	16	200.8	893	121290	16.85	1.000 (0.00	2.02.10	3.756.20 . Sel. C	5 /51 /s	8.5600	53895393 121-11	1.530.00	3.326.00	2.10146	1.000.00	2,000,000	1921 #	27699	18,619	1.356.49	1.990.03	6.90 E SE	NO	NO.	89	N004049
123 A . B	33-21	1.0	. 1-5	2.1	282 4 1	15.15	1 % 11	111	2.61 C	5781 5	192.15	12131	1 % 0	289 #	26. 8	- 21 - 1	3.5% 1.1	164 8	11111	1 801 %	2.01.01		_				
133-6 -, 0	34247	1,1	. 1-8	2,1	1,1,2,5	14.5	12.11	100	2.04 %	8 191 - 5	535,21	-25, -1,	, C ),	182, 11	6 .1 **	1,,121	10, 11	(1.4	42	1.3.5	1.91.41						
A000 00 04	0.5616	4.7	;	199	1000kg	10.93	1.731.17	3 6967 + 65 L C C	581	4.95E(3)	498930	6.30E353	151.0	1880-0	7 8180-6a	34-06	1.11	2.96.6	485-01	1798.00	1365-01	307007	50	1.545991	80	3.105+5	179, 61111
VW-6 - 1	3.2	1.0		4578	121211	15.50	11.1.	2.2%	.81 C	. 141. 1	Ostro	8-1-1-1	- 1 0	101 11	1 1 1	135.11	361, 11	1.24	8 10 01	. 19 %	-11.0						
333-6 -, 1	35211	1.00	. 21	41578	28.2 4 1	IN.	1.6, 13	2.5, 1,	231 0	1391.0	538.00	C 851 o 1	6.161.0.1	2.73	1.00	-61,121	47.50 1.1	1,100	501-4-1	1.4.5	1.91.01						
700.32010	C1247	105	70.1	353	107096	1.5	\$10° 0°	280.00	2.50 (4.5	671 i	4.98" +1	8 (* )	2.000 0	581111	661 a	566.48	49° a	2.00 (3	17.0	91 1	2456.0	CEST 15	- V	V.	N.J		N W 67 319
333-6 -215	3.2	1.6	215.5	155	12124	12.0	118.11	201	. %H C	1.11.	CC at	9171		(11 "	307.00	560.00	-26, 11	18-1 *	9.521.1.1	1.551.75	91.11	0.000.0		-	3.3		
335.6 (215)	31211	1.6	215.8	-2151	28.2 * *	I. I.	1.2.1.	271, 14	2 M C	18.10.	87.5 - 5	9.601.0.1	287. 1	1.01 1	19.0	1501 #	15.11	17.1 *	.14.01	1.941 %	139.01						
A5Wes*-215	04211	1.1	215.8	-21 1/2	1.1.2.6	1.11	114.17	2.680 12	2 11 12	-, 3,5 4 1	237.41	5.6644	23664	-342 11	5.700.00	74 4 1	525 11	9 10 11	(17) 11					ļ			
A200-001-200	Q1-3069	1.0	2253	2628	12/200	1900	1167.17	5.090.00	971 C	7.791 (5	5,932,00	. T. I . I	5 I	5   F   10   10   10   10   10   10   10	1,77 #	* 8.1 + 1	517 11	A SOTT BE	22.1.1	1.6851000	18000	100000	- 50	- 50	N2	302	MR 6 25
1.40.42.42	(22.24.)	1.6	^*61	7/7 8	-26247	1 15	11" 1"	2/31/12	2.61.0	***41 1	4981	- 161 CT	1.817 (1	5 (1 )	101110	181 -	3717 (1)	151.4	10100	1.79 (	1.791.11						
300 6 -2 7 300 6 93	31-24	197	200	-,r, s	1, 1, 1 %	1	3.97.40	135.	3.594.1	2.19.0	\$17,41	9,5 () - 1, 5,850 ()	551, - 1, 4780 49	5.21. 11 3.309-08	9 5 4 1 10	- 101 H	130000	3.805+90	10056	1.501 1.	151.0		- X-1		- 23	No.	200.61304
\13\ 4"\13\	C1.04.7	-3	570.5	168	101017	10.00	1 / 1-1 *	1.65 (0)	871 (4	2015-1	7136 1	8.21	4 701 11	1 35 -11	1471 - 4	2.5 (6.4.4.4)	197 40	1331-11	1 Sec. 10.	2 of 9	1 (126-e)	1996-17	***************************************	***************************************	***************************************		******
335-6 013	31211	1.6	4,21	-11.75	28.2 * *	15	116.15	2.5. 1.	211 0	3 U. C	521, 03,	10100	4.54, 0	3.731 8	10, 4	43, 43,	N 11	154 0	2.04 (4.1	1.91.5	. 14 11						
320.6 0.3	36211	1.1	V2.	-11.78	1.1.2.5	1. 1.	Laur La	17	.6N L	.1741	186.41	255.	.1 t.J 0	b ! !	8 41 4	12.01.1.1	8141 #	55.11	. 91, 11	. 24 1.							
3,840 (C) 466 173 (6 - 18)	61.099	1.0	525.8	3203	107200	12.5	9.340 at	330.40	. %) C	119.5	561.7	690148	1.5. 1	3.728-360	£190°m	4.966.66	3,000,000	1 651 #	2.760 409	1.680.490	198899	5 (17) (12)	80	80	- 83	No	ACV0.6"-6.86
7.47.42.49	(121)	1.6	115.5	10-1		1.5	157.75	4441	2.60	1011	100.00	230101	4 (8) (1	1-1 "	131 4	150 (1	4147 111	161 1	1 711 1	1 491 1	2101.01						
7,47,32,44	\$1200		115 4	107.1	1176	1.78	49" 1"	100.0	49 11	4 11		631" 1	317.4	177 11	618L a	* 161 m	47T a	\$10° cc	781" =	191 +	-1.						
Attes		106	32	2.1	10,000	12.9	1.96.15	151,115 180,110	88.10	519673	4 Studie	2.526-24	1310.00	#.8659. 24151	2.2 Total	1244490 1244443	2000-03	Australia National		- X.		Fisher C	136.49	V.			33 cc - 111 34 55 - 1 2 1
713 1	21247	(3)	4.4	2.1	1 ***/	15.18	2.767 1.1	1.92" 1."	91.0	8 1/1 / 1	4 77 11	574"	51F C	3511 11	(79) 0	191 1	5.71 =	7/81 1 1	3.5	- 51	3.4						
( t-4)	(14290)	142	25.5	45%	1392909	18.15	180,00	2.86, 7%	100.00	9356	5 (fg + 6)	6.0,15.0	3.8 C7(	2.5610.0	1800-00		502.00	0.840.03	553	8.0	54	135 C	N.)	× .	- 20		Chan
13.40	03/24 /	121	25.5	-, 15	85047	INS.	180 12	83	. SH C	57.11	515.0	7317.7	2917.	5.8 11	15,1 =	31 cc	161 0	5751 11	7.1	11	11			_			
5.40	Sign	144	25.6	-, 15	1,5211	1515	155	. 25. 1.	. 44 C	425.4	1 191 4 1	0.08, 01,	1.01 10	184, 11	f   H	7971	921 8	101 11	17	- 11	11						
CA.	0.00	63			1800.0	17.60	5.79545	9-41	3345-665	2 militaria:	11.504	315.00	Sheet (4	4.600 000	1997-00	g Sellia	2 89-se	2 187 - 63	Ν.,	N.	N.A.	1.85.70	1 (14 (14)	- 22	No.	24	15.1
13.1	213.6	61	2 -	* S	1-25	15 00	3.76 (.)	1 (4° C	251.	500 1	677.1	5.89.01	- 51. 1	5 (SI ) II	161 #	124 6	137 11	1.7.00	7.1	N1	3.1	_					
Usel.	312.5	26	-	2.6	1,122.5	10.15	1 % 1-	1.5 C	200.00	10.21	5.79(4)	((), (),	-68.1 a .	335 11	2.61.0	. 141 1.1	614 #	1, 11	- 17	- 11	- 11						
U1.75	0.700	525		20	78 20 6	1.36	5.135.00	289.40	2,016,102	600000	8.8855.07	6.786.64	2.190.51	7.438.00	278,00	102.00	2.5(6) 69	2,677.03	500	344		1612-05	1.762.100	X0	300		13/12
LUP	(2.2.0	(1)	4.5	27	11.5.6	1.5.	1.65.14	15" (*	285.74	50.01	86.171	5.5% - 1.	132 m	100 11	1.9 *	4 121 - C	1101 +	197 11	7.4	7.1	7.1						
1 5-12	310.6	91		2/	1.16.2.9	12.54	8 fs. fs.	15 C	250, 12	121, 21	55-1-1	1,10	196.46	(() 11	(10)	-20 5 1 1	5.29	575.11	- 27	- 11	- 51						
31-038	200 00000000000000000000000000000000000	ie j	1-	e:	3/38/25/36	1104	2.4 (0.02)	1,650,012	5534,000		2,946+36	921×.6	2.002, 8th	5542-63	2047.90	2.908.53	7.946.36	10.00	6.186.30	19.6-91	27. 0	1,945.6	2.28,998	80	N)	N9	01/05
1178	(21217	1.2		- 1	101017	18.7	138.13	281111	30 0	3.50	24.1 a	5 381 1	L C II	5 24 11	671 #	3/1 a	3 (4) a	17F ()	127.0	2011	231.11			_			
1000	01/2869	16.		· · · · · · · · · · · · · · · · · · ·	111200	1838	21444	2 (80 -12	COV.C	201000	8.01	6,632,00	280000	260	12900	960.00	28334		6835-62	1011000		128.11	2346-95	2340-01	100	1319-152	No. New
diNo	35-24-1	6.			1 12 1 1	12.15	No. 11	1.8.1.	. N C	1.21 C	4 *	Sec. 15		266, 11	. 1.5	2 (1 )	1 -6, 11	315, 10	1.911.	5.01 %	191.01						
.170	25 % 6 Mar	1.5			1122.6	1 n n	247 (3	3.86" (*)	* 61 /* Ski ul	3-1 C	1.81 *	5117 1	1.35, 41	557 (3	91 -	\$71 pg	5.39° m	136 11	5.11(2)	3 00 L 01	2300 01	_					
	V-263	101		-	114200	7.0	1600	335000	E SECTION AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRES	5,029,0148	163.0	8.33.5	6.305.04	331	2.25.06	040.00	1920 35		100	1826.35	1800-01	8	3 150 10	9.00	323	- 40	5+58405
, I-b65	V2-2 1 1	1.15			1 124.1	a. 10	1221.0	2.89 1.	111.0	+ 201 3 (1	1.04	1000	\$1.5 00	48.11	2.91 (4)	2.191 #	18 0 10	1.5, 11	25 ( ) 1.1	1.21 %	2.91.71						
14-5005	Q5-2 4 7 C1-3 5 Vac	1.8			11 1 - 2 5	5.0	7304 0	2.79(-12)	2.791 (2	250, 5	257 4	37 C 4 C	1.21 4	5 di 10 8 de 10	191 4	5.00 4.1	1-0 0	558. 11	510 O	214 0	214 11	-	-		-		
1817	02.249334			-	61.300	1141	100	1973-03	130	2200	6.21.41	8.481.33	1.2	100	618.00	7.001 - 1	186	173	. BI .	. 91 11	****	110	322			8.0	381.8
30.165	2023 Uslic	15			8.00%	10.15	36, 13	. 4. C	2.8.1.	5.161.6.1	554 at	5.7100	87.5 - 0	5.581 1.1	6.4 *	. 11 1	531, 11	91.11	7.1	11	- 5.1						
101.05 1.67.090	31-3 % 31-3-9	- 11		91.6	1,10,4.6	1, 11	136.02	1.00, 0	3.396-70	150, 41 Total	53 p. 1	161 or 1 r 497 18	-5 a6, -11 78F -60	555-00	1 9/F-66	3.376.61	7.22, 11 3.99(++10)	1505-13	2315-13	- 92Fet I	* -90 - 13	ND:	- 60	ND:	80	ND	1.41 69
2.000	01217	112		27.5	1 19 5 6	10.35	1.00-40	110.40	49 0	ST 1	5131.11	207 1	111111	851 11	1.01 1	1.201.1.1	3.58	100000	227 11	1171	58L L	70	1 40	705		- 10	1.41 611
3	02-20-93464	984			6/12/09	11.9	8 901, 10	1 5.55 92	3 62102	1013402	991501	21953	9.218190	1.116.61	1,678	3.29° m	6.2% (6)	18/1 17	S.A.	V,A	N3	\$810.10	V)	V)	NO	50	R-1
347	33-190y Mac	1.06			6329.9	9.01	1.386.00	2.166.402	2.638+10	( -0)	0% +0	\$13f-c1	. 30[.0]	1.190° 95	98'-9"	1.241'-06'	< 961.60	491 0	8.4	5.1	5.3	NJ:	50	ND	5.3	5.5	B-5

TTTO CIRSOS (TWO TWO SENSED OF COME LERBIS TO CATE OF COMBINED VALVA OF THE SENSED OF

<sup>##</sup> April 19 | April 19

## TABLE F 2008 REQUARTER GROENDWALER ANALYTICAL RESILES INDIAN POINT ENERTY CENTER RECENTALY ANALYTICAL

											110	BLCHANAS BLCHANAS												
		1											17 JUYSE	RFS1 1. [S					_					
Well ID	SAMPLE ID	SAMPLE COL	LECTION		IRITE	d (gCrL)			N <sub>1</sub> .90	(pCrL)			C+137	("Pic"Aqi			Cu-60	(μC ω1.)			No 63	(µCrL)		Well ID
		Date	lime	Result	Std Des	VIDE	11.5	Newst	Std Dri	VIDE	- 11	Result	Std Des	YHH	11	Result	Nid Des	VIDE	- 11	Recelt	Nid Drs	AUK.	- 11	
MM-546C	*	197.00	1.5	5 Hr 3	1.66	80 to 0	1640 HS	-1 '6 - 1 885 at	6 (4)- (	811 - 1	2.06	1 6 40	5370.0	5.30.0	1095,16	335 40	5.41	158 0	Leafer Leafer	NA NA	VA VA	NA NA	LOSEP 2	MVV-20-84
MW-41-19	- 50	10 25 30 3	1.58	5 10010 134	8 65E ( E)	5 (-s) - (C	3.55500	265 -01	8 15-1	96 - 1	2.06		6 b 0	6.830.0	10%, 16	-3 [set]	5 SE 0	5.6Hr	Testine .	VA VA	VA VA	NA NA	LONGE S	MVV-31-49
79 (6.707)	1.50	10 25 20 S	32	North 11	\$350.00	6716-112	3 oSh int	mb 22	7 (81) 11	- 3 1	Stuters	158 01	\$500 in	6.73b ir	parte	A 241 - 111	9-120-17	1.506-11	reserve	NA.	NA	NA.	positit :	MW 31 65
MW-31465 MW-31465	51	10 ** 50 g	151	1.60	5 (6)	6 F 02	× 31: 03	5.55 -01	6.6 (6-1)	980 - 1	2.06	3.5 (4)	6 9 0	6.695.0	Lang. La	3 mb = 0	5 F 0	- 10	near ne	VA	VA.	NA NA	posite z	MVV-21-55
/III 35.88	5.5	10 22 2005	1 1	5610 5	3 83E 52	550-112 550-112	8 F 00	10 5.05	6 30cc	5 117.14	2006-00	. 561: 141	5 (6) 0	5 50 0 580; 0.	positive positive	2000 0	91- 5 1- 10.	987E-00	positive reserve	NA NA	NA NA	NA NA	postrue postrue	MW 32 59 MW 32 55
V3V 32 . *	5.3	10/22/2005	3.3%	2.66.12	. 556 52	. of h 10	. 53[: 113	7560,12	1516.0.	5.330.00	2 506 555	6.751; 10.	5 444 00	1.581.10	postare	5 881: 01	874: (C	8 301; 55.	2000.00	VA.	VA.	NA.	postra 2	MW-32-147
1711-15-1	t	po ve to g	~ 55	1911/19	Pod- ,	680-003	3 2 15 113	4.01 - 1	4.85(-)	195 - 1	2.00	20.1	58400	66 F 0	LONG 16	68 4	8 01	661 0	positive.	VA.	VA.	NA.	Long to 5	MW-32-173
VIII. 36.7 c	- 6	10 % 50 g	5.18	531- 1	2101-12	6 F 02	2.241-113	6.367.00	3.50(c) 8.51(c)	140 - 1	2106	-1.6 ft 0 -2.3 C 11	5 1: 0 3 (-51: 10	5 550 O	Long. ce	3111.0	5 95E-0	66 F	1697.16	NΑ	NΛ	NA.	Longe S	MW 52 193
MW-86-II	- 0	10 % 10 9	6.3	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.396	5.10.00	29-16	5 10 ( )	198-100	96:401	2100 8	-295 - 1	1 1 0	3 10 0	paurie 10stile	SH 101	Lapti	5 8 11	pant te	NA NA	VA VA	NA NA	pouritz 1 mirez	389-36-21
VIW 36-52	5.,5	10 28 2007	.5.35	8 23 E 1/3	3.926.52	. 97E 02	2.33[: 01	3.511; 12.	. 05), (0)	6910.01	. 251: 5	. 281: 144	1.381; 10.	1581: 10.	ромпле	3.630, 000	11.5]; 10.	5 . 31: 14:	2080.00	NA.	NA.	NA.	positive	WW 36 52
700/37/22	5,6	10/28/2005	.13%	1.50() 1.3	2 964: 12	. 926-02	50.26 (03	. 246 %.	. 5.1. 00	1867, 51	2 (01) 5.	5.80,02	Sood: 10.	0.30E-10.	риктие	3750,00	6 Ch to:	7-700, SO	pontac	NA.	NA.	NA.	positive.	WW 37 22
MW 37 32 MW-3 - R	5,76	10/28/2005	.137	1.46E-1.3	2 885: 1/2	5 % H 02	5871: 03	2.5% %.	2011, 00 , 75E-491	100.00	3 -01; i., 2 26Be x	370E (C.	5.5 (c. 6.5)	550 m.	posence Loss' ne	2 ,21, 6,	1 (7) (a) 6 (3) (a)	5.380, 00 8.39b	pontac	NA NA	VA VA	NA NA	positive Losefe e	MV-37-32 MV-37-40
VIII - 2 - 2	16	1 8 . 0	. 0	120 3	18.6	Solvery.	80.000	1980 1	2500-000	88 - 1	191h 1	2011	58000	6.5%(1.00)	lon, in	J. 19000	55 1/10	200	2591.10	VA.	VA VA	NA NA	198737	WW 3/5/
/III po 6"		1.5.25 (6)	ς	1.016 1.7	2010-0	Switch in	111-103	2.376	2.246.0	51127 - 1	2017/01/01	0.210.01	517h (r	State in	pastro	2081.20	5.5 p. m	p. 80p. 11	nosmine	NA.	NA.	NA.	positive	MVv-39-67
VIV. 4948 - 12		.1 5 2000		2.000.00	. 08h 52	9.58E-0	10.03	10 Nije 32,	6 86-1 (No. 10)	6.78 ± 1	2.576-55	21.750-0 23.06-0	50 m	Seeds to	Jose ce	5 15 O	5 585 0 7 206 tal.	676.00	, P.M G	AV.	NA.	NA.	positive.	MW 39 54
VW 45 32	12.7	.1 5 2006 .1 5 2006	.5.2	2 (47): 1/2	. 088 52 . 008 52	144E 02	, tale 63 , tale 63	. 2 Hr 12.	8 (81:0)	1660,01	2.816.50	2.196.65	5.881; (0.	1 550 1C.	positive positive	1 22E 30 - 13E 00	7 (11) (4)	8 980, 00	pontac	NA.	NA.	NA NA	postrice postrice	MW 39 102 MW-30-124
1715 - 10 - K1		15.5.00	2.5	9.696	9.5%	3×1- 0	Jr. 115	4 401	He r	808 - 1	2.00	641-	93460	5 F 0	Toru, i.e.	93 0	5 31 11	3611	meating.	VA.	VA.	NA.	Longer	MW-33-183
174.55.35		1 5 7 (6)	٠,	96.	9.56	9.851- 0	1: 03	. 85 201	(401-1	8 - ( . )	2.00	short o	p. 0	58]- 11	Ton. re	400 0	8 11:	9 [8 0	positive	NA.	NA.	N.A.	Longer	Myy-32-195
MW-1047 MW-10416		11 9 70 9	15	5.7 Hz 2	9 15h	3 SE0 5 8 Ye in	15.03	25 SE 2 F	11-1 4 31-0	597001	2.06	- 06E - 25 575 2 E	1.58E-0	5.136 m	DBC 10	15km	1.516-11	\$ pr   0 \$ 35° 50	positive positive	AV AV	NA.	NA NA	poste z poste z	MVV-40-40
VRV-10481	- 0	11 20.9	4.5	9 Hr	× 8 st-	9.356.0	1: 05	-1 58 - 1	6.646-7	81 -1	2.06	-13  - 0	5 50 0	5 50 0	100,10	2835 0	1.51-11	LXIII	2691.16	VA.	NA.	NA NA	LOSEP 2	MW 40 81
VW 25 100	5.2	11 (7.200)	. [34	7.30E-0.	5.038, 5.	5.85(), 01	, tall; 103	5.080,000	6.511; 0;	1900,01	2006.00	1005 00	3.721; 10.	1.26 (0.	ровеле	4.50(5.0)	1.505 (6.	199: 55	ромпле	VA.	NA.	NA.	positive	M/W 40 100
VW 452"	5.,2	11 .7 2005	.132	. 5 Ht 52	5.336.50	5.856: 0.	, talt 03	2.640, 01	6.568.00	7.951, 14	2 501: 55	. 346 55	5.581; 10.	0.00E-00	posera e	\$450,00	6 (8): 55	7.66, 30	pantaz	VA	VA.	NA NA	positive.	MW-40-127
MW-H-R	- " -	11 50.9	3.3	5.56	8.5%	9 8 H ()	10.00	-1 88 + 1 1 00	6 %H-1	816 - 1	X-961-	9.5 20	5 10 0 3 S 10 0	5.3 E 0 5.30 0	10%***	5 %SH 11	5 (5) (0 1 (5) (0 (1)	6.9 F	1697.10 1697.10	NA NA	NA NA	NA NA	posite z posite z	MW-43-162 MW-41-40
VIII III 45	5.3	11 (6.2065	.3 %	1.646.12	. 2.E 52	5.56E-0.	, talk 103	3 8841 100	9.586.00	5 921, 14	5.356.55	, 07E 55	3 - 3 : 10.	124:16	DANGAR	103[10]	134:16	1804: 144	2067.50	WA.	VA.	NA NA	DOMESTS 2	WW 41 55
700 - 12 - 16	1.0	10 m ne 5	< 3:	751-13	2.5 15 + 2	p*16 m*	8.2 16.03	5116.1	5077.00	. 16 1	56h - 3	2.116 13	K31: 03	p30-11	3 Tole 1.5	- policial	site point	4 76 11	3.80	835-07	31.000	2.516.5	8 150 mg	MVV-45-40
VIV-12-8		11 5 7055	1.6	5 (H) 2 13E (2	58 °	664-02 5-44-0	20 ms	1.511.00	5 Men.	6.530 - 1	2 of	19H 5100,40	3 800 IC.	1.76 (0.	, et- ,	2176.00	3.63E-0	5 III: 1967, 50	near ne panta a	-8-191- NA	NA NA	NA.	59192	MW 42 78
VIV 13 42	5.3	11 (4.200)	.21.2	. 68:12	. 0.E 52	5836.00	, tale 03	. 216:34	7,060,0	65%, 14	2306.55	3000.01	5 , 41 10.	\$7.00 m.	positive positive	4876.01	5.50; 16.	\$10E 55	positive positive	NA.	VA.	NA NA	posmic posmic	MW-43-28
MW-11-66		15.5.00	ъ.	Sp. 1	3 p. 3	9 Je 0	Jr. 115	5.75 (40)	B 04-1	6.9 - 1	2.06	-1940-0	× (55) - 0	5 F 0	10% . 4	8 1150	1 × 5 - 11	5.541	near re	VA	VA	NA.	Long to 5	WV-44-88
120,000	`	1 5 2 60	~ ',	5.36.3	586 5	9 80 0	10.03	8 -01	5 July 1	811 - 1	2.06	0.16	5.2900	28 F 0	Jose' re	-118	S 10 00	1680	5645 1 G	NA.	NA.	NA.	Lost, 6.5	MW 44 102
VIV 15 12 VIV 15 61	118	1, 15,2559	. 1 19	2,500,03	2.246.12	130.02	3321:03	6 (1.5 (0) 3 (0) (0)	6150.00 5 2060	5.000, 51 5.00 (c)	2 10 05 170	1835.0	\$ 541; 95. \$ 550; 00	5 , 7(; e.c. ; 7 () ; e.c.	positive positive	8 721:00	5.57[crez.	5.866 (4)	pontive	VA VA	VA VA	NA	posenie posenie	WW 45 42 WW 45 5
7187-10	5.8	.1 × 2tary	.3.21	1.085.03	. 67 h 52	. 57E 02	, o.l. 03	8760,01	5 095 00	11.6.31	2006.00	2.846.00	~ 25h: 10.	7 (a) (c)	postrate	316C 16	+ , 2h + C	5 TRI: 10.	10811.50	NA.	VA.	NA NA	positive	M VV 45
VIII 19/26	5.3	10.25.2005	.3.1	31,75,03	2.9.16.52	. 881: 02	8 321: 03	. 331: 5.	. 1.5, 00	8200.01	3 (91) 50	1310.01	9 . 3E 10.	95,836	рингле	5.060, 50	5 381; +C.	\$ 56h ha	powrale	120,00	, TE 0.	2046.6	pestace	MW 48 25
MW 19-12 MO - 10-05	5.3	10.25.2005 10.35.003	.34.4	2.51E 0.3	2.766 52	. 881: 02	5.5 () 113 5.5 () 115	. 7 He Sc.	. 9.1, 00	7.500, 01	1805 5.	6.3.01	9.27E 00.	7.22h (c. 8.35h ()	positive	5.326.00	7.2% (C.	8 251; 10.	2081'A C	646 00	, 73E 0.	2.036.00	pestive sestive	WW-49-85
MW-maga	- 0	10 % 70 %	13	1.00	836	881-11,	1: 03	6.31	165 111	155 - 1	6 391	-48 I: 0	1: 0	% O	10%,16	.2.4	6.675	15 0	Leaf to	- 1  - 0	1.461-		125737	WW of 42
MW 50164	1.21	10/25/2005	.135	2 866 13	2 826 52	. 854: 02	5.501: 03	\$ 00h h.	2310.00	53 0.04	1.291: 5.	1.15.01	5.850 00	11 St. 10.	positive.	2.5(4), (0)	94.3h (C.	1 90h 55	positive	9.15, 00	. 895.00	2.76 %	pestae	WW of 66
VIW-41-10		11 8705	15	441-11	3-1	3   00	111-16	-1161-11	6.35169	8000.01	2006-00	-1 170 or	South of	1226.00	Pose ve	418.0	1.551-17	6.5716.11	104116	-5.68" (10)	580-0	7.94	2000.00	WW 51 40
VW 51 %	5.3	11 (8200)	131	5E 52 . 5B: 52	. 80E 52	2 (8): 02	, talt 103 103 (tal)	1500.02	6.87E 0.	8 110.01	2 to 6 to 6	8050.01 9300.00	\$756 (C) 1376 (C)	0.150, 10. 1.80- 0	positive positive	2.786 (0)	9 58h (C	8 0.71; 0.0. 6 901; 0.0.	2080 A C	2.9KL 61 3.030 (0.	. 98E 0.	1.586.5	pestad	MW-6179 MW-51-104
VII. 2 - 12	1	11 8 70 9	1.55	9.0	126.0	235-112	p 115	-561 - 1	b bl-1	81 - 1	2.04	+ N' + I	5 5 de 10	S 10.0	10%, 14	2.81-00	× 0)-	611 0	Louise	1.86	1.516 1	188 1	League A	MW-51-125
174-5- 61	1	11 × 50 §	1.55	3.34	58E 1	195.00	Jr. 03	F-9K 201	6.6 H- 1	96 - 1	2.06	-16al- n	5.86[0	6 30 0	lost is	76 F 0	5 55 11	6.511:	"lost" ne	23.5 000	56E-0	1.930	nestre.	MVV-51-163
VIII. 53.82	1 2	10 27 2005	1.5	× 491	956 52 956 52	87E-02	16 03 , felt 03	1897.34	3 36E 0	6.58 - 1 1567.131	2.00E-00	* 95E	2761: 00	5 50 0 3 150 00	LON, 16	2 (2)(0)	1.35.55	6.18 0	post se	5.596.00	1.0% 1.798.0	2.10C, SI	198752	MW 51 189
VIII-53-82	1.2	10.25.2005	1.57	515613	3 FE 12	8 1: 10	50 ms	3. op. 1	2.4800	1181-11	2 30 ft 5 a.c.	2.75 2.1	2 685 0G	, 550 m	posence posence	2 125 00	1.76 00	7116.0	panta c near ne	1 8 D O	8, E 0	2.0003	pasca c c 8 c - c)	MW 63 52 MW 53 120
MW 5131	5.1	11 (3.200)	.   35	, sells 1.3	2 974: 52	2344: 02	2371: 03	4.77[g td.	100, 00	166, 11	. 221: 5.	+ 200,04	5 o St. (C.	+ 281: 10.	ромеле	2.295.00	6.55.00	6315, 50	pantale	1.98(1)	1806.5.	196, 0	pascar	WW 04 a7
VIW 5158	5.1	11 (3/2005)	.151	8 38E 52	2 (8): 52	23/36/02	, 33); (03	, 5He as	7 (28.0)	6000.03	7 3715 535	3.295 (4)	5071:00	985E 00	positive.	1.34C, 65 6.15E-00	5.2% (C. 9.5%)	3 S21: 10:	positive	70,58,00	. 835 0.	2.678.60	postave	MW-64-55
P 2010		11 3 70 9	159	200 1	1886	2. 36. 02	2.10.03	SIE	85 10	8 8 - 1	5 1 Te	-1 681: 0	250 0	580 O	LONG 16	5 ISE 00	3 70 0	1.176	positive positive	- 3 5 10	4.900	1.40	p35732 325732	MW-54-123 MW-54-144
/38. 41 ". 3	5.1	11.32005	.214	. 831: 13	3.15h; 52	2335.02	3.83[: 03	1 (2): (4)	. 2%, 00	1360,04	2776.50	130,01	- 35E 10.	1 3045 FG.	postar	1.250: 00	1.276 (4)	686), 50	pantae	, Tale 06	1.916.55	200.0	pascas	MW 54 175
VW 51.50.	:41	1, 13 2009	.2*	2.01is 1.3	3.276-52	2335702	135003	. 98is 31	, 535.00	1.100, 04	1706s 34	. 5% (a)	godina.	5 (21) (1).	positive	3.8560	5 (2l) (14)	74(%) (4)	positive	. White	, Sols or.	2.2% (4	positive	MW 54 190
VIII 55.35		1.2.2000	111	381-13	2.646.52	881: 02	3.775.03	2 89h h	2 83, 00	1.807.2.1	575h 5.	6.511.01	9.60 takes 1.231; (c.	4 650 cm3 4 5 dg mg	(3.64), 37	3,877, 50	1, 31-17 1, 101: 10.	5.721; 10.	1660 A C	27 187 00 9 162, 00	735.0	2.026.0	nestine pestive	M9V 55 24
VIV 55 55	5.2	.1 0 2009	.2.33	5 KCH 1/3	3.65h 52	. 87E 02	. 381: 00	2 331: 44	2 125, 00	176, 14	3 of E 5.	. 231: 141	5731: 00	9 5 SE 10.	positive positive	2 821, 101	+ 25E + 0	7 551; 141	20803.0	2770,00	. NE 00	2.306.14	pestate	MW-55-94
Millioners		1.12.09	1.9	5.466	1Kl- ,	5E-112	Jr. 115	193 (4)	6 05-1	681 - 1	2.06	8.1 (0)	6 90 0	5 E 0	1081,14	2 0	5 1 F O	5.40	neafine.	NA.	VA	NA.	positive.	MVV-06-53
VIII - 56-85	g	117.00	* 1	5 71: 5	, RF ,	71-112	1970 09	1.80	8 15-1	1.0 - 1	5 (40)	200 (6	5.290.0	6 80 0	post re	415 0	* 901-	6.55 0	Lealing	NΑ	NA	NA.	Longer	MWv ou ba
VIV 58 26 VIV 58 65	139	10/23/2005	.2.43	1 23E 1/2 2 37E 1/2	. 67E 52	. 981: 02	, tale 03 , tale 03	4.750,01 4.330,01	6.250.	6.290, 61	2 (of) (iii) 2 (of) (iii)	1.761: 00. 1.30.01	50.5k (c. 570k) (c.	5.580; 10. 0.420; 10.	positive positive	2 PG 00 2 PG 00	5 (6); (C. 5 (7); (C.	9.5 Hz 555 7.38E 555	pospine pospine	NA NA	VA VA	NA NA	posmic posmic	MW 68 26 MW-58-89
330 00 35	1	10 x, 20, 3	.2	2 20% 1/2	. 52h 52	. 6.6 (C	2 and 108	2.230.00	or official.	Stand	2.000	20 to 00	. and 10.	28: 0.	positive	- 15h 00	0.26	8 11, 50	pontac	VA.	VA VA	NA NA	positive	WW 60 35
VIII. 60 53	5.1	10/8/2005	.1.5	. FE 52	. FE 52	. 9.E 02	2354; 03	1230,01	1588.00	6120,01	2,006,00	2860.01	~ 88E 00.	" 53(; 10.	рингле	330,02	6.568, 55	745, 50	pantas	AV.	NA.	NA.	positive	MW/ c0 ba
VIV 40.72	5.1	10/8, 2005	.158	. 131: 1:2	. IBE 52	. 9.15.02	2 tal: 03	- 020, 02	3 895 0.	1830, 01	2 506 55	3 131: 00	5,850,00	\$50E 10.	positive	2.57E-00	7 (2): (A)	8 351, 100	postaz	VA.	VA.	NA .	positive	MVV-60-72
Villaboration VIV. st 40	5.1	10 8, 2005	0.55	1000 02	55E 52	5 F 102	2354: 03	. 161. 01	8 90E0.	9.500, 61	2 (0): 10:	3.34666	5 KSH 0	8 F 0	positive positive	375.00	6.580 m 6.276 m	5.650	nostine postac	NA NA	VA VA	NA NA	postine postine	MVV-80-125 MVV-80-174
1,11 11 , 11		1 100 00 2000			1	1 1 11 114	1 2 1 1 1 1 1 1 1	1 - 662 11	1 0 000.00	1 12/02/01	1 2 10 11, 110	1 1.40:400	1 -01,-101	2.145.1167	I Investigate	1 0.775	1	1 1447 001	I positive	1 444			I bearing	n vie Dale II

J. 17 000 18 388 (1884), 1864 (1807 000). Qualet Harles (1884), 1884 (Quajet Hermitel MN 858). Vasci de el

Page 1977 See By a 170 Noves

# TABLE I 2-09-46-QUARTER GROUNDWATER NATIVER VERSITES INDIAN CONSTRUCTOR VENSITES BECHNANA, N

												BUCHANA												
	_	1											ANALYSI:	S RFSULES										
Well ID	SAMPLE ID	SAMPLE COL	LECTION		1 RITE V	I (µCr/L)			<b>\1.90</b>	ipCrL)			C+137	(pC'a'L)			Cu-60	(μΓω1.)			No. 63	(pCrL)		Well 10
		Date	Lime	Result	Std Des	VIDE	11.5	Result	Std Des	SUBL	11	Result	5td Des	MIN	111	Result	Ntd Des	VIDC	111	Result	Nid Des	AUR	- 11	
V10-10-1-10	1	DO 6 20 6	1.9	11: 1	5:51· ·	6 F 105	1 1000	211 × 1	1.681-1	69 - 1	2.00	8:38:301	5.250-0	5.950.0	Long. c	2.4 (6.10)	53 5 0	65%	aret, co.	NA.	NA.	NA.	Long to 5	M-W-S3-178
MM-67-18	1	11 1 20 9	* 15	2.635	1.51- "	56.02	2 July 103	4.3 (4.0)	20-1	801 - 1	2.00	4.835.0	5 5 D 0	58 (6.0)	past re	-16st- 0	500-	6.68 0	positive.	VA.	VA	NA.	Long. Long.	WW-62-15
MW-653	1	11 120 9	* *	2 10 2	0.16 5	50.00	3 July	-3 H + 1	214.7	8.68 - 1	2.00	-5x 3 st - 11	10.00	D-10	post re	-1 006	51: 0	19-	Tarsal" free	NA.	NA.	NA.	Longa 5	MW 62 a7
110 67 53	5.00	11 2005	3.38	2816-12	16k ± 3	1.15.02	20010-03	3.501.01	6.381-9	1	2006-00	2.511.101	2 kel - 10	3.3% in	pasitive	6521101	3.751-17	3.511- **	188011.0	NA.	NA.	NA.	positive	MW-80-5s
MW-62-1	1	11 1 20 9	* 1	1.680	196.3	36.00	3 July 105	\$107,001	b febl- r	5 - 1	3.00	1.846	5.38(0)	6 salt 11	post re	41.5	5 35E 0	6.10	Tiesd" ne	NA.	NA.	NA.	Longe 5	WW-62-71
MW-67-92	1 -	11 2 50 9	1.45	1.43)- 1	56.3	26.00	2 15 03	10 07	N (++ )	8 6 - 1	2.00	6.5.44	5.25[6.00]	N# 16 0	positive.	1.98(-0.1	5.550.00	5.860	Jest, 16	NA	NΛ	NA.	Long a S	MW 62 92
730 (2.18)	5.1	11.22005	.3	5.74E-12	. 356.52	. 67E-02	2350 03	\$ 83E-C0	- 98E 3	(82) (3	2 00B-00	, 046 55	7 (21) (C.	8 304: 10.	рангле	120042	7.50E-55	8710, 50	pantaz	AV.	NA.	NA.	powrise	MW 52 135
VW +2 .82	5.1	11 .2 2007	.5.5	5.00(3.2)	. 27h 5/2	. 036: 02	23545-03	1.530, 01	5 (H: 0)	6.321, 61	2 001: 00	3 (w): (C)	Fishle (c.	807/45 007	posesse.	2.77E-00	while or	7.500 (0)	positive	NA.	VA	NA.	positive	MVV-82-182
3.00 (65-18)	1	1.5.2.00	. 4	216 2	151- 1	5 to 02	3 It 05	25,800,50	8.5 Ho (	5 . 1	2.00	69-1	5.396.00	S 80: 0	post re	\$10.000	500	\$100 11	positive.	NA.	NA.	NA.	Lost P.2	WW-62-15
MW-63-3 -	1 -	13.2.00	1.2	5 10 1	2015	6.26 (0.5	2 15 00	-4 4 - 1	1.66-1	681 - 1	2.00	-6.67 - 1	X 5 1: 0	9 9h 0	past re	8 4 4	> 6F	6.6 0	positive.	NA.	NA.	NA.	Longue S	MW 63 34
100,6350	* 1	13000	0.55	Apade 13	Sigh + 5	p. 6 (10)	20010-03	18.30, 71.3	5.3] (-0)	69E 23	Senderer	2 (2.0)	pig to or	1.5 do or	pairte	3 300 00	2 to 17	1,816.00	neuric	NA.	NA.	NA.	positir e	WW4 7-50
MW-63-95		13.2.00	0.55	5 Hr 2	~ sl *	6 E 02	2 15 03	1 - 201	les t	5 - 1	2.00	-1 Jet 0	5 × 9 × 0	S 10.0	past re	5 (n)(a)	5 P 0	5.761	JP491, 1-6	NΑ	NA.	NA.	Long. Long.	MW 63 95
7/37/+3 2	5.1	.1.3.2009	.1.7	1 445 52	. 62E 52	. %.E 02	2356 03	3.07(2.0)	8 311:0.	9.250, 01	2 505 55	130.01	9 , 5h (C)	989E 00	postale	1821, 10.	7 (14) C	9.72E 55	positive	NA.	NA.	NA.	positis a	MW 5a 112
VW +4.2.	5.1	.1 3 2000	.1.59	504E-02	. 646.52	. H.B. 02	2354: 03	5760,01	8 731: 0.	9.671, 64	2 (0): 10	5.331; 10.	5-88E 00	8 13h (c.	positive	2.078:00	9.351; 55	8,770, 00	pantaz	NA.	NA.	NA.	positive	MW 53 121
130, 02, 03	5.1	.1.3.2009	.3.0	5 22 E 1/2	, 63E 52	, 9.E 02	2350:03	- 30,00	8 281: 0.	9,380, 61	2 001: 00	5720.01	2.50[; 10.	\$ 330 rc.	ромпле	0.800, 000	1.58E 0.0	1.076.00	208177.0	NA.	VA	NA.	powrise	MW-53-163
378 ASS 1	1	13.7.60	455	1.89	P2F ,	6 F 02	2 15 00	4001 4 7	9"1- 1	991 - 1	2.00	441	6.660-0	X [c. 0]	post re	5.13(.00)	6 II:	8.1 0	positive.	VA.	VA	NA.	Longe 5	MVV-83-174
NRV-66-11	21	11.1 70.9	4.56	3 HF 2	28 p. 2	2. \$6.002	530.03	4.500,000	8 " 1-1	91 - 1	and a	2588 a 1	S 10:00	6.260.0	post sv	36.00	s 46.7	6.680 15	most sign	al 2014. 1	1.686-7	190-1	106730	MW/ cc 21
7177-66-36	2.00	11 7005	3 ×	1378 13	1   11   12	21.00.02	511-04	6.8716.11	75' 10	6700-21	2711	3.74(- **	p 54H 01	K3 I: 00	pakere	-837FeH	7 (7) (7	- 24F - 1	Testine	-3.9 1 (0)	776.0	7186.1	nextise	MW-s t-a5
VRV-6 -50	1	11 70.9	1.9	1400 5	2.186-2	65E-02	180-03	550	314 111	81 - 1	5 8bl-	4.705.0	8 1: 0	KKU-0	postine.	4 935 0	1 00	10 1	Losters	- 5 % 5[- 11	1.01	1.8 1	196739	WW 67 39
VW 67 113	5,0	11 2005	.13.	20,28,33	3.326.52	23/31: 02	1.541: 03	8 PC 01	5 (9E.0)	1851, 51	2 . 16 %	1955.01	5.874; (0.	97.Jt 00.	positive	1211.6.	7 901; 10.	7,670, 50	pantas	2.76.06	1716.50	1.9%, GI	pascar	MW 57 105
738.02.12	5.1	11 2005	.135	8.06.52	2.196.52	23/46/02	, 56E 03	1.6%, 01	6.78E 0.	8 180, 61	2 001: 00	20/0.01	58.1; (G)	world on	ромпле	1.52h (a)	6.5816.000	1,530, 50	pantae	2.76 (6)	1 865 5.	246, 6	pascas	MW-67-173
1.4.9.1.0	- 0	11 50 9	1.6	510 4	1,500-1	2 10 002	25 10 03	.130 . 1	Date:	86 - 1	2.04	xl-	1860 0	58900	LONG LG	219 Hunt	6 50 m	6.900	Send" ne	6 M 0	36.00	19.6	1695112	MW-87-219
1747-6-276	- 0	11 70 9	1.5	51: 5	8×0- '	65E-02	2.5 p. mg	135 401	8 9h-i	9.59 - 1	2.06	93(1-24)	82100	95900	positive.	- 15E-00	9.36	11 1	Lositive	1.44	1.56F	191 1	198799	MW-57-275
1.47-6-11.4	- 0	11 50.9	1.50	1.316 2	Pate ,	65E-02	16.103	3.9" . 1	Light- i	78 - 1	2.06	30 b 0	8 T- 0	85 b 0	Lant. or	21.15	× 1: 0	850	and co	23.16.0	5.86-11	1 10	1616.1.1.2	MW 57 325
77547-39	2.0	11 50.5	1 %	5.376 1.2	98E-12	150.00	10.03	25.55.04		93121	Single or	35621	5:30:00	1 St. 01	positive	2.50(00)	6:36:11	8.33, 10	positive	-58 F W	1 895	11	positive	MW-57-240
1785 1	91	1.1.3.00	> 56	1.406 - 1	5.036	× 10 105	250 IIS	N 16 - 201	8 1940	878 24	5.10(1)	5 (d. 20)	53.100	6 (6 0)	Last, in	- 551% I	699E0	691-	red c	W	VA.	NA.	Length 5	399-111
13.40	1,22	.1 % 2009	.3 .5	4.7316.332	. 286 52	, telt 02	, tale 03	*0.000, 1,2	5 995 0.	6.680, 61	2 501; 55	. 02h 55	5.800, 00.	977E 06	positive.	3 351: 01	9-25da 06	7331:00	positive	NA.	AV.	NA.	positive	J3 43
13.11	126	11 13 2009	16.35	3,760,10	8L 12	1336.52	1.281: 53	3.87E 0.	5 950, 00	9.630,01	206,00	6.8.0.01	5 331: 14.	5.76% (2)	positive	335 (0)	6.396.00	1.376,00	pantas	NA.	NA.	NA.	positive	1,3-71
1.5-1.	- 31	11.16.1 9	1153	8.31 *	521 2	1 36 5	1 10 3	s Miles	6.51 - 1	15 401	* 0 0	3.0.4-an	654)	6.20	positive.	- 116	5 95E-0	6.946	16971.6	NA.	VA	NA.	Loste 5	1.3-72
1 0788	i.	0.8.003	-	2,916 (4)	78.15.1	851-113	3 50 03	1746-4	. 885-111	+ 36 -01	3 48%+ 1	- 0 - 1	539-0	6 P.O.	post re	-196 0	* 911:	5 0	positive	0.00	1.00	131 1	126732	J1 088
X01.5	507	11.15-2009	11.0	6 28E 32	. 391, 32	. 67E 62	1.850: 03	3.546.00	6.570, 00	7,390,00	206,00	5 %(), 01	1.671: 5.	1.76%	[S89][4.7	2756 (0)	~ 25d; +G	This is	postave	NΛ	Av	NA.	positive	MH 5
2 Alexand 2		1.9 % 6.5	* 35	2" 4 p. m	P.F 5	: 40-10	positive	48127	4 (1)(0)	7.597.211	peserve	1111140	85 F W	1.791.00	pase se	1.951-00	9.815.00	1 *** 1	positive	2.500 11	1.783	1.681 11	positive	A1+002

- Note the second section of the contract of the

J. 17 CO. 18 306 (1884), 1864-41 NG 2006. Qualer 1 Lades ( CASE 1 Quajer 1 Terming J MA NAS.

Page 2 of 2 See Page - por Sings

## TABLE S HISTORIC GROENWATER AND VIC VERSAL IN INDIAN POINT ENERGY CENTER BYCHANAN, NY

Well ID	SAMPLE ID	SAMPLE ZONE CENTER depth it below	SAMPLE ZONE CENTER.	SAMPLE COLL	LC HON								NALVSIS RESUL	. FN							Wallib'
	""	top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC FL			Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC ld.)			NL63 (pCFL)		_
				Date	Loar	Result	Std Dry.	MDC	Result	Sfd. Dev.	ADC	Result	Std. Dev	ALDC	Result	Std Dry.	MDC	Result	Std Dec.	MDC	
178-4-50	100	59.1	5.1	1 91 1 16	9.50	23 (6.05)	3 35E HS	6.95	3 3 (1 m²	AV	VA.	NA.	NA.	A.V	1231-101	NA.	NA NA	ΑA	NA .	NA NA	MW-30-8
	503	69.3 69.3	6.1 6.1	6.23.25.6	10.50	3 921, 43	1.200:03	5100, 10 . 100, 10	8 , 41 0 .	8.2 % % 1 1.100, 00	1 50E 55	2.990, 00	1.00.01	H: 5.	3.541:00	5.53E-00	1.1%, 01	1 (2): (4) NA	. 27t: 1c.	1.3/C, O.	+
	105	60.7	6.5	1 50 500	D. 15	1067 13	8,1: 103	5.317.02	250.00	8 2 1 2 1	8 15 3 40	3.131.03	330 1	3106.11	1.505.00	2.286-07	2.67, 101	1.51-1	1.545.0	20[-0]	+
	2000	107.3	6.1	1 62557	1:05	8170.04	8.21/2.113	9340, 00	. 63.01	1.1%, 06	1 905 55	0.062, 00.	2400, 00	2 901: 555	1300.00	2076.00	2.802, 000	7 07E 00	1938 0.	2.20(: 01	
	307	107.3	6.1	6 2 25.67	16.2%	2.970, 43	8 _ 3 2 + 1/2	9.3 C. (C	2630,01	1,984	~ [5], 0]	3 130, 14	3.750, 00	1195 111	+ 880, 12	1085 00	39%, 00	NA.	NA.	AV	
	110	693 693	6.1	8.1 2007	9.55	8 210, 64	2 felt 03 8 felt 03	7 (KC), (C)	AV AV	AV.	VA VA	NA NA	VA VA	VA VA	VA VA	NA NA	NA NA	VA VA	NA NA	NA NA	
	::11	69.3	6.1	88.207	10.00	996. 11	2504:13	+ 320, 00	AV.	AV.	VA.	NA NA	VA VA	VA VA	VA VA	NA NA	NA AA	VA.	NA NA	NA NA	+
	1312	69.3	6.5	8 5040	1.06	2 331, 13	9.55E-53	+330, 00	VA	VA.	VA.	NA.	VA.	VA.	VA.	NA NA	NA NA	VA.	NA NA	NA NA	-
	:13	69.3	6.5	8 2, 5*	9.14	10% 65	3.2.E t/3	1050, 02	VA.	VΑ	VA.	NA.	VA.	VA.	VA	NA.	NA.	VΑ	NA.	NA.	-
	- 11	60.4	6.1	8.5 "	1.32	950 1	1991	115 112	AV.	ΛΛ	AV	M	AV.	NA.	VΛ	NA.	NA NA	- VV	NA.	NA.	
	18	60.4	6.5	9.91	1.0	9.50   1	1.51-3	0.75 0.7	- VA	ΑΛ	- AV	NA.	AV	AV.	- NA	NA.	NA .	AV.	NA.	NA.	
	16	60 1	6.5	2.1.2.08	1.18	18 3	55 1:45	195 0	15 (sa)	5 56 I 5 686 I	12 201	5 Ph. 0	3.6 0	1000	-5 (ii) 31	5.65E-11	\$ 56 mm	NA NA	NA NA	NA.	+
	18	69 4	6:	56.508	1.0	133 3	5 1: 115	506 07	3 5 (100)	5 (M) - 1	6 40	191 - 1	183 0	3.316	-5 0 -0	F 0	2 3 101	NA.	NA.	VA.	+-
	19	60 4	6 -	56"") #	1.0	46 "1	5 mg + 1G	506.00	1 900	3 275-771	5.59 40	-5 X"I	210.20	121. "	19 -1	2.24p. 172	\$305 (0)	A.A	NA.	N.A	-
	50	60.4	6.1	8 5 7 10	1.22	100 -	154 111	195 07	1 (84)	3 19 1	5.31.30	- 5 b-	1.15 0	1.881	1.116.0	50-0	1.65 (0)	AA .	N/A	NA.	
	-21	69.1	h 1	13.236	121	8 53.7 64	2 (3): 03	556, 02	312,701	5 (20 ) 4	1 201	189, 00	2 22.5 50	3 401:	NA.	NA.	AV.	NA.	NA.	VA.	_
	122	69.3 69.3	6.1	11.7.2548	1, 06	9350, 51	2 85h 103 2 5.h: 103	3.040, 00 . 980, 00	10/H; 0; 8/5/0 m2	5.53(; ; ;) 7.58(; ; ;)	5.737.01	1.13%, 00	3 (6), (0)	3 (6); 10. 2 (6); 10.	1.070.00 1.000.00	2 % lb (C) 2 % lb (C)	324,00	NA NA	VA VA	VA.	+
	10.1	00.3	6.5	121 200	10.00	100.33	3 - 41: 113	1020, 00	.30.01	1 285:14	90,500	, PG, 96	1110,00	3.7 Hz 5.5	2.780, 0,	3.06.00	160,00	NA NA	VA.	VA.	_
	123	69.3	6.5	+1.200	12.02	8 200, 64	3.2.E (3	3,770, 00	3 , 26 0.	5 - 31: 14	~ 321, 01	2.191; 00.	980(, 0)	5 50 to 144	8.2%,04	9 (7); OC	7 (2), (0)	NA.	VA.	NA.	
	126	(4)	6.5	8.6.2009	12.1%	161, 13	577E-03	2594, 02	6754:02	9.08.01	7.1,000	216(), 101	8 321, 00	7 30() 111	2578.00	5.445.00	970, 00	NA.	VA.	AV	
	- '8	60 1	6.5	0 110 0	D 15	901 1	2.6 de 115	76 07	33 [5 art]	5.556 T	815.00	- 3 5 Fe	2.52 0	5.10	[158]c.00	5 35 11	6.5.00	AA AA	AV	AV.	
VW 35.81	100,	83.8	81	8.22.206	3.3	. 250, 00	2 (30, 43	1 -11: 13	1 % 20	9825.0	1135,00	1 881; 10.	, 45E 0.	.00.01	2,520, 16	1000, 54	6 5 III	NA AA	VA VA	AV.	N/V-30-
4.01 50 51	900	83.8	B.	1, 2/200	1135	1.01), 3.1	50E 18	. 184, 103	2.65.01	1 85E 51	8 %, 01	290, 10	1.680, 61	\$ 00t 55	3000,00	376db 06	186, 00	1.00, 00	1.76.0.	1.30(: 0)	10000
	0.0	83.8	и.		9.14	1330, 13	7 Std: +0	\$300,00	1864; 0.	1.500, 00.	1 905 55	. 181, 16	2.610, 50	2.906.55	0.00 (0.00	25.600	3 (6), 00	NA.	AV	VA.	
	501	83.8	я,	6. 2.25.7	16.1+	7.790, 10	5.0% (0.00)	4 121, 102	. 155.01	4.338.61	94.5.01	105, 00	2.290, 00	2 (11) (4)	4930,00	2.386 00	2.5%, 00	3.57E 18	1736.00	2336.01	
	3/6	93.9	и.	1 8 25.0.7	16.25	1800, 13	1.258:02	1000,00	AV	AV	VA.	NA.	VA	4.V	- VA	NA.	NA .	NA AA	NA.	NA NA	—
	20%	83.8 83.8	К.	10.23.2007	13.00	5 (C), 13 1271, 13	1.095.02	2 130, 02	1.50(c)). \$55(c)	3 (53) (1) 5 (53) (1)	3 (80, 01 3 500, 01	2831: 00	3.381, 00	3 380 10.	2336.00	2.5-Ja (G. 3.7-2)- (G.	3.5%, 00	NA NA	VA VA	VA VA	+
	1164	83.8		2.12.08	1.15	1315 13	26 5 102	351.112	-108, 401	- 556-7.1	5 (5) 40	4 00 00	2.551.10	3-31	-1371-01	157F W	2.797 (0)	A.A	VA.	NV.	<del>                                     </del>
	16)	545	-×	56.508	In I	118 3	, x 4- 11,	5.5 0.5	4.39(4)	5 X91+- T	5.5 401	133 - 1	2.3 0	3.00	3 F 0	2596.0	566 00	AA.	VA.	AV.	
	10	515	-×	5610	121	49	2 445 112	505 07	15000	1,396-1	131 (0)	-8 g Js	*16 0	15.15	5 Sp. 00	13 (-11	19 00	NA.	AV	ΑV	
	70	515	.×	3 4 7 100	15.1	141 4	2.36.02	5.35 (0.7)	-161 art	16 16 1	56 and 906 and	- 8 1-	1.11 0	1 800	-101-0 NA	, Av	*66- 00	NA NA	Ay	AV.	+
	13	818	-8	1 1 8	11.5	2 2 3	3 31 11	46 02	1 1900	5.55.1	6 40	661 - 1	163 0	2.3.1	3 30 0	2.335.00	623 101	AA AA	AV.	AV.	+
	111	838	-8	, 10	11.	169 3	5.385.02	95 111	0.585-012	59 16 1	19 40	8910	131 0	3 %	48 18 302	5 500-11	58 101	NA.	NA.	NA.	_
	18	838	-×	15.5.0	113	531 3	4 8E 02	34 05	- 19 -41	3 16 1	5.79 401	15 0	621 0	1 (6)	58 - 101	5 7-11	18 00	AA .	NA.	AV.	
	116	93.9	К.	+1.200	13.23	5 8 30 1 13	5 (2E (2	3.7%, 02	133(0)	1,968	8 221, 01	3.9 ()	1.015.54	9.75E-55	8 TVL/42	octob oc	680, 00	NA NA	VA VA	VΑ	
	18	93.9 83.8	. K	8.6.200	12.38	6.5.3	5 KSE 112	33 02	60.8E-02	286.1	\$150,01 89,00	, 88h (C.	900 0	5 16	5.55[: 10]	5 SH 0	582 00	AA AA	VA.	AV.	+
	19	838	-×	13.0	111	6. 1	5 161: 113	9 01	88000	150-1	8 12 201	* 6 - 1	5.97 0	5 III	-3 Jr 0	3 995 11	196 101	AA AA	NA.	NA.	+
1117-4-20	100	14.4	'68	6	1.38	2.000-02	1.1.	1.00	000 0	595 0	1 00	NA.	NA.	NA.	130 0	56 F H	\$11 .00	1.376.3	1.656-02	1.800 011	MW 31
	102	18-8	% ×	1.87	9.1	1.50 3	5 F 5	53 07	3 [60]	16.	1 4 4	VV	NA.	NA.	21po - o	8 01-	\$5 E 0	NA.	NA.	AV.	
	- 03	18 8 18 8	25.8	8220	15.75	1.18 3	5 536 05 2 E 06	5.15, 00	23.00	8 30 of	52 au	1 835 T	1.15 o	1 500 1 5111:	% . . 8	5 p. m.	1.79 (0)	II III II	T I- II- III	1 *91- 01 VA	-
	305	18.8	2-8	8 - 271	13.15	6980, 13	3.27E (C	. 5%, 00	226.01	1.23(:1.1	90,5,01	1.70%, 000	3.010, 50	3.216.55	0.000 00	1764: 10	175, 00	NA NA	VA.	VA.	+-
	306	8.8	2-18	15/21/2007	15.5%	8770.43	5.50E-10	1000,00	5,4002	1.296.01	5340,01	9 Tole 5.	3.9 E, 30	3.571; 1.1.	1.351; 00	3.2.1: 06	3.525, 000	NA.	VA.	NA.	<del>                                     </del>
	507	18.8	29.8	. 102008	16.3.	3.970, 10	748.00	. 753, 00	91/07/00	0.895.01	8.900.01	115,00	1710, 50	\$ 0.7 p. 000	976,0,	13,600	[65], 101	NA.	VΑ	AV	
	509	18.8	298	+6208	15115	300, 51	33); ((3	1.650, 100	28300.	3.35(1.1)	5 720, 01	. 1.1: (6.	1930, 50	3 (7); (4)	1.726.06	25.15.06	3.825, 00	NA.	VA.	VA.	$\perp$
	510 511	15 5 15 5	2-8	8 7 2008	12 13	590, 30 136, 31	33E 10 8 5 E 10	3.530, no	2.35(c)).	2 9715 04 4 8045 04	3 [3], 0] 8 061, 0]	271:00	3.630, 50	2 23% No.	T (8), (4) NA	, (0); (6) VA	2,540, 000 NA	NA NA	VA VA	AA AA	+
	312	18.8	218	1:.30.208	1. 35	6 180, 142	2256 (2	. 7.1. 00	7 - 41 02	- 868 G	, 931, 01	. 3%, 00	6271, 50	251: 11:	90%, 0,	9 Cd: 00	7-NS, 101	NA NA	VA.	AV.	+
	13	19.9	% K	1 18 700	1.15		SE 115	65 05	1 100	55 15 1	5.9 ard	2 0	118 0	5 36	4 4 .	1991-11	585 00	NA.	NA.	AV.	
	- 11	18-8	% K	, 6 , 110	1.05	111 1	851-115	95 117	1 80-01	5 10 1	5.5 40]	- 6 P-	10 11	5 551-	-161 -0	, 821- 11	3   2   101	AA .	NA.	NA.	
	18	18-8	% ×	1 1 1 0	11 35	181 1	CN-109	55 117	1850a) 8 (9a)	5590-1	59 40	-5 K II- - 85II-	648 0 980 0	5 %	1.5 (0.00)	5 % h 11	16 00	NA NA	VA VA	AV.	_
	16	18 8 18 8	74.8	5 5 0	1.35	041 4	76 to 112	3 11	1 (1 (1))	5.36.1	5.75 401	- 801-	5.48 D	5 541-	1 H: 00	5.53E-0	166 00	NA NA	VA.	4//	+
	18	16.6	16 ×	81.506	11.33	1,201-114	180s Z	5 alcinos	2.585- 1	1.296-0	1 (81-0)	, 91-10	16E-19	1751 1001	-5895-1	2.556. 0	58050	NA NA	NA.	NA.	<b>†</b>
	:19	18.8	2+8	5 1200	1.13	311.51	5.335.10	. 740, 10	32,0,00	7.296.01	5,350,01	19%, 00	5,310, 00	5.511; 10.	3 231: (0)	\$7.15.0G	6.121, 000	NA.	VA.	NA.	
	20	18.8	7:×	1 22 206	1, 4	1381 1	×635 02	63' 11"	55 No.	×170-1	56" ad	1.87.1	61" "	5 × II+	41700 att	5 51-11	00, 181	N.A	N/	N/A	
1.47-4-94	107	65.5	1.4	1.50.6	2 m	589 H	1 H 3	5.5 0.5	5 9 0 0	180.0	1.06	1.996 5	\$5 F III	1/90 ti	5.80(-0)	191 0	4.5 (0)	NA NA	NV iv	AV 1 Auto 11.	MW/ 31
	105	611	'',	6.11	1111	500 3	851-02	1.86 0.1	1 200	6 sels 1	6 8 20	-5 B-	1.02 0	1.00	48 8 20	91-0	2.5 (0)	1.7	90H-	-1 0	+
	- 01	64.4	٠,	8220	1.15	106 1	111111	223 112	- 1 - 40	836.1	9 29 40		3.56 11	1.80	310 10	11   0	175 00	NA.	VA.	VA.	<b>†</b>
	115	64.4	1,	9 "	13.55	3	5 - 115	5.5 10.5	. 3 20	3 5 No. 1	6.15 401	-1 (0)-	3.81 0	5 80 41-	48.61.40	1971-11	8 (5 10)	NA.	NA.	AV.	
	116	633	,,	1 21 200	15.86	3.49	\$10 ms	500 02	- (55 44)	1.58[6]	6.35 (0)	0.0	53] 11	3.116	1.11/-00	3.5 [6.00]	11 00	NA.	VΛ	NA.	1
	10.00	63.3	11	5 ° 8	1.0	121 1	55E-103	8 07	-688 at	5 (30-1	[5 40]	25 SQL	201 0	3.366.55	2018 31	1 (0) (1	137 00	NA NA	VA VA	AV.	+
	510	63.3	11	67 200 87 200	16.16	1.70, 51	1.75E (0	\$100, 100 . 900, 100	2120.01	2 9 de 64 2 9 de 64	5 (17), 01 3 (6), 01	1 15), 00 , 80h; 5.	1 281, 50	2.66.55	3.737 (c)	23.6 (6	2 15, 00	NA NA	VA VA	AV AV	+-
	:311	43.3	.23	8 4: 2:3	12.22	2 211, 141	57E 103	\$ PG, 02	5340.00	138614	5.750,00	3.766.61	2,351, 50	\$ 5.0E 555	NA.	VA.	4.V	NA.	VA.	VA.	<b>T</b>
	1312	73.3	.23	1:.30.208	12.1%	2,300, 54	18h (4	. 730, 90	2.281; 0.	233633	2.521, 01	2.2.1, 00	6481, 50	1 371: 111	. 47E-00	1.29E 96	1.11(), (0)	NA.	NA.	NA.	
	14	64.4		1.18 346	1.58	2.55	8 15 115	\$4.00	4.95(-0)	3.16.1	8 45 and	1.1.1.1	5 (49 ) (1	6.115	25 [8:20]	6 5 SE 0	69 101	NA.	NA.	AV.	

Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER,	SAMPLE COLL	LCHON							٧	NALYSIS RESUL	.rs							Well
isen in	ID	depth it below top of cosing	elevation It mst <sup>2</sup>				TRITIUM ( pC lel.			Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC i4.)			N 63 (pC H.)		1 ""
				Date	1 mar	Result	Std Dry.	MDC	Result	Std. Dev.	ADC	Result	Std. Dev	ALDC	Result	Std Dry.	MDC	Result	Std Dec.	MDC	
11/1-1-63	013	63.3	11.5	16 109	158	26 00	\$ 40	13.6 1	6.1464 2.546-0	6.11.40	5.8714	3.95.0	3.5% (0	1.050-101	2.335-101	3.871: 10.	1.750,00	NA NA	VA VA	VA VA	N/V
	116	63.3	.23	42000	12.34	3 0 fb, 64 3 1/0, 64	.58: 13 5 3 E 12	. 180, 00	3.45(1.0)	5.580: GI	900000	. 79E 00	668), 50 10%, 51	7.26.55	2.29(10)	9 8 E 10.	7,350, 101	NA NA	VA VA	AV.	-
	-11"	63.3	* 3	- 1 - 1	15.5	1 181 11	8.28E-102	33.00	19900	1.4367.1	51 '20	3.8571	3 907 10	- 3°1- · ·	- 50E-10	3 881- 17	875 00	NA.	- VV	AV.	_
	18	64.4	1,5	91,700	10.5	1.01	5 95 02	218 02	15 (9)	3.55fs T	115 201	-1 35 (6)	6.6 0	5 P	50° 1	5 100	8 3 100	NA.	AV.	ΛV	
	10	633	2.5	9 5 5 0	12.15	200 1	5.58(4.00)	6 01	8 Jun 1	8 No.1	9.75 art	1.96 00	1 S 0	5.50	2.3 p. m.	5.8 (0.0)	6 9 101	NA NA	NV NV	NA NA	-
11-1-6	100	K: K	.0	1 50.5	13.7	165 05	5.85[- 117	F 00:	996	130 0	16 10	1.5%	81 F II	170 0	1 0 501	210 0	25 (6.0)	150	5.94	1 00 0.	MW
11-1-4	117	818	-9 1	8.	9.5	100	5 F 115	5.5 0.5	25 9 AN	189 0	1 44	-190 (0)	8 0 0	01:	-6101 at	8 F 0	10 01	8 15 101	2.10	* 49 11	16.93
	118	818	-9 1	6 11	1305	31 1	6.36-112	65 01	-485 44	55%-1	93 40	3 (94 - 1	* 6 11	\$H+	28 (1.40)	5-SH-11	185 (0)	NA.	NA.	VV	
	- 01	818	-9.3	8730	11.58	. 90 4	- 11°	53 07	2 19 201	6 a 16 T	93 20	-5 Fe 5	4 *9 n	1.701-	- 3 F 0	3.351-11	4.4 (0)	NA.	- AV	AV.	
	005 006	818	12	10.21300	13.25 15.65	1321, 13 5 511, 13	\$ 326 FG 8 35 FG	3.980, 00	6 895 O. 2 536 O.	1.085.01	1.900,01	Totale to.	3.0 (0.00)	3.26E 10.	4078-00 1790-01	2.75E-10.	320,00	NA NA	VA VA	AV AV	$\vdash$
	307	818	1.5	10.21348	1, 24	1310.43	2 8.1: 10	. 840, 00	6771:00	7 971:01	7.750.01	2.681; (6)	10%, 30	1831:	1.301; 00	3 804: 00	1621, 00	NA NA	VA.	VA.	+
	16)	818	-9.5	56108	15.79	5.05 4	6 + F 10°	210 11	15390	3 In I	5.66 -01	-× 1	2.50 0	1.75%	1.911-00	1.15E-0	158 00	NA.	NA.	VV.	
	10	818	-9 1	8 100	1.15	1.60	X31-113	95 07	1 100	28 16 1	53 20]	46 S. H-	122 0	5 H+	65 - 1	5 F 11	*18 (0)	AA .	VV.	AV.	
	- 11	818	-9.1	85 5	1208	831 3	E 115	555 05	13950	18 16 1	8.1 201	-55 Ju	186 0	1 1-	NA.	NA.	AV	NA.	NA.	NA.	_
	-13	818	49.5	1, 18 20 8	1206	1 H	2.536.00	6 01	1.800	335 I	875.00	215, 0.	61 0	1 4b	28000	5 98E H	215,00	AA AA	VA VA	NA NA	+
	311	818	1.2	26200	1. 22	7370, 63	9.83E-10	2020.00	38500	5.58(; ; ; )	9 190 01	. 226 (6)	3.500, 50	1001:00	1 (9); (0)	3.5"  : 16.	1230, 00	NA NA	VA.	VA.	_
	015	818	- 12	1.1200	1, 1,	188], 51	8.596.00	. 500, 00	53500.	15,831	*60,01	0.085.	320,00	3 001; 55.	1.16.00	3.50E-00	115, 00	NA.	AV	AA.	
	516	818	5.2	3.25.25.69	12.5%	8.851, 13	55E 18	3.750, 02	1.83(0)	85,553	5,350,00	8.5 ()	100, 61	9 (8 h 5 h	9.970,61	5.5°E 16.	73.0, 00	NA.	VA.	AV.	$\overline{}$
	:17	818	52	12, 249	12.13	3 521, 13	9 days 9 days	2 250, 02 2 120, 02	2.280, 01 1.26 0.	5 % [1 13] % , \$1:13]	8 081, 01 9 8,1, 01	2.5 E. 00 8 38E S.	5 (E, 5) 1 (C, 5)	1.221: 11.	2.39E 00 5.3(C, 03	37.16 (G	175), 00 686), 00	NA NA	AV AV	AV AV	-
	119	818	- 3	1 1249	12.05	51 F. 13	3.085.02	. 590, 90	1.00.00	5 (SE 64	817.01	8 (80 to )	1985, 30	5 (21) 144	2.910.00	5 31:00	5 22, 00	NA NA	VA.	VA.	+
	120	818	1-2	19,22,300	12.51	1500, 33	3 (a) (C	. 671, 02	5.5%; 0.	997834	1 180, 01	3.276.01	6720, 00	9 891; titl	1.25.00	9 lb 06.	2005, 00	NA.	VA.	VA.	-
-12-4	100	58.8	18.5	1.9.50	6.40	6 19	80 1	5.50-2	6.90-	3 pc 0	16 10	-8 60 - T	90 0	130 00	190-01	1.76 11	15 F 0	A.A	NA.	AV.	M
	115	18.8	× 1	5 % 1	13.55	* 10 1	3 F 105	9 0'	- 65 41	59 lo 1	9 201	4 1 00	3.81 0	1 9/1-	1.19 0	5 × 1- 11	4.43 (0)	AA AA	NA.	VA.	╄
	- 01	19.9 19.9	× 5	1.76.700	130	111 1	5 F 02	95 01	2. 24 3.29cm	5.586.1	56 JH	18 0 - 5 de	240 0	1 5 1:	-166 -0 2.186 mm	3.51-11	\$465 HH   1186 HH	AA AA	AV.	AV.	+
	- 02	18.8	N 1	8.8	15.5	18 1	9 1-10	86 01	16 150	6.986-1	5 40	9.8 - 1	125 0	1.01	1.50)- 11	3 8 1: 11	165 00	NA.	VA.	VA.	+
	115	*8.5	N s	5 5 7 106	1135	115 3	3 p. 103	85.05	5 (60)	52.16.1	9 40	- 56-	189 0	5 11-	1.286.00	2   1-11	3 101	NA.	'VA	AV.	1
	- 01	18.8	× 5	90,06	PT	195 3	28 F 02	216 11,	233 24	9500 I	6 40	4 27 000	191 0	1.801	- 10 at	2.536.00	30 101	NA.	AV.	NΛ	
	116	49 p	× 3	7.116	13.73	141 3	1935 H2	523 07	17900	38 (6.1	9.9 1.01	186' - 1	195 0	3.331-	- xt- n	' .sj. ::	NA.	AA AA	AV	AV.	+
	10	19.9	N 5	1 1 700	15.59	113	2 1-102	3 112	15400	5 56 I	15 401	-55 Pr	51 0	911-	- 5% 0	5 50 0	6.66 101	NA.	VA.	VA.	+
	16	18.5	N 1	11,100	To 15	1.8 1	5 - 115	96 07	- 11 - 21	5 86 1	66 -01	1.1 - 1	3 8 1 11	5.3114	2.000.00	5 5 (F 1)	133 (0)	NA.	NA.	AV.	1
	16)	18.8	× 1	27.7.0	14.85	613 1	5  - 115	5.73 117	[25]car	5 No.1	5 5 401	-3.7[ 000	188 0	5 ** -	28 8 205	5 % (F 10	11 00	NA.	NA.	NΛ	
	10	18.8	× 1	847.00	14.59	669 4	36 F H2	5 117	4.26(ca) 1.8.1(a)2	5 sto 1 5 s to 1	5.55 401	1.51 - 1	96' 0	5 HF	- 66 -0	5.636.0	613 00	AA AA	NA AV	NA NA	$\vdash$
	11	19.9	× 1	X 5 * 10)	11.73	186 1	3.636-00	216 02	1 8600	5 5 Fo T	8 30	15 - 1	161 0	5.96	3.5 - 1 2.25b - 0	58 1:0	5 15 100	AA AA	VA.	AV.	+
	:13	58.8	.83	5 5000	11:33	5 921, 13	3 (4) (6)	. 550, 100	1 (2), (4)	0.758:31	5 (02), (0)	350, 10,	1706, 50	5 101: 111	115.00	5.56.06	5.671, 000	NA NA	VA.	VA.	+
	:11	58.8	.83	15, 22, 2006	13.3"	5.610, 03	3.33(: 10	. 640, 102	3 (2), (0)	9-18E-13	5 800, 01	551:01	\$360, 100	9 (SE 12)	30.86.00	7 . RH: 10.	700,00	NA.	VA.	NA.	
12.45	100,	K 5 3	85.3	1.9200	5 [0	. 121, 03	8 100, 12	5.306.02	3.5000	, 175 10	165.00	1.571; 10.	2 821; 16.	3100, 00	9305.01	12(6, 50)	1804; 00.	NA.	VA.	VA	N
	900	85.3 85.3	853 853	9 28 2007 8 3 7007	15.05	5 120, 43 5 700, 43	3.77E-02	2005.00	1150.01 2.150.00	5.050E	9.75), 01 5.75), 01	3.286.01	2 810, 60	3 (3): 10	3050.00	3 (56) 00 2 580: 00	3 2.0, 00	NA NA	VA VA	VA AV	+
	501	85.3	853	15.26.200	1 12	1.76 51	1756 FE	277.00	100 of	5.276.04	9.250, 01	3 2811 of 8 851 of	2.973.40	3 (5) (10)	1851.02	3.238.06	3.637, 101	NA NA	VA.	VA.	+
	0.6	85.3	84.1	8 2048	11.50	10% 61	9.56E-10	. 831, 02	3.03(1.0)	4.386.13	1,350,00	3.576.61	260, 50	2 (71) (4)	5.3%, 0.	. STE 96	2135, 000	NA.	VA.	VA.	T
	16)	94 k	85.3	44216	13.1	8 36' 3	2.646.02	8 . 02	49.65° 44°	3896-1	* 59° and	961 0	2161 0	3 >61:	3.01, 10	2.56.0	5 20. (8)	NA.	AV.	AV.	
	16	9 × 4	Kh 5 Kh 5	59.108	13.35	111 1	8 7 10 107	95.00 02	1 5000	55 to 1	12 au	89 11	201 0	1080	28   20	, the m	8 (5 (0)	AA AA	NA NA	NA NA	+
	16	85.4	X1.1	9.7.10	15.85	18 4 848 4	5.5 1. 11.	555 05	1 1 1 (4)	5 556 T	60 40	43 00	2.06 0	100	NA.	VA.	NV.	NA NA	AV.	NA.	+
	10	85.4	×11	1 1 1 1 1 1 1 1	11.8	861 4	5.551-111	5 05	1 30-01	1.586 I	568 40	49 11	5.8 0	5.5%	3 80 (0)	5.895.0	C 101	NA.	NA.	- VA	+
	:11	85.3	gi l	2.12509	15.15	65 E. 13	~ 38E TC	. 960, 102	5.29(0)	7.796.61	8.501, 01	1881.01	2,851, 100	3.316.55.	2.2% 06	3.254; 00	115), 00	NA.	NA.	AV	$\Box$
	1/12 1/13	85.3 85.3	K11	12" 25.59	15.31	8.071, 13	.7h 16	13.1.02	1.2.1:0.	5.33(1.1)	9 PL 01	2070, 00	6110, 50 1300, 51	0.07(c.00) 8 (45) (0.00)	1 (9); (0)	1 0.8h (C. 8 75h (C.	1982, 001	NA NA	VA VA	VA.	+
	11	85.4	K1.1	8.3.3.00	151	916 3	5.0F-103 5.4-15-02	8 07	8 [60]	9 (7 (4 (d)	7 687, 01 12 - 01	1 1 1 2 0	197 0	5-201-	8 98", D	5 80 0	613 00	AA AA	VA.	AV.	1
	18	85.4	X1.5	X 5	131	8.08 4	1.596.005	211 02	1285-02	5 16 1	9.15.40	8 5 - 1	5.03 0	5 (90)	44 F 0	5.836.0	5.45 (0)	NA.	NA.	NA.	+
	16	ps 4	X'1.5	9.51.0	1.06	0.3	1 E 02	8 02	1 800	6 sto 1	16 -01	1.795.0	184 0	5.960	11.55E 0	5540	5115 1111	NA.	VA.	AV.	
	1	pr- 4	X1.1	1 22 500	13.53	\$0.0	3 8 31- 115	66 0.	1 100	3.5 [6.1]	5 [5 20]	~8 H	111 1	230 0	25 50 0	55 F 0	6.8 (11)	AA AA	VA.	VA.	1
37-151	101	14.5	-05	1 0 '0	5 Js	15 05	8 to 1	School	a relian	S Figure	5.8450	-600 m	5 SE 00 5 035 00	1.00 00	\$ 0[40° \$ 88[40]	Side of	1.90.00	AA AA	AA AA	NA NA	y
	118	918	-55	8.2.	1.6	1.0	1.00	8 0,	169(4)	3 Sto. 1	K 5 41	-8 Sh-	186 0	1 884	- Sh H	5 SH 11	3.12 (0)	NA NA	NA.	NA.	+
	501	, 3118	53.7	1026200	D. L.	371,00	234: (2	2 (2., (2	23780.	0.035.01	*100,70	. 8.E.S.	3 18., 50	3 8CH: 55	2,550,00	3 (26.06)	3975, 101	NA.	VA.	VA.	t
	505	, 918	53.1	. 8208	1, 23	500, 32	2376.92	. 750, 00	5.460.	1.798.61	8,521, 01	8 (7):01	21%, 50	2.211: 55	8.101,02	, 18th 00	2.180, 000	NA.	AV.	AV.	$\blacksquare$
32 1 19	(3.6)	, 31g	53.7	5.5.2008 .0.25.2007	12.35	2.921, 03	3dt 02	1.830, 00 1.906, 62	2850.01	3.58E 01 Decl. iii	7.75(, 0)	1.210, 00 950, 01	2.280, 60 3.00 m.	3.551; 10.	3.260, m. 1.950, m.	2.27E (G) 3.56C, (a)	3760), 101 1700; 121	NA NA	VA VA	AV AV	M
A. 139	1005	115.3	72.2	. 8 25.8	1.18	2.921, 03	29E, (2 294E) (2	1.50E-02	2.186.00 36.46.00	1890.00 8.25h:01	5.530, 01	290.00	3 (5h 06 12%, 50	3.510, 000	8 TE. 0.	2.82h (G	2.945, 00	NA NA	AV AV	AV AV	1 3
	2/6	. 20 4	12.1	5.5.2016	10.51	8 830, 42	3.1: (2	. 821, 00	7 Vil. 0.	5 0.5E 0.F	1990.01	2.9%, 101	2.670, 30	3.711; 55.	25.11:00	2 , 21: 14:	1121, 00	NA NA	VA.	VA.	+
	507	. 29 3	122	7 3, 2008	1.15	5,121, 42	3.1: (0	. 90, 00	1.381: 02	3.00(0)	9800,01	. 160, 16.	1.650, 00	2.871: 141	1.01:00	. 54: 00	28.1, 00	NA.	VA.	VA.	t
	1166	51.3		1071708	10.78	2.1131 112	3.15.103	24, 112	1650.0	0.42611	9.957, 01	800 00	6 255 700	and The sec	1.285-101	\$ 56de 18	685, 101	N.A.	VA.	'VA	
	16)	10 s		11100	1112	165	80.00	1 02	Indian.	6.56-1	\$1 and	531 - 1	100 0	1 101	347 - 1	16 1- 0	4 % (0)	NA.	VA.	VA.	1
	510 511	. 59 3	72.2	1.27.2539 +2.2549	13.3.	3 010, 40 0 0 0, 40	79E 02	. 870, 00 . 420, 00	70.000 2800.01	6.085.01	5 250, 01 7 980, 01	2.680, 00	1000, 00	2 8 H; 10.	1830, 02	2.345.00	2.5%, 00	NA NA	VA VA	AV AV	+
	917	20.3	-4-	83.200	12.13	3.000 52	246.00	50,00	9 (2)(1)2	9794534	285,01	2.867 (6)	6.635 50	7 701 12	9.16.0	8 35 16	8 (5., 00)	NA NA	VA VA	AV.	+

To 8 8 963 1 869 - 866-9 NG 3 003 - Quarter 3 Lidles Table Signatur 3 Formatical VIVI costs Mana Lither

See Page 2, for Note)

	1									BUCHANA											
	SAMPLE	SAMPLE ZONE CENTER	SAMPLEZONE	SAMPLE COLL	LCHON							•	NALVSIS RESUL	FS							l .
Well ID	ID	depth if below	CENTER, elevation It msl <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC i-L)			Ni 63 (pCi/L)		WHI ID
		top of casing'		Date	Loar	Result	Std Drs.	ADC	Result	Std. Dev.	AIDC	Result	Sid. Dev	MDC	Result	Std Des.	MDC	Result	Sid Dev.	ADC	1
	14	19.5	. * *	× 5 . 0	1.9	18 1	2.56.02	215 02	- 3 - 41	5.56-1	68 -01	4 18 00	5 66 0	6.36	4 40	1800 0	8.65 (0)	NA NA	AV	AV	
7117-3 21 30	1015	1103		1022 200	15.3%	93 112	1 lb 1 50h (C	1.506.00	26 (card)	10.10.0	95% 53%,01	7.75°, 101	9 (0), 50	5.65 mm	5 880, 00	873: IG	8 82, 00	NA NA	AV AV	AV AV	MVV-32-1
MW-32-165	000	63	-850	1.9500	6.60	Shire	870	5 Tup. 2	N/A	NA.	VA	NA.	VA.	VA.	VA.	NA NA	AA .	VA.	NA.	NA.	MVV 32 1
	117	15.5	\$61.9	6.81	1116	×81 .	2. 3[- 112	9 01	+ 85 and	150 - I	9 and	851 - 1	188 0	1916	-8 16 -0	1.35(0)	*6 101	NA.	NA.	'AA	1
	113	153	\$6.9	8 5 1	1.35	101 .	2. 31-112	, UK 11,	25 08 201	5 % To 1	5.85, 401	4.15 00	3 65 11	1 5 P	159-00	5-31-11	10 (0)	NA.	NA.	ΑV	
/IV-37-1-3	00	1.18	-05 -05	9 To 8	6.55	589 04	18 1	82.07	×61	8 8 30	5115	5.02 201	5 F IC	1.81-00	-99 15-1	1.01-11	3.76	AA AA	VV.	VA.	MW 52
	115	1.8	- Sh	2.5.106	1.05	1 60 1	1   p. 102 526   102	81 01	1 850	6 No. 1	64 -01	135.1	118 0	1610	46 I I + 0 5 I + 1	2.200.00	49 (8)	NA AA	AV.	VA.	+
	- 01	1.8	,Gh	5 ' 8	11.52	116 1	581-112	475 115	68 150	15% 1	1 40	411 00	1.58 0	2.5 (6)	516 -	65E-0	105 (0)	NA.	VA.	NA.	-
	105	1.8	.95	9.5506	1.3	9 ' '	3 71-115	5 8 07	Likhlan	1836 1	8 [ 20]	400,00	'b 0	5 1011	NA.	W	N/A	NA.	VV	NA.	
	505	.72.8	95.7	1021208	16.25	1 (80, 13	2 (71), (2	. 740, 00	1550.0.	3 (01) (4)	1390,01	8 - 31: 1.1	5.670, 100	9 9 11: 54:	2.30(5.00)	- 3-lt 16.	7.75, 00	NA.	VA.	VΑ	_
	500	.72.8	95.	2 12000	13.32	786 12	186 (C 1776 (C	170,00	2.87(10)	1.29E34 1.38E34	5.181.01	3 200, 00	3.650, 00	3.31E-55.	2.86(00)	3 (7); (6) (77); (6)	1.150, 00 5.550, 00	NA NA	VA VA	VA.	+
	161	1.0	.95	5 1 1 100	1.58	1 3	2.38.02	68 0	1.550	5 85 1	5.66 40	4 33 101	9 % 0	5 10	1 3 E 0	5 1 1 11	6.25 (0)	NA.	VA.	NA.	_
	10	1.6	.05	63,110	1,3	108 '	- 11°	85 117	-16 ar	5 KSIG 1	514.00	52 0	531 0	5.761	- 1.00	1990	5.25 (0)	NA.	NA.	AV.	1
	- 11	1.8	.4h	85.0	1.3	* q *	3 St. 113	113 02	-106 art	5 56 1	8 40	8 0	196 0	5345	1580-00	55% 0	85 (0)	NA.	NA.	ΑV	
	-1.5	1.8	.6h	3 5 5 0 10 200 c	13.60	1.0	65E-02 68E-02	5% 0° , 68, 0,	25 0 g - 21 d 2 H - 2 H -	5 sto 1 5 885 of	8.5 (a) 1.95(, 0)	5 B 0 2 5 B m	5800	9.846	-6.66E 0	900 00 2 od: 150	65 00	NA NA	VA VA	NA.	+
VBV 32 150	00,	196.3	113.	1 9207	13,65	137.00	8 101 101	5.36.12	12000	5 8 80 cd	1755, 00	2 (60, 0)	296.00	. 100, 00	7.00.01	1.5(0, 0)	. 745 (6)	NA NA	VA VA	VA.	MvV-32-
	9.0	,413	1.37	+ 28 Dat	1300	2 111, 13	2726.10	. 871, 02	\$160,00	0 . 2h til	8 202, 01	. 521. (6.	3.071, 50	3 (41) 55.	. 2%: 00	3.2% (6.	3.371, 101	NA.	VA.	AV.	1 111-32
	318	,913	31	8 3 2 3 7	1, 25	1 120, 43	2 %TE +02	2030, 02	3.650, 01	8 : 26 : 3	1.5 Hz 35	6.211:31	2 195, 50	2.591; 55.	(4): 30	2.386 (6.	2,3%, (0)	NA.	AV.	AV.	
	201	,913	31	10.24.300	7.53	9.760, 13	1808-10	. 930, 00	505), 0]	11860	5.70,01	9.76%	3.07(), (0)	3.27h (a)	195.0.	3.85 (0.	3.571, 000	NA.	VΑ	ΑV	
	505	,503	1.37	8 2048	1.35	8 890, 13	- 321: 10	. 830, 00	1281; 0.	7731:0	8,650,01	6.57[: 0]	1710, 00	2326.34	5.180,01	-51; 10.	1985, 00	NA.	VA VA	/AA	+
	505	,503 503	3.7	5.5.2008 7.3.2008	10.57	6.730, 13 1711, 13	2.336.02	. 820, 00 900, 00	. 680,01	1.28E (4 3.35E (4	8.1-0, 01	1.181, 00 8.5.4cm	2,080,00	3.211; 14.	2 525 00	3 , 45 (6.	3.3(7, 00	NA NA	VA VA	VA VA	+
	16	90.5		0.106	1.23	381 3	5.5 (6.05)	5.15 02	3.2 (cm) 5.9 (cm)	28 (4.1	923 40	69 11	181 0	1646	2.22E-00 NA	AV.	NA.	NA.	VA.	AV.	+
	161	9113	. 1	[10.2] Now	10.3	3.15 1	3.5 (- 112)	3 112	Ly bury	5.56.1	1 40	5 800 - 1	5 13 0	1.581	3 850 (0)	5 (60) 11	16 00	NA.	- VA	NA.	_
	- 10	9113	. 3	11,100	13.15	, 90 3	1.86.00	96 07	1.13[60]	55 fo f	6.1 201	3.500 (1)	, P 11	1.541-	3 - 1	5 70 11	3 [5 (0)	NA.	AV.	AN.	
	- 11	913	. 3	15.5.0	13.75	281 3	5.680-02	5119 117	2.8 40	5.586-1	68 40	-5 K-31	101 0	26.0	51 -	23 (6.0)	, 98 (11)	NA.	NA.	NA.	
	13	911	- 1	9,,100	120	108 4	5.56.02	5 8 07	8.5 (car) 1.55(car)	5 36 1	59 40	3.5 Ho. 1 9.5 Mo. 1	5.78 0	5 F	1.365.00	5   6 0	66 111	AA AA	VA VA	AV.	+
	11	31.5	- : :	84 1 0	12 B	211 3	26 5 112	214 02	1 Salan	55961	5 (6) 40	20.00	61 0	5 811:	2 95 00	5.95E-0	186 (0)	AA AA	NA.	VA.	+-
	15	913	. 37	9.55.0	12.13	1 3	2.28(112	531 117	373(4)	2.22(4.1)	8 15 301	797 0	TOP 0	1 89)	1 (10)	1.59E-11	5 13" (8)	NA.	NA.	NA.	_
	16		- 1	[11.55, 2405]	153	168 3	, 81-11,	6 11"	85 %-00	55 to 1	139 40	-16 00	611 0	5.086	5105 -	5981-0	66 (11)	NA.	NA.	VV	
V'11-55	100	4.	21.]	215 50 5	800	12 05	1.6 3	100 1	NA.	NA.	NA.	N.A.	AV.	NΑ	AV.	A.A	A.A	NA.	NA.	NA.	MW/3
	105	10.	- 1	1110 Mrs	1.34	100 5	5 6 F 3	0 0"	VA.	AV	NA AV	NA NA	AV.	AV.	AV.	AA AA	NA NA	AV.	NA NA	AA AA	+
	91	10.	1	9.749	113	189	56 F 3	0.00	VA.	VV.	AA	VA.	- AV	AA	NA.	NA NA	VA.	NA.	NA NA	NA.	+
	115	10 *	. 1	1 3 5 6	121	141 1	5.951- 1	0.00	AV.	NA.	AV	NA.	AV.	AV	NA.	NA.	NA.	NA.	NA.	NA.	-
	191	10.2	. 1	12.2.6	10.1	2.260	4 x)- v	0.5, 02	AV.	AN.	NA.	NA.	ΛV	NA.	- AV	NA.	A.A	NA.	NA.	AA.	
	507	192	5.5	1.21.2006	1, 15	2 120, 13	7.296.13	7,000,000	NA.	VA	VΑ	NA.	VA.	AV	VA.	N.A.	NA.	NA.	NA.	NA.	
	10 (s 10 ty	192	5.4	2.3.20%	12.15 16.06	21.0, 33	2.835.03	+330, 00 +370, 00	VA 1 3ol; n,	NA Stoletal	- NA 250, m	NA AV	AA AA	A/A	AA AA	NA VA	A.A VA	NA NA	NA VA	NA VA	+
	Shi	192	5.4	2 62556	13.55	260.45	25.8.53	0.300, 00	VA.	VA	VA	8.4	VA.	VA.	VA.	8.4	4.4	VA.	NA.	1.4	+
	:11	190	5.5	1.3.2576	16.25	1 530, 13	54: :.1	100.00	NA.	NA.	VA	NA.	VA	VA.	VA.	NA.	NA.	VA	NA.	NA.	
	:42	192	5. 5	17.20%	16.25	2 211, 43	N: :.1	7,000,00	AV	AV	VA	NA.	VA.	4.V	VA.	NA.	NA.	NA.	NA .	NA NA	
	:11	192	5. 5	5 1 255A	12.5%	1350, 45	25.45.05	. 60, 10	77980.	1 120, 00,	1.76.00	. 170, 0.	1.1%, SI	, VI: 5.	1528 00	. 3.lt 0.	1.280, 01	NA.	NA.	AV	
	18	10.	- 4	5 100	0.15	1.01 5	85F 16	185 03	6 (for) 1 (for)	5.596-1	5 15 au	6 (5 × 1	8 ' 0	0.581	8 F 0	8 (6 str. 1) (80 - 1)	802 00	AA AA	AV.	VA.	+
	18	10.	- 1	811106	× 5	181 5	1546 1	8 03	NA.	NA.	NA.	3.53E-0	641 0	×II-	39-100	150:00	×6 (0)	NA.	VA.	NA.	+
	19	10.	- 1	83.0	150	115 5	F 5	1.49 (0.4	VA.	VA.	NA.	-6 go - 1	X   100	8.30 0	3.1	THE	85 F 0	AA .	VA.	VA.	
	50	10 .	2.5	6.57	Li B	916 1	5 595 115	36 01	- 81 - 44	1896-1	150 (0)	- 1 KH-	3,65 0	1 fil-	. 53k tt	9.13(cm	4.65 (10)	2017 201	1.95.0	1.5 (-01	
	121	192	5. 5	83.200	15.00	2,300, 64	7 586 02 of 03	2,000,000	580E0.	8 OE 0	5,330,01	8 (8), 01	1870, 00	2 831; 144	2 150.01	2.35.00	3 (6), 00	NA NA	VA VA	VA VA	-
	122	192	5.7	1.28.2148 5.1.2148	11.1	5.850, 0.1	821-113	5 171 00	13300	27 1534	5.220,00	1.58,, 51	1.611 10	3 (21: 55)	NA NA	2 , 21; 16	VA.	NA NA	VA AV	AV	+
	- 1	10 *	- 1	1 5/1 0	DEP	3.11 1	3 1: 113	3 112	1 300	5.19% [	619 20	4.06 00	8.03 0	191	189-00	5 75 11	6 101	NA.	VA.	AV.	_
1777-1	101	N 9	20.1	213.50.5	3.53	5.49 (6)	10" 3	1001	AV.	AV.	AV.	NA.	Av	NA.	AV.	AA.	NA.	AV.	NΛ	NA.	MAN 1
	105	18.9	- 1	15.10 years	11.35	171 8	5 (15) 5	0 02	AV.	AV.	AV	NA.	AV.	NA.	- AV	NA.	NA.	AV	NA.	NA.	
	115	18.9	- 1	12.50 Nan	III S	11 5	3.5 F #	0 0'	NA.	- VA	NV.	NA NA	ΑV	NV.	AV.	NA.	NA.	NA.	NA.	NA.	-
	01	18.9	and	6.106	11.35	1.50 5	1946 3	00:002	VA.	NA NA	NA NA	NA.	AV.	NA NA	NA.	A.A A.A	NA NA	NA NA	NA NA	NA NA	+
	16	18.9		1, , 0	10.00	211 2	5 151 1	0 02	VA.	NA.	NA.	N.A	AV.	NA.	NA.	NA.	NA.	NA.	NA.	NA.	+-
	507	18.9	5.5	1.27.2536	16.5%	2 120, 43	0.40h 5.4	7,000,00	AV.	NA.	NA.	N.A.	NA.	VA.	VA.	NA.	NA NA	VA.	NA.	NA NA	
	0.6	18.9	5.4	2.3.250W 2.7.250W	12.2%	2.2 E. 4.5	2996.53	+ 330, 102	NA.	ΑV	VA	NA NA	VA	AV.	VA	NA.	NA.	VA	NA NA	NA NA	
	0.00	18.9	5. 5	2 7 2006	1515	1.7 E. 43	2.386 00	+ 371, 102	9 221: 02	3.786:03	1670.01	NA.	NA.	NA.	N.A.	MA	VA.	NA.	NA.	ΑV	_
	530	18.9	5. 5	2 9 2546	13.55	190, 35	2.55(: 1.1	9390, 00	VA.	VA.	VA VA	NA NA	AV AV	VA VA	VA VA	NA NA	NA NA	VA VA	NA.	NA.	+
	511 512	18.9	5.5	1.3.2576 1.7.2576	10.05	2,700,43	8 28E 13	7,000,00	AV.	VA AV	VA VA	NA NA	VA VA	VA VA	VA VA	NA NA	NA NA	VA.	NA NA	NA NA	+
	513	18.9	5.4	4 1 2004	13.15	360, 61	5 521: 113	835.00	2.50(.02		5.000,01	* 8 d ; (c.	1.2%, 01	. 59: 5.	2.721; 101	. 3.1: 0.	1.10, 01	NA.	VA.	VA.	_
	21.1	18.9	1.5	p. No. 2016	1) N	1.05'-11	× 52)- 112	3.1 1.02	37 [61]	0.30831	1.751.01	831: or	1851 10	8 56E ***	5.8 (0.00)	1 3 SH 17	0.3 101	NA.	AV	NA.	1
	- 15	18.9		4.0	10.5	10 1	35 1: 113	5 113	* 80-00	83.16.1	1.60	- SF-	18 0	5.206	2181 00	56900	6.8.101	NA.	- VA	ΑΛ	
	116	18.9	5.5	8.24.2556	12.18	669, 14	0.51: 0.4	3,350, 103	NA.	VA.	NA.	. (21) (6)	5.810, 00	+ 781; 14.	, std; 100	5 8545 FG.	5 85], 101	NA.	AA.	NA.	-
	117	18.9	5.4	5.2, 2006 8.3,2007	9.14	1.610, 54	2.786.03	\$800,00	353002	1.121, rc.	1.315.35	439E3C	16%, 50	. 851: 14.	2.100,00	3 035 16	12%, 00	NA NA	AV AV	AV.	+

	1	ı	I	I						BUCHANA	N. M										_
Well III'	SAMPLE	SAMPLE ZONE CENTER.	SAMPLE ZONE CENTER,	SAMPLI, COLL	LCHON								NALYSIS RESUL	.rs							Well ID
Wellin	ID	depth if below top of cosing	elevation It ms/2				TRITIUM ( pCFL)			Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l41.)			N 63 (pCFL)		1 """"
		·		Date	Loar	Result	Std Drs.	MDC	Result	Std. Dev.	AIDC	Result	Std. Dev	ADC	Result	Std Dry.	VIDE	Result	Sfd Dev.	MDC	
737. 14	100,	10	0.1	.2132K3	.3.90	1235 01	3 180, 13 3 180 A	Tools 32	AV AV	AV AV	VA VA	NA NA	VA VA	VA VA	VA VA	NA NA	NA NA	VA VA	NA NA	NA NA	MW-30
VW-55	1015	- 4	40.1	15/5/5	1.0	80500	.1. 3	00.	AV	NA.	NA.	NA.	NA.	A.V	VA.	NA.	NA.	NA.	NA.	N.A	MVV-30
	- 01	19		0,10	1 1	94F	1 KOH 3	2012.02	NA.	NΑ	AV	NA.	VΛ	ΑV	AV	NA.	A.A	NA.	NΛ	NΛ	
	118	19	- 1	1 3 6	10.8	9.8 1	1986 8	0.00	NA.	NA.	AV	NA.	VΛ	ΑV	AV	NA.	NA.	NA.	NA.	NA.	
	16-	19		1 6	9.5	101 S	5 11- 5	0 0'	NA.	AV.	AV.	NA NA	AV.	AV AV	AV.	AA AA	A.A N.A	NA.	NA NA	NA NA	+
	16	19	- 11	14,100	11.7	511 1	591-1	6.45 11"	VA.	VA.	VA.	NA.	AV.	AV.	AV.	AA	NA AA	AV.	NA.	NA.	+
	16)	19	. 1	3 3 100	13.1	8 11 1	664 nd	6.4 07	16 %00	13951	5.78, 401	VA.	NA.	NA.	NA.	- VV	N/A	NA.	VA.	NA.	_
	- 10	19	- 1	. 5. 0	153	901 1	79- 1	6.36 07	NA.	VV	NA.	NA.	AV	NΑ	AV	AA.	NA.	NA.	NA.	NA.	
	111	10	5.5	5 5 5 mb	9.5	119 *	5 % (F - 5	2007.02	AV AV	AV.	NV NV	NA NA	W/ AV	NA VA	VA VIA	A.A.	NA A A	NA AV	NA AA	NA NA	+
	513	19	5.1	3 1006	13.3"	10%, 51	10 S 11 S	8 721, 102	175E 0.	* 43E H	1871.01	- M: 10.	2073.54	, oll; 5,	3 6 11: 06	, 3"I; II,	1335.01	NA NA	VA VA	VA.	+
	51.1	19	5.4	625246	16.15	170,00	3"]; 113	4250, 02	2,365,01	0.004534	8 65 [, 10]	131, 00	100, 61	101: 5.	2 (8): (0)	8 526 06	936, 101	NA.	VA.	VA.	+
	15	10	- 1	d, , P	9.5	1 4 3	SE 115	317 07	6.791-01	130 0	1.316	-5 %-	1.96 0	K*1-	2.18.5	596.00	169 101	NA.	AV.	AV.	
	16	19	- 1	6.5.	15.58	203 3	58 (6.00)	581 01	1.79(14)	1336.1	19 40	1660-0	887 0	1811	2.2 pc. n	2580-0	*65 (0)	6.88.0	97F NA	2.20 0	
	18	19	- 1	1.87.8	11.55	101 3	5.58)- 0.5	119 01	9.59m² *9.9m²	5 50 I	5.08 and	1, 344m v	2.1 0	1311:	5.3 - 1	, 491- 11	5 (5 10)	AA AA	VA VA	AV.	+
	19	19		150,000	1, 1	1.100.00	5 a 41 02	. 3. 0.	2 5,00	5, 4t al	5.3801	118., 101	9	* .81:	. 8 1: .00	5 4: 14:	10134,, 101	KA.	VA.	VA.	+
XW 30-21	100,	.00	13	21206	.700	VA	NA NA	NA .	. 295, 50	5 (8): (3)	5.530, 01	NA.	NA.	NA.	NA.	VA.	VA.	NA.	VA.	NA.	MW-36
	900	161	1.3	2.21.2536	9.15	300, 51	0.046.03	0.300, 102	AV	AV	VA	N.A.	VA	Αλ	VA	VV	NA.	VA	NA.	NA .	
	503	161	13	3.23.2556 15.2566	16.00	3 (2), (4) NA	181: 11g	. 841, 103 NA	9750.00	9 (2E) (4 1 (64) (4	9 (20, 0) 1,350, 01	3 8/C, 101 NA	1 010 01 NA	. 131: 1 NA	512E 00 NA	5.33); (C. VA	1 220, 01 NA	6 OE OF	1.59E 0.	1 531: 01 NA	
	501	161	- 11	15 2006 + 5 2006	10.30.	NA 2100/42	50E 02	. 5.17 HZ	37000	189511 199511	1350.01	3.99); (C.	1.0%, SI	. 211: 5.	- NA - MODIC	NA . 12h H.	1.125, 01	NA NA	VA VA	VA VA	+
	506	161	13	8 28 2006	16.35	2 150, 12	804: 1.2	7.5,00	VA.	VA	VA.	5.35.00	3,270,000	3,320, 00	1.660, 100	3 161: 14	5 50 00	NA NA	VA.	NA.	+
	507	161	1.3	+ 2" Dat"	16.16	1317, 30	758-102	931, 00	\$160 m	7.528.04	8 (45, 0)	3.315.61	2811, 00	3 75 55	1005,01	3.135.00	3 [5], (0)	NA.	VΑ	NA.	
	16	161	-1,	88.00	13.15	1.63	850 00	200 02	25.55 24	68 16 1	93 20	1586.1	3 (0 0	3 P	3.566-100	31  - 11	11 00	- 151- 0	5.00	281.0	
	10	161	-1.5	1 18 500	11.16	, 50	2 h 11,	50 02	8.550 are	5.16.1	9 % and 9 % and	No. 1	1.80 0	3.5 1:	31 - 1	5 1: 11	3.1 100	AA AA	AV.	VA.	-
	11	161	-1.5	15 1 8	1518	116 3	100 00	65 07	5 380-01	5 No.1	8.25 (0)	39.1	100 0	1511	-181 at	15  - 11	385 00	AA AA	AV.	AV.	+
	1	161	-13	1 10 208	1131	201 2	5 (- 02	6 11'	55700	536- I	806 40	0 0	681 0	1.36E	2. 25.00	5 8 5 11	51 00	NA AA	NA.	VA.	+
	13	161	-1,	*** 0	11.18	11 1	51: 11"	106 117	-6.75 -44	3 Po 1	9 [K at]	8 316-1	188 0	5.5 H+	515 - I	5 550: 11	385 (0)	NA.	NA.	NA.	-
	11	161	-13	51.500	13.55	198	90-11	9, 11,	- 3(-4)	196.1	8.98.40]	* 0	3 11	5 56	411.0	3 (8) 0	135 00	A.A	NA.	AV.	
	14	161	-13	8 12 00 1 78 300	In the	202. 3	3 2 1: 115	9 n,	15 Jun 6 (6)	6.626-1	7.797 and 9.38 and	-2 y 16-	612. 0	1981	301.0	5 57 E 0 5 85 E 0	8145 (0)	AA AA	VA VA	AV.	
120-06-11	16	161	-1.5	1 8 400	15 B	1.1 3 1.56 mi	121 1	6 00	NA SHA	X () () ()	VA VA	-9 1 II-	3 P2 11	NA NA	NV	0.4	AA	NA NA	NA.	NA.	MW/ 38
	10.5	1	256.5	ь	13.15	158 1	19- 1	6.35 07	NA.	NA.	NA.	NA.	AV.	AV.	AV.	AA.	A.A	NA.	NA.	NA.	
	115	4	25/2	4 75 7 16	12.15	8.87	1,65E-10	86 03	5 18 0	5.396-1	3.15 -00	25.01 (0)	149 1	184	19 (4.00)	585.0	1.3.01	1 × 1: 1	1750-0	681-01	
	- 01	4	456.0	15.506	12.89	N/V	A.A	W	5 ~ 6 11	6.19651	5005,001	- AA	- VV	A.A	AA.	A.A	AV.	AA .	NA.	NA.	
	100		256.5	5 × 5 mb 8 28 2 m	1.3	208 1	3 F 113	6 to 10"	, en	6 toller 1 VA	61 -01 VA	24.4 mm	115 . 0	541-		31- 11 3 3 5 1- 11	1.15 01	AA AA	AV.	AV.	+
	507	3-	25.2	6.25.25.2	12.3%	6115/32	3.5th (0	750, 00	2180, 00	1177, 16.	585, 01	130501	1615, 50	, TH: 55	1.30(0.00	25 5 16	360, 00	NA NA	VA AV	VA.	-
	5/6	3"	25.2	51 20m	13.15	1.135, 54	1.294: 10	. 640, 100	1000, 00	110, 0	13,570	2.594.55	611, 50	1186: 55	. 055,55	31.35 (6.	326.00	NA.	VA.	NA.	+-
	509	3"	25.2	8 1200	1425	1.010, 64	3 - 46 - 12	. 571, 02 . 471, 02	1125, 00	131, 00	1.10,01	3115], 16,	43%, (0)	7 884; til.	7.35000	1, St. 16.	963, 101	NA.	VΑ	VA.	
	510	31	28.2	15.28.2076	16.13	1.0E; 54 2.2dc 05	1256.02	, 67), 02	31 E. 00	11%, 66	196,01	2.586.55	1177, 50	\$ 70E-55	1.795,00	1.50(1.00)	5.3%, 101	NA.	VA.	AV.	
J.W. 20 C	900 900	69.7 19.7	37.9	2.00206	12 (15)	2.5%, 64	8.550, 03 5 , de 03	6 38E 52 9 39E 02	AV	AV AV	VA VA	NA NA	VA VA	A.V A.V	VA VA	NA NA	NA NA	VA VA	NA NA	NA NA	MM-3
	303	10.2	37.0	3.21.2554	1208	2780, 61	3.575.03	. 871, 103	1115.00	Soule (d)	510.01	5 177, 16,	916, 01	5.115.5	2.176.00	5 (4) (C	1.05.01	1.87.01	104	151.0	+
	-01	10	.3 9	15.716	1113	AV.	A.A	NA.	501 0	*slo-1	6.76 401	'VA	NA.	NA.	A.A	VA.	NA.	NA.	NA.	NA.	-
	118	10	.1 0	5 5 7 106	1.3	2.10 1	3.590-113	5.1 01	3.P 0	× 151 1	5.54 att	4 B 0	1.08 1	116	18 .	Qr. 0	1.18 01	A.A	- AA	- AV	
	191	10	.0	8 % 1 6	10.0	1.11	* 3F s	5.55 (1)	- VV	AV.	NA.	106 - 1	65, 0	sol-	-169 -	5.585.0	566 00	NA.	NA.	VA.	_
	10	10	.1 9	88.10	1. B	1.01 1	1.896-02	95 07	161 0	100 0	183 40	- 5 % '-	2.0	1901	9.50 cm	16 1- 0	\$15,00	NA L' le u	- VA	NA 11 In oil	+-
	500	19.7	3" 9	23 2548	1013	1135, 51	1176.00	. T.D. (C	1850, 00	0.608.04	120.01	28965.	200,00	2 251: 14.	1080.00	. 804: 00.	2.252 (0)	NA.	VA.	VA	+
	510	19.5	3" 9	1.21.2008	1606	1,260, 61	7 506 102	\$70,00	\$670,00	1 (2): (1	1730,01	1776.1.	2.2 E. 30	3 (0); 11.	2 773,42	215.06	3.535, 101	NA.	VΑ	VA.	
	*11	10°	3" (1	1.10308	16.53	1.107 2.1	5.00 E-105	63' 11"	8 *** 10	1.11.00	3.877 01	3.886	3.865 10	(MI)	1.56 00	5 67 E. 07	565' 1111	N.A.	VA.	NA.	$\perp$
	1.5	10	.0 5.	51.500	11.89	6.9 4	5 35 00	05 07	230 0	8396 I	50 40	45 Fe	13 0	5.50	1.685.00	5 Mile ()	51 00	AA AA	AV.	AV.	+-
	- 11	10	.3 9	8 1 1 100	1500	8 61 3	2.330.00	9, 0,	3.00.00	108 0	5.9 an	1.90(-1	86 0	5.901	. 3 1: 0	halo or	10 101	NA AA	AV.	AV.	+
	15	10	.3 0	1.38 7463	1 + 39	8 14 4	1971	6 0.	5 % [ 11	108.0	5.9 art	280 0	148 0	1.981	505 11	5 50 0	515 00	NA.	NA.	AV.	1
1.47-4-14	101			2.71.7.00	C 511	11 115	×92 3	0.50	NA.	ΑΛ	NA.	NA .	AV	AV	AV	AA	NA.	NA.	NA.	NA.	MWV
	11.5			. 8 . 00	1 ( 5)	365-14	1004 3	311:103	237 (00)	8.91160	8 Man	131100	9% 14	5 (0)	Sp. a.	1.589	100	[54-70]	481-1	11- 35	$\vdash$
	503		- :		16.35	NA.	2.57E 103	NA . 280, 10	256.20	9 16 1 589601	9.16 (40) 7.871, 01	NA : (4): (6)	NA 1 KG SI	NA sale :	5 (5) (6)	- MA - 35h m.	NA 1.511, 01	5.00 E. (c)	NA 1.27b; iv.	1 331: 01	+
	901	i-	2	3.21.2546	16.35	3 190, 61	3.781: 03	. 8.1. 03	1050, 00	879E3	8 J. 01	9755.31	166, 00	5.211: 144	7 FG.34	1.085.00	1975, 00	5 (3)E (4)	1.506.55	1.526.01	+
	50.65	i-	2	6.21.2536	16.25	1.051, 5.1	8 550: 10	3 80, 00	5570,00	1.2(6, 16,	1872.01	3.250, 10.	6.921, 101	8 001: 00	8050.00	4 5 th 10.	130,00	NA.	VA.	NA.	
	506	1"	2	9.25.246	9.30.	7,170,13	225: 13	\$750,00	. 120, 64	1800, 00.	5000.01	3.8.45.52	8,510, 00	5 595 555	, 5.8E 50	1.31:10.	18%, 00	NA.	VA.	NA.	
	507	11	2	6.21.2547	10.3%	1050,43	3.35[: 1/2	. 941, 02	. No. 61	2.120, 00	8 120, 01	2.260, 000	1880, 00	3.50(1.11)	28: 50	3.236.00	330,00	NA.	VA.	VA.	+
	0.00 0.00	1.		81207	10.55	2,790, 43	2 996 10	. 850, 00	257 H	2071, 00.	8,570,01	2.79; (6,	3 930, 100	3 781: 144 3 781: 144	1230,01	3 0.75 00. 3 0.05 00.	3.50, 00	NA NA	VA VA	VA AV	+
	100	- 1		13373	11.75	6.571 13	3.50(-10)	7.60,00	8 737 FO	1 250, 10,	1631.01	2187, 100	2.000 00	3.78() 1.11	126.00	3.15() (C. 3.18() (C.	3 (5) 101	NA NA	VA VA	VA VA	+
	111	1		11.1.8	111	144 4	1.50-111	95 112	9 1	1.55 0	15 401	15' - 1	*13 0	1001	3 10 000	25 (-11	185 101	NA.	VA.	VA.	<b>t</b>
	512	1"	2	1.10308	12.2%	2,680,40	372E 02	. 10, 00	.800.01	1880, 00	5.080, 01	28.5.06	19%, 50	4.56E-55	2.850, 0.	1.53() 16.	1885, 00	NA.	AV	VA	1
	513	1.	2	1.2, 250	14.25	50% 10	\$30E (2	208), 02	8815.00	1.330, 10.	9.750, rd	3.,26%	3 (21, 10)	3.2% (4)	2036.00	33.56 (6.	2825, 00	NA.	VΑ	VΑ	T
	:11	111		51.2549	12.1%	3.851, 13	* 535-10	1.731.00	5,370, 00	1.3" 10.	48.1.01	, 051; 06.	* 6 E, 50	\$1001-144	8000 0	\$ 131: 10.	5 10, 00	N.A.	VA.	VA.	1

Ligar Feet 21

IPEC00224884

		SAMPLE ZONE																			
Well ID	SAMPLE ID	CENTER. depth it below	SAMPLE ZONE CENTER,	SAMPLE COLL	LCHON							,	NALYSIS RESUL	.is							Well
	110	top of casing	elevation It mst <sup>2</sup>				TRITIUM ( pC FL,			Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC ld.)			NL63 (pCFL)		1
				Date	loor	Result	Std Des.	MDC	Result	Std. Dev.	ADC	Result	Std. Dev	VIDC	Result	Std Drs.	MDC	Result	Sfd Dev.	VIDC	
	515 516	1-	2	123 2539	11.15	1700, 13	157E-02	2270, 02	2010, 01	1.5/C, 10.	1270.00	1 221, 12 5 , 86, 12	3 960, 100	1 384; 133 - 301; 133	3.950.00	3.50); (C	3.5%, 00 6.7%, 00	NA NA	AV AV	AV AV	-
111-1-5	1007	39		28,100	1.0	196 00	1 4 4	137: 3	1.3.01	1915 Oc	2.22 (0)	1.74	985.0	21 01	2.000.000	190 1	2.24.0	11 01	2011	1.18.0	NW-3
VA + 42	III C	21	.4	2.38.2006	.2.00	VV	NA NA	NA.	. 82 of	1 25 05	2.286	AV.	NΛ	NA.	A.4	NA.	VΛ	NA.	NΛ	N/A	MW 3
	118	10	-11	з , р	12.8	183 1	2 31-119	'X 113	87 1	1.39 0	1.946	B 0	189 1	81-	1.500.00	5 8 0	1.65 01	1 36	1.761	1.5 Hr. Of	
	- 01	10	-0.1	6	1.1	1.40 1	5.6 to 105	196 01	.dk 1	189 0	2.516	- 1 - 0 - 2 4 Hs	8.21 0	5.5%	20 Str. 20 27 (17 20)	3.5 p. 0	18 00 8 × 00	-10 d	NA I	VA.	+
	100	*0	- 41	0 25 P	0.15	115 1	XXI- 115	186 01	55 1	130 0	1.9115	-5.71 000	8.98 0	86.1	2505.00	8 M: 11	106 01	AA AA	VA.	AV.	+
	- 01	*10	411	* **	11.55	301 1	9.931- 3	6.49 0.1	NA.	AV.	NA.	NA.	AV.	AV	NA.	NA.	NA.	NA.	NA.	NA.	+
	- 0	*0	-11	6 ' '	15.5	3   3   5	3 30 115	0, 11	85 1	2.8 0	1.5116	-1 J9 nm	356 0	1.881	169-101	3 35]- 11	115 00	AA.	VV	AV.	
	0.00	*1)	-11	15.15.200	11.36	2.190, 43	2304.02	8 00	2130, 01	2190, 00	2.966.00	99 o	1611, 10	5 10011	2.53[-10]	3.75h nc.	170,00	AA AA	AV.	VA.	+
	510	50	11	1.23.2538	1.03	676.13	3.5°E 10	, 760, 10	2130 M	1.5%, 16,	3.640, 01	8 95 0	2.500, 50	3 (6): 100 3 (6): 100	5.321.02	2 725 16	2,550, 101	NA NA	AV AV	AA AV	+-
	:11	59	11	21208	12.28	516, 13	2.150.102	. 95, 10	206, 61	1.511, 00	873[,11]	108600	1.581, 50	2 .81: 14.	1.16, 0,	25.95.06	2.580, 000	NA.	VA	VA.	+
	1.	*0	4.1	1 10 Yes	15.5	180 3	3   E 02	10.5	86 I	1.95 0	\$ 96 and		533 0	5.1Hz	1.09	5310	615 00	AA .	ΑΛ	AV	
	13	*0	411	1 , , 0	113	3.6 3	28 F 02	500 00	11 1	1 19 0	5.7 (40)	89 0	181 0	5 500	4,15,40	5 5 7 1 11	3  9 101	NA.	NA.	AV.	
	111	10	411	21,100	1213	183 3	8.66E-02	5.35 (0)	. 48 1	180 0	5.65 401	-5.5 In	18 0	1.98)-	- 19 n	5 (66) 11 5 (6.11)	315 00	AA AA	AV.	AV.	+
	alo	_9	11	128.300	1.3	150	2886 (0		220.00	201, 00	0,01	500, 101	20.00	291;	212	5 % E 14.	5.48,, 101	NA NA	VA.	NA.	+
VW 37 30	100,	17.2	212	2.21209	.135	, 685 HI	7 01. 13	6.791:12	AV	AV	VA	NA.	NA.	ΑA	VA	NA.	NA.	AV.	NA.	NA NA	MW
	9.0	30.2	242	2.28.2536	1. 15	1.171, 5.1	2.36.53	. 321, 113	1860, 00	1.230, 00	1.9635	. 796.00	1.710, 64	. 96h 5a	1.50, 00	, 445.00	. 8.1. 01	5 (SE 14)	1 (5); 0,	1916.01	1
	0.0	39.0 39.0	212	2.28.2536	1, 15	NA 1.705, GT	NA 1305.03	NA NA na	1911, 10 1351, 14	1 230, 00, 1 320, 00,	1 (81: 0)	NA 3.5,1; (c.	NA LISTER	NA etha	NA 196, 00	NA CTr. III	- VA - , 421, 101	NA 130-1	VA 1.35E 0.	NA 1 : II: 01	+-
	503	39/2 39/2	212	3 2 244	1, 55	1.96, 51	2 826 53	. 821, 03	. 350, 61	1 321, 06	5 950, 01	5 5,1; (c. 3 3 0); (c.	41 E, 50	5 (3); 55.	100,00	1715 00 1715 00	5.3%, 00	1.21E 01	1350 0.	1.510.01	+
	30.65	392		6.27 2006	16.15	1 (2), (4)	.35.53	3,810, 00	2.10.01	1715. (6.	7.030,01	8 - 81; 10.	7.680, 00	5.251: 10.	1.36[: 10]	+ Till: 16	9.607, 000	NA.	VA	VA.	+
	500	by t	24.2		1.06	638, 13	3.556.10	98', 02	1767, 101	111, 06	8 (11, 0)	3.50F.01	3.367, (0)	3.5(1): 0.0	57E-00	3 5)- 10	3.225, 101	NA.	NA.	NA.	
	16	(4) ,	.111.1	8 50	13.15	-9- (	3.5 (0.11)	58 H	9.6 0	1.81 0	6.5 201	1 0	312 0	3 11:	27 Br 20	3 351- 11	\$ 100	AA.	VV	ΑV	
	161	60 ,	255.5	1 15 500	150	6 3 3	3 3 - 112	69 0°	5/95 (i) 9/18/10	1.28 o 8.535 J	18 201 8 15 201	536.1	101 0	1.981	5 0 g .	2.826.0	196 (0)	AA de	NA 1 350 0	L ob of	+
	- 11	80 *	24.5	11.18	1312	5.11 3	2.15[-112	9 11	31 11	11161	50 40	-1 10 00	1.82 0	1.381	- 55F 0	2 10 0	* 101	35F	NA.	NA.	+-
	111	40 *	.*: *	1 10 508	16.1	s 10 - 3	5.356.02	6 07	13 0	53.19.1	181 -01	3.5116-1	603 0	5.831	S II: 00	19-11	9.15 (0)	NA.	NA.	NA.	+
	13	50 .	215.1	*** 9	1405	101 4	5 35 02	20 02	51 0	××5-1	5.69 401	-161 00	3.8 0	1.5 15	15 (100)	5 3- 11	[106 101	NA.	NA.	AV.	-
	- 11	50 .	215.1	51.500	13.15	1.48 4	× 151-11"	5 9 11"	11 0	S. Slo. I	3 40	- 1 X-01	0.0	5 46	* II- 00	5.5 E.O.	6.13 00	NA.	NA.	AV.	
	16	50.	27.7	1 % 100	13.18	157 3	17000	2.26, 11,	60 1	1.80 0	3 (8" 40)	- 35h-	6.00 0	5.50)	3 80 0	5 75 11	8.387 (0)	A.4 A.4	NA NA	NA NA	+
17-1-1	100	25.	- 18	1.71.7.06	11 18	6 1: 16	11 3	6 501	VA.	NA.	VA.	N.A	AV	NA.	AV.	AA AA	NA NA	NA AV	NA.	NA.	WW
	107	54.1	.48 *	1.81.9	14.55	133 1	1.56	45 04	111	1.5.0	1.86	× 1: 0	200 0	2.516	5.37 (1)	×4- 0	215 01	*31E T	1 x 10 0	LSIE 01	1
	- 02	54.1	.48 *	. 8 . 9	14.55	AV	A.A	NA .	3.5	200.0	1.76	NA.	NA.	NA.	NA.	- AA	- AV	A.A	NA.	AV.	
	118		-58.1	4	1.15	1911	15.45	26 . 03	1.50	1.17%	(11, 20)	391-0	1.6	It.	1.0	585.0	5.01	Late 1	1.550-0	1.39(0)	$\perp$
	- 01	44.	-34 °	62.2.6	13.55	1.857 1	180F 3	684.00	62 1	1.890	66 at 18, at 1	, 2, de 10	NA	NA A	201.0	1890 0	5.55 (0)	NA NA	La Irin	1 39E 01 NA	+
	306	53.2	38.2	9.25.546	D. E.	105, 41	7.05.13	1,520, 102	. 815. 01	1880, 10.	1870.01	3.357, 101	8.00, 50	7.811; 555	2.400, 00	8.8% (6.	100,00	NA NA	VA.	VA.	+
	90"	53.2	38.2	4 2" Stat"	12.25	5890, 13	3.854; 102	. 95), 10	2 (2), (4	3100, 10	880,01	2 150, 16,	3.511, 100 3.271, 100	1 32H; 544	9.580, 02	1975 06	1845, 00	NA.	VA	NA.	-
	0.0		38.2	8 7 2007		6.66, 13	3.980, 102	. 880, 100	2330, 61	2.151, 10,	30,000	1.350, 00	3,270, 00	3 Ch (a)	3.640, 02	3.895.00	1,330, 000	NA.	VA.	VΑ	
	509	53.2	38.2	15.15.200	1500	188), 13	2850 02	, 480, 102	2781, 13	2 (9), 10,	5.53[, 0]	3 (2)(3)	2.67), (a)	2726 (6)	. 201.00	2 0.6 00	2 22 100	NA.	VΑ	VA.	+
	510	59.2 59.2	38 I 38 I	2.1.2006	16.3.	6430, 13 5 330, 13	3.46 (C 2.76 (C	. 330, 00	2390, 101 2120, 101	3.2(0, 0)	5 (27), (0) 5 (27), (0)	5 (d. 6)	3 723, 50	3 (64) (6) 3 (7) (6)	2,990,00 Th: 00	3 , 2h (G) 2 , tile (G)	3.150, 00	8 ITES.	. 55E 5.	1711. O.	+
	:12	53.2	38.0	1.10208	1, 00	1271, 13	1776.00	. 1.1, 102	2 (6, 6)	2.2%, 16.	6.360, 01	. 57 le 5 c	6181, 10	+ 80 dg 5.5.	1.780.5s.	. 8b 16	815.00	NA.	VA.	VA.	+
	13	44.1	.44 "	0	13.77	804 3	5.5 [6.03]	202 02	90 1	19 0	5.68 401	3 16 5	3.11 0	1 (0 ()	1.85.00	5  - 11	135 (0)	A.A	NA.	AV.	-
	- 11	84.1	.44.	51.500	17.89	501 4	8.246.02	6 01	, 10 1	218 0	5.66 201	- ' × sl '	% 0	S. III	5.0.	1.89(-0)	×6 m	A.A	NA.	NA.	
	18	44.1	.4x *	1 36 3000	1512	108 3	18 E 02	61 01	1 188	1.16 0	5 1 aut 88 aut	959-1	50 0	6.97E	9 41 . -1 20 an	5 F H	255, 000	AA AA	AV.	AV.	+
'A-58	101	5.1	- 1	1.8 , 102	1.91	5366 H	136	150 2	-136 (0)	8 38F 0	5 0	190	××1- ×	55 101	100	898 0	29	AA AA	AV.	AV	1.
	0.0	25 1	1.1	12,30,2005	15%	2,900,00	1296.12	17.0,00	AV.	ΑV	NA.	2.80); (0.	8.510, 00	9 301: 121	2.816.00	8 (3); 10.	97,5,00	NA.	VA	VA.	
	501	25 1	1.1	1 5.2556	13.5%	1.015, 32	1.506.02	1660, 00	NA.	VΑ	NA.	37.15 (6)	1115.01	8121: 14	3 551: 00	, 395, 0,	802, 00	NA.	VA	VA.	$\perp$
	100	51	-1.1	1.55%	13.14	1.11 3	1 mg/s - 5	16 01	AV.	VA VA	AV.	3 30 m	1.10 1	8.316	3.711- or 1.81- or	50 m	S 101	AA AA	AN AN	AV.	+-
	106	51	- 1 1	1,2,00	133	339	1.596	16 01	AV.	AV.	VA.	3 O D D	919 0	6 (1)	3 31-11	9 9 11	3 181	AA AA	AV.	VA.	+
	16	25.1	4.1	18 100	1.15	1.88	33 1: 112	5 B 07	1.59500	3,4516-1	5.15 (01)	5.50-0	1.16 1	51 F	1310.00	Jr. 11	13 01	AA	AV.	AV.	T
	16)	28.1	4.1	. 5 . 0	11.05	11 1	5 p 5	1.81 07	NA.	AV.	NA.	19.10.00	8 1 0	5.5 Ib	1.381-11	130-0	515 101	AA .	ΑΛ	NA.	
	- 10	51	4.1		13.75	. 94 4	1-98)- 1	56 11"	NA.	NΛ	NA.	3 1: 0	8 00 0	2.55[6	1 (8) 0	5.636-0	5 [9 00	AA.	NA.	NA.	+-
	11	51	- 1	14.500	8.90	50.00	1.916.0	1561-001	NA LS Sair	NA	NA C all	155100	934 on 1 03 - 1	5.3 <b>x</b> (m)	183 av	1.368	80-10 94 IIII	AA AA	NA NA	NA NA	+
	311	25 1	1.1	62.246	9.18	916.32	1.381; 1.2	140,00	2 (6): 14.	216, 16,	2.906.55	2 521: 16.	7.560, 50	5 (SE 10)	2.90, 06	7 (%) (6)	5.5%, 00	1.06.00	5 Tale (G)	6.30[: 00	+
	:11	25.1	1.1	6.2, 2556	9.18	17421, 12	77E 52	. 760, 100	AV	VA.	AA.	5.900,01	2,100, 50	2 501: 55	1.50:00	2076.00	2.232, 000	NA.	NA.	AV.	L
	:45	25 1	1.1	1.6.2006	1200	5.030, 42	12(4) 02	1,520,00	3750,01	1.50(1.1)	\$ 200, 01	3 (6), (6)	1,000,00	7.70() 555	2.781; 000	87-5h (C.	7 (.1. 00)	NA.	AV	Aγ	
	516	25 1	1.1	8 7 2046	13.23	2 150, 42	84, 10	. 750, 00	5144:02	0.301(0)	7,150,01	2.291.00	6 (7), 50	5.511; 55.	7,221, 0.	4 State 100	933), 00	2.75% (4	2 9 41: 0.	3 .31: 01	+
	517	23 T 23 T	1.1	1, 22, 2006	1, 35	3 530, 40 1 780, 40	85E 02 108E 02	1,870, 00 1,890, 00	5,350,00 1,60,00	7 805 01 9 905 01	8 750, 01	3 811: 01 3 130, 00	1780, 00	8 (01) 00	1 ISC 0. 3 (81: 00	9/25E-06 5/25E-06	6 (20, 00)	NA NA	VA AV	AV AV	+
	518	23.1	1.1		7.58	220,40	9 138E 102	5,310, 10	516.00	1,325, 06	1.90.00	2731: 10	1920, 00	2 001: 00	3381100	- 1.15 (G)	382, 00	NA NA	AV AV	AA AV	+
	120	23.1	1 1	2 2 2 3 4 7	1.3	601 12	531-112	187 107	92.102	65801	8.85" (1)	2.00	3.071.50	31-51- **	280 (0)	31 1: 17	3.96" 1111	NA.	NA.	NA.	+
	31	28.1	4.1	2 55 5 0	H 15	2.1.2	6 F 102	112	35900	5.16.1	8 19 201	235 Pa	1.11 0	1916	55 - 1	2556.00	100 (0)	AA .	AV.	AV.	
L 42.00	100,	- 67	.3	3.22.2007	5.53	1730, 02	1,770,40	1.316.42	2.7%, 00	8,5%, 0,	\$711; S.	. 230, 01	, 97E 06	. 850, 101	. 841, 141	1885, 50	2585.00	3 .11: 55	1 (e); 0,	1.230: 01	MV
	9.0	6"	13	8 7 2007	16.35	3 250, 12	85E 10	. 95, 02	3.557 (0)	1.1%, 00,	9.321, 01 8.531, 01	2.5%, (c. 286 h.)	3171, 50	3 571; 14.	2.621, 6,	2.55(: 10.	1280, 00	AA AA	AV.	VA VA	+-

1 age 5 of 21

IPEC00224885

<sup>1</sup> to 8 950 L 800 - 8500 VG 2000 - Quarta 3 Lilles Table 5 Quarter 3 Formatio IVVV coss. Macclithas

## TABLES INSTORIC GROENWATER ANALYTICAL RESULTS INDIAN POINT ENERGY CENTER BITTLINANN, M.

	_		1	1						BUCHANA	., 11										
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLI, COLL	LCHON							,	NALYSIS RESUL	rs							WHID'
Well III	ID	depth if below top of casing	elevatina It msl <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			Ni 63 (pCi/L)		- WHILD
		top or Caring		Date	Loar	Result	Std Drs.	ADC	Result	Std. Dev.	AIDC	Result	Sid. Des	ADC	Resulf	Std Dry.	MDC	Result	Std Des.	ADC	1
	501	107	11	51.200	13.18	3.180, 32	24: (0	. 940, 02	2210, 90	91,716,61	9 T81, 01	35.165.	1.580, 100	2.531; 10.	3760,50	. 85.l; +C.	34.5.00	VA	AV	AV.	
	0.6	67	13	10.23.2008	12.53	3.380, 52	2 to 10 to 1	. 976, 102	3311, 00 3381, 00	1.121, 00 5-88-11	5.50,01	1.280, 00	\$ 160, 50	\$ 151; to:	1.220.00	\$ 385 FG. 3 (G) FG.	406, 00	NA NA	VA VA	AV AV	+
	-21	- 6	13	11.5.50	151.	111.7.52	3.45 (C)	184 - 01	13	20:01	502.00	6.14.0	20 - 00	9 301:	2 (8): 00	2.7 15 45	6.73 . 00	NA AA	NA.	1/2	+-
7/W 35-84	100,	83.4	3.5	5.22.2507	, 138	\$9.1, 02	1890.32	1.296 (2	1 *25, 00	* 221, 0,	5.57h h.	9070.12	, 535 16.	, 69, 101	5 911:01	1.581, 101	. 8.1; 00.	1 991; 55.	5 996 55	1.36.01	MW/358
	107	915	-15	8 50	103	141 1	F-105	9 0.	§ [ca)	XI+- 1	3 -01	3.55 - 1	30 0	4 5 Hr	- P 0	3 No. 10	\$ 6 101	A.A	NA.	N/A	
	115	84.5	-15		13.75	1.18	F-105	\$1.07	3 0	93 to 1	75, 901	27 J 00	* 99 11	, x01-	x 46 .	1996-0	4.8 (0)	A.A	VA.	NA.	_
	- 01	84.5	-17	5 1 7 08 1 73 5 6 6	111	130 1	881- 11°	95 01	01 0	5 ( ) ( )	8.95 and 5.86 and	25 Mg	5.88 0	4.0 H	27 J 1 30 1 25 00	5 (00) (1)	\$6 m	AA AA	AV.	VA.	+
	16	81.5	-17	1.0 5 60	15.5	185	581-115	5 02	202 0	16.1	50 40	-5 %-	119 0	1.0]-	159-00	26.6.0	3.15 (0)	NA.	NA.	NA.	_
	- 11	p3 ×	-35	15.5.0	1513	.1	36.115	9.95 01	11 0	5 86 1	6.28.401	4.28 00	106 1	DI:	3 35 (0)	5 '56 11	\$ 000	AA .	AV.	- VA	
ZIIV 39/1/C	100,	10, 5	21.5	5.22.2007	, (3)	8 05), 02	2.130, 142	1.296.12	1.325, 00	2170.00	+ 211: %.	3.990,00	. 8.1; 00.	, 59%, 100	6.511:01	1.780, 00	2.16.55	6.39(1).2	. 157, 141	1,321, 6.	MW-39-
	900	.14.5	2.3	87,207	11:24	3 010, 40	156 (C 676 (C	. 881, 00	17.1; 0. 9.88(-0.	\$50,1004 8300.04	5.95], 01	7 (A)(1), 7 (C)(1)	3.350, 00	3 (0); 10; 2 (3); 10;	2.978.00	\$ 7585 HG	2280, 00	NA NA	VA VA	VA.	+
	01	1.5	2.5	13.5	13.55	5113	69E-02	2.15 02	5 K (0 m)	5 (80.1	95 and	400 00	263 0	3 00	188	9 1: 11	3.45 (0)	- 1:	1 5 10 00	181101	+
	105	1.5	25.5	[11.55 Aug	13.55	1.68	K31-117	20 02	33 11	80-1	5.92 (4)	65 ls 1	618 0	5 50	- 3 F 0	55 (6.0)	5.55 181	AA .	NA.	- AA	<del></del>
	16	1.5	25.8	50.710	15.38	2.50	231-112	8 02	2 (0 - 0	8 1 No. 1	63 40	-8 Jr. '	80 0	1.181	1 90/- 100	5 70 11	38 101	AA .	AV.	NΑ	
VW 59 121	100,	15	25.8	11 5 2 - 9 5 2, 230	13/12	16	1 19.,	395 H	*1 0 +24:55	9.10,00	1.86 1065.00	2319 mi 112d	6.91 0	5 80) 101	25.2% (in 2.5d) of	15L at	5 5 00	NA ESS. att	NA L. B. m.	NA 1 39: 01	MW-39-
VIV 39 121	90	121	11	87.207	13.15	1921, 42	731: 112	1.816.02	576E0.	8 57 E G	5 (3), (0)	115, or	2.910.00	3 (A) (10)	1971.44	3.75 (G	3.6,1,00	5.55., JH	VA.	VA VA	W VV-39-
	9.0	12:	ii ii	1 12538	15 15	1 671, 12	646.00	. 730, 100	. 181, 101	97,1631	8760,00	6.551, 64	2.610, 50	3 (00): 101	1.851, 1.1	2331.00	2.5%, 00	NA.	VA.	AV	_
	201	12:	ii	130,2008	1821	2 150, 42	5.808.00	. 530, 00	. 76, 90	0.003(33)	8.9.17.01	1.230, 000	2 130, 50	3 50); 55.	5.871,03	2.95.00	38%, 00	31: 61	. Ch %.	2.521, 0.	
	305	124	- 11	19, 22, 2008	1006	2,310,42	881: 1/2	2060, 02	9.328.00	9.000	\$60,01	, ((3)) (0)	66[], 10	7.416.00	1 (3): 00	+ 58h nt.	81.1, 00	NA.	VA.	AV	1
	0.0% 0.07	121	11	19 (500)	1. 14	1 980, 40 2 680, 40	50E (C	. 340, 00	9.950.	9.33E.0	5.050, 01	5 (SE 52 5 (CE 5)	\$160,00	3 (H; ))) - 55E (h)	1.550.4.	3.30E 00.	8285, 00	NA NA	VA AV	VA VA	+
VIV 39 183	100	182.5	102.5	5.22.200	12.59	2 177, 112	1.157, 10	1.295.32	9.511:5	8.985.0	5.53(-).	9 12°, 01	5.880, 00 880, 00	897, 101	3 (201:00)	1.581, 101	798, 101	5.067, 00	NA N/ SI	105.6	MW-39-
April 17 Day	10.5	87.5	- 15	8 10	12.1	138	31: 112	89 01	Part I	8 % 1	8.37 (0)	38 11	212 0	9 16	2.5 (0.10)	1566.0	5 B 00	AA	NA.	NA.	1839555
	113	87.5	2.75	1. 9	1.55	165 1	561-117	\$65.00	8 19100	5 Io I	287.00	-5 11	3.5[ 0	1571	0.05.00	3 35 11	5.5 (0.0)	AA .	AV.	- VA	
	- 01	87.5	2.75	15 1 8	1105	112	51-112	10.5	12 0	5.686-1	85 401	1.596.1	2.18 0	3 10	95 .	26-10-0	1 K 101	183 0	1.390-0	, 201-101	
	18	87.5 87.5	- 16	10.77.708	130	5 80	56-117	9 02	8 (Span) 3 (span)	586 T 6.656 T	6 40	-116 00 3 0 Ho T	688 0	91-	5.05 - 1	5  - 11	135 101	A.A.	VA VA	NA.	+
	100	87.5	- 15	15 1 9	1.5	985	3 24 11	98 01	1 par	200 F	8 10 40	64 0	6 1 0	5.1E	1300 00	5 10 11	[6 00	AA AA	AV.	AV.	+
XIV-40-105	100	g.	4115	5 25 5 11	7.08	235 112	180 *	1 331- 1	13 00	690 -0	55914	0.06	5 5 00	531 00	3.5 Head	116 0	189-0	-15%	9.681-	1.900	MW 39
	102	195	. 4	872.07	120	2000 2	2 10 02	85' 07	55900	6.230-1	5-55" and	-1 8H- 2	TTF 0	1 61	17. JP, 111	1.56(-1)	13.7 00	AA .	NA.	NA.	
	118	195	4.8	1 . 8	1.3	0.04 I	5-34- m2	\$1.07	8-3 (ca)	X5 to 1	8.38.30	5 + 1	108 0	5.86	815 - 1	5 529- 11	500 000	A.A	VΛ	NA.	
	00	195		13.18	16.1	* 1 *	5 F 115	2.00 (0.00)	N 100	55% I	8 % and 6 88 and	3135.0	5.5 0	5 115 5 905	1800	5.55.0	98 (0)	- 156F H	VA.	7.81 0	+
	100	195		19.100	1208	Io I	43F 112	18 m.	68950	66.15.1	1 401	-2.316-	865 0	3.36	- 35 O	1 ×  - 11	50 00	AA	VA.	VA.	+
	- 0	195		11.5.2.59	1505	110	9 451: 11	986.01	13950	factori	8.55.501	4208 ( 000	001,000	1911	- a F 50	8 E 00	9 (5 , 00	AA .	NA.	A.A	
178-1-5	100	4	16 ~	5 × 5m	1.0	46 H2	1.58	1336.3	- 8 Yeard	6.8 -0	8.50%	2 202	5 15 00	y 30 mm	18	190 0	5 10 0	AA.	'VA'	VV.	MW 40
	102	26	16 n	23.2	12.35	1.627 2	53F 02	, 66, 02 82' 00	3 (2) (a) 1377 (d)	5 8 16 1 3 30 6 0	5.62,501	2.526.0	1.7 E. 50	871: 10.	59 July 2	4 Sale or Tale or	186, 00	AA AA	AV AV	VA VA	+
	301	-6-	51.4	8 7138	13.1	11167 04	Solt (C	. 721, 102	3 mole III.	1,700,01	7.050,01	6480,01	2.285, 30	1005.00	3 *** 0	2.5-4: 10.	3835, 00	* \$*I; i.i.	1.4: 0.	2:31: 01	+-
	505	24.5	54.5	10.28.20.8	11.58	1 (2), (2)	8th (C	. 25, 10	1181; 0,	5.83(1)	9 150, 01	1.55;, 00	5 730, 100	+ 22h na	, 108, 50	9 89E 16	* 1,5, 00	6.281, 101	1 (4) 0.	1.831; 01	+
	0.65	-24."	54.5	. 5249	1429	1,000,32	34: (2	. 180, 00	1826 0.	0.30(3)	9.821, 01	4 251, 61	3.115, 50	3 864; 10.	1.565.06	2.508.00	3.580, 101	. 895 00	. 80: 5.	2160, 0.	
	597	24.1	59.5	1 1200	1517	1980, 60	386.02	. 340, 00	5980.01	1.856.13	5680,00	455.	74860, 100	1.57 E. 55	601[], 02	3.426.00	38.1.00	2 301: 144	1.826 0.	2 (2): 01	
	D166	24.7	59 S	1, 19 200	11.5%	1.5 E. 12 11 T. 12	546 (C	2140,00	2.076.00	10.5E.01	5 PG, 01 8 TG, 01	1.50E (C.	8 Mt. 50 15%, 50	5.56E-00.	2.536.00	\$ \$ \$1; (C. \$ \$3); (C.	5 880, 00	NA NA	AV AV	AV AV	+
177-1-16	100	26.1	20.5	5 5 500	130	12 02	1.58	1.566	-3 (ca)	5 8 1 au	X XXII-	9 40	5 hole 10	1 39 101	2.545 (0)	1 11 11	2.5 [6.0]	AA	NA.	AV.	WW40
	102	Rs.		19.1	12.15	9.18 1	55 115	0.5	45 (60)	55 lo 1	5.38.401	-0 XI	3.9 0	: 01-	. % 0	5 (- 1)	10 101	A.A	NA.	NA.	
	115	ю.		1.12.800	13.15	-1.500	526.00	1.07	+ 11 401	5 19 1	685 401	-5 × 1	3 7 0	1.501-	191 - 1	5 Ye ii	1.9 00	A.A	NA.	NA.	
	- 01	10.		5 1 6	13.12	-1 560	156 (C) 16 (C)	8 01	8 300	X SSE I	8 5 20] 806 20]	125.7	1.99 0	3.01-	1.60.0	2 sale ()	585 00	NA L II: U	VA.	. VA	_
	306	16.2		10.08.008	15.35	1.68 °	7.00	. 980, 00	65300	7 (2): (4)	7 250, 01	2 820,04	6580, 10	7 301-12	1 831:10.	- 30 m	1 RC. 00	5.300.0	. 16.5.	195, 0,	+-
	507	16.2	3-	1.0049	11.28	7.76, 61	331: 10	. 180, OC	20000	55,1551	5.670.01	8 (8), (4	2880, 00	3 301: 111	1,745,00	2781: 16	2880, 00	4 (3), 00	. 891: 5.	2.223, 00	_
	1166	16.*		3 200	13 P	14** **	3"1- 112	361.00	3.1.01	52 (41)	. 15, 01	113' 00	6367 10	1.501-11	2 22 11	37 E 06	135,000	4376 ***	15% 0	2.320-01	
	16)	16.		0	151	1.18	946.03	213 02	58 (60)	58 lo 1	6.03 401	403.00	bl 0	5"1-	. 380 0	5.5% 0	666-101	AA.	VA.	AV.	
Villar ad	100	16 .		1 19 Yes	110	5 1 1	1.50	985 H	958002	5 85 1	5 92 aug	49.9 Fe	1.75 m	5 00	1 95 00	5 % Sp. 10	5.6% (0)	AA AA	AV.	VA.	MW 43
· ((= : = A)	100	N		24.7	150	90× 1	536.00	1 250	15500	6 10 1	9 H5 6 95 ard	- 81-	105 0	5.50	2.511-100	58 (- 1)	195 00	AA AA	AV	AV.	B 27 4
	118	\$0.0	- 5	1 15 800	10.82	6.00	251-112	5 102	-9.05 at.	2.26.1	1 40	8.5 [6.1]	100 0	1.381	5 -	5 % 10	164 00	NA.	NA.	NA.	1
	- 01	8	+ 5	See	1138	ngs-112	1.616.2	811-002	18 1401	(ispa)	x 761-40	- 49p-	28.6 (iii)	138 (0)	- 166% I	1.1 E. G	\$50 to	A.A	NA.	M	
	118	\$0.1	- 3	X ' X	9.54	2 12 2	51-112	0.2	1.68(-a)	3.55lo. I	6.83 (0)	- X-I 1	160 0	* 81-	16 - 1	9.16-11	3.75 (0)	-199-11	00-	1.05 0	$\perp$
	0.00 0.07	301 T		15.28.2008	1, 25	3 (E. 5) 1 (E. 52	6.E (C	. 90, 00 . B0, 00	2.926.01	5.7654 5.7654	9.281, 01 9.531, 01	2000, 00	5 280, 100 3 620, 100	9.2 Hr. 10.	876C, 00	9.75h (C. 3.77h (C.	3 920, 000	2 380: 100	2.33(1.0)	2000.00	+
	0.6	S01		1 3 254.9	1 05	2.311, 12	5.8; 10	. 350, 00	3.355.00	9 (5) (4) (4) (5) (4)	8.177.01	126 (10)	7170,00	1786-10	3.785 00	19719 86	606, 00	Nr. 11	2016.5	216.0	+
	300	Ser -	- 4	12.549	1. 28	2 130, 42	586.00	210.00	2230.00	1351:11	5 (80, 01	7.786.00	1980, 50	4 501; 12.	2 di 100	5.50); 10.	5380, 101	NA NA	VA.	VA.	1
	540	\$0.1°	* 5	1,11300	13.5.	9111, 01	8.83); (1)	5.150, 01	. 580, 01	0.038.03	8.170,01	1315, 00	44,000,000	5.66.00	2.836.00	\$795.00	18.5, 00	NA.	VΑ	VA.	
AM 10 100	100,	100.2	2"	+3.200	.1.3	. 56, 62	1,610,42	1 5 15 3 2	3.90(1).	616,0,	9.5 Hr. Sc.	. 526 06	30.06.00	300,00	1980, 06	38%, 00	3.45(), 12.	NA.	VΑ	NA.	MW-/
	500	.072		1.23.2007 11.10.500	13.25	8 121, 51	55E 10	. 750, 00	25(80) 53(10)	9 (8E) (1	5.890, 01	1 of E.S.	3.577 (m)	2 (0): 55 3 871: 11	1,181.13	3.30 (0.00	2.200, 00	AA AA	VA VA	VA VA	+
	901	10.5		11.15.200	1 103	1.08 1	231-112	8 0	1 10 10	2,850.1	8.0 vol	3 304 1	44	1601-	881 - 1	3 3 1 17	286 (8)	AA AA	VA VA	VA.	+-
	306	.002	2*	4 31, 211,8	12 15	116.30	5.835.00	. 60, 10	1.980.	5-03:01	58,5,01	7.136.55	2 120, 60	3 381; 5.0.	8 730, 0,	2104:00	315, 00	NA NA	VA.	VA.	+
	90"	.002		8 . 248	16.15	1980.30	535.10	. 7.5. (0	3.150,00	288601	5.83[, 0]	81:5.	13%, 50	2 (61) 555	9.380.5s.	. 526 (6)	2.50, 00	0.90(, 00	. 091: 5-	1897, 0.	
	14.00	.502		10.28.208	1.30	8.660, 131	731: 102	25" 11"	1 30 0	0.3710.01	1831.00	1.55' 101	6.507 300	* 16.00	3.12(6.00)	7.035.16	8.637 101	17960	Solic 2	2.057.01	_

Tige of 21 See Fige 2, see Note:

Well ID   SAMPLE										BUCHANA	1, 11										
10   10   10   10   10   10   10   10	SAMPLE CENTE		SAMPLE ZONE CENTER.	SAMPLE COLL	LCHON							,	(NALYSIS RESUL	FS							Well ID.
1500   1500	depth if h		elevation It msi <sup>2</sup>				TRITIUM ( pC isl.	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)	_		Ni 63 (pCFL)		WHILD
540				Date	Loar	Result	Std Drs.	MDC	Result	Std. Dev.	AIDC	Result	Sid. Dev	ADC	Resulf	Std Dry.	MDC	Result	Std Dev.	MDC	
141   172   173   174   175	.003	12	27	1 3 7 10	1, 52	12 0. 01	30E (C) 50E (C)	350, 00	1 to 6 0 to 6 to 6 to 6 to 6 to 6 to 6 to	5 5 No. 14	7.250, 01 9.820, 01	6.30.01 2197.000	5.9%, 50	1.651; 1.1.	2.250.00 2004-00	3 , 5h (C	36,1,00	5 (60); (30) 3 (30); (0)	. 89h h.	221, 0,	-
MR 1012** 09, MR 1012** 09, 102 103 104 105 105 106 106 107 107 107 107 107 107 107 107 107 107	.00	2	- 3-	13.349	1. 3.	1765, 12	71: 10	2.180, 102	. 150,00	5 - 31: 1.1	1240.01	139:51	5.520, 101	+ 32 h his	1150.50	5 "51; 10.	665, 00	NA.	VA.	VA.	
We have yet and the second of	507			1.17.506	1030	- 11	9 : 31+ iii	5.85" (1)	0.8005	. 3 10/1	19/14/1	4 00' 00	3	5.7(6.5)	-190°-0	5.5° [+ 10"	1965 00	NA.	ΑV	VV	
101 101 102 103 104 105 105 105 105 105 105 105 105 105 105	127.7		51	+3.200°	.2.55	. 871, 02	1.620, 12	1 -31: 42	25000	\$150.00 \$150.00	5711:54	7,570,01	2586.06	3 H15, 000	5.59(.03	2.90, 50	3.295.00	NA NA	NA NA	NA.	MVV-40-12
10   10   10   10   10   10   10   10	127.3	2	- 51	1.17.20	.5.3	126.00	1.10, (2.0)	1 (8E )2 61 07	1 150	5 150 Pc 1	\$736 to . 6.75 and	2.7E 00	3.90 O	, 7/0, on	2.5 (6.0)	1.592, 304	3 9 mm	NA NA	AV.	AV.	WW 40.12
10   10   10   10   10   10   10   10			- 21	1.10	12.3	9 5 0	580-115	9 01	5 160	6 K str. 1	74 401	6.25 - 1	111 0	7 15	3.73 - 1	1.50-11	189 (0)	NA.	AV.	VA.	
18		4	-51	73.7.8	150	4.1	9.50-0	65 07	-185 -01	53.16.1	568 201	6.9714-1	2.14 0	1.14)-	1.80.00	2 p. 0	465 (0)	AA.	AV	AV.	
1999   150	,	1	-01	8 1 8	D. 35	168	35.00	95 02	1,65150	23 16 1	3.19.401	233.00	1.65 0	1811	1 . 1	386.0	2.8 (0)	-8 (t t)	1,650, 0	201 0	
5 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)		,		5,750	1 1 74	44	331: 10	. BC, 00	13950	16.1	8 and 5000.00	120,00	3.750, 00	5 881: 3 5 H; 55:	1 (8); (0)	8 286 0 3 mile 00	115, 00	330.00	. 851: 5	139-01	
17		2	31	1.3 (0.49)	1, 21	130, 10	376.10	. 340, 10	5.596.02	9.183	7.660, 01	100, 00	716, 50	1776 55	354: 00	1.580; 16.	175, 00	5.35.00	. 891: 5.	2.22, 0,	
Microbiole*   100	.2"	2	51	1 20 2009	12.05	175,42	581: 10	2.180, 02	3.381; 0.	0.305.01	11,000	3.306.02	60%, (0)	9 30h 55.	1.55:00	5.50.15 (10.	74,380, 000	NA.	Aγ	VΑ	
12 12 12 12 12 12 12 12 12 12 12 12 12 1	,	1	- 61	1 1 Yang	15.32	101 1	9.550.00	989 01	163000	6 986 T	95 301	35 0	5.78 11	5.300	as Qs arr	5 8)- 0	6.66 (0)	AA AA	ΑV	ΑV	
201 206 206 207 208 208 208 208 208 208 208 208 208 208	16	_	-46 h	5 - 501	138	2.80	1.56 °	1516 2	1916	1.356.1	5 16	- 5 F 0	5.550 00	5 JS 100	3.89(-0.0)	168 0 356 0	159 00	NA NA	AV AV	NA NA	3897 4C 15
201 206 206 207 208 208 208 208 208 208 208 208 208 208			84.5	1012.50	12.85	118 1	10h 112	69 11	25 JK 217	61161	K19 an	4 11 00	11 0	3.86	- F 0	5 5 1: 11	3   101	NA NA	AV.	NA.	t
1500   1500			88.5	. 208	1410	1985,	Note 10	. 82 0.	98.02	425 Mg all	1 [8] , 0]	Level	_ S on	28 1:	s ost, and	2.546.06	2.00	NA.	NA.	VA.	
150°   150°	.41	:= I	88.5	8 . 25.58	1. 1:	2,300, 62	58E 02	. 180, 10	7736.02	4,363	18.1.01	6.251:01	2 131, 100	1,66,55	3 .51: 00	2076.00	11.1.00	\$25, 50	. 221: 1	216, 0,	
158	.41	- +	88.5 88.5	10/28/2008	1315	1 100, 40	331:10	. 940, 102 BC, 102	2 80E 0. 1 32E 0.	5 04 G	5350,00	2,000,000 3,588,00	5 8 E. 100 3 321, 100	9 25th 101	2.31(.00	2.50E-00	3 1.1, 00	3, 76.00	1.850.00	200.00	-
2500   1500	.41	- +	88.5	1.3240	12.24	1 (2), (2	371: 102	. 360, 10	3.280:00	17053	5 (s), (d)	2830, 00	5 8 E. (0)	3 801: 144	6 150 00	3 8.1: 10.	106, 00	2706.00	1891 0.	2.76.01	<b>!</b>
\$\frac{\text{VW} \cdot \text{3} \text{ or \$\text{VW} \cdot \text{3} \text{ or \$\text{3} \text{ or \$\text{3} \text{0} \text{ or \$\text{0} \text{0} \text{ or \$\text{0} \text{0} \text{0} \text{ or \$\text{0} \text{0} \text{0} \text{ or \$\text{0} \text{0} \te	.91	-	88.5	1.5.549	12.5"	100.30	525.10	2140,00	1 (2): 02	1.295.14	5.170,01	2.20(5).	5.750, 000	9.311; 55.	1.5 H; 00	5 15 10.	6.5%, 00	NA.	AV	VA.	
ot     ot			88.5	1117.206	1515	2.870, 01	8 521: 0.	5/802, 01	1380.01	0.085.01	8,270,01	9.751:01	3700,00	9 3715 333	3.99(10)	5.13[5.16]	627), 00	NA.	AV	NA.	
101 105 106 106 107 107 107 107 107 107 107 107 107 107	311		20.5	1.0206	100	7 266: 02	2,070,02	1 560 1.2 86 0.1	2637, 16.	7 (p. 50) 1 (b. 0)	56°, m	2.5H± 50 4.85± 0	2 (2)(0)	3 (31), 101	581:01 - 68:00	235, 00	27 11: 00	NA NA	VA VV	AV.	NVV-41-40
100   100			1.5	6 11 0	95	0.0	2   1   112	2 02	579 0	6 8 8 6 T	53 40	53.0	100 1	91-	9 12 - 2	9 12 11	102 01	NA NA	AV.	AV	+
10   16   16   17   17   17   17   17   17	311		2.5	11.0	8.35	983	1646 1	200 002	0.0	183 0	1.00	1100	1.90 1	541-	2.5H: 00	1: 0	59 01	NA.	NA.	NA.	
10   10   11   11   11   11   11   11			3.5	8.5 5	1515	11 '	5N+ '	98 11,	NA.	NA.	AV.	40 . [	681 "	8 81-	- 1	5.351-11	5 (0)	AA .	ΑΛ	AV.	
192   110   111   113   114   115   115   117	411		* *	1.13.206	12.89	128 2	481-117	3 11"	361 0	× 10-1	5.9 =01	8 06-1	8 11 11	5.90	1 91/- 101	59 F 0	\$11 (0)	3 (4) (4)	8   D   0	6.50)- (0)	
10 11 11 11 11 11 11 11 11 11 11 11 11 1				8 11	13.85	101 1	\$76.00°	36 02	596 0	1.18 0	16 au	23.00 00	112 0	1.101	1.50(00	1 X (+ 1)	10 00	- 1 I	NA.	1 10 m	
17 13 11 14 17 17 18 11 18 18 18 18 18 18 18 18 18 18 18	311		* 4	21.2 8	16.78	. l e	8 F 102	93' 0"	3115" 11	107 0	* 50° and	267.0	7.66" 11	2.211-	-5 [8, m	2  - 11	2.187 (0)	NA.	VA.	NA.	
13. 14. 15. 16. 17. 17. 17. 17. 17. 17. 17. 17. 17. 17	311			1 27.746	13.19	1.1	%H ,	20, 0,	591 0	1.10 0	5.5 (4)	4 P.O	644 11	felt	. 5 Selle 181	8 5 St 11	× 1 (0)	AA .	ΑV	AV.	
11	411		1.5	5 5 100	15.86	61 .	9 E 02	5.75 07	5.88 0	111 0	5 88 and 00 and	5.75 iii	3.7 0	1 ×61-	16 -	5 1 F H	\$ 6 mm	AA AA	AV AV	AV.	
107 108 108 108 108 108 108 108 108 108 108				1.10.206	11.15	61	15 15 15	485 OI	200 0	1.10 0	806 an	- M-	120 0	5.86	2.30.00	16% 0	1 1 101	NA NA	4//	47/	_
101 201 204 204 205 206 206 206 206 207 207 207 207 207 207 207 207 207 207	29.2		-16	1.1.106	1.15	0.702	114	1.536.03	5 B 00	3.3 p. 0	160 00	5.98 -01	2.2 (4.0)	187 0	- s ×61 1	168 11	5 80 0	NA.	NA.	NA.	MW 41 83
151     152     152     152     153     154     155	×0 ×		-16	2 22 5 B	10.2	3.61	3 p. 113	475 117	5.77 0	1 54 0	1.00	9119-1	963 11	511	3.5[]- 00	8 F 0	10 01	AA .	AV	AV.	
1500   1500			25.4	4 22 6	11.05	2.68.7. 2	6.10.00	. 52., 02	8 Infort	5.286 (1)	586,501	83571	8 0,00	0.550	2.,26.0	50.0	8 24,700	NA.	ΑV	AV.	
1500   1500	59.5		5.0	7 8 3145 8 6 3445	13.00	3.560, 60	95E 92	. 920, 00	2170-00 NA	NA NA	NA NA	3 (10), (6) 3 (6): (6)	9 (9), 30	11: 5. 33: 5.	. 730, 6.	8 0.015 FG	8.750, 00	NA NA	VA VA	VA VA	
150°   150°			444	1, 13 300	13.15	130, 12	350:10	. 365.00	206, 00	resident.	5.665, H	146, 00	8121, 50	5 Tol: 55	0000000	4 0.6 06	660, 00	300,00	910[: 55	1300, 06	
599   141	59.5		4.0	42.20.7	1, 05	5 521, 12	57 h + 02	. 800, 02	1080, 00	1.280, 00,	5 2°1, 01	3.565.	2,370, 00	2 (8): 10.	1.060, 02	2330 00	248), 101	1356.00	. 24: 5.	1.180, 0.	
130 11 11 11 11 11 11 11 11 11 11 11 11 11			5.0	8 + 2007	1e 15	5 FG. 30	23.46.02	. 94. IC	1550, 00	94.26.41	\$3.0.01	2830, 00	3.100, 50	3.206 (4)	. 321.5.	\$ 585 FG	3.871, 000	NA.	AV	AV.	
H 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18		5	10	15-22-268	12.31	3100, 12 6910, 12	2.79E (02 3.73E (02	2.930, 02 5.920, 02	\$760, 00 \$600, 00	1.13%, (c. 1.13%, (c.	8 220, 01	2760,00	3.330, (a) 5.590, (a)	. 89E 55	5.230,52 5.030,50	1.64E-00.	188, 00	NA NA	AV AV	AV	
14   15   16   17   17   17   17   17   17   17	39.5	2	-16	1711 0	1235	5.76	85E 02	84 07	108 0	8836.1	13 40	1.96-1	680 0	1546	1 27 5 100	1 (8) (1	195 (0)	AA AA	AV.	NA.	
VH-23/29 00 00 00 00 00 00 00 00 00 00 00 00 00	V() V		-16	11.1.0	13.13	1.10	1,600,000	1.76 (0.1	26 0	× %-1	5 6s and	-x 'x	3 (91) 11	1851-	28.88 (20)	3 75 11	4.4 (0)	A.A	AV.	'VA	
00° 200 201 201 00° 48 00° 10 11 11 11 11 11 11 11 11 11 11 11 11	NO N		-16	1 10 506	1115	180	5 E-05	39 nj	529 11	9.586- T	5.92.401	0.0	464 0	3.206	-165 -0	1.450-0	18 00	NA.	VA.	VA.	1
201 97 98 100 11 11 17 14 11 15 20 20 20 20 20 20 20 20 20 20 20 20 20	116		. 1	6 16 1 10	1.5	, 10 4	5.60 °	- 20 H	813 OF 210 T	9- 0	1300	E 75 5	10 m²	1 01-	2.396.04	1.8.1	2.5 01	NA NA	AV.	AV.	MW 42-49
201 97 98 100 11 11 17 14 11 15 20 20 20 20 20 20 20 20 20 20 20 20 20	12.6		2".	13 T 5	17.52	2 510, 13	1 886: 02	7.370, 00	106.32	2.160, 00.	5.6 ×01 5.050, 01	81.0.00	7.080, 32	. 411: 42	8 811: 01	2 521: 10.	1275, 01	2 22E 13	. 701: 4-2	58 E. O.	<del>                                     </del>
10 10 11 11 12 12 12 12 12 12 12 12 12 12 12	12.6	6	2".	4 8 Cm.	1500	130, 13	\$10.8 (C	3.70,00	1.780, 04	[11]E, 16.	9000,01	, 950, 06	1850, 13	. 311: 5.	129:00	37,15 (6.	1821, 00	1.038.03	1531; 0;	. 411: 01	
10   11   17   18   14   18   316   317   318   319	15.6		,-	0.5 50.5	15.15	, 10, 13	, 8, F. 11,	98, 11,	1631 11	31" ir	502,01	3.657 115	311, 13	×31- 1	1.50(-11)	15E-17	3.6 , 101	1 -13	163E-0	884-101	
11 12 13 14 14 15 16 17 18 18 19	110			2.2.8	16.1	141 4	5 55 H	115 07	331 1	151.0	9   20  5   8 20	9.58 (0.5	103 3	3.6	1.596.00	5 SE 0	5 [5 101	5 116 2	51 July 5856 0	1580-01 1 00-01	-
17 13 11 15 16 16 17 18 18				81,06	15.55	316 3	2.650-002	9 10	5.95	1 5 0	5 [8 30]	16 16	613	506	48 1 205	25000	15. 101	3 3)	2850-0	20100	1
111 18 316 317 318 319	1.0		,	0 = 1.06	15.65	132 1	8 (6) 11	518 115	966	198 0	\$107,000	3.5 0.1	148 4	1586	NA.	W.	- VV	16"	* p. o	5 30 01	
18 516 517 518 519	116		,	1 31 746	15.5	191 4	5 1- 115	61 11"	961 T	131 0	5.15 (40)	8 10	1.58 3	×41-	586 -	5 (5)- 11	× 101	. 11	1 30 0	1-30-01	
016 017 018 019	116		` `	1 1 70%	1156	126 (4	101E 7	40.002	107 -107	5.086 0	1.56 (0)	541-064 8 05 - 05	156 mi	4 (0)	3.76 at a	5.70 e.e. 5.70 e.u.	5 60 00	1 J4 01 1 0 - 1  - 1	STORE T	strik an	1
517 518 519			N*	1 6249	14.55	7 221, 141	1.31: 113	1,442,102	5890, 12	8.571, 10.	7230,01	, Id. 05	3000.01	2306 5.	5 231: 101	3.500.00	2.171, 000	1.66.3	1531:0	200:01	+
519	12.6		2".	1 7 25.69	1, 03	2 221, 13	324.10	. 870, 102	2.581, 12	6630, 10.	\$ 670, 01	8 631, 111	1860, 01	3.216 5.	2 (81: 00)	1976.00	5.750, 000	9.66.12	116.00	2.96.01	1
	12.6	6	2" .	8 S. 7539	12.00	1.0% (2	2.25h: 10	. 75, (6	1831: 00	10%, 16.	5,300,00	5 (2), ((3	1310, 32	9.576 (0)	28: 100	1805.00	1600, 50	1 set; 14	2 371: 0.	2 381: 01	
	12.6	6	2".	19.27.2006	14.31	175, 43	2.2.6.02	. 671, 02	. 915-34	2000, 10.	7 (60,01	2 10, 00	1.830, 43	, 9H; 5.	166,0,	1706.00	5170,000	1.810, 00	30.11; 5.	2.115, 00	1
	1 3	-	13	3.21206	17.58	. 280, 03 1971, 67	5870, 10 1346, 10	5.75E-02 7.300, 00	309E0. 103E0.	3 80 ( , 0 ,	3.981, 01 3.981, 01	1.50[: 03	. 30E 02 1190, 32	2 121, 01 3 ,31; 5,	2.39(.00)	2.356.00	2385.00	NA 3 (6): 14	NA . 190, 14	NA 1 (3), 0,	MW-42-7
5/3	1 -	-	13	5.7.2006 6.8.2007	11.58	3.780, 10	88E 02	. 880, 00	3 831:0.	3 (8): (1 5 3 (8): (1	3.980,00	98E 03	1.1%, 32	3 (3); 5; 4 (1); 55;	2.335.00	2.35E 00 3.0E 00	1067, 00	2.986.55	. 101, 14	1.325, 0.	_
206	1 -		13	To a feet of	13.74	1317 17	54:10	95' 10"	2330.0	315611	3 13' 10	3 ((4) ((2)	3.115.71	1711-11	3 05 0	\$1.5E 16	518, 101	6-86° 01	131 11	1 0	t
	1		-7.5	1 1 1 8	1135	3.16	85E-115	08 m²	27.5 (44)	68 16 1	937 40	080-02	1.85 1	5 521:	- 1	3 3 5 5 11	3.65 (0.1	9 3)- 0	1.176	5.8.0	
0.00		<u> </u>	13	8 1 206	1200	6180, 60	84: 02	. 9.0, 00	35,100.	2.576.01	3.740, 01	27.1: (6)	2,020, 60	3.751; 144	6.115.6.	2.06.06	3,5%, 00	1370.01	1 521: 0.	2:81:01	
510 511			13	15.31.208	13.34	3.650, 10 3.650, 10	2.26.02	200,00	1,76.02	35,1551	3 (87), 01	3.310.01 6.700.01	3.321, 10	9 3 Hz 144	8 321.44 1 891.44	9.726 FG	3961 101	3 role to	. "T: : VA	2 (2), (), VA	_

<sup>1</sup> to 8 950 L 860 - 8500 NG 2000 - Quarte 3 Libbs Table Signation 3 Ferroacted VIV. sees. Make Libbs

										BUCHANA											
	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE	SAMPLE COLL	LCHON								NALYSIS RESUL	. FS							l .
Well ID	ID	depth it below top of casing	CENTER, elevation B mst <sup>2</sup>				TRITIUM ( pC isl.	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			Ni 63 (pCFL)		WHI ID.
		top or casing		Date	Loar	Result	Std Des.	VIDC	Result	Std. Dev.	MDC	Result	Std. Dev	MDC	Result	Std Des.	VIDC	Result	Std Dev.	VIDC	1
	:12	-1	1.3	1.12539	D. P.	2.16, 42	881: 10	. 850, 02	1671:00	67,91,91	1 (5), (4)	, 6ds 06	5.851, 101	3 (90); 133.	50.04	Voids (C.	114, 00	6.505.10	. 71. 0	246.00	
	513 514	-1	1.3	8 1,21,9	12.15	5 190, 42	82E 02	. TKC, 102	556E0.	6.30E.0	9 730, 01 9 731 01	4570.61 156.00	3.00,00	3.5 Hr. 55.	8 TUDGE No. 100	33,6 (0.	370,00	5 (2); (C. 8)	1.985.00	2 321: 01	
1777-13-76	1002	*3.5	74.3	1 06	2.56	3 1.1 02	120 12	1.99	5.000	7 (0.00)	8161-1	- 130 m	2.526.00	2.5 F 101	6,7.77	2.21.30	2.3, 10.00	NA.	VA	N/A	MW 43.26
	115	14.5	5.1	5 55 ° B	121	1.50	× 51- 11"	89 01	262 0	189 0	1 F	-8 5 de-	91 0	4)-	4 44 40	9.19-11	1.06 - 01	NA.	NA.	AV.	
	301	23.5	253	9 2 256A	12 15	2,300,32	:21: +2	. 320, 00	1.35(1.0)	4.276.04	5,270,01	2.841: 00	6930, 00	7 8CH: 144	1,550,00	5.53E 00.	6,3%, 000	NA.	NA.	NA.	
738, 13.28	1115	23.5	25.3	7 2 250%	5.10	. 160, 10	1.890, 12	1.55E-52	1155, 00	. 658: 50	1 720, 00	2 (1): (2)	5.87E-00	. 111. 13	7,981:01	8.580, 00	50.15.00	NA.	NA.	NA.	MVV 43.76
	190	1111	*** s	8.6. 9	121	160	×31- 1	1 01	- AV	7/A 7/3 (5) [	NA 186 art	5 T + T	8.13(-0) 8.13 (0)	9.56 201	25 16 2	33 5 0	\$ 900- \$ 16 000	NA Calcum	VI.	AV.	+
	16	114	14.5	8.5	1.35	9.56 1	Jr. 112	05 02	49.75 401	5 16 1	1.36	- 101-	3 - 11	1081	7 .	3  - 11	\$12.00	NA.	NA.	VA.	
	160	13.4	19.5	50.0	1.1	316	1876-01	108 07	1.3960	6.66.1	38 201	880 0	116 0	1.001-	1.365.00	25 (4.0)	C115 101	\$ 516 0	1.86.0	50E-01	
	510	23.5	25.3	15.31.308	1117	2,651, 12	581: 12	(w), 02	.081.01	3.55[:13]	5760,00	\$1075, 16.	51%, 50	9.3 Hz 55.	1,198,00	+ 2.E + 0.	6.63], 101	NA.	VA.	VΑ	
	511	23.5	243	1 7 2049	12.14	3110.30	65E 02	. 5.0, 00	2.150,00	5 mig (d 4 , 30 (d)	5 (6), 01	3.40,01	3 931, 50 60 ft, 50	3 1/8 (- 1.1.	1.315.00	3 (4); (C. (23); (C.	3.77), 00	NA NA	VA VA	VA VA	-
	13	13.4	25.5	1 10 206	13.1	1 3 1	9 70 00	966 01	15 1502	5 96 1	6.54 401	-5 No. 1	386 0	1.781	2 10 000	3 50 11	105 (0)	NA.	AV.	AV.	+
178-1957	1015	- 5	.**	1 1106	1.55	211 112	1.65	1.580	3.5 Ho	163.00	1880	3.24	5 Sp. oc	9 5 181	8.5	\$110 11	5 f 10 0	NA.	AV.	NA.	MW 43 50
	118	81	25.5	12, P	12.3	121.2	p. 115	85 05	8.29(4)	161 0	1 P	4.31.00	1.6.1	sol-	25 p. 0	3810	102.01	NA.	AV.	NA.	
	316	81 81	2.2	6 ' ' 6	12.1	1.50 °	5 (F 105 5 (E 102	88 07 , 68, 11 <sub>2</sub>	1.900	5.586 - 1 1.16, 16	5/85 (40) 1/8/15 (40)	10 p. n	1.10c, of	- 581: - 501:	-681 -0	31- 0 - n-1: 0.	85 00 1101	NA NA	VV.	AV.	
	306	51	33	8 5 2556	1, 55	1080.00	671: 1/2	. 760, 00	VA.	VA	VA.	2 230, 64	5 (5h 0)	. 40E a	1951.5.	8337.01	9 365.	NA NA	AV	VA.	+-
	507	51	2.2	6 9 247	934	1970.12	881: 10	2 (2), (0	8 551: 0.	58E: 1.1	+ BL 01	977E3.	3 210, 50	3 Ch to	8.521.44	3 .54: 05	3 250, 00	1 385 00	. Ul	1350.00	-
	0.8	51	2.2	8 3.2507	12 12	1110, 32	735.10	. 921, 02	1.2%: 0.	6.5045.04	8 270, 01	11K. 00	3.651, 101	3 801: 111	. 530.44	3.3,1; 00.	3.802, 000	NA.	AV.	ΑV	
	0.00	.51	2.2	1.25.2008	16.57	1,030,00	7.95 (0)	. 930, 00	.000,00	9.078.01	5.520,00	130.0	2 (2), (0)	2 391; 101	E 30	2076.00	2 100, 000	3.76E-00	1078.00	190.0.	
	510	51 51	2.2	10.31.2008	13.5%	1.10,40	50h (02 13h (02	. 640, 100	1.57E.0. 689E.0.	1 , 31; (d) 5 880; (d)	570,01 590,01	3 (5)(1.3	615), 50	4.56E-555 4.0E-555	2.99E 06 1350.00	9 30E 00	1/22, 00	NA NA	VA AV	AV.	-
	311	51		1.3 (550)	12.52	118, 30	545 HZ	320, 00 397, 00	689E0.	5 88E G	3.500,00	8 201 5	5167, 00	\$ 1015 till.	2.267.44	7.251-10	6.375, 101	NA NA	VA VA	AA AV	+
	13	- 51	22	1 10 206	1202	1.96	1-10	981 01	21 0	16.1	6 5 401	160 . 1	216 0	5 11:	-18 -0	5535.0	× 0.1 (m)	NA.	NA.	VA.	<b>†</b>
178-17-56	101	62.5	31.1	1.8.1.00	1.5	5.38 (17)	191 '	1.31/-2	80.0	585.0	16	5 % 2 001	56.00	1 01	2.8 0	102 1	SIL II	NA.	AV	AV.	NW 44 5
	11.	611	,	4 15 1 B	9.5	14 1	\$ 15 m2	0,5 11,5	5 [60]	3 16 1	5 [5 30]	-5 F-	80 0	9.501-	1850 00	9.51-0	11 01	NA.	AV.	VV	
	- 118	61	,	6 N .	1.15	8.07	3 5 p. 115	85 07	-1.5 -01	386-1	1.51b god ant	5.85 iii	3 1 1 1	9.50h	6.15 .	11 10 11	\$ 16 mm	AA AA	AV	NA.	
	108	9,1	,	8 11	13.1	11 '	361-11,	20.02	9 ( 100)	- N- I	3.3.40	-K d M	191 0	5.81	-1 30 -11	3.5 (-0.0)	3   101	NA.	VA.	AV.	+
	161	61	1	1.31.50	1113	514 1	X3-105	8 07	4 (4)	3 16 1	1.1 40	1.5.0	1.9 0	1 811-	1.90 00	15 F H	1 00	NA.	NA.	NA.	
	10"	67.1	3	21.7 8	12.55	2011 2	5 July 105	2.15, 02	285(14)	1.53(-) 1	1 Oy' and	731- 0	134, 11	2.311-	1.50(0.00)	3 75 0	2 (31 (0)	NA.	NA.	AV.	
	16	6,1	1	15 1 8	1 1 36	Let ,	St. 115	98 07	1 1602	4.66-1	86 401	-8 No. 1	106 0	1 181-	∜15 - I	2.00(-0)	12 000	NA.	NA.	NA.	
	10	9.1		1 3 3 9 8	1518	3.18	2.55E-02	5 5 H2	4 par 12(a)	5.550+ 1 5.850+ 1	5 L au	21.88 mm 23.70 mm	283 0	5.905	2500 an	5 35 0	585 00	AA AA	AV AV	AV.	
	11	6.1	,	14.100	9.1	106	975.00	0 11.	15/150	980-1	X 95 20]	991- 0	454 0	1.80	5 Q)- 11	3 51: 11	112 00	AA AA	VA.	VA.	+
	12	63.1	,	1.96.0.0	11.51	3.10	581: 11°	106 . 00	1.3 [ca)	Lastest 1	5.59.501	- 1 (-	6.9800	1.56	4.81.50	1.198-10	19.,00	NA.	NA.	NA.	
	14	61	,	91.0	11.56	11 2	3 B 03	\$66.00	65350	6.16.1	808 201	881.7	601 0	5 01	1.80(0	5.58(-0)	669 (11)	NA.	- AA	AV.	
ZBV 11 DC	111	62.1 80.	13.5	1152.0	16.2	150 2	2010, 62	9 01 1 769: 02	\$2460. 3.5300.	4 [c.] 998 H	6 4,501 1.757 HH	3.226 (6)	8 feb. 0	50h	800.000 77.1604	1845 O	8.575.10	NA NA	AV.	VA AV	WW-44-10
210 11 DC	900	80.	3.5	6 3 526	16.55	316, 32	821: 1-2	60.00	3.350, 01	1 (6), (6)	1.296.10	25/0,00	9390, 00	5.831; 55.	2.3 H; 100	5 80E 00	5,350, 00	NA NA	VA VA	AV.	317.5-44 2
	9.0	(81)	.14	8 1 20%	9.45	7611, 12	2.304: 52	8.1.00	VA	VA	VA	15.95.00	8 165, 00	7.760, 500	200.00	* 0.1 E 0.0	9.826.00	NA.	VA	VA.	
	501	(811	,14	9 3255	1.35	247, 32	546.52	2000.00	VA.	AV	NA.	1,56,00	978], (0	21: 5.	176,5,	8 . 85 . 00	8.974, 101	NA.	VA	VA.	
	9.6	\$0.0	,15	9 5 2567 8 1 7567	11 19	2,980, 62	Tal: +0	, 830, 00	. 330, 01	58,1531	9.350, 01	. 881, 00	2.15%, 50	2 (31) (4)	9 1.1.5.	2 (2); (c. 2.7%); (c.	1.380, 000	- 12h (0)	. 316 5.	1.580, 0.	
	0.05 0.07	S01 S01	.15	8 12557	11.55	2 8 E. 32 3 5 E. 32	856: 02 Tel: 02	. 970, 00	1.57E.0. 2.5KC.01	7 (A) (A)	8.950, 01	1.46, 00 9.86E5.	2.76, 30	2.776 sa. 3.116 sa.	. 35E 00 . 23E 00	2.75E 0G	2730,000	NA NA	AV AV	VA.	-
	16	80	33	10.31.300	1310	331.75	199-01	196 07	1 (444)	5.66.1	6 (45 a)	181: 0	161 0	1.11:	-111-05	2855.00	31 00	NA AA	AV.	AV.	+
	16)	\$00	5.5	13.1.8	15.38	126	131-111	96 07	d harr	5 Pr I	[1 -0]	091-0	2.03 0	1646	25 B 0	5 10 0	185 00	NA.	NA.	AV.	
	10	\$0.0	3.5	57.8	12.18	13 1	1.350-011	3.5 02	2.88.207	Kalin I	3.7 201	-1 P-	1.8 0	1.8941-	1.38[-101	X 1: 0	3.1 00	AA .	- AV	NA.	
	- 11	501 Sur	3.3	1.13.500	13.18	1.5	680 m²	65 0°	1 par 166par	5.55E-1	5 15 401	9.0	6.11 0	1.11	2905 00	8 Ye o	8.1 00	AA AA	AV.	VA.	_
	513	501	3.5	1.28.2549	13.30	51 E. SC	821: 102	. 800, 00	370E0.	6 No. 1	8.031.00	9.46, 11	827, 00	5.511-10.	2670.00	5 ,81; 10.	585.00	NA NA	VA.	VA VA	+-
	911	301	3.5	125249	12.08	190,42	8:d: 10	870, 00	1336.00	+ 50E M	7.730,01	1 (2): 1/2	6130, 50	9.76E-14.	3.580, 0.	51.51: 10.	5 FG, 00	NA.	VA.	AV.	_
	115	80	3.5	1.5 *****	14.13	414	251-112	5.781.01	58950	7.000	812 01	0.15.07	4 *** 10	1.511-11	1.88 10	5"  - 17	165' 101	NA.	VA.	AV	
178-15-17	107	,	166	1.1 506	- 51	548 02		1 p 1	×80-	5.91 at	5.59%	1.916	351-11	51 01	-1 (8)-	125 1	V31- 0	NA.	VV	ΑV	NW 45 4
	113	1	6.6	6 3 5 0	9.35	187 3	5 31- 5	2.15 (02)	9 80-0	58.19.1	1.86	9 65-1	2.08 0	5.301	2511000	5.686.0	6 00	AA AA	AV	VA.	+
	- 01	3	5.6	1 6	9.5	119	. 81- ,	20 02	100 10	1.18.0	1.500	2700	81 0	9.516	232 11	387-11	15 11	NA NA	AV.	AV.	+
	115	3	5.5	8 ' b	11.0	316 3	55 F 3	5 105	NA.	AV.	NA.	-I I6 - I	N 100	61 0	-4.7911	1.50%	590.0	NA.	NA.	NA.	
	16		6.5	d 4, 11P	11.40	1356-114	316.0	8.5 Julio	AV.	NA.	NA.	. 505 (0)	7.826 110	\$100 (00)	-1 46F OD	× 40)+ (t	5 1 1000	NA.	NA.	NA.	1
	10.00	3"	5.5	1 13 506	15115	2 321, 13	981-112	1 02	5080.00	5 Is 1 9 25k (d	8.8 (a) 7.5(1.0)	1 22 11	S [0 0	1.501-111	2.800 000	5.9 H H	8 (	3.505 (2)	36 Je 0 30L 5.	5 (0) (0)	+
	0.00	3-	20.00	6.2. 2557 8. 5.2557	1. 35	116. 3	9-27E-02	1390, 02 , 170, 02	3750.00	0.28633 7.74633	5 (5), 01	1 311, 61 , 921, (G	2.76, 50	3 (1): 55	1.96.00	2 82E 0G	3.230, 00	2.58E-10	. 401: 1s.	1 195, 0t.	+
	510	3"	200	30.5.25.67	1, 05	2 221, 13	31.56.10	. \$60, 00	3.55(:0)	5.06.0	5.5%, 01	0.001:00	1130, 50	. 90E to	3.650,03	. 54h 06	22.5 (0)	NA NA	VA.	VA.	_
	:11	3"	29.9	. 25 2048	12.15	1.110.13	376dt 02	2.940, 02	2080:00	5 , 51: 1.1	9.030,01	, 6th (c.	2 130, 50	2 881: 144	5.960,04	2.3.1: 00	2790, 000	NA.	NA.	VA.	
	312	3"	200	51.208	1515	1.130, 43	5.1: 102	1,940,00	1185.0C	30,1804	9250.01	6.951,04	1980, 00	3 (T): (A)	1.7E 00	3 (2): (0)	155), 00	NA.	NA.	NΑ	
	513	37	200	7.25.2548	16.15	2,321,43	377E 02	3.740, 00	33,25 0.	275634	1 120,00	1.77, 00	176, 50	2.596.50	1 (8); 00 Vall; 10	, 76E 06	3 150, 00	NA NA	VA AV	VA VA	+
	111	3"	.00	10.22.208	11:54	3.1.0.43	8 0.3E 02 3 27E 02	5 (2,1), (0) (271 - 112	152E 0.	5.5511	8,250, 01 6,631, 01	1.60, 00	3.07), 50	5.25E 10.	375 50 275 50	2.535.00	139), 00	NA NA	VA VA	VA.	+-
	16	1	6.6	1 15 1 0	15.5	5 00 1	95 F 115	2.100 11	15 9000	5.335-1	5.08 40	-1686-	1.01 0	1916	1.39 0	1.596.00	18 101	NA.	AV.	VA.	_
	31"	3"	,44	121200	11.35	190, 0	3.500,00	23.17.00	5004:02	7.678.04	5450.01	1-30,01	5 250, 100	4 00h tit.	1.221: 06	3 (5) 16.	1180, 00	NA.	AV	NA.	
	:18	3"	,44	1, 10 206	13.15	2.900, 13	224: (2	, 05', 02	615.02	0.0604	160,01	1830.01	110, 50	4 , TE 100	8 125, 0,	4.4" E 14.	586), 101	NA.	AV	VΑ	$\perp$
73V 33 of	100,	58		11300	1 .730	2.960, 02	2.180, 12	2 231: 1.2	. 82E ii.	5.030, 0.	5 39E h.	800CH 555	48 00.	1 . 321, 01	I . B.C. 146	1 1 000 st	T Tk 0.	NA.	VA	NA.	NVV-45-61

1 age 8 of 21

IPEC00224888

See Page 2, for Netco

<sup>1</sup> to 8 stort 860 - 8669 May 2005 cannow tribles Table Squade (Formated MAC cox. Mane) that

$\overline{}$	_									BUCHANA	N. NI										
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLI, COLL	LC HON							•	NALVSIS RESUL	rs							
Well III	ID	depth if below top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			N 63 (pCFL)		Well ID
		·		Date	lisar	Result	Std Drs.	VIDC	Result	Std. Dev.	AIDC	Result	Std. Dev	ADC	Result	Std Dry.	VIDC	Result	Sfd Dev.	AIDC	1
	9/0	58	5.5	5.25.2544	7.5	1.710.43	3.57E-10	2,371, ((2)	5 (4) (0) 18.1: 0.	5 8 3 5 3 1	1 (3): (4)	176, 61	911, 50	1,126 to	5.351; 00.	1, 37% (C. 127%)	13.1.01	NA NA	AV AV	AV AV	+
	301	58	- 11	1 20 2004	12.5%	3 721, 12	88E 10	. 640, 02	5,000, 500	1360, 10.	1 905 10	3.986.00	5 (80, 10)	5 301; 111	1.336.00	3 Sels 16.	5 (2), (0)	NA NA	VA.	VA.	+
	1116	ck	-4.4	8 2	9.15	116. 11	*xx  *	9 102	VV	ΑV	AV	. 530- or	947 10	61- 1	18 33.75	6 th July	5 "5" (0)	NA.	VΛ	NA.	
	190	-9	-5.5	d 1, P	9.5	1.18 3	5 SH- 1	205 02	AV.	ΑΛ	NA.	45.550-0	1 00	5.27 0	.5 6 11	171-	5 K I+ 0	NA.	AV.	VΛ	
	10.06	59	25.5	1 13 No.6	12.55	1.177 (3	136 m² 3 (26 m²	1.00	5 0	5 Red 1	6 40	3.520-10.	150 0	3.571-10	23.7 (6.00	3.50 m.	3.650, 00	7.50E-0	66 to 0 1 35b to	901-000 - 711: 01	+
VW 15 of	10.6	58	11	8 5 2007	.1.35	. \$12, 113	1880.00	1.016.52	17 11:32	19(6.0)	9.416.6	3 331: 14.	1.25% 00.	197.00	9 5.11 M	386, 00	3 504: 00.	NA AA	NA.	- NA	MW 45.5
	100	- 1	-5.5	1057	1.3	*15 4	3 31: 112	57 117	18 150	5.286-1	5.46 401	- 46-	1.13 0	201-	5 % . 1	39-11	6, 111	NA.	NA.	VA.	1000-000
	- 11	-9	-111	1 % 5 8	1.35	100 1	18 (- 02	106 011	1.9950	5.86.1	6.7 201	2.126.0	Spir ii	1516	2505.0	1880-0	\$19 00	AA.	- VA	AV.	
	12	**	-111	51.506	11.16	2.9 3	8 1: 11.	95 02	69890	1,996-1	65 401	3.6 - 1	20 0	1-001-	- 19E 0	2.556.00	3.55 (0)	NA.	VV	- VA	
	513	.58 58	11	1 25 2008 10 22 2008	13.5.	1.800, 13	3.50E-10 33E-10	\$750, 00 \$560, 00	2.39E0.	2 (5): (4 5 82): (4	5050,01	1.885, 00	1.910, 00 3.070, 00	2.800; 100 5.301; 100	1.830,04 1.046,06	573E (G	3 (E), 00 638, 00	NA NA	VA AV	AV.	+
	:15	58		22.200	13.13	136. (3	324:10	. 970, 10	1.055.01	7 9 4 64	5 (5), (4)	9 530, til	3.5%, 00	1206 10	2.350, 61	3.23(: 0).	3707, 101	NA.	VA.	VA.	+
	16	- 55	-111	1350	10.5	1.16 3	5.356.00	516 H	4 1 44	5 16 1	816-311	-1 16-	11 0	1.81	1 30 0	2500.00	311 101	AA.	NA.	NA.	+
	1	**	-414	17.0	1.55	111 3	, 68-11,	1.79 101	1 150	K 36-1	89, 40	-5 YOF-	3.43 ()	1991	5.08 - 1	5 100 11	585 (0)	NA.	AV.	NA.	1
	18	*8	24.4	114, 0	11.55	13 3	- 11°	10, 11,	8.53pan	82464	5 5 40	-1564pc	× 90 n	5 00	-5 St 0	Sp. 10	6.05 (11)	NA.	'AA	NA.	1
1,47-39	4015	5 105	6	1 1106 224 June	12.55	910,	181 1 .E 08	6h 1	5.286 36.400	187 at 9 (86 at	1.00	3 % 201 2015 02	28 J. J.	3 31 · · · · · · · · · · · · · · · · · ·	5 881 06	88-E 0-	1 01	NA NA	VA AV	AV.	MV9 45
	3/8	105		5.21.2004	12.55	6230,12	224: 52	. 871, 10	VA.	NA.	VA	NA.	VA	VA.	VA.	NA NA	NA AA	VA.	NA NA	NA NA	+
	301	10.5		6.3.2556	13.1%	6790, 01	80.8: 10	. 9.1. (0	3.596.00	1000.00	1.33E (a)	2.580, 10,	7.280, 300	8 291: 144	9.795, 00	8.236.00	88.1.00	NA NA	NA.	NA.	1
	0.6	10.5		1 2 2554	13.23	1860, 62	2.346.02	. 920, 02	5771:0.	1.210, 00.	1 231: 14.	3.980, 10.	9370, 00	, telt 5.	1.99(1.00)	8 -81: 00.	106, 01	NA	VA.	AV.	
	306	10.5		8 12506	F 12.	1157, 13	2736.02	, 980, 00	NA.	VΑ	VA.	51: 10.	\$ 050, 00	14 50 h 10 h	3.400,000	5 801; OC.	\$970,000	NΑ	VΑ	VA.	
	507	10.5		9 3 2006	13.15	3 (3), 43	\$ 30E 02	2.1%, 00	2.50.0	1 - 51: 1.1	NA 5.350, 01	3 730,04	6011, 50	6.781; 555 6.371; 555	2.75% 06 8.520,42	7.27E-06	9.273, 00	NA . 1.51; 00	VΑ	1.785. 0	-
	376	10.5		81.200	1 34	662, 12	3.50-10	2 10, 00	7891.02	3 500 01	3 55 0	6-31-11	3.920, 00	3 80 (- 1.1.	0.337.00	2 (3): (6)	2 ***, 101	NA AA	. 521; 1-; NA	NA.	+
	10	Jus	6	1 22 500	111.1	16 3	5.5 [6.05]	30 02	1 100	1 10 1	5 15 401	168 - 1	10 0	3.511:	- 20 -00	1996.0	\$115 1111	AA.	NA.	NA.	+
	- 11	Jus	6	1 8	12.17	2 lo .	31-115	0.2	5.5 [140]	16 T	8 1 201	-35%-	'61 U	1811-	1 30 0	26 8 0	2.0 (0.1	AA .	ΑΛ	AV.	
	1.	Ju S	6	1818	16.0	8.91	235.112	5.5 (65)	1 150	35 Is 1	5.64 401	8 - 1	212 0	5 %	18 (1	2.256.0	50 101	NA.	NΛ	NA.	
	13	Jus Jus	- 6	1 50 506	16.86	1.88 4	5 SE 05 5 SE 05	5 07	1 State	5 16 1 5 856 1	51 40	6.5 - 1	1.96 0	5.80	- 850 m	5 July 10 5 SAME III	816 HI	NA NA	AV AV	VA.	+
	18	DOS.		18.100	11 15	100 3	, 881-11,	96 02	- 1 - 41	6.286-1	8, 40	-1.68 (0)	1 8 0	1 11:	107 -	2.8.26.00	3 % 101	AA AA	NA.	VA.	+
	16	DOS	6	1 . 0	12.3	*6	2   1-112	18 H	2 19 and	N 3814- T	561 40	9.63 - 1	5.58 0	4 19	1.5 Ib. 00	5.690-11	11 00	NA.	VA.	NA.	+
	1"	Jus.	7.6	* 1* 0	13 5"	8 377 7	2.245.00	23.7 02	5.75p.a.r	" yylo T	8.88, 101	- 1	3.071 0	3.50)-	2.3710.00	5.7(6.0)	145' (0)	AA .	NA.	NA.	
	18	Jus.	6	116.5 0	13.75	1.10 3	6 15 105	0.02	85 (a)	5 36 1	111.40	1850-0	6.2 0	50)-	-3 5h 0	5 % 11	5 8 (0)	NA.	NA.	NA.	
1,47-1-40	103	55.5	1.1	1 5 1 10b	10.13	P 05	95E-112	1.5 F 2 96 m²	13 (4)	65.40	9/15	4 11	5.556.00	5.35 (0) 6.51b	-3.55bs 1 -3.5 b 00	S 80 0	5 F 0 1 S 01	AA AA	AV.	AN.	MW 47.5
	- 01	54.1		6	10.00	5.10	55E 10	85 01	2 (4) (4)	5.5% 1	5.1 201	0.15.0	6.00 11	3.3.1:	5 x 1: 00	A 1: 0	1 5 00	AA AA	VA.	NA.	+
	- 01	×4 ·		6 5 5 5	10.0	N/A	NA.	AV.	AV	ΑV	NA.	10.00	1.28 / 20	1 91	1.69(-0)	3 E 10	3 5 , 101	4.811	1370	5H: 01	_
	115	×4.1		* .	1.0	2.00	881-115	202000	S [60]	8 36 1	89 20	- 5 × -	3 (8 0	3 31:	- 19 × 1	1996-0	4.4 (8)	AA.	- AV	- AV	
12/1/21 201	100,	- 4	.3	1.32.06	.138	235,00	1.28.7 2	2.298 2	2 5,700	English,	6.4814 .	2822 T	1.180 (6)	511, 00	2.25(40)	19],, 11	5.50 0	NA.	VΛ	- AV	NW 47 8
	900	- 1	3.7	7 8 2004	1,16	1870/43	3.87E-10	2.580, 00 3.580, 00	2860, 00	1 130, 00 8 58E 01	1 . H: 05 5 281, 01	2088 00	3.810, 50	1.985 M. 1.885 M.	2.39(10)	5 2.15 (G) 5 82E (G)	1060, 01	NA 1081.0.	81: 1:.	NA 1387, 0.	+
	501	-1	3."	6 5 2007 8 0 7007	12.2.	3.511 (.3	7.251: 10	4,520, 102	3,550, 00	1.210, 10,	5.050,00	5.354-1.2	3 210, 00	3.561: 10.	2.27E 00 8.200, 02	3 ,81; 14.	3.925, 000	NA.	VA.	VA.	+
737.38.23	100,	25.4		28.200	1,1,0	. 641, 102	3.260, 12	3 (2): 12	. 131: 5.	5.000,00	3 5 He 6 c	210.61	, 5.4E O.	. 130, 01	. 100, 66	995, 00	26: 0.	NA.	VA.	VA.	N VV-48-2
	9.0	201	· ·	1.22536	9.58	1,2,67,32	1086.02	1,520,00	. 165, 01	3.50E.01	1 (61, 01	3.25% (6)	9750, 00	1 28t; 14.	2.99(00)	7.476.06	6180, 00	NA.	AV	NA.	
	503	201	5	1.27.2536	13 12	2,380, 32	546.00	2 (30, 102	2.8(0.00	1.586:13	\$100,01	1881, 00	5.0%, 100	5 (5h h)	1195.00	1.08 00	5.271, 000	NA.	AV	AV.	
	301	201		5 22 2556 6 9 2 106	16.3%	7.850, 42	1246.02	5 Hd, 02	2 (2): 0. NA	2 88E G	3.150,01 MA	3.22E (C.	9.671, 100 NA		1291: 06	. 2'd: 0.	962, 00	NA NA	NA NA	NA NA	
	118	50.1		5.9 1.06	1.15	6116	1 401-111	6.75 07	4 par	35 In I	50 40	1.591-0	6 0	5-901-	3.29(-1)	9 9-11	6 111	1.600	1 (4)	150:01	+
	115	50.1		5.0 1.00	1.15	105	1.046.02	1.53 07	4 par	9 KM 1	1.761-	061-0	8.11 0	5.800	5 (8)- (0)	53 E 0	S Q5 (11)	NA.	VA.	NA.	
	181	50.1	-0	6.10	120	131 3	5 p. 65	185 05	4.7 (4)	3.5 (6.1)	19 40	2.88E-0	61 0	5 591-	*50b-00	SE 11	5 8 100	NA.	AV.	VV	
	57.6	201		8.8 5.06 5.5.200	10.05	2.10, 91	50E-112	. 721, 102	9160,00	6.3 to 1 Table 01	6 401	250, 00	1.6 0	5 56F	1.99(-0)	8 585 FG	102, 01	AA AA	AV.	AN AN	+
	509	201	,	1, 22,300	7.73	1.677.47	1085-02	1300.00	2160.00	904:01 305:01	7 157, 01	3.9 1, 10	82., 100 1.171, 101	8 (21) (A)	3 221: 00	8 48E FG	1757, 00	NA NA	VA.	VA.	+
	210	50.1	5	20.200	10.33	4 4 4 7 4	- est- 10°	200 00	61.01	137 0	1.506.11	3.70811	1.807 10	2006-00	8.5.	21.75.17	2.307 (0)	N.A.	NA.	NA.	+
	- 11	50.1	-5	8.61	1.0	101	6.00 (0.5)	6 01	2400 and	5696-1	8 [ 20]	651: 0	10" 0	3.7811	5.65 - 1	3 31: 11	\$55,000	AA.	- AV	- AV	
1745 - DC-4	100	55	- 515	2.0.2.06	1.0	F-10	1.9	1.36.3	AV.	ΑV	AV	80.0	3 5 1 11	154	2 100	5 1 F O	5.89 (0)	NA.	- AV	AN.	NVV 48
	115	\$6 \$6	-2.0	1 2 2 0	11.0	25.50	5 No. 112   10 Hz	2.82 (02	108 ar	5 % for 1	13 and 13 and	991-0	9.91 0	5531	3.5    0.0	8 1 N - 11	689 00	NA NA	AV	AV.	+-
	- 01	- 46 - 46	- 6	2 22 2 B	11.0	1.80	5 79 112	3 IS 07	106 20	3 SIG I	31 -01	350 H	108 0	1916	2.815.00	549-0	S11 101	AA AA	AV.	NA.	+
	105	- 46	-316	5.9.546	11.90	456-117	16 8 7	560 102	NA.	NA.	A.A	NA.	AV.	NA.	NA.	AA .	ΑV	NA.	NA.	NA.	_
	108	ib.	-1 6	5.0 5.00	1.3	~ 06 ·	141-111	5.75 07	1.560	×31 1	1 46	8-16-0	5.1.0	5 1 Hr	. SSE 0	5.5km	8.82 (0)	A.A	NA.	NA.	
	3/6	344	25.76	14.9 25.0K	1.35	1740,02	1ls (0	1,530, 102	2081, 10	1.504:14	1061.01	2 lide (G	1200, 00	178h (a)	1.46.06	. 236 0.	8.502, 000	1.581; 1.0	. 351, 61	1.16, 0,	+
	50%	36	25.6	7 6 2006 8 8 2006	8-15 10-25	1.0% (4)	55E (0	1,520, 00	1.75E 0. 655E 02	8 JOE 01 9 SQE 01	8 801, 01	2.15h (G	5.680, 00 5.680, 00	0.0 He 0.0 9.95 He 0.0	1.211; 00 2.950; 01	5.25E-0.	\$ 771, 000	NA NA	AV	AV.	+
	0.0	36	75.6	8.8.2386 5.5.7586	16.25	\$ 730, 17	2 . 21: 10	75.00	5000 DO	9 70 E M	7 742, 01	2 804: 10.	\$ 500, 100	9 (1) I (1)	1905.00	5 351: 10.	6.371, 101	NA NA	AV.	VA.	+
	300	36	25.6	1, 22 3 0 0	9.37	2,620,42	115.10	1,510, 10	500C 00	0.308.03	1,060,00	, 65E 16	1800, 00	3 301: 111	3 881: 00	1,476.00	1 (1) (0)	NA.	VA.	VA.	_
	530	36	24.6	2.9.2007	16.55	2,700, 64	65b (C	. 50, (0	1.85.01	1.380, 10.	1.905.55	9.06.0.	1.2%, 50	501: 1.1.	150.00	. 381: 16.	160,00	NA.	NA.	VA.	
	:31	36	25.76	8 n 2007	1, 0"	1,290,40	508-10	. 750, 02	11:02	9-276-01	190,01	, T81: 00-	1350, 00	1.01: 10	1000,00	15,600	30(5.00	NA.	VΑ	AΑ	
VW 5 %	101	5	111	2 at 100	5.91	9.10 3	281. 13	1.870 13	187 of sus o	996' H 83 Holl	5.35 (0)	3.781.11	5.0 E in	4.96	1.35' (7	8.98° 10 5.686 0	5 nSE 11	AA AA	VA VA	VA VA	MW49-
	503	191		5.5006	11.55	9 (0 3	15 to 13	1.06 0.0	VA.	VA VA	NA AA	NA	VA.	y or	VA.	NA	NA NA	NA AN	NA NA	NA NA	+
	501	191	4.4	5.6 206	7.55	1.10(, 5.1	2.95.03	198), 10	. 00.01	117, 16,	5 (60), (0)	910,00	1.18], 51	. 41: 5.	2.428.00	. 526 0.	1.2.5, 01	NA.	VA	VA.	

Logic Sect 21

										DIAN POINT ENE BUCILANA											
	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER,	SAMPLI, COLL	LCHON								ANALYSIS RESUL	.rs							
Well ID	ID	depth if below top of cosing	elevation ft msl <sup>2</sup>				TRITIUM ( pCFL,	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC i4.)			NI 63 (pC FL)		Well ib,
		top or Caring		Date	Logar	Result	Std Des.	MDC	Result	Std. Dev.	AIDC	Result	Std. Dev	VIDC	Resulf	Std Dec.	MDC	Result	Std Dev.	MDC	1
	306	191	1.1	8 1 250%	9.28	1370, 64	. 45: 1.4	9 191, 02	AV	NA.	VΑ	\$545.00	9.06, 10	1.5/0, 100	3.000,00	5 . Ht 144	13,1500.	3.671, 64	Vista to	3.270, 00	
	0.6	191	11	8.28.2537 1. 13.2006	12.3%	1.100, 64 6.395, 63	381: 113	1,040,00	AV	1 VS. 10.	NA.	2 6/4: 00 8 00E 0	3 (00, 00	4.500, 000 3.00h; 000	3.470, 00.	1.786; 00. 1.256; 00.	\$7.15 (G) \$160, (H)	8.0C (III	VA 20 II: 10	2200, 00	+
	2161	191	-11	1, 13, 300	12.25	7.67 1.1	3 381 117	757 107	220.00	1 100 00	* 13"01	3,100	2.661.70	2 831- 11	48 787 40	2.236.00	23.7 (0)	- 571-11	1.285.0	1.905.01	+
	10	191	25.5	89.0	1.1	6 . 4	95 E 115	165 05	18 1	16 0	\$16, 401	1.96-1	4 2 0	1.34)-	1905-00	35 (-11	185 00	95 20	21.16	111 0	
	- 11	191	25.5	24.7.8	16.78	111 3	5 (4) (0)	196 07	1.59 [	2.10 0	8.57 (0)	-1 19 101	1.95 0	7 P	14 .	5 F 0	1.9 00	5 6F 0	Logic tr	1.86.01	
	513	191	-111	1 % 1 8	15.03	396 (3	3 31-113	15 07 367 07	67 51	1.37 0	566 40	168 0	136 0	3.510	1.30 00	2. The re-	3935, 101	1 6E 0	Listen Listen	2.50(0)	
VW 15-26	011	191	111	1, 5 2008	3.51	3 171, 03	1550, 12	1.916.32	1.530, 01	239130	9 00 5	341.00	\$ 0.3E 00.	4 260, pp	3.71:31	165, 00	5 (80) 100	2.9%, 00	. 775. 64	20200	MW 49 26
(34 31	15	191	-11	16 1 10	13103	3 [0 1	1664-01	69 0	8 1	191 0	8 29 40	. 174, 165	131 0	150	1 701-101	3.56E-11	175 00	2305 1	2.311	2.12.0	1041-57
	16	191	-111	565.00	D. 16	3.50 3	5 SE 02	8 07	50	185 0	10 an	195 0	9] 11	5.7 (6.	200 - 1	5 8 - 11	135 101	* 20	6.0	191.0	
	317	191	4.4	87.200	16.55	3.960, 13	2.578.02	, 750, IC	331.14	160,00	9.7%, 01	5-22E to	3,270, 50	3 176 10.	, 335,50	3 mile 10.	3782, 00	177E-00	1995 0.	2 221: 01	
VW 45-42	518	191	23.1	10.29.200 3.22.2006	13.14	3170, 63	2.550, 13	1.880, 02	190, 0	1.715, 00	8 200, 01 4 301, 01	7 511; (d) 3 301; (d)	6130, 00 5k m	9511: 55	15%, 00	\$380 (C.	\$980,000	- 24: 10 NA	1 111: 0. VA	230E01 NA	N-VV-49-42
VII -11-2	113	18 1	-25.1	5.91.6	150	9.19 1	191-119	1.00 (1.00)	20 1	95 16 1	1.81 and	2.16 0	1.39 1	201	3 Sale on	3 (6.0)	165 01	AA	AV.	- VA	16.800-0-12
	118	9.1	25.1	* 4 ° 6	150	883 3	5.551: 5	6.19 111	NA.	NA.	NA.	NA.	AV.	NA.	NA.	NA.	NA.	NA.	NA.	NA.	
	-01	81	-25.1	56396	0.1	8 '8 4	571-115	185 07	63 1	12.0	56 40	188 0	13 1	181-	- 19E 0	p. 11	1.15 01	AA .	NΑ	NA.	
	118	48.1	-25.1	, 110	9.5	5 85 4	X1+ +	55 (6)	d. I	4 14 11	1.206	* p. o	1111 1	911-	5H: 00	51-11	1 01	A.A.	NA.	NA.	$\vdash$
	306	.94 I	23.1	8 1 2346 8 28 2346	12 (6)	830	1.67E-10	9 190, 00 9 100, 00	AV AV	AV AV	VA VA	4.226 0c 8.310, 62	1,65,100	8 (s.l., 50)	67 E. (G	9 305 9 305 35	9 (4) (6)	NIII., JII	- 84; VA	110510. NA	+
	0.08	381	23.1	1, 15 3 0 6	11:2.	61%, 13	385 03	. 000, 00	2115.51	2 16, 16,	8 (107.0)	words to	2.251, 101	2 901: 55	1 .81: 00	234: 00	2442, 00	2.9(0, 0))	5 Tale (G.	6.20(:00)	+
	0.09	38.1	23.1	9-29-2007	12.3%	1110, 13	2.545.02	. 890, 02	2080.04	1.655, 10.	~ 220, 01	3 (2): 5.	1560, 00	1.301: 10.	25/46/50	Tools III.	3.5%, (0)	5 .9h ta.	1.35E 0.	1.511: 01	1
	510	38.1	23.1	8.9.2007	12/05	1300, 33	15.6.00	1370, 00	2.5%; 1.1	2 773, 16.	8,210, 01	1175, 50	3,270, 60	3 37H; 121	2.77[5:00]	3.526 (0.	1867, 50	1080,00	2.58 0.	2.94; 01	
	:11	381	23.1	. 28 2008	15 P	2810.43	1726.02	2 980, 102	2910-01	2.572, 10.	5.580, 01	8 (81) 01	2100, 50	2 (3): 10:	8.950,00	2.35 (6.	2,520,000	3 TME 00	173: 0.	1.571; 01	-
	512	38 I 38 I	23.1	1.25 (0.08)	12.38	3 300, 13	2.5% (2.5%)	367, 00	2330, 61	1 10, 00	42 C. 01 9 0 C. 01	1 (2) (3) 1 (2) (3)	1825, 50	3 (81) 144 2 791: 144	59,0,0,	2.37E 00	3167, 00	2.736.00	1.75 0.	23/15/01	+
	11	9.1	-23.1	15 8	113	251 3	3 34 00	0 11	2.06.1	2.50 0	0.40	4.7 0	643 0	0.575	- 585 0	8 1: 0	16 0	1.0.0	189-0	2 91-11	
	15	18-1	-25.1	.0 , 100	95	114 1	2.5 (6.00)	11.5	2. 6. 1	*3 0	9 1 40	36 (0)	3.81 0	1.30	25 ESE 0	5 58]- 11	311 0	23 Mc 0	1.50	18 0	
	16	9.1	-25.1	565.00	18.5	250 3	5 (55) 112	9 11"	5 [	501.0	3 401	3 11	28 11	183)	× .	5 [6.00]	119 101	- Sp 0	6.0	191.0	
		81	-25.1	8 100 1 20 Med	D 85	168 3	2.636.02	9 11'		19" 0	5.95 40	- 5 fml-	3 [8 0	1 91	9.85	5 550 H	8.95 (0)	- 8 (-	1.595.0	1 86 01	
1711-1925	18	81	-79 T	1 1/ 1/16	9.55	5 15 105	113 3	1871 1	185 01	191 0	5 34	6 II I	135-11	2 01	39 47 307	13 1	8 5 00	AA	I str u	NA.	MW 49 80
11-19-1	114	60	-15.1	+ 3 * 6	13.55		1.5 1- 5	6.19.01	NA.	NA.	NA.	NA.	W.	NA.	NA.	NA.	NA.	NA.	NA.	NA.	10 64 -5 35
	113	60	-15-1	6 4 D	13.99	5.707 3	9 3×1- 112	387 07	13, 1	× 9×10-1	1787 401	-, 80, 101	8 (1, 1)	8 (CT)	4 (37.4)	9 391: 11	1 (0) (1)	AA.	NA.	'VA	
	- 01	60	-15 T	56106	0.1	147 4	2 10 102	, 9K 11,	1 1	130 0	51 40	4.82 (0)	1.11 1	546	120 00	50-11	185 01	NA.	NA.	NΛ	
	105	60	- 15 T - 15 T	*105 *1 *105	0.0	164 4	51: 115 × 1×1: 1	611 07	VA.	4.1 n	1 ×64:	-1 6 00 - 1 100	6 19 m	5 (\$4) 18 (1)	1 8 H (00)	5 (S) (1) 8 (8)	\$5 mm	NA	VA Fel:	115 II	-
	- 16	60	-15.1	X X . P	12.55	221 3	8.3 (- 0.3	6.16 0.1	VA.	VA.	VA.	-3 P.O	9.78 100	510k 11	4.2 0	176	5 1: 0	AA .	AV.	VA.	
	161	60	- In T	1.15.506	1 + 15	3017.03	54:09	0.01	d., 1	231 / 00	8.1 201	2127.0	2017.00	1901	300	2 or 15 miles	21.00	- 8.1- 11	6900	0.0	
	16)	60	- 15 T	6 % .	11.3	.9. 4	2.556.02	\$65 07	-9 I	1.98 0	8.28.301	- 101- 1	3.06 0	3 841-	- 3 Yell - 11	13 (4.0)	2.5 (00)	- 1911	13.100	1.680-01	
	511	60	-15-1	8920	1. 2	2.00.3	4 (2) (C	160,002	206.7 1	2.105/0	41,500	3.516-1	2 65 0	4,30	1.550 00	3 35 11	3 4, 101	1 (d.) (d.)	2115-1	2.19, 0,	
	1012	741 741	15 I 15 I	1.28.2048	16.52	1950, 13	1.22E 1/2 8/dt 1/2	2.950, 00	2730, 61	2.790, 00 9.928.01	9.2%, 01 3.6%, 01	2.830, 00 8.486.02	3 720, 00	3.811: 10.	1.100,00	3 ,715 (G) 2 2545 (G)	3360, 00	6.815.00	1 55h 0. 9 50h (0.	2.20E 01 1 (2E 01	+
	113	741	15.1	13,000	13.58	136. (2	236 (2	. 362, 02	. 50. id	1.290, 10.	5.5,0.01	3 TE 5.	220, 50	3 (0): 55	8 121, 1,2	2 (.2): 16.	3.3%, 101	+ 53E DO	, 67E Sc	256.0.	
	:11	741	15.1	11.52538	1:13	100.43	3326.02	. 921, 102	. 725, 64	2.2%, 16.	5.97(),10]	1987, 101	440, 00	992E 55	2.50(00)	9 July 16	11.5, 00	8 121.0.	1866 0.	2006.01	
	:15	201	15.1	2.6.2099	935	1 120/10	2.34:02	. 760, 92	, 730, SI	2.100, 00,	5150,01	5.365.	2980, 00	3.206 (0)	16,1,5,	2 + 45 (0)	32.1.00	2.706 (0)	2.221, 14	2.5 E. O.	
	516	701	15 I 15 I	5 /s 2000 8 T 2000	15 1s 12 Is	1 3 E. 13 1 6 E. 13	2.836.10	. 800, 02 . 800, 02	. 280, 61	1.790, 06	7.130,01 7.150,01	1 90E 01 5 00E 01	3 130, 50	2.51 to 10.	3 070, 00 5 170, 60	2.5% (G. 3.2% (G.	376, 00	3.28E (G	1.79E G. 1.89E O.	2.36.00	-
	18	60	-15.1	1 20 2003	12.18	100.3	2.400.00	88 0	11 1	1 58 0	8 15 - H	2.000.01	9 18 0	8 (0):	1.500.00	8 381 0	88 00	-6.66E U	1890 0.	2.36.01	+
118-2-11	101	- 11	-2	4 55 5 106	1.8	9.5.19	* k *	1 10 1	195 01	9- 0	5 6b-	- 35E-0	3.5 F 10	13 01	25 Ho. I	8.55 0	9-0	101 0	5 H+	1.361-01	MW at 42
	115	111	2.1	× 0.1 P	13.55	158 4	5 X Cl 5	6.3 07	NA.	NA.	NA.	NA.	- VA	N/A	ΑV	AA .	NA.	NA.	NA.	NA.	
	115	11	2.1	5 100	13.55	1.9 (	15 m²	5.55 117	95 1	1.28 m 6.96 T	5 40	181 0	8.05 0	80%	410 at	X 1: 0	102 01	AA AA	AV.	VA.	
	205	<del>   -</del>		13.206	1 34	3160,10	2 85 02	2020,00	3 151, 101	2000, 00	1 1555 333	9.857, 16,	1.381.01	8 0 TH	1751: 00	5.00	1 307, 01	NA AA	VA.	VA VA	+-
	306	12	311	81,206	1.34	1.115.13	+ 12h 1/2	910,00	VA.	VA	VA.	870E G.	1.015.54	. 391: 5.	6.211: 06	5296.06	. 240, 01	1.26 %	1 531: 0.	, edl; of	_
	207	I*	1	8.26.01.0	1 4	311: 12	854-105	797 107	AV	ΑV	VΑ	57) - 01	5841.00	9 THE 11	3 (9) 17	3-de 17	2.00, 000	NA.	NA.	NΑ	
	16	P.	2.1	1.15.506	1.5	1.0 3	j. 113	11 113	13 1	1.25 (1	83 .01	2.0	120 0	1 90)	20 mm 20	3  - 11	45 (0)	- 16	61 1: 0	6 0): 00	-
	16	P P	2.1	6 % *	153	118 1	16 00°	96 07	91 1	135 0	65 and 53 and	9 0	1.11 0	5.081	2.500 m	1 Sh n	132 (0)	4510	19 10 0	*19 n	+
	- 11	h	2.1	1 18 500	1208	101	51:11	9 0	215 1	181 0	5 5 40	3 36 1	3.48 0	184	5.5	3 350 11	38 00	2011 20	6%	18 0	+
	13	10	2.1	14.8	PD	613	199-111	18 07	2 (0 - 0	85 10 1	85 40	-1.05 (0)	180 0	1.661	1 1000	19 1-11	168 1111	1.16.1	*3 p. n	28 15 01	
	- 11	P	- 2	81.7.08	[5:54]	5 - 50 - 117	1316.2	\$11c00°	3.78 (0)	S edition	1 gd[ran	-0 dop	934 min	5.70 cm	9.54(40)	191E G	3.5414.00	1.88 (0)	16H 1	106 (4)	
	18	I.	-21	11.5 1 8	10.13	1.0 .	50-10°	9% 11*	386 0	98 to 1	5.85 401	651-0	198 0	5 1-	5.18 - 1 5.18(-))	5 (6) 0 5 (1) 10 (0)	61 00	0.00 0 330 m.	ol-	218 0	_
	117	Li Ii	2.1	1 22 2549 5 5 2549	15.23	2 150, 42 3 920, 42	386 (C	. 180, 00 . 721, 00	238L (0)	8 5 Me 5 I	93.1.01 990.01	5 890, 01	9200, 00	2 37H; 555 9 (3H; 556	5 180, 00 2 50E 00	2.3.1: 00 5.7.51: 00	2,350, 000	3.33E 55 5.55E 50	1.735 Oc. 2.676 Sc.	2 (3); 01	+
	:18	12	3-1	8 7 2000	13.13	100, 3	23/4: 02	. 750, 00	5,330, 00	1 250, 10,	7.230, 01	7.5 4: 52	3.66, 10	5 (All 55)	3.080,50	3.271: 10.	3730,00	. 251: 61	2.6 H: 5.	195.0	<b>t</b>
	319	12	211	15.26.2000	11.1.	1000, 32	831: 10	. 880, 00	9730, 00	10%, 00.	1,530,00	387, 00	1.015.54	26 %.	2.520.00	2h ic.	150,000	. 101: 5.	1.890 0.	2 221: 01	
VW 40.56	100,	10.	3.	3 22 2006	. [9)	98,17,03	1915/32	2.36.52	2,550, 01	. 2.1: 50	1708.5	1975 00	1,848,00	, 66, 01	2.180, 96	1.680, 51	. 8.1: 0.	5,330, 00	. 351: 5.	1.376.01	MW-50-98
	0.0	60	15.1	5.5046	15.25	106, 51	\$100,003	+310, 00	VA	VA.	VΑ	3.23); (6.	1.0%, 51	. 231: 5.	7.780,04	21: 11.	. 250, 01	NA.	VA.	VA.	
	503	741 741	15.1	5 5 2006 p. 7 2006	18.25	960, 0	52E 13	1990, 00	.955.01	1.221, (c. 1.181 ) (c.	\$150,01 5560,01	1 o nn	NA 8 711 111	NA 5 80 11	NA * 500 mm	NA NACES	AVA Trust int	NA NA	AV AV	VA VA	+
	105	601	-15.1	3 100	1.0	86' 3	) [- 115	5 2 113	183	1 18 II	15.0	201 00	9 1 0	7 880	34 -	8 3 H H	9.3 00	AA AA	AV.	VA.	+
	306	7611	15.1	81.20%	9.28	1980/18	5.396, 52	9490,00	AV	VΑ	VΑ	3,5%, 01	5.980, 00	9981: 144	13,15,00	91,8E 00	\$160, 101	1.66E.5.	1 tel; 0;	36: 01	
	50"	741	[5]	8.28.21074	12 05	677, 13	45E 1B	. 310, 10	ΑV	AV	VΑ	146,12	16"), 50	4.864; 1.1.	1316.00	1230 (0.	538, 101	NA.	ΑV	AV	
	10.00	60	15.1	1, 15 300-	16.37	5.050, 13	321: 113	, (G), (3	2150, 61	2.3 E. (6.	8 151, 01	2,006,01	3.300, 00	3.70(: 55)	2305.00	3.30/1.00	3.500, 00	1.50% (0)	5.756:00	5-30[cm)	1

Table Square Decembed VVI VOS - Quina Chilles Babe Square Decembed VVI vos.

Paper Novel 2. See Page 2, for Note)

			1			ı				BUCHANA	N, M										
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLE COLL	LC HON								ANALYSIS RESUL	. FS							Well ID
Well III	ID	depth if below top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC i4.)			Ni 63 (pCFL)		- WHILD
		top or canal		Date	Loar	Result	Std Drs.	ADC	Result	Std. Dev.	MDC	Result	Std. Dev	ADC	Result	Std Drs.	MDC	Result	Std Dev.	MDC	1
	510	781	15.1	626247	1102	1010, 13	2.85E (2.	. 891, 02	2991, 14 3107, 14	186, 16	5.250, 01	21%, 00	2.610, 50	2 191: 10.	16% to 2	2.346 (C. 3.546 (C.	270,00	605), n. 1 506 (d	1 80h 5.	1.7 E. O. 25215 OI	
	:11	781	15.1	1: 18 200	11.36	3 851, 13	+ 53E 10	367.00	17 F. M	3 771, 16,	1 970,00	2.28. 00	1615, 50	1.361; 1.1.	1 (5): 00	1708.00	1984, 00	37 1: 55	1.565 0	1.831: 01	+
	-113	60	-15.1	7 5 7 18	13 L	3 T F 13	581-112	53 1 02	3.58: 1	1361 IF	7 81 401	1876/1	207.10	3.86.11	1600	2.535-17	79,7 101	1875.10	No.	212 0	+
	18	60	-151	4 11 8	18.1	7300 4	1.461-111	15 07	3.58 1	188 0	0 40	81 1	2.71 0	1×1-	1.345.00	3 51- 11	585 101	Xbl- 0	761-	21 0	
	16	60	-15 I	3 5 5	16.7	716 4	2.00p. (c2.	9 01	5 40 1	1.66 0	102.00	-3 S In	187 0	1.00	5-64 - NA	SH- H	166 (11)	4 (g) (i)	50b 1 20b 0	2.13 o	+
	18	611	-15.1	11.6 1.8	12.38	16 1	3 P 02	96 01	5 50 1	1 00 11	1 401	-8 66F-	5.9 0	5 ool:	15 N 10 11	8 55H- 11	NA 8 fs (0)	- 0.01	1 100	, 301-111	+
	:39	701	15.1	1, 19348	16.25	2 (3), 33	2.06.10	. 730, 100	196. 0	3.750, 10,	876(10)	2.501, 00,	5.260, 100	2 (41): 144	\$130.50	2768.06	3175, 00	3060.00	, (8h h.)	2290.00	<del>                                     </del>
VW 50, 96	00%	10.	15.	1.22.2009	, 604	2 3(2, 1)3	2.160, 12	1.985.42	2,740, 01	2.281; 100	3371634	1,1981,100	4.20ds 00	3595, 101	. 976.94	3.320, 101	Annaly 10.	9.336.00	. 881: 4.	2.231: 01	MW 60 8
	11	601	-15.1	4 % , 0	15.15	315 5	36.115	258 07	2.12	1.55 ()	915 201	1.9916. 1	2.5.0	5 851-	20.3 20	5.551-11	\$495 mm	1 554 0	1 10 0	910-01	
	102	741 741	15.1	4.5 2000 8.7 2000	1e.33	3 150, 43	2.756.02	. 70, 10	2800.04	2,330, 10,	9.130,01	1,570, 00 2,631:64	3.351, 00	3 80 h (a)	6.210, 03	5 87 E + C	630,00	, 53E 50 , 35E 0.	1.83E 0.	2.96.01	
	121	741	15.1	15.26.306	13.15	286.43	2 826 10	. 850, 00	3000, 61	231, 16	5.340, 01	1.11:31	5 890, 101	9 751: 144 9 751: 144	2.866.00	93,816	7 (6), 00	9 4 31: 30	184: 0.	2.06.00	+
17/1-20	100	19	*	5 91 5 11	1.38	96 (12	162.5	1.580	as a fear	6 3 20	9.87%	10. 201	5 NO 10	5 181	- 6	121 0	5 E 0	NA.	AV.	NA.	MW/ o1 4
	102	80)	'%	11.1	1+3	1.15	595.00	6 0.	Shirt,	3 16 1	5.38 (01)	165 - 1	3.30 ()	5 851-	- 5°P 0	5 35 0	115 000	NA.	AV	NA.	
	- 01	80)	**	113.	D.I.	11. 1	22/1/10	10.7	×16 ×11	58 16 1	1.82 (0)	68 0	196 0	15%	28 1 405	5 50 11	3   G   101	NA.	NA.	- AA	
	- 115	60	'% _8	8 1 08 5 50 2008	Di 1	586 I	55E-02 	9 0°	1.5 for 3. deni	5 To 1 59 Bal	432 and 432 and	1 83 - 1 3 -2 - of	105, 30	1 94) 1 910 mm	80: 0a	2.96.0	55 mm	AA AA	VA AV	NA.	+
	378	30	28	88208	1:16	3.290, 12	55E 10	2030, 02	374:00	1026.0	+ 750, 01	. 5%: 16	2 195, 50	3.386, 555	1 995, 00	. THE OC	2970, 00	8 331: 10	1 (2): 0.	. 831: 01	+
	0.00	39."	28	10.27.308	131.	1780, 32	850: 10	. 950, 00	1.830.02	4.294634	5,677,001	150.01	1281, 100	1 894: 144	, 54E 00	~ 15h nc.	6.8%, 00	\$1.35.00	2.16 %	2.16, 0,	1
	:40	39.1	28	1.25.25.59	14.5%	2,370, 61	ist: (0	. 921, 02	1.526.00	7.58E.01	5,750,01	9 890, DI	2.810, 50	3.266 ta.	1331.00	2.736.00	3.302, 000	8 55E 10.	1,670,04	18%, 0,	
	:11	39.1	28	4 T 2000	14.27	2 (8), 42	Toll: (C	. 8.1. 02	13260.	98.834	8,270,01	. 181: 00	7 (8), (0)	1726 00	1,35,50	5 talk (6)	5085, 00	, tel: (C	1830 0.	2.11: 01	
	912 913	397	28	8 2049	13 12	1.550, 40	70E 00 32E 00	. Troute . 1.1. to	6.395.02 2.150.01	5 + 0 ( ) () + 3 5 ( ) ()	9850, 01 8 050, 01	2,530,64	3,350, 00	3 (H) (A) 9 (10) (A)	1 00E 06 3E 00	3 (c.) (c.) 0 (15) (c.)	3.5%, 00	4.55[; 10. 4.60], 0.0	1950 0.	2.276.01	
VW 4 19	000	787		5.30.2007	11/29	5 857 . 0	135, 30	1.728.142	2.366.0	6.98", 11	5-84-1	2.50 (4)	3 (3) (6)	3500, 101	3.521-01	3.317, 30	3700.00	NA.	VA.	VA.	N/W-51-7
	102		-11	11.1	1.0	121 1	186.00	6 01	8 1999	nanh I	6.15 -01	-6 s I	158 0	3.916	2583.00	15 F 0	105 (0)	NA.	AV.	- VA	
	- 01	8	-11	187	16.18	500 1	5 (- 10)	102	-10 ar	1996 1	\$27.00	166 0	2.0 0	1001	25 13 20	3 79 00	115 101	NA.	AV	- AV	
	115	8	-01	8.108	11.08	9.56 [	201-117	9 112	-165 -44	16-1	9 5 401	- 9.16	111 0	1.5%	186.	23 5 0	5 100	NA.	NA.	NA.	
	16	8	-01	5 5 1 B	11.85	6.0 1	93 p. m	6 02	1.55(ca)2	1 (10 () 1 1 (10 () 1	9.95 aq 5.18 aq	943.1	3  3   0	1800	28 [3] an	2.4 (0.11)	13 mm	NA IIII	NA LL LL II	NA SB of	
	16)	· ·	-11	1 , 248	1113	111 1	676.00	96 111	\$ Share	5 30 1	85 401	8 17 - 1	80 0	5.50	1 SH- 00	5210	6 1 101	3 % 0	1 10	2 75 01	+
	10	8	-11	0	14.7	1.01	55F 115	18 m²	- 41	3 No. I	502.50	5 (315-1	8.8 0	4.650	-191-0	3 1 1 11	4.55 (0)	1.586-1	1 40 0	1.905.01	+
	- 11	-8.	-11	5.5.5.00	13.1	6197 1	58)- 112	8 1 07	6 y Tour	1 SN(++1)	8.797.401	4 " .	68' 0	5.76	2.330-0	\$79E-0	6971 (0)	20 S (F 10	1.130-0	2.00.00	
	12	8	-11	8 0	1.1	1.00	6 F 02	\$ 10"	5 Spain	35 16 1	5.55 40]	-1 SH-	187 0	1.510	- 10 m	1.50(-0)	12 00	- 51:	1.830-0	* 9E-01	
MW-81-0-1	18	8	-11 -35	1 18 Nod 5 90 No	113	5 0	851- 115 1 18	1.116.2	45.40	5 % To T 50 an	8 (1) and	-K No	5 1 1 10	5 (8) 1 (8 m)	5 85 00 0507	5.50E-0	55%	-190- AA	781- VA	101.0	WW 51 11
4111-1-1-1	107	1.17	-56	11.1	1.06	90 1	3 p. m2	65 01	35 950	1.896-1	5.1 201	-170 00	161 0	1971	1.375.00	5.53E-0	5.33 (0)	NA.	VA.	VA.	101.0
	- 01		-361	1925	11.35	51 7 01	55F-115	. 00	+.1 -01	5 8Fs.d	186 201	-1.36 . 00	285 / 50	1971	1.85.00	16 F 10	\$18.00	AA .	NA.	A.A	
	115	1	-36	8.14	1215	-1×II-	15E-02	8 07	-619 art	296.1	935 20	-9 t F-	100 0	1.161-	381.0	250000	2.5 (0)	NA.	- AA	NA.	
	307	537	.3n	882.06	10.8	2827 2	35E-02	206, 02		3 16 1	92,50	, 56,, 11	203,70	4.50þ	4 21.50.	2 F 0 8 53E 0G	4.66, 101	91	13000	2.90(-0)	
	308	137	36	10.27.208	16.19	1 010, 40 9950, 61	331:10	. 160, 00 . 180, 00	1.560. 9076.03	3.786.01	9 130, 01 3 000, 01	56,5,06 1330,00	6811, 00 2871, 00	8 501: 10:	572E 00 . 5JE 00	2.371: 16.	2 (20, 00	256, 50	2 00 to 6.	2.120, 0.	+
	10.00		36	4 T 20 and	1, 18	110.32	6.E (C	. 780, 00	.3301	0.304.14	1860.01	87500	3.790, 100	3 804: 111	1671.4.	3.5,1; 16.	10,5,00	330 5.	2.396.00	2716.01	+
	:30	.431	36	8 22549	1, 13	2.910, 42	7.8 (0	. 800, 02	1.2% 0.	3 (8) (4)	1360,01	8 0/5, 61	4.581, 100	3 801: 144	. 050.01	3.535.00	13%, 00	2 935 00	. 895 5.	216, 0,	
	:311	.131	34	1, 18 206	1, 35	1.110, 32	331: (2	. BC. 60	3678.00	1.296.01	1970.01	93 E. 00	1000, 01	. 58E 5.	1190.00	9 lt 96.	7670, 100	3 (31, 10)	1 (2): 0.	1.810.01	
MW 51 135	900	135.2	67.5	5 40 2007	12 %	9310.00	1.5(0, 12 (3): (0)	1.706 (2	1980 0. 5 330 02	5.530, 0, 50.06.01	8 901:00 5 7-00 01	1011, 51 1301, 51	3 (2h (0) 1071, 30	1.36E, 00	3 (2), 54,	3 8 E. 10 3 3 E. 10	3.85, 00 3.85, 00	NA NA	AV AV	AV AV	WW-51-13
	101	.02	40.5	1.0.1	12.16	931	240.00	. 5%, 00	2.12.40	2506.1	118 -01	- 1041.00	3.85 0	5 00:	3 11 40	3 SE 0	336, 101	0.0	NA.	70	+
	105	35.7	40 5	8 , 18	111	191 1	55E-115	8 01	4.5 pare	36.1	8 9 -01	6.91	138 0	1 91-	15 - "	P-11	19 101	AA.	NA.	VA.	1
	161	35. 1	4) *	88.10	1.8	.10	46F-115	95 01	s glant	23.16.1	1.8 (40)	4105 000	108 0	1 '91-	0 - 2 5	2 F 0	\$ 43 (00)	-5 N 0	II+	202.0	
	16	32.7	40.5	10.5 No.	1.00	68 1	50 m²	96 07	1 Month	5.36.1	5.64 401	4 1 00	5.6 0	1.816	8 97[- m) 6 81	5 SE 0	65 111	- NI:	1 35 0	2.016.01	
	300	.35.2	6.5	4 ° 2000	1, 53	2.15.31	131: 10	17.1.00	8 5 9 : 02	5 T JS J	5.750, 01	3000,00	700,00	1991-10	7.330, 0,	3 77 1: 10.	160, m	2 15 51	2.2 0 0	200.0	+
	540	35.2	67.5	8 2049	1, 22	981, 0	6.E 02	. 75, 10	. 621, 01	1736.01	9.570.01	11% 00	3.750, 00	3716.00	2 (80) 000	3.305.00	12%, 00	. 901: 5.	18.1: 0.	2.76.01	
	-11	34.5	6" 4	11.18.200	1 34	1.307 12	321-112	131 00	562° (d)	0.006.01	8.177.01	471	143, 70	4 TH 11	7.18E-00	\$1.58 or	612 00	108' 00	relle 1	188' 0	
71/1/21/163	100	167	-95	5 91 5 11	150	18 02	1.56	1396 1	5 NH.	SE 0	1.6 00	-181 - I	5 SH IIC	3 15 100	I Isol	181 0	5 1 F	AA AA	AV	AV	WW 51 15
	- 01	61	,0%	197	15.05	108 1	235.00	66, 11,	1 5500	1896.1	3.12.301	1.31 - 1	3 4 1 0	3.81	864 - 1	3 1-11	31 101	AA AA	AV	AV.	+
	108	62	.0%	8.10	155	-1 -996	3   102	85 05	13 150	87961	9.59.401	4 1 00	100 0	3.501	N 69	3 36 11	2 15 (0)	NA NA	NA.	NA.	+
	160	61	.05	88.18	1 15	69" 1	8 1 1 11	1 02	2.15.44	2530-1	5 15 401	4.81.00	2.75 0	1001	5 % -	9 1- 11	8.89 (0)	1.531- 0	1.290-0	2 80 01	<b>T</b>
	- 0	6.	-05	1 , 208	1 ( 5)	7.505-11]	Lett 2	\$80.00°	1586-01	× 168411	55 bit	5- (0)	5186 on	5 4 (0)	5.22[40]	5 480 C	5.286.00	10.00	889 1	1 [8] 31	
	16	61	.05	57.200	1 15	160 1	1 1: 10	lx o	- 94	19 (4.1	6.98 .00	-9 In-	311 0	1 1 1	- 0 at 5	5 14 11	\$ 85, 101 Sections	- 11t	181:0	* II: 01	
	510	102	95 95	8 2 2540	12.09	5780, 01 1 H1, 02	Salt (0 a2h (0	. 8.1. 02	5 150,00 12 0:00	\$ 70E ST	9130,01 990,01	7.568.50 7.865.51	5 (6), (a) 3 TE, (a)	3 30E 10.	2.23E 00	3 (3); (C. 3 23); (C.	33%, 00	1.8E 00 3.79E 00	1.85E 0.	2.36.01	+
	:311	1/0	1/2	1, 18 300	1. 33	9 185, 51	24: 10	. 130, 00	6/98/02	0.0000	196.01	2430, 000	5 895, 101	9 (all) (a)	2 (41) (0)	5 331: 10.	630, 00	2.211, 101	1 861 0.	1935, 0.	+
MW 51 189	00,	189.2	12. 5	5.30.2007	. 100	. 870, 02	1,670,42	1.716.32	2 885 02	8.9(0.0)	11.5 00	3,620,42	3.586, 00.	3825, 00	1,540, 10.	3.5%, 00	1 + 30 00.	NA.	VA.	NA.	WV-51-1
	900	.87.2	. 21 5	1.25,000	1314	9 190, 01	5dt 02	. 630, 00	3.53(10)	10.88:01	5, 180, 01	8.871; 1.	1110, 50	3.581; 144	1.57[; 000	11.26 (6)	13.5, 00	NA.	VA.	AV	
	503	.87.2	.21.5	10.2.2047	12.2%	8 151, 50	708.02	. 980, 00	5060,00	2.963	2.580, 01	. 381, 0,	5 (5), (0)	2.1016.000	1115.0.	2.756.00	300,00	NA.	VA	NA.	_
	501	. 857 2 857 3	.21.5	.1 5 2567	13.05	6.26E 10.	38E 02	. 5.0, 00	1.53E 0.	36,634	8.927 (0)	3 ((5)) (6) 34" (6)	3.270, 50	2076 St.	\$000,02 1,026,00	3 (4) 10.	105, 00	NA NA	VA AV	VA VA	+
	116	80.1	- 115	18708	131'	1.10	88 5 0	15 02	- 15 -44	V 180 I	20 00	35' 17	213 0	1 201	1.575.00	58E 17	\$12.00	- NA 11	NA NA	YA U	+
	500	.87.2	.21.4	1027.208	16.1.	76%, 51	74: 12	. 96, 10	3501:00	7,963	13.5.01	6.11:01	6,381, 101	7 30(5 55)	35/8:00	0.35.06	160, 00	9 78 E 144	183: 0.	2.76.01	<del>+</del>
	100	.87.2	. 21 5	. 2. 5.5	1, 33	3,320, 61	3.6 (0	. 180, 00	2145.01	3.18[:1.]	3,5%, 01	20%, 00	3 (8), 50	3 (Cl) 100	1.518.00	3.32h +c.	1265, 00	8,330, 00	, 19E 5.	2415.00	
	0.09	.89.2	.21.5	5 " 2549	1 55	2060, 61	521: 10	. 8.1. 02	1.53500	\$330.01	5 I 1 III	707 (6)	9.395, 50	9 26h 55	220, 244	\$756 HG	61.5, 00	3.36(- 10)	1.89E 0.	* II: 01	T

<sup>1</sup> to 8 Mol 1 Mol 1 Mol Not 1 Mol 2 Common 3 Littles, Table 5 Quality 3 Format Little Coss.

Mac Little 5

Fig. 1, et 2. See Page 2, set Note)

										BUCHANA	N. NI										
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLE COLL	LCHON							,	NALYSIS RESUL	FS							Well (D)
Well ID	ID	depth if below top of casing	elevation It mst <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			NI 63 (pCFL)		- Well ID
				Date	limi	Result	Std Drs.	VIDC	Result	Std. Dev.	AIDC	Result	Std. Dev	ADC	Result	Std Dry.	VIDC	Result	Sfd Dev.	AIDC	1
	:10	.872	.21.5	8 2 2559	1.1.	2.750, 64	35E (2	. 441, 00	77 old 01 3 old 01	8.836.01 \$1006.01	5 1.1.01	9 351: 61	3 821, 101 5 581, 101	3.57E-33.	1.47E-00 2.88G-0.	3 800 HG	180, 00 640, 00	. 301: 144	2.36.00	2.5% 01	
VW 52 .1	00,	.52.2		6.20207	.2.35	. 171, 02	1/80, 12	1.816.32	3.585.00	6,330, 0,	8 33E S.	1.766.34	2.5% 00	25%, 00	6.26.01	22%, 00	2 15 10 10	1560, 00	. 281: 5.	150.00	NVV-52-11
	202	10	6×	×6 ~ 11"	1/14	2.41. 14	-31-11*	9,65 117	23 BY 201	. 1671	9.38, 101	-2.167 000	3 127 100	3 231- 11	3.301.713	2 TOP- 17	314, 00	A.A	ΑV	NΑ	
	115	10	6 ×	1.8.1.8	13.3	113 3	535-115	98 0.1	1.6 (40)	1 sto 1	8 R 201	5 9 - 1	198 0	1 101:	27 SB 0	\$520.00	108 00	AA.	NA.	VA	
VA-52-8	- 01	100	6 ×	15 1 0	15.5	2 10 °	16 (4.00)	1.550	15/502 21/100	5696 I 198 at	90%	5 (8 × 1	5.2 to 5.30 to	5.116	3.13	5 1-11	5.1900	NA -I 9I-	VA GRTE	VA.	MW a2 18
	100	1.5	- 16	86 10	13.15	63.1	30.00	96 0	. 0 . 41	6996.1	895 201	4 13 101	3 20 10	10.1	313	3 30 0	385 000	NA .	VA	VA.	1047.32 10
	- 01	1.5	-15	15 1 0	16.15	1 1g 1	3 p. 103	21 02	45.50 44.5	5.556.1	3 30	- 116.5	80 11	n hit	No -	1.196.0	8.75 (0)	AA.	AV.	AN.	
VW 52 %	100,	18	3.	5.21207	.135	7 (2), (),	1.180, 32	1 976 92	35.100	* H5.00	10.5.00	3.69(1.0)	2.546.00	3,390, 00	5.5cH; 61	3000, 00	315.00	2716.55	8.06.00	9 551: 00	NW-52-48
VW 42 %	501	18	33.1	8.6.300 51.200	1, 34	. 150, 02	176, (2	1.568, 52	5.5% in. 1.5% in?	1830.00 01.26.01	7.331; 6.	7.850, 01 , 15t; 00	3.20E 00 7.6E), 00	3.750, 000 5.0715.000	2.326.00	3.2%, 00	3.7 St; (c. 12%), (0)	AA AA	AV.	NA AA	MW 52.46
X3V 32 of	100	18	20	3.21.200	.131	1 130, 40 3 820, 00	5 83E 0.	1.786.02	3.256.00	1680.0	5.77(-5)	. 1/4: 00	3.256.06	3 150, 101	2 (20) (0) 8 (00) (0)	3.5 E. DO	315.06	2.831: 1.1.	5 .25 to	1575.01	NW-52-64
- 1.01 12 11	9.0	61	15-1	86.207	15.50	3 721, 141	7.E (C	, 260, 100	1,50,00	* 226.14	5 230, 01	5.00.01	3.500, 500	3 (64) 555	1.800, 00	9 L8E 05	112, 00	NA.	VA.	VA.	10.000
	- 01	61	- 16 T	51.500	155	4.36	8 5 15 10	0.00	15800	16 T	, 201	89.0	621 0	- sol-	1.200.0	5.55(0.0)	58 00	AA .	ΑΛ	AV.	
MW-854-8	10.65			191510	1.3	18 02	100 '	1 6h 1	3 (\$)	1.50 au	5.895	2.00	8.58) 10	5 5 000		168 0	5550.0	AA.	NA.	ΑΛ	MW 52 118
/1/17-2-11 ca	107	110	40.1	8620	155	5 X 0	1.1 2	1.56E 1	-119 at	66' -0	95 lb-	990.0	5 55h 10 100 - 0	575° 101	4.6.0	2 55 11	5 500	-191 H	9.98 III NA	113	WW 52 122
	303	122		1.288	15.5	88	8 % E 0.	. 15 0	12.60	2 (2)(4)	3 22 . 01	12., 101	_05,0	+ 210: ····	I: 00	2 480 14	18200	NA NA	VA.	AV.	+
VBV 52 162	100,	16, 5	1.19.6	5.21207	.1.35	2 821, 102	1950, 32	2 (3)( (2	5 , \$E 0.	1871.0.	8.26%	5.800, 61	3.5% 00.	3.290, 101	. 5%. 14.	3 151, 101	1,881,10.	130.01	9.75E-144	1.36.0.	MW-52-162
	9.0	.415	, 55.6	8.6.2007	1.35	2.111, 32	8.4: 10	. 951, 102	1.53(:02	47964	5030,01	3 (41):12	3 HE, 50	3.776.00	3.730,02	3 , 21; 10.	3.521, 000	NA.	AV	AV	
	0.0	.41.5	36.9	1,28,254,9	10.22	1 150, 42	8 7 M; 10, 1 581; 102	130,00	1031, 00	3 (2)(3) 5 (0)(3)	1.130,01	5 (Mg).	2 030, 100 8 5 F. 100	3.3(1); 1.0. 5.00(; 1.0.	2 331: 00	2 (3): 00 5 (4): 00	11 C. 00	NA NA	NA AV	VA VA	
MW 52 181	00,	.81	16-1	5.21200	.236	2 160, 02	190,00	2 9 16 9 2	3.76.00	5.070,00	7 881:34	5 995 M	3.30E 00	3 522, 181	2.8.1:31	376.00	1.95.15	223:0.	. 40.01	1177.54	MW-52-181
	9.0	18.	.96 .	86.200	1. 6	1.1%, 40	111:10	. 970, 00	589:02	5.59(3.1)	9.770.01	1.210, 00	2.870, 00	2.976.56	1.281; 00	2 505 06	3.570, 000	NA.	VA.	AV.	
	503	18	16	125 2008	16.23	1.860, 10	8775-0	187, 00	1 = 21 = 0	2.94(0)	4,080,00	198] - 10,	2.25%, 500	3.56(+.55)	41.541	2 25 00	3737, 101	NA.	AV	AV	
	- 01	18	- 9b	15 ' 0	120	11 '	9.950-0	0.00	-195 arr	5.895.1	15 -01	27.8 (0.0)	582 0	1 101	3 5 F 0	5 p. m	12 00	AA	- VA	AV	100.000
1.47-22-02				8 '1 ' 0b	12.5	18.00	185 3	5.76.7	568 O	3 1: 0 NA	NA.	935 1	5.8 0	561 0 5 t b	Livition	5 100	53 00	NA	\$19 n	NA.	MW d3 62
	102		- 14	114. 0	1.6	181 3	981-11	1 02	8 1607	8 10 1	90 40	4.5 00	3101 11	1500	- 3 P 0	551:11	10 00	1 900 0	12 10 0	1500 000	
	118		-1	6	153	8.68 3	51: 115	4.4 07	5 (\$ 11	1.18 0	T. III	18 0	3 8 0	1546	1.38[-10]	5620-0	165 (0)	1536	81 1	1 0	
	- 01		-1	80.11	1.3	6 '	* 54: 11°	208 02	33   305	5 K Io I	88, 201	6.9 - 1	133 0	, pl-	- SE 0	2. July 10.	21 00	23.5 p. 11	VIII-	* 36 0	
	100		-1	1 21 200	1124	9 (** *	1   1   10 °   1   10 °   1   10 °   1   10 °   1   10 °   1   10 °   1   10 °   1   10 °   1	2103 107	* 950m	5 Fe I 1286-1	1 11 - 01 1877 - 01	0.100	5   20	3.73)	- 50 0 - 300 0	289-9	7.80 (0)	3 KH 0	NSD	2110.0	
	16			8.12.08	12.5	11 3	X31-115	9 01	6.550-0	3 30-1	195 40	1 31-11	1.60	101	199 . 1	1 9-11	5 28 (8)	1.86	1.70	* 91- 01	
	16)	- 5	-1	1 40 708	15.82	91 '	2.9 (F. 112	65 07	-1.9 -01	1996-1	110 401	1691-0	6.1 0	261:	. XI: 11	5 11 11	665 (11)	- · × sI+	1.650-0	1376.01	
	10		-4	1.81.0	120	1.6 1	5 SE 105	0., 0.,	2.50 0	10 0	9 5 401	1 0	1 06 11	1500	25.58 (4)	4 No. 11	58X (0)	8 H- 0	6.05	181 0	
	10	1		1 1 1 0	16.09	980 / 60	3 45 02 26 E 02	39 07 200 000	3 m ant	596-1 83-1661	89 an	50 0 3 1: 0	58	1.50)	3 10 0	1 site ()	555,00	- 99	18.10.0	216 0 25 1: 01	
	14	-		1 2 706	120	661	S54: 10°	8 07	- 89 40	3.305.1	196 an	3.1: 0	190 0	1 100	2.120 000	1 M: 0	189 (0)	26 351 11	Sh.	2.10 0	+
MW-53-120	100,	1068	. 49 5	8 912 06	.1 91	1.12., 03	1.2% 3	214 - 5	- VA	AV.	- VV	A . W . O	6 [6], mi	\$ 100,000	1.98[40]	8 964	989-0	AA .	AV.	AV.	WW 53 120
	9.0	.528	31.5	.1.5.2536	1.25	1900, 13	CE 18	, (G), (9	2 (7), (4)	1830, 00.	1950.01	190E 5.	2700,00	3.06.00	3.5(0,0)	2796.00	3.302, 000	27,0,01	, 32E S.	1300, 0.	
	503	,528	35.5	9 22 2347 8 9 2347	12.15	960, 0	(A) (A) (A) (A)	1,320, 00	3.37E SI 3.70C SI	3.180, 10.	500.00	371 (6.	3.621, 50	2.83E (C. )	5 (F), 5, 1.5%, 0.	3 7 51; 10.	3725, 50	1.530, 01	2 . 10 . 5 .	1.1%, 0,	
	305	1028	31.5	1021200	13.38	7 100, 13	5.256.10	1020,00	3810.01	2.27, 10,	4821.01	53.4:1.	3.510, 100	3.296 (6)	2.23. 0	3.35(: 16.	3 "25, 101	706, 00	2.06 %	2.380, 00	+
	27.65	,59.8	31.5	. 2. 2538	16-13	180, 13	3.486.02	. 121. 00	3122.01	2.100, 00,	× 160, 01	. 381, 16.	3 (21, 10)	3 (81: 55)	. 150.50	\$ 35.6; etc.	31,1,00	1715.01	. 851: 1	2000.00	
	37.66	.59.8	35.5	5.13.2538	16.15	5.911, 13	3.381; 10	. 130, 00	3.16.51	1.730, 00,	9.730,00	1,390, 50	1981, 100	3 (58 55	1.35 00	2.56.00	3 990, 000	2 221, 14	1.281; 0.	2 (8): 01	
	309	.528	35.5	8 12008	10.15	5300, 13	3.5dt (C	. 9.1. 00 NO. 02	3000, 61	1.521, 10,	31.0.0	97 46 5c	1930, 00	3126.00	1.150.00 NA	2.33(: 16.	3.202, 00 NA	2 (5), (4	1 35E 0.	2.11:01	
	10	9 %	.49 %	111 Str. 7006	11.00	* 6 1	5.9 E-05 5.99E-05	50.00	510 I 2536 I	189 0	18 40	-5 5 -0	1.5 0	3 SH-	0.00.00	9 st- 11	9.9	191 1	Light 0	1 991-101	+
	1 12	9.4	.49 *	111 508	11.3	801 4	3 735 117	68, 11	1.55	464 11	6 1 40	4 25 L	1 2 0	5 761-	-1.95 -0.2	1 (0) (0)	1 15 00	111 01	1131	1.41 0	
	14	9.4	.49 %	4.1.0	12.19	5.00	3.595.00	92.01	161 1	13 0	5 201	- 5 ft - 1t-	183 0	5.00	1.575-100	1.600.00	5.49 (0)	12 1	2.296.0	1.39[0]	
	1.1	9.8	31.5	1.1240	9.1	545, 13	85 F 02 3 G/F 02	390,00	29%, 01	21%, 00	37 and 5760, 01	2010,00	615, 00	684 1 0F 55	6.330, 0.	3 800 Hz.	138 00	1.31 I 87e/L00	1 45 0	1,9115,01	$\perp$
	115	228	31.5	1 1 349	13.18	5 (S), 13 5 (O), 13	3 SE 10	2000.00	29% (4	2.1%, (%) 5.59E.01	5.6%(), 01 5.931, 01	2.260, 001	3 (2), (0)	3.501: 121	6,330, 0, 3, 7[+ 100	3 80d; 10.	\$100,00	\$7eC, 00 1.97 - 00	. 831: 5. Luck 0	1 885 01	+
	117	2008	81.5	1022 200	1 4"	5 (6) 13	3 (2) (12)	88' 0"	3.00.01	2.11, 0	118, 01	1.000	5 807 70	- 441	2.36.50	9 9 TH 10	201, 00	68 101	861 1	2.100.00	+
Mallanda C	100	85.5	. 14.1	5.5.50	9.9	800 00	311 3	3.76.3	1.5 01	5 % 10	9104	2.5 (0)	5 (15) 10	3.12 000	4.13 0	2.1 0	25 (6.0)	610 11	5811	2.2 (6.0)	MW 64 37
	102	46.5	-25.1	, ,	D 3	8.88	5 36 02	, 98 .0 ,	530 0	1.11 0	6.76 401	B 0	251 0	5 (1)	-161 aux	1870-0	3 [5 101	1 U	83)	211.0	$\perp$
	113	46 *	-25 T	1 10 No	15.75	[11] 3	1.55 p. 115 1.55 p. 115	546 0°	5 9 11	13 0	513 aut 35 aut	6 Hs I	181 0	5 11:	56 -	3.00 m	115 m	1 1 01 -188 art	70 (4) (4)	1 0	
	105	46.5	-24.1	577.08	1515	8 0 1	3   10	15 07	518 11	196.1	5.86 40	-0.50-	212 0	3 11:	- S - S - 21	1961-11	116 101	1 58 24	2180-0	212.0	+
	16	46.4	. 14.1	** * 14	1 0	3 5 5 10	Leke 2	311/102	5.50 (0)	Super	15400	540-10	2.126 (00)	5 M (0)	-14% 1	1096 0	5.50(-0)	T.P. (0)	189	105 (1)	
	- 0	40 *	-14 1	1.11.508	13.15	1.78 (3)	, h ,	3 0"	33 11	1.18 0	5 5 40]	258 000	6. 0	5 × 1-	181 0	5 35 0	5.5 (0)	1.50 (1)	1.6% 0	2.316.01	
	0.00 0.00	34.5	23.1	2.3.2549	15.31	116. (3	86h 52	. 640, 00	\$931, 101	11/6, 06	6.760, 01	, Tale 00.	3 331, 101	3.70 h 14.	51: 101	3.20(10)	310,00	3 , 45 55	2.98.00	2.500.01	
	510	36.5	23 (	8.6.2000 8.1.2000	1. 5.	1 12 0, 43	2.786, 52 3.266, 52	2.371, 00	5.530, (a)	1 200, 52,	1.750, 01 9.880, 01	1.81E 52 3.76E 5.	3.9%, 00	2 81 h 144 1 29 h 144	1.6E 00 85.E51	2.75h (a)	1,530, 00	1330, 00 5 800, 00	2 (41) %. 2 (.1) 00	2.160, 00	
	311	36.5	24.1	1 13 200	11.34	100.0	1.906.02	2000,00	5771, 00	1 000, 55	1760.01	6.778.0	5.600, 000	+ 28E 144	2.216.00	9 50 to	53.5.00	136, 01	2 (.16 0) . 80h 5.	1300.0	+
VW 41.88	100,	57.5	313	13.367	6.15	1 648 02	3110.10	3 (2): (2	2.226.06	0.000, 10	1126.4	3770.01	28.6 %	3 (0), (0)	1.150.00	2.710, 00	3 005 00	15(0.0)	. 881: 5.	2 .26 %	NVV-54-58
	900	57.5	16.1	13, 200	7.55	6930, 10	3.726:02	2,621, 00	, 760, 50	8.53(1.1)	7,520,00	1,320,000	3 120, 100	3.231; 10.	8 170,03	30.15.00	3.350, 00	, 975.0.	1.854; 0.	2086.01	
	3/8	313	18.1	15.19.200	13.34	5.610, 42	2346.02	. 90, 00	1381:0.	8 (3): (1	5350.01	23863.	3 (3), 50	3 501; 53.	3,540,00	25% (6	3,350, 000	2 885, 300	1.5% 0.	1.811; 01	
	201	4.4	18 1	4713	13.15	6.1" . "	1 0 F 10	13 0°	100 11	1 m/ m 3 k lo 1	8 137 01	2.16° or 8.695 I	1397 50	3 30-11	7.3 (* n 1.63): nn	3 hole of 3 hole or	155 00	1.37 00	23 16 2	2.500.00	+
	305	3-3	15 I	1 22 2148	17.05	5780, 10	5 (4) 11,	. 3.1. (0	. 10. 00	52960	5 FE 01	3.781; (4	20% 50	3 501; 1.1.	1.05.0.	2 17 6 100	1235, 00	13% 01	101: 5.	2850, 00	+
		47.4	18.1	1.11.508	13102	6981.12	851: 10	. 10, 10	5000, 00	1765, 10,	58"1.01	7 (3)(5)	3.710, 60	3 891: 101	. 126, 50	3.50E-16	3.315, 00	30.5.00			
	100°	2.2	1 - 1	23.200	11153					8 526 (4		2 84:11		3.20t; iii.			3.357 (0)		. 911: 5. . 951: 5.	2485.00	

<sup>1</sup> on 8 969 F860 - 8699 VG V09 - Quarter VT diles Table 2 Quarter Charmagical VVV voca. Vicas Chinas

IPEC00224892

Fig. 12 et 2. See Page 2, set Note)

			ı	1						BUCHANA	. , , , ,										_
Well 10	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLI, COLL	LCHON								NALYSIS RESUL	.FS							Mali D
Well III	ID	depth if below top of casing	elevation ft mst <sup>2</sup>				TRITIUM ( pC FI.	.)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC i4.)			NI 63 (pCFL)		- Wallip
		top or Caring		Date	loar	Result	Std Drs.	MDC	Result	Std. Dev.	AIDC	Result	Std. Des	AIDC	Result	Std Des.	VIDC	Result	Sfd Dev.	ADC	1
	510	57.5	13.1	8.6.2509 8.1.2509	12.13	6.580, 12	2.236.02	780, 00 230, 00	2006, 30	Rocked Rocked	990.01	2.1%, 06	60%, 50	3.37E-10.	2508 00	3 - 31: 10.	3.325, 001	1,526,50 8,336,0	2.36.0.	2.90(:01	
	:11	51.5	15.1	1, 13 3 0 0	11.51	8 380, 12	2.985.02	2030, 02	. 915, 50	7 (2):14	5030,01	320, 6	5.671, 101	+ 80/E DD	, 30E DI	5.254; IC.	5.520, 000	135, 00	1831: 0.	2371: 01	+
/11/10/11/2	100	-1	-116.9	\$3.500	1.8	1 1 105	1 -4	3.364- 1.3	*15" 01	8.5 p. 50	81,614,	1200	3.5% (0.00)	36" 1111	2.04, 14	2022.30	331	- 185 - 001	597-11	2.085.0	MW 54 12
	115	13	. 04	1 19 50	1.1	494	1.50 m² 3.6 le m²	165 0	16 I	1.1 0	X8 201 X11 201	1.76.7	168 0 Usj 0	1.00(-	1.561-00	1 No. 0	5 (6 m)	-16.95	1.896-0	2.000	+
	- 01	125	- 04	1.51.8	11.52	- 44 .	1.75(-117	118 01	550 0	10, 0	5 40	8 344 1	3 (8 0	1 5 11:	31.5	3 1: 11	3 15 101	0.80E-0	2.50-0	1-81-11	+-
	115	125	. 09	5.5.50	11.06	6.06	\$50 m2	19 11	5.5 0	× 396 - 1	5.96 (0)	4.78 (0)	2.12	5.1%	1.25.00	2.656-0	8.55 (0)	-5 11-	1 80 0	* 80 00	
	16	125	. 03	1 11 508	1.05	611111	9 F 0	32 02	551 0	K 56-1	5.85 (0)	- 18 Ye	211 0	3.75	2680.00	2.53(c.)) 3.53(c.))	555 (0)	1.53 0	1.830-0	2.30.01	
	378	123	595	2.3.2000	1.55	5.311, 12	646.10	. 65, 02	5910, 00	1.151, 10,	5 755, 01	933133	3 (3), (0)	3 501: 14:	5.330, 5.2	335000	3.525, 00	5065.0	2000 0	2 301: 01	+
71/7-21-173	1115	**	-Jus/ 9	56 509	1.50	5.00 111		1.80-	192 00	D 0	5.80%	- st- 0	55000	1 % 1111	716	418 0	3.931	18.14	*6 I	*13.0	MW-54-12
	:30	123	,595	8 12000	13.15	6290, 10	2 (3): (2	2,380, 02	4,530, 00	1.210, 06	1.760,01	6.281:01	3.500, 00	1166 15	2.3%, 4.	3.27E (C.	3.7%, 000	1.5% 00	20.48.00	2 (1): (1	_
MWSHILL	:11	123	.095	1, 13 306	14.55	7 (9), 52 31 (0)	2.98 (2.	2000, 02	3.77), (0)	1130.00	8 781, 01	1.2634	1.25% (4	7 (84) 144	6.5500	5.43E (C.	580, 00	311. 01	2.86 5.	2390.00	MW 04 14
***************************************	102	183	- 915	, ,	1133	189 3	56 8 02	166 01	9"	1.98 0	6 40	-1.19 00	190 0	5 31-	502 - 2	3 330 11	3 101	4 1 0	8811	2.13 ()	1 11111111
-	118	144	- 915	1 19 Viii	PP	181 3	5 50 115	56' 11'	98 1	118 0	69 401	8 535-1	188 0	5 550	-1.11 -0	5 ×1- 11	4.49 mm	2 Seption	139:0	1.80-01	$\perp$
	316	155	- 913	1.57.8	1 25 Dr	1.10 3	5.846.00 6.96.00	146 0°	. 59.,	131.0	(15, 10)	16 0	\$01.00	1 90)- 4 9111 mm	188 - 1	2 4 E 14	50%, 00	230, 30	5 846 m 2116 m	2.5 He of 2.11 a. 0.	+
	376	111	,305	1.22.2538	15.35	1 130, 13	31: 10	3.1.10	. 600. 131	1 230, 16	\$0,0,0	. 571, 16,	1.915, 50	3 (84) 144	1980.00	2 (3): (6)	3 (%, 00	1.15.01	. (Olt 5)	2871.00	+
	507	100	, 30.5	1, 11 3 08	1,0%	110.0	2331:02	. 720, 02	2001, 64	2.273, 16,	17750,00	91. Kli 14.	3.9(0.00)	5 301; 55.	\$671.5.	5.7h (c.	5390, 101	1381, 101	2 (/4): 0.	2 391: 01	
	D16	100	, 30 S	2.3.2500 5.6.2500	12 1.	1.130, 43	2335 02	. 771, HC	. HE SI	1.76, ic. 1.89, ic.	9.5.1.01 5.951.01	\$ 385 t.3 1 95°, 101	3.15%, (a) 197%, (a)	3 (6); (a). 3 311; (a).	2006,02	2 % It 10. 3 38h 10.	3.202, 000	2.210, 00	2 VII. 5.	2.76, 0, 2.211, 01	+
	510	100	3015	8 1 2 3 8 7	1, 15	1.00,43	3.86.02	23%, (0	. 180, 61	170,00	1920.01	6 TOE ST	2.910, 00	3 331: 144	. 5,15,00	3 721: 10.	3740, 101	1.01:51	2.29: 0.	2.90(.01	+
	:11	144	,300	1, 13 3 0 6	12.13	1.100, 33	2 881: 1/2	2.030, 02	. 510, 01	1830, 00	7.720,01	1.685, 00	1380, 00	1.516: 55.	, T.E. 00	3 , 21: 10.	2 125, 00	4 o H; 10.	1 921: 0.	2.211: 01	
71/4 41 1.3	100	1723	185.1	53.5iiC	13.1	200, 103	6.071, 0.0 5.939, 0.5	1711: 52	2065, 01	2 (4) (0)	8 31 F G	1300 M	3.628-00	116', 00	921, 144	3 (6), 50	1.279-100	\$167, 00 63° 0	7 F 51	2.015.6	MW-54-17
	113	15	- 10 1	[11]9 Yan	12.13	191 1	2.00	202 11	30 1	185 0	6.7 401	986-1	3.50 0	3 01-	2106-20	18 1- 11	3 18 (0)	13 111	20)	1 0 0	+
	- 01	*5	- 50.1	51.8	I b	181 3	5.83(-0.0)	3.16 07	0.1	180 0	9.39.401	- 5 (-10)	181 0	5 80	5.5	5  - 11	3 Jg 181	19.00	, 84-	,9, 11	
	118	- 15	- 101	11116	11.35	211 3	2   [-112   45[-112	15 m²	77	1.18 0	5.75 at 1	6 1 de 6 1 de	20 0	1001	1 10 00	2 10 11	318 00	85 10	1.296.0	2 00 01	
	160	- 15	- 50 1	1111 346	158	I to	420-117	5 0	91 1	1108 0	2 40	1.010-1	13 0	157	281.0	3 5 3 1 - 11	119 00	1165 141	671	2.50 0	+
	16	15	- 50.1	13.100	PD	1.08 4	5.356.02	585 01	9-1	1.18 0	5.94 401	4.85 0	3.03 0	3 (4)	23 a 16 - 0	5 5  - 11	191 11	10 00	13.11	1.6.0	
	10		. 90 1	81,100	1.15	18 3	3 3 - 112	8 1 07	\$ 90° 0	1.165 0	95 40	3 Sale.    6 0	916' 0	3.111-	45 51 40	2,636.0	3   2   101	- 38" 11	576	2.207 (0	_
	10		- 10 1	1113 306	1206	184 4	3 20 11,	209 02	37 0	1.50 0	35 401	900-1	645 0	901:	- 25h 0	, l- 11	686 (0)	-1 0 0	911-	2.50 0	+
XBV-51-190	100	gu	-1.69	53.500	8.0	\$ 115	6.11	1.10-2	1.95 - 01	1591-0	014	1 ×1.	5 151-110	9.20 000	131501	190 0	5.5 [- 11	181 0	30(1)	* 80 01	MVv ::4 19
	115	16	- 65	1 19 50	13.15	115 4	5 % 05	. 66- 11	9 1	218 0	56 201	4.017.00	3.45 0	1 15	941.	3 SE 11	56 1111	-1 11	Pol-	191 0	
	101	197	- 69	1.57.8	113	214 / 3	5.59-05	3.6 × 0.0	701 1	2.16 / 00	9 ,01	6 (25) (1	3.15 / 20	1 / H	258 20	1.58 O.	\$ 65 , 101	-1 80	1.00	13 1:01	+
	115	14	-, 64	9.22.06	Ji 3	181.7	68)- 02	. 180, 02	, 95,7-1	1.105.0	88,501	8.96.1	1.98.7 0	v Ship	88	, 95E H	35,500	5 F 0	1.250 0.	2.30 00	
	305	1%	.765	7.22.2148	15.5%	1.050/48	.51: 102	. 390, 00	2130, 61 3380, 61	1.3%, 00.	9.100.01	8 (5): (3) 5 (1): (4)	1 980, 00 5 000, 00	3 (11) (A) 5 5 H: (A)	, 53E 00 6 EU.0.	23700 0G	37(2), 101	8 (C), 50 1 80b (c)	. eH: 5.	2.920, 00	
	5/6	156	765	1, 11 20 8 2 3 25 pg	12.35	1 130, 13	2.58: 02 4.88E-02	386.00	5,98,5 GI	3 121, 00 1 851, 00	3.850, 01	1.180, 00	3 181, 10	37.01.00	7 87 5	3 0.80 00	3 %, 101	5 (14) (4)	2.371; 0;	2.800.00	+
	509	1%	.765	\$ 6.2000	16.27	140, 0	3336.10	. 860, 02	. 981, 131	2071, 10	4155.01	2.3.1.06	* 557, (0)	1811: 35	8.9 E. O.	3 804: 00.	[105], 001	2 804: 100	1938 0.	2.23(: 01	
	:10	1%	145	8 1209	1, 25	1915/3	3 (2): (2	2,361, 62	. 981, 13	2000,000	97.1.01 3 (a), 01	550, 00	3.310, 50	3.501; 14.	5 281.5. 3 80 00	\$55E-00	15%, 00	1.37.00	2.45.00	2.476.01	
VW 55.21	00,	156	76.5	1, 13 200	.3.51	200, 03	1.27E-10	2.030, 02	1.690, 61 1.690, 01	1.9 E. (c. 2.0E. (d)	1955.00	7000.04	8 6 E. 100 1 Std: 00	5 (2); (a) 5 (0); (b)	3 .80: 00 130b 01	5 (2E ) G 5 (0C, 10)	973E 00	1100.00	5 tide (G	2.260, 00	MW-65-24
	102	16	- 1	6 % .	1.1	316 3	1981	8 07	5.75	4.8] 0	1.61	D: 0	100 0	1.00	1.6.0	5 ×  - 11	16 101	NA.	NA.	NA.	1
	118	16	.,	8770	1.1	2.1.3	581-115	5.1 0"	231 1	16 0	616 201	-19 %	1.9 0	s 11:	1.50[00	1996-0	3.1 00	- 935-0	21 1	231 0	
	101	16 16	-,	1.16.50	10.15	111 3	5 45E 115	5.68 0.1	1.50	161 0	8 15 and 9 75 and	6 '61 1	161 0	1.916	E	3 SE 0	23 00	AA HEL	NA I KTI-	, of of	+-
	16	16	٠,	151.8	13.15	108 3	59E-115	15 02	255	15 0	189 401	100 0	231 0	5.79	.0.33.20	Sask or	102 00	1.256	11 1	1.9 0	
	907	16	2.1	81.208	1315	1.100, 13	531: 10	. 9.1, 02	2,220, 04	1.360, 10.	5.73(),01	1,37(; ; ,3	21%, 50	3 (4) 10.	2.850:00	2345 00	1180,000	6.11: 55	1.216.50	2.416.01	
	316	16	2.3	15.21.208	13.1 -	1820, 12	2.57E-02	380.00	(65, 11	1800, 00	5.550, 01 3.850, 01	350, 00	5130, 00	5 (C): 10.	3.55§ 50 1.33§ 00	3 Shift	6.5%, 00 3.5%, 00	177E 00	2.181.14	2100, 0,	+
	10	16	- ,	1.97 0	1.3	111 3	1696-01	8 01	22 1	188 0	65 40	- 8 1-	100 1	6 1:	2081 20	19 1-0	5 [3 100	1.891-0	950	2.22 (0)	_
	- 11	16	٠,	855.00	1557	1 49 3	5.595 113	53 02	50 1	2.82 0	27, 201	- 9 1-	3 1 0	3.0116	1. 85.00	1976-0	3 5 7 101	1830		* 50E O	
Phases	1.5	16	- 3 8	11, 0	150	138 3 316 19	180 3	\$16 0°	98	1.08 m 18.16 m	59 Jul	. 100	9.5] 0 5.5 lt 00	5 30 11	3 8 15 mm	5.50 0	18 00 1 10 0	180 0	5.50)	5.80(-00)	MW ab 3
	100	3.	-118	6 % .	1.8	316) 3	391-113	81 01	5 % 1	331 11	9 5 40	-15-0-	3 16 11	5 81-	- P 0	3676.0	3 5 101	AA AA	NA.	AV.	16.43 (9)
	118	41	- <×	87.50	11.50	5 650- 114	911- 2	5.940.002	\$ 10 -001	5.4%-0	8.59(-0)	9.45 20	5136 on	1.74 (0)	(All-art)	1.94k (t	5.0000	199 (0)	968	1.18.35	
	101	37	-118 118	1 28 2538	1, 19	2,330,43	15/4: 02	2970, 00	316 I 26E, H	2740, 10,	1 Hr 52.0.01	5.286 G.	2.120, 00	2.266 (4)	1.3 Hz 00 A 900, 00	2.74:00	2.325, 00	NA 1.26.01	NA 1 191: 0.	NA 1.56E-01	+
	306	32	118	125 2538	1207	100.3	8sh (C	. 120, 100	3 115, 51	186, 16,	91.5.01	. FG. 00	2.260, 50	2 200 Miles	2.3 H; (0)	2 04:00	16.1.00	5 22E 00	. 251: 14.	21 E. O.	+
	507	32	13.8	81.208	16 F	1.730, 43	2.086.02	. 9.1. 02	2.5 E. 14	1 121, 00	1,280, 01	3.501:01	2,170,000	3 TH: 10	2.5%, 5.	2.33(; 10.	3.950, 000	1.26E G.	. 230, 64	2080.00	
	0.6	32	13.8	2 1200	13.19	8 530, 42	1.28E-10 3.77E-10	3.8 C. 00	3.510, 61 3.510, 61	1,821, 00,	1,350, 01	105, 00	31 E, 50 67E, 50	3 (8); (1); (1 (8); (1);	. 580,44	2.786 (G) 1.286 (G)	315), 00 500), 00	8 PC/01	2,900, 01	2.690, 00	
	510	32	13.8	8.5.200	13.15	2,830,43	3.71E-02	2,860,00	3310 GI	2,880, 00	1 280, 01	105, 00	3 520, 100	3 16H 144	2.660.00	3.35(; 16.	3.7%, 00	2 (81) (0)	2.03(; 0; 2.03(; 0;	2.281: 01	+-
	:41	32	13.8	11.2.2549	12.34	2,370,43	2 + 46 + 12	. 880, 00	2860, 14	2.100, 00.	7,170,01	6.501(3)	1230, 00	1566.00	2.57[5.00]	5.30(£.00)	5.725, 000	5.5E-00	. 131: 34.	2020.00	
7,45,43,41	100	- 47	%×	1 9706	3.30	3.5 (6)	1.68* * 3	1.506-13	2.287 (01)	340 10	8 0b2	1206.22	3.3° F 100	380' 00	3.57 17	1500, 500	\$75 p. m	1.500,000	13010-11	5 301/2000	MW-65-5
	0.03	-	78.8 78.8	6.78.1	1206	2.9E. (3	5 SE 03 ,5E 03	\$5.0, 00 53.0, 00	21 1	2.380, 10,	985 au	1.995 1	3.6%, 00	3 80 () 1.1.	-160 at 1.555 00	2.876.00	3.50), 101	6.3E.00	NA - sels in	NA	+
	901	i-	28.8	15.16.200	10.05	1000, 61	556b (C	34,0,00	2 231, 14	2 (9), (6)	+150,01	1/804:00	2 821, 100	3121: 14	8 800, 10	3 - 41 16	29%, 00	NA.	VA.	VA.	_
	0.6	1-	28.8	1.28.2538	1 12	T 181 1.3	* 331: 10	2077 102	2.587 (3)	2.100, 00,	5.357 (d)	8 (TE).	216, 50	2.30(1.55)	250 50	28.1: 00	2.252, 00	1.59E-51	1.89E 0.	2396.01	$\overline{}$

The State of the S

IPEC00224893

																					1
Well ID	SAMPLE	CENTER.	SAMPLE ZONE CENTER.	SAMPLE COLL	LCHON							١	NALVSIS RESUL	FS							Well ID
Wellin	ID	depth it below top of casing	elevatina ft mst²				TRITIUM ( pC FL.	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			Ni 63 (pC i/L)		1 """"
		top or country		Date	Loar	Result	Std Des.	MDC	Result	Std. Dev.	MDC	Result	Sid. Des	MDC	Result	Std Dry.	VIDC	Result	Std Dev.	MDC	1
	0.00	I.	28.8	125.2538	16, 35	5 9/0, 13	139, 12	. 10, 00	26% (4	1701, 10.	6.5%, 01	. 10. 16.	2,350, 50	1.251: 11.	1 (3); (0)	2.5% (6.	178, 00	1 (0): 01	. 251: 1	2130, 00	
	508	17	28.8 58.8	8 1 2008	16.38	6310, 63	3.35(1.102	. 9.1, 02	2,921, 61 1,945, 61	1.300, 00,	3.540,00	6 53E 01	\$795, 10	3.50h tit. 5.27h tit.	1.295 00	. 75E 00	3.302, 00	1 801: 50	. 260, 64	2060, 0,	+
	110	i i	-74.8	2   200	12.12	7.131 1.1	9:91:10	387 07	2111 11	2012.00	3.65" -01	-3.3-4	3111 10	3 961- **	-161 -0	3 331- 17	3.65* 101	4 No. 30	739-0	2701-01	+
	10	1	.18.8	18:0	10.85	101 3	5.58.03	8 07	5" 1	288 0	5 18 401	4 (May 1	694 11	1876	- 58E 0	1.195.0	133 (0)	1566 0	1 30 0	5 He of	
	- 11	1	.78.8	8 ~ 5 (10)	14.5	51 3	5.356.02	1.65 (17)	285 1	118.0	6.15 401	- 31-	* 6 0	3 H:	. RND 0	5 SH 11	3.1 (0)	8 abl: 0	13900	2591-01	
174.55.3	1.5	- 1	.78.8 18.3	11 77 0	6.10	5 07	5 (SE 02)	8 07	5 (cm)	517 m	1 (6 a)) 8 (6)) (4	1 801	18 (-00	5.5 Hr 3.50 mm	2.87(-10)	5 1 p. m	58 (-0)	27 (6.0)	511) 5 (0))	5 50 m	MW as t
1 35 20 5 11	100		8.5	6.61	11.5	189	10.00	82 02	-1 19 ar	55 16 1	6.66 40	-0.3 [-	1.16 0	3.10	2.380-000	1 889-11	181 00	1 900 0	1.5 fr 0	671-01	R 49 GO 2
	118	5.1	× 1	8 '	12.29	116	K51- 113	2115 112	-2.65 44	6 16 1	906 40	8 51 - 1	* 9 . 0	5.715	5.99	1561-11	285 (0)	AA .	AV.	NA.	+
	- 01	4.5	× 1	3 . 8	1,3	. 93	5 p. 105	3 07	8 [60]	XX [+-1	9 40	3.85 - 1	3.60 11	5 × 1:	59 - 1	5 (8)- 11	500 101	T. III	55 I	180 0	
	118	5.5	× 1	1 11 248	15.5	3 00 1	646.02	65 01	8.3 pan	53.16.1	5 [5 40]	- 9%- 1	538 0	6.610	8.1% 0	136.0	6 '5 101	NA.	ΑV	NA.	
1.47-16-15	507	31	18.3	1.6 5.00	100	50 0°	381: 10	1.986	25 (Eq. ()	6.11 ±0 9.63E.61	545 68,1,01	5.65 201	6 SE 00 6 TE, 50	5 80h 555	2.776.06	5 H = 0 5 2.E (G	1.440 0 1.630, mil	NA NA	VA AV	VA VA	N/W-58-9
12/25/23	100		.0.	48.566	1.5	5.1 (2)	161 1	1 765	2 (4)	70.00	9,000	1.676	55 1:00	8 15 (0)	- 1: 000 - 1: 010-1	5.21 0	58 F 0	AA	AV.	AV.	MW 35
	11.5	1	- 1	113. 0	10.2	1.65	55E-115	1 02	part.	2.16.1	81 40	0.71	* 11 11	5 01:	25.50 %	19 (-0)	5.5 (8)	3 900 11	5.500	5 \$00 - 00	1
	118	- 1	- 1	150	15.7	1.8 3	5 F 105	27 07	280 0	9 16 1	8.9 art	180 0	180 0	5.50()	0 - 1	5  - 11	36 111	- 00 - 1	80 0	8 80 0	
	0.1		-1	6 *** *	D 13	185 4	5.56.02	5.3 10.5	8 0	1.18 0	1.96	13 le 1	3 40 11	5 851-	- 8 h - 0	1876-0	, R (m)	1 gsp - 11	, h	1 16 11	_
	306	-	1-	8	9.35	1.19., 53	552E 10	13%, 00 . 340, 00	2 (8), (0) 3 (6), (0)	131, 0,	5 (5), 01	8.5 Me 5.	3.6%, 50	3 (23); (a)	1905.00	2 St. 00 2 St. 00	3.5.2, 00	IVA IVST III	NA . 591, 131	18S. 0.	+
	507	<del> </del>	1-	15.21208	12.22	2,980, 13	7 Sub-10	59.1.00	2131, 101	1326.0	1911.01	115, 00	1621, 30	1786: 55	3.295.00	5 581: 1C	8075,00	NA NA	NA.	NA.	+
	0.6	1	1.	1 n 249	1. 15	3 2 E. 13	1 mile (12	1310, 02	2710, 00	7.496.03	12,0,01	6130.13	5,3%, 10	3.90(: 00.	1.381; 06.	1li (G	[92], (0)	NA.	VA.	AV	
	509	-1	1.	11 1049	15 [*	3.151, 13	2.545.02	. 100, 100	2.780, 00	8.2534	1750.01	2001:00	\$ 220, 50	9 (3E 55)	\$5.00	\$ 50 to 10.	635), (0)	NA.	VΑ	ΑV	
738. 45. 1	00,		5	6.22.2007	.2.1	16,1, 03	8100.02	1366.02	1550, 01	\$50(c.00)	7.578.54	2.29% (4)	93.05.00	1310, 00	3 (44): 0C	3.870, 00	137[10].	220,01	1.79: 0.	1.91; 01	MW-57-
	503	10		8.6.20F	12.3%	1060, 63	3.2.E (6) 2.25E (6)	265, 00	3.7%, SI	1 95, 16,	5,350,01	3 150, 00 8 110 01	2.21% 00	3 831: 10.	3.95), 03.	3 to E (C) 2 25E (C)	3 1.0, 00	3.751, (d. 26.76)	1.35 (4)	2300, 0.	+
	91	10	-	1.17.348	11.55	178 1	2.56.00	2355, 112	110 1	4 80 m	65 -01	3 55 0	25 0	5 bl-	1.811-00	5 80 11	5115 101	-218 - 1	21.31	2.551-101	+
	115	10		11.0	1208	125 3	3 St. 02	0 112	3 1	19 0	55 40	189 0	6.1.0	3.5 (6)	1.10.00	2.56.0	3.05 (0)	13.6	158 1	2.24 (1)	+
17/12/19	101	4	-1	0 24 2 11	1.91	65 115	* **	1.576 3	1.95	D 0	95.14	- 550:00	5 fish in	5 30 100	-95 to 1	100 11	\$800.0	2 pag	1.890.0	1.59(-0)	MW o/
	11.5	10	- 24	86.0	PB	9.06	2. 36. 02	08 112	13 11	55 to 1	5 8 40	2.16.00	3.40 11	1610	505 - 1	2.56.0	5 15 (0)	- SE 0	100	1.361-101	
	118	19	- 24	1.15.506	1513	181 3	35E-02	9 11	5105 11	2.66.1	185 40	-191 00	3.91 0	1×1-	2061 at	56 F H	1.95 mm	-5 Kills ()	911	161 0	
	105	19		1 1 1 1 1 1 1 1 1 1	11.5	181 4	38 10 00	9 0	3165 11	100.0	1 Hr 85 and	-191 00	5 6 0	1×11-	2.57(-10)	3.51:0	106 00	1.40	0.00	2.915.01	+
17/1-97-15	100	- 1	-25	8 71 7 106	6.30	116, 113	887. 7		NA.	NA.	AV.	-1841-1	3   100	1807 0	- 8 b- 1	3 891-	137E-0	NA.	NA.	NA.	MVV 57
	- 01	10	275	8 77 7 6	9.5	100 3	5-941-115	31 01	88 I	3.8[ 0	* 116	-5.5 [6]	6 5 0	101·	1 95 00	5 (5) 11	5 101	8 101-	0100	9.00.00	
	0.5	10	278	6	12.85	955	1886.00	1.85 (0.7)	gu u	108 0	×65 -01	- 9 1-	3 [0 0	1×"1-	48.81.00	5 % (F. 1)	\$65 (0)	5 15 40	241-	1.13 0	
	113	- 10 - 10	28	86 ° 0	12.56	10 1	5 (F. 112)	96 11.	2.26 0	X 16-1	5 (6) a(1)	- 5 0 P-	118 0	1806	489.00	9 % (F) 11	1.75 mm	- SE 0	9 (8) (1	5.59(c.6) 6.7(c.6)	_
	105	10	.75	1.1,700	13.03	1111	3 to 11 to 1	3 . 00	50 0	29 To T 6 9Hout	108 301	1 1 1	168 0	1 (A) (A)	915 a T	1.176.00	51 , 101	-18 h to	191-0	2.275.01	+
	100	10	.25	17.7.0	11.55	119 3	2606.02	9 0	3.25 11	8 995.1	6.15.401	181.1	201.00	1 DI:	1 1 1 1	viole ti	112 000	8 96	1.61	2.35 (0)	+
101-18626	100,	2	-5.1	16.50.6	.3.25	-25m; of	1.500, 2	1.600-2	V 01% ;	90,000	8.54%	2.6	81100	150, 00	44 De I	430, 0	3 x 10 0	-3.59	5.00	A 501- (0)	MW cb 2
	9.0	20	5.1	. 5.2007	N 5"	240,42	84:10	. 800, 00	8000.00	7.505.01	8,500,01	2.34) (6.	2.970, 60	3.206.00	550.01	2735 00	3 (60), (0)	3.50(g. 00)	9.90(j. Si)	1 (0), 00.	
	518	20	4.1	6.2.2567	1, 15	59%, 40	2346.02	891, 02	.00,00	9 (55E SI	5.250, 01	. 621: 10.	2 (2), 50	2.861; 10.	3.910.00	2 (2); (6)	280, 00	1,078,00	. 211: 5	1.85, 0.	
	501	20	5.1	1.35.75.58	1, 06	8.560, 02	3.556 ±0. 626 ±0.	2,580, 02	1.181.01	0.33[cd] 1.03[cd]	5.780, 01 9.660, 01	2.25.51 2.25.51	2.310, 60	3 831; 10. 2 971; 10.	5 111.02	3 to 15 oc.	25.5,00	NA NA	VA VA	VA.	+
	200	20	5.5	11 1 25.58	13.35	2.380, 62	551: 10	630, 00	2.3.16.00	0.00000	186,01	3.380, 101	60 E. 50	5 (9); (d)	3 230.00	1.581: 15.	1841, 00	NA.	VA	AV.	+
	907	20	5.1	2.3.2009	12 F-	5 190, 32	2396.02	. 980, 02	8,350,10	5.276.01	9830,01	. Bl: 06	2.76, 50	3.296.55	. 151, 141	30.745.06	33.1.00	NA.	VA	NA.	+
	0.00	20	5.1	1242559	12.2.	1130, 32	181: 10	. If 1, (C	570,00	1.53(1.1)	5.900,01	. 291: 00	1281, 50	2 851: 144	. 021.44	23.1:00	2.570, 000	NA NA	NA.	AV	
	16)	50	25.5	1 13 Yang	111	178 7	6 E 02	9K 11.	1 950	5 (6l) I	6.95 and	640-0	848 0	5.581	1.996.0	5.680-0	6.00 (0)	A.A	NA.	NA.	
1.11-28-22	000	51	- 90 t	15 50 5	9.55	20 (c) (d)	1.80 ° 5	1.506	46 (64)* 1.6 (64)	8 16 I	8 0[s 88 a)]	1.50p -1.95 00	5 5 00	1 00-	-9 1s-1 -1 80 a0	2.36.0	5 (E) (III)	24 50)	5.00	8 0 0	MW db t
	115		-19 [	6.1.1	9.5	315	4 x 15 m²	8 0.	4.9 20	3 9010 T	36 20	-1 99-	2.3 0	1000	2,360-0	3 1: 11	2.35 (0)	2.80 .00	A11-	1.15 0	+
	- 01	51	.39.1	, .	1.0	3.15	3 71- 113	3.3.02	6.3 1503	5 55 1	6.53, 401	1180-0	3 (0) 11	3.3 1:	1.25.0	5 10-11	3.45 (0)	AA.	VA.	NA.	
	305	51	31-1	1.22.2548	1206	3 130, 30	::21: +/2	, 6%, 10	1.2.1:0.	5.85[; 1.4	1,220,01	5.510.01	3.93(), (0)	376E 35	1.230, 4.	3.2% (0.	3.05), 00	NA.	AV.	NA.	
	506	51	35.1	11 1 2 3 3	13.55	2,810, 42	55E 10	. 621, 102	8.50.0.	877501	8/820,01	9.30.40	3.380, 00	3 854; 111.	, 58E 00	3.2.1; (6.	2580, 00	AA AA	AV A	VA	$\perp$
	16	41	35.1	13330	1205	144 1	2136.02	196" 10"	2.65 and	877F1	6.56 (0)	96	3.711.10	3.016.00	4.81 40	3 1 SH 1 H	3.8% (0)	AA AA	AV AV	AN.	+
	16	-1	-19 [	1.3.306	12.53	11 1	264-117	60 01	0.39(-0)	6 % 1	6 % 40	3.1	7 11 11	6.176	1.800.0	56 1:0	18 101	AA AA	AV.	AV.	+
1.47-22-0	101	1 1	- 15	16 50 6	1.5	18 0	1 .	1.600	de Tear?	Strate	3015	86 44	19 15 00	9 301 181	3 0[50]	150 0	33 10 0	-1506	5.000	201-101	MW d9
	11.5	,	428	8.20	9.1	138 1	F-112	8 02	3 par	5.16.1	K 2 30]	8.10.00	3 841 11	2.00	1.90-0	59 F H	11 00	- 5 h n	5.30 0	840 0	
	115		428	6 ' '	15.35	16 '	5.25(6.112)	1.35 (17)	4-9K m.	5 Klo I	91 40	6 1 - 1	3.06 11	1.50)	-119 at	5.35(0)	1 00	-13 -24	1.296.0	1.38(-01)	
Andreadas	- 01	- 1	- 15	91 ° 0 16 50 6	1138	635-117	1.501- 2	540 m2	1 01401	6 Plen	361-0 8 01-	1.7pc 201	5 4 5 mm	5.20.00	g jani	\$10p. ct	3 SE00	AA	NA Nub	NA A Sub- uu	MW of
4 11 - 10- 14	500	i i		. 5 207	7.18	8 800, 51	80.1: 10	. 855, 02	506, 50	7 80E 0	8 755, 01	. 196.02	126.0	1 701: 141	2000.00	3.50E-06	165, 00	2.50(: 0)	7.500, 000	8700, 00	16 AA CON
	3/8	12	27.5	6.2. 2557	15.25	7.5 (0.142	1374.10	1310, 02	274.01	0.801:13	5 150,01	158 5.	2.5(0, 10)	2 831: 144	8110.02	2.06.00	2 (%, 00	110.00	1 (fl. 0)	1.716.01	+
	201	12	27.5	13, 255	13.58	2 190, 42	100.00	. 650, 00	1 645 0.	\$700,00	1.060, 01	1.380.01	3.521, 100	3.70(), 55.	7.600,01	3.35[: 10.	3.955, 000	NA.	VA.	VA.	
737.35+6	00,	58	9.4	15 2005	.1 %)	5.500, 00	115.42	1.896; 3.2	. 2010	12(6.0)	8.06%	1 .51: 42	E 0.	460C, 101	100,00	3000, 00	Vol.15 (C.	2 301: 55	\$ 70E to.	6.30[(.00)	MW-56
	300	.58	13.5	.3200	10.06	1.960, 30	831: 02	. 800, 00	3.301/01	8.46.4	8 850, 01	4 Tel: 0.	680, 00	3.0E 35	8000,00	Social Co.	185,00	1.908.00	1.90(1.00)	8 100, 00	+
	503	59	13.5	6.2, 2007	15.25	5 WC, 42 8 DC, 42	1.10E 02	13%, 00 2480, 00	257E 0.	8 704: 01 7 080: 01	1 03E 00 1 98C 01	6.3%, 61	3.500, 00	3 801: 10. 2 161: 10.	1 27E 06 3 72E-01	2 % It + 0 G	3.625, 00	- 23t: 50 NA	, 301; 5; NA	1.360, O.	+
VW 61.38	00	31.5	15.5	5 8 No.	1 5 5 5	91% 50	1.197.10	1.596.13	1.536.0	3 28, 11	58,70	1.016.0	2.881, 101	3 307 100	5 15' 11	3 757 710	\$17,000	100100	41, 11	*1** II	MW-60
	115	410	22.1	4 4	150	61 '	25 (6.02)	8 02	6.38500	58 16 1	166 401	2.92 - 1	1.76 0	1 141-	28.81 20	3 1: 11	8.89 (0)	AA .	AV	AV.	1
	503	319	22.1	3075 (2007)	13.25	180,00	181: 10	. 3.1, 00	35.150.	\$500,00	9.780, 01	. 5.15 (C.	60%, 00	3.516.55	0000000	2 - 45 00	26,5,00	NA.	VΑ	AV	T
	501	319	22.1	. 1208	1" (15	1.181. 14	581: 10	. "80, 00	51.40.0.	8.58.51	8.981, 11	. Lib (G	3.210, 60	3.79(5.55)	916,0,	3.30(1.00)	330, 00	AA .	AV	AV	
	505	319	22.1	1212008	15.35	5.510, 61	. 4: 02	. 95), 10	3.15(1).	1836.01	8,340, 01	8 5,155,	2060, 00	3 37 (: 1.1.	8 730, 00	. 985 00	2,562, 101	NA.	AV	AV	_

<sup>1</sup> to 8 950 L 800 - 8000 NG 2000 - Quarta 3 Libbs Table 5 Quarter 3 Formatio DVV soss. Macclibed

		1																			T
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER,	SAMPLE COLI	LCHON							1	NALYSIS RESUL	rs							Well
Well III	ID	depth if below top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC FL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l/L)			NL63 (pCFL)		- ""
		top or Caring		Date	Loar	Result	Std Dev.	VIDC	Result	Std. Dev.	AIDC	Result	Std. Dev	ADC	Result	Std Dev.	MDC	Result	Std Dev.	VIDC	1
	0.69	319	22 1	1 40, 20, 3	1615	1.950, 42	2.1: (0	. 9.1. 02	28960.	3.504.03	5.921, 01	. 8.l; (C	1.930, 50	3.50); 1.1.	1.198.00	2 %7E 0G	3 202, 000	NA.	AV	AV	Ť
	207	319	22 1	.1 5 25.08	1513	2 000, 42	85E 02	. 970, HZ	1 (2); (); 3 () () ()	\$ 0.10 M	5.050.01	2,380, 00	5 870, 100 3 mg 100	9 . Th. 55.	3.535.00	8 52h (C.	3.225, 00	NA 3 NO 111	VA.	VA.	+
	216	319	22	2.9.25AW	190	138.12	, St. 102	. 96., 10	28,100	8.2 1534	5 (2.70)	1.15.00	8767.10	5 8 He 11	7.00,00	\$ 12.00 P.C.	658 (0)	130, 31	2 (7): i	- NZ., II.	+-
	10	419	22.1	x . 0	11.1	60	56E-115	55 07	4 (9)-40	11 16 1	3 401	2.116.0	26 0	6.640	4 360 000	5 (4) 11	58 101	5 E 0	1 80 0	1 9:01	+
	- 11	410	227.1	[ An York	To I	q .	526.00	6 01	1.19(4)	6 19h I	5 401	-46 (0)	100 1	16	1.85.00	5 14 0	8.15 00	NA.	VA.	- AA	
174-6-3	100	23.1	.513	1/8 500	155	5.00 0	1.58	1 876 ° 5	-19 Year	5.57 (0)	8 560-	288F-0	1.850 oc	\$11 000	1 51501	4 50 m	1 % 1 d mi	1 × 111	4 I I	-11- 0	MW
	113	53.1	.1 9	119.5	12.5	113	15 m²	8 07	6 950	5.366-1	5 9 40	1 345 T	3.01 0	3.5H:	20, -	3 50 0	8 101	AA AA	AV	AV	+
	- 01	83.1	-1.9	1.8	Dil	5 (5 )	201-112	8 U	- 65 44	5.386-1	59 40	-1 10 00	1.8 0	1.681	- 89E 0	1996-0	2.5.101	NA.	NA.	NA.	+
	108	83.1	-1.9	1313 8	1213	-1 P	26.112	06 11"	8.5 [ca)	5 96 1	8 57 40	-18-0-	*1 0	5 414	- 550 O	25 (-0)	\$ O <sub>2</sub> 1111	NA.	AV.	NA.	_
	0.05	53.1	E-9	1 8, 25, 8	13.23	1,280, 02	5 80h (0)	, 74U, n2	6.53(10)	\$335.0	8.581, 01	. 985.5.	20%, 30	3.08 (6)	1355 00	23.45.00	3750, 101	NA.	AV	AV	
	- 0	83.1	.1 9	157.8	15.32	1.48	X  - 115	95 111	- 95	5836.1	X [ -0]	8 15 1	188 0	5.2%	1 90/- 101	5 80 0	664 111	NA	VΛ	ΑΛ	+
1.4% 23	160	53.1	.513	10 has	1.78	100	1.0	1.80	58Hs 63 Iso2	\$10 at 5 No. 1	9 6b- 802 ad	3.1	118 1	89)-	5 SH501	8 5 1- 11	\$150.00	0.06.0	1.500	280.01	MW
	10	83.1	-1.9	8 ' 9	13.76	2115	261-112	66 01	Lyden	80.1	Stei att	1.15.00	186 0	2.231	362 - 1	1 880 11	845 00	-3.230	1 1:0	2 00 01	+-
	- 11	83.1	-1.9	Sir Yang	1310	11 '	3 (6.00)	6 11"	1.29(4)	1356 1	612.40	-1859-	688 0	531:	28.81 202	5 951-11	65 111	NA.	NΛ	NA.	+
1.47-6	101	* 4	-40.4	58.50	,	-0.,9	187 7	1.876	18 16	813.00	9.115	1.510	5. 36.00	9 88 181	9.50[60]	3.31 0	5870.0	K What	60)	13 1:01	MW
	JUL.	- 1	519	2	14.2	1.10	690.00	, N II.	52.00	3 (2E of	5. %, 01	1.96 of	3088, 30	5 SH;	1,108,00	x -45 0c	11., 00	I.A	NA.	'VA	+
	503	201	5% 9 5% 9	.015.25.67	1:15	136, 32	13h 10 15h 10	. 540, HD	1.581; 0.	9 (A) (A)	7 120, 01	7 (80, 61	3 780, 50	1.27E 185	9 120 01 8 170 01	3766 (C) 2776 (C)	3.5%, 00	NA NA	AV AV	VA VA	+
	305		51.9	1.12008	12.25	1765, 12	.71: 10	. 930, 00	3080.00	1.826.01	8.381.00	5 (2), (3 5 (3)), (4)	2,370, 30	3 (Cl) 55	80.1.01	2.231-10.	375), (0)	NA NA	VA.	VA.	+
	0.00	-61	51.9	1 8. 20.8	13.25	8 270, 33	5 (5) (0)	. 630, 102	17300	. 1.1:11	2.330, 01	879bb.	23%, 50	3.916.00	1.15.00	2.175.06	3980, 00	NA NA	VA.	VA.	+
	507	72.1	51.9	.1.5.2048	11.58	196,32	646.02	. 780, 00	23/4:00	0.40(0)	7,780,01	0.43(1)	5.680, 100	9 (8) (1)	135 00	5.3-4; 16.	560, 00	NA.	VΑ	ΑV	
	0.6	72.1	35.9	2.9.2009	1. 25	1,670,30	550: 10	, 650, 10	1160.01	1,060	5/800.00	0.5 (6.5)	3000, 00	3.30[: 11.	7.830,00	30.06.00	3.6%, 00	525, 00	2.211: 5.	286, 0.	
	10	721	45.59 .59.9	4.5 20 and	16.32	1370,40	50 F 10	75°, 00°	6.32(-02	5.885 1	55.50	2.25(-10)	1100, 61	7 30H 555 4 6 Hr	1.59-101	5 SE 0	7.50, 00	- NA -2119-	1 N- 0	, III of	+
	10		.599	I by Yard	1.08	1.3	380 m²	6 0	1 2502	5 380 T	58 att	211 (0)	155 0	n sints	25 1:00	75.0	8.65 (0)	NA.	AV.	AV.	+
Science se	100	1810	42.1	18.30	1.13	2.85 (0)	1.85	1800	5.5%	5 0	Illa	- NF H	5 % (F. 10)	510 111	1 1501	311 0	55%	185 (0)	3/3	202	MA
	11.5	319	. 14.1		16.0	3.07	3 Str. 113	8 02	- 15	5 Slo I	169 40	1.80-1	2.00	5 P	× .	2635-11	\$145 101	NA.	AV.	NA.	1
	118	51V	- 14 1	114,	15.5	8.50	×5 - 115	8 02	- 19 41	1.386-1	63 40	4 88 (0)	3 [0 0	3.575	488 40	55 F H	84)/2 (11)	NA.	ΑV	VV	
	01	91-0	2 99 5	11.8	1513	3 9 1	80)- 11°	94 07	. 96 41	5 16 1	8.85 art	4 33 00	311 0	5 %[-	1.75	36 5 11	3.55 mm 4.04 mm	AA AA	AV.	AV.	$\perp$
	100	310 310	. 27 1	73.7 8	13.33	101	131-117	91 07	17 100	3 100 1	5187-01	-1500-	1797 0	1 (A)	1.33(0.00)	2 1:0	505 101	AA AA	AV.	AV.	+
		110		15. 8	D 19	120	2 [6.02	96 07	- 40	5 10 1	[8 40]	-1 86- 1	8 1 0	5.500	- 5 % 50 - 11	5 Nr. II	8486 101	NA.	NA.	VA.	+
	16	310	. ** 1	.0 . 100	1204	191	6 F 02	69 11	88960	5,996-1	6.89 40	P 0	106 0	1 341-	1.11	5 SE II	\$ 65 (0)	3 1 00	2.5 p.	1.88 0	-
	16)	315	. ** :	5.5.5.00	10.83	31 1	85E-03	10.5	- 21	6 Ye I	[5 at]	25.77 (0)	1.9 1	× nl-	512 -	5×1-0	65 (0)	A.A	VV	VΑ	
	10	110	2 44 5	x . 0	10.82	5 16	64E-02	69 11	16ston	5886-1	8.18 +01	5 0	446 11	1.46	144.	35 F 0	495 (8)	-1 Tr	1 1:0	1 1001	+-
No Zerut v L	11	119	41.19	10 40 No.	10.55	3.1 2.00	351-112	6 . 00 Later	5 OF-	5 9 8 5 cl	6 501	5 , 0 9 , ad	683 J. JO.	8H:	- 2.3 Me 200 BS	5 h8F (U	1.150-0	NA nation	NA 681-	NA LS Ion	E/VA
INSPECTO	92	.513	-, 11.4	12 101	16.13	162., 2	2 99 02	. 8., 02	1, 23, 40	1396.1	5104,501	8 96 1	13.0	1500	3 11-100	2 (2)(0)	38 , 101	NA.	NA.	VA.	1000
	0.0	.511	.45	2015 (2007)	11/23	5800, 10	881: 1/2	. 50, 10	. 920,00	1788114	+ 330, 01	1735, 00	33(0.0)	3 (61) 144	2.200.40	3.30(), 10.	3.7%, 00	NA.	VA	AV	-
	501	.511	.45	1 12008	12.35	5390,00	2.35.52	. 75, 10	.100.00	1177, 00	1.216.35	. 551: 10.	3.8 E. 10	1.56[; 55.	2 921: 91	134); 16.	182, 00	NA.	VΑ	AV	
	505	.511	.45	121203	12.3%	1530, 10	281: +0	, 95), 02	2.150.01	3 (8):13	1.775,00	1.250, 00	2,370, 50	3 (6)1; 14.	1.29:00	2306.00	3.7%, 00	NA.	VA.	VΑ	1
	50%	,511	.45	7 80 2008 -1 10 2008	13.35	5160, 12 6870, 12	13h (0 1,5h (0	1,9,1,00 1,861,00	5.5800 132600	2.50E.01	3,360,01	8 80E 0.	2.6%, 50	3 Set; 10.	5 PG-50	5.87E (C.	3.250, 00	NA NA	AV AV	VA VA	+
	27.00	51.1	0.0	2.0.2000	12.73	1151, 12	151: 112	. 671, 10	1530.0	7.566.03	836,00	7 10 (3)	3000.00	3 (5): (4)	1318.00	3.516.00	11%, 00	37 E, 50	Profess.	2.125.0	+
	300	.513	.43	5.5.2000	1, 15	1390, 42	25.15.02	. 720, 100	7.394.02	5.70E.01	9.881, 01	2.526.55	6300, 500	1.501: 1.1.	. 37[5:30]	5071: 00	5 (2), (0)	NA.	VA	NA.	+-
	10	513	- 11 4	8 . 0	1.13	818	F-115	69 11"	24.55 (44)	XII. I	969 40	- 5 % 51	801 0	56 F	- 1586 O	5 51:11	8-41 (0)	19 0	1840	5 80 00	
	- 11	513	- 11-0	[man Ying	11.55	100	56h 03	6 11"	1.00(-0)	X 3 [6, 1]	9.5 20]	41 0	0.0	6.691-	4 37 40	8 1 F O	0.00	A.A.	VA SI:	AV.	1
A-6041 6	00	1.59	-164 I	58.50	5.6	8 19	2.500 02	1.60	-16 -01	5.66 40	896 8 art	5 10 401	1.516 (C	1.06	. 66 0	4 90 m	5 (30) 11	69 ti	477	1 561: 0 NA	1/V
	115		- 64.1	11.9.1	1115	8 19	3 1- 113	23 07	-16 an	2 10 1	8 50	-1600-	163 0	1 851	19	3 1-11	\$115 101	AA AA	AV	AV.	+
	501	.78 %	.41.1	. 1258	12.25	6.680, 12	2.25% (02	. 830, 00	766,00	7,876,04	1546.55	2 221:34	3.990, 100	1.50% 0.00	4 PG-84	3.50), 10.	106, 00	NA.	VΑ	VA.	$\perp$
	505	.73.0	.914	121208	131:.	1770.30	2446.02	27%, 10	2.985.00	17,1831	850.01	1815.00	270, 00	1005.00	9915.00	2.53); 10.	395), 111	NA.	VΑ	VΑ	$\Box$
	106	74.5	- 64 C	161.8	1008	8.00	5 to 100	586 07	2.08, 02	5 (6.1)	5.88° 01	3 Sp. 1	210, 10	3.516-11	4.06.0	2135.00	6.35 (0)	NA NA	AN AN	VA.	+-
	16		- 64.1	19.19	1508	916	5 to 10°	9.80- 11	12960	68 16 1	5 5 20	27.576	2.16) 11	1001	31.5	5 SH 11	8 1 101	- MA	71.01-11	, tille of	+
	16	4.0	+ 64.5	55310	1.18	101 3	2636-02	5 105	15 [60]	5 to 1	5.9 att	-110 00	8.15 0	5 (54)	1.39(00)	5.695.0	6.25 101	NA.	NA.	NA.	+
	- 10	* 9	. 64.1	8 ' 0	1.16	1.03 3	936-02	69 11"	2. 45 art	\$ 236c. I	164 401	5.0	181 0	5.116	5.58[0.10]	1 891-11	×0 m	-1586	1 100	2 10 01	L
_	- 11	4.0	2.54.5	Justin Yang	1.9	102 3	K5 - 115	6 11'	2.7 (4)	1,680-1	69 att	8 5815-1	8.78 0	5.950	2.3[]) (0)	53 (6.0)	0 2 , 101	NA.	'AA	ΑΛ	
-6 '-18	- 01	155	1.5	N 111	18 0	1896 (1)	1836.0	580.002	1-380-472	5.53(60)	2 Juni	as tope 1	16 5 101	'89 inii	0640	* 10k d	5 98-10	161 -00	N7F 1	1 4 30	N
	903	13.5	1.5	15.10.200	13.55	376.52	7.36-02	. 550, 00	1580an 801.00	5 d alto 1 5 o 5 l t t l	5.85 (0)	9 1 - 1	3.397.00	1 950 871: 111	238 Julio 0	1 (C) 11 (C)	1921, 00	A.A A.A	AV.	VA VA	+
	501	13.5	1.2	13, 248	15.15	3 800, 12	34: (0	. 340, 02	1586.00	7.550:01	8.270.01	. 181: (C.	1230, 50	1 101: 14	523031	3.386 (6.	3980, 00	NA NA	VA.	NA.	+
	0.65	13.5	1.2	8.6.2008	12.55	2 690, 42	1.15 (0)	2.250, 02	53.1:0.	3,304;03	1850.01	9.400,12	1.6%, 50	2 KG I: 144	1.260, 00	. 506.06	3.330, 000	NA NA	NA.	AV.	$\pm$
	507	13.5	1.2	10.07.3 08	13.2%	1080, 32	65h 02	, 6vd, 02	5.2%: 0.	0.036.03	+370,01	3.056.02	\$100,00	5 only 12.	376,15,00	5.25% (0.	1700, 000	NA.	VΑ	VΑ	
	0.6	13.5	1.2	1.23.2949	1.34	1610, 32	35): 12	. 000, 00	10%, 30	9.078.04	9.060,01	9.884; 01	2,550, 100	\$1.61; 1.0.	3 (20.0)	2.986.00	275,00	NA.	VΑ	VΑ	+
	509	13.5	1.2	1.4000	13.18	1360, 60	851: 102	340, 00	1.798.00	5 (0) (3) 9 (2) (3)	7.1 (0.0)	3.4 (6.5)	5.810, 00	3.871; 1.1.	1.5H; 06 2.5H; 00	3.256.06	1260, 00	. 881: 00	. 891: 1 VA	2175, O.	+
	:10	13.5	12	1 12 206	15.36	2360, 12	2.96.02	2070, 00	15300. 33000	** (2): (1)	7.95(, 0) 8.05(, 0)	8 756 to	2.9 E, 50 6 for 50	3 (81) (1) 5 (0) (1)	2708 00	3 mily 16.	3.280, 00 6.680, 00	NA NA	VA VA	VA.	+
4.65	100	\$3.5	. 9.8	5 10	1.0	10 10	1.0	1.506	5.94%	8 8 40	9760	98 40	7 1-16	23 (8)	412.0	1.54 11	7.3 1-	0 0	41 1	'11  11	N/A
	900	313	15.8	1.29.2007	15.35	2,500, 32	756.02	. 750, 00	2370.01	4.3631	5.180, 01	· 88E: 02	2.610, 100	2.506.00	1230/00	2 % 45 00	28.5.00	NA.	NA.	AV	
	503	313	158	15.10 200	14.55	3 (0), (0)	581: 12	. 150, 02	. 6"[, 0]	4.445.01	9465.01	20,21534	1815, 50	2121:11	* 6*, 0,	, Tale oc.	183), 101	NA.	AV	AV	$\perp$
	201	315	15.8	1, 71.18	13.55	3.977 5.7	::8E: 10	1 2 10	1.33(0.0)	0.0.50-0.1	1 5.50 ml	8 351 1.1	1.130, 500	10716-00	2.100,00	3.8"1; 10.	1157 00	NA.	VA	AV.	1 -

Fig. 15 of 2. See Page 2, for Netco

		I																			I
	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER,	SAMPLE COLI	LECTION							•	NALVSIS RESUL	rs							
Well ID	ID	depth if below top of casing	elevation ft msl <sup>2</sup>				TRITIUM ( pC i-1.	.)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC ld.)			N 63 (pCFL)		Well II
		top or Caring		Date	Logic	Result	Std Dev.	VIDC	Result	Std. Dev.	AIDC	Result	Std. Dev	ALDC	Result	Std Des.	MDC	Result	Std Dev.	AIDC	1
	0.69	315	15-8	8.6.2008	1206	3.910, 12	.5E (C	. 180, 00	2.2%: 0.	2 4/4:31	1541.01	2.550, 000	1.521, 100	2 (74): 101	1,086,00	, 5-d; 10.	2.380, 000	NA.	AV	AV	
	007	315	15.8	15, 29, 2008	13.51	5 350, 42 1870, 62	135.02	, Avd, 102	. 3/C, 101	0.678.03	5.230, 01 5.020, 01	1306.0	3.127 (10)	5 331; 10. 3 131; 11	2.20E 00	5 (4) (6) 3 (4) (6)	5.202, 00 3.367, 00	NA NA	VA VA	AV	
	216	315	-15.8	1 3 7 19	13.13	18 12	32E 02	35' 00'	1 280: 00 -3 1, 1 and	3,1134	8 15° +01	- 736-7	3 (20, 30) 3 (4) (3)	3.56E-11	6 10, 0, -6 16' -0	1 1 1 1 1 K	18 100	41	174-0	* II: 01	-
	10	415	-168	*** 0	16.02	181	3.39-115	2.4 02	-164 40	6 In I	88 at	4 9 00	100 0	1×1-	- 5 E 0	3.56E-11	48 00	NA.	NA.	VA.	
	- 11	415	-168	1.11.509	15.7	11 1	Jr. 115	15 07	-3.1 -201	56-1	8 (8 20)	2014 (0)	100 1	H+	. 80 0	SE U	5 100	NA.	VV.	VA.	
1.4757.3	107	33	-51.5	9.1	5.0	505 113	1.01	1 Th 3	1.1Hs 1.6Hs	9 20	8 S615	55 201	5 T F 00	186 (0)	-9 19-1	3 p. 0	3 Sh 2 In 100	NA NA	10 I	1.68 0	MW 63
	113	*31	.1 3	4.	1635	3 (8 )	545 m² 5 to m²	8 0,	Espan Espan	6 986 T	85 and 8 [5 and	0.100	167 0	150	-8 11 at 68 - 1	7 880 11	3 (5 (0)	AA AA	AV.	AV.	-
	115	441	-1.3	86.16	12.35	3 4 7 1	531-112	24 62	95900	1836.1	195 40	38) 0	2.21 0	1 %1	200 - 1	1 5  - 11	3 8 101	NA.	NA.	VA.	_
	161	~3.1	-1.3	1 50 Yest	14.5	116	5 F 102	6 01	65400	58 10-1	5 Q5 -arg	- 5 9001-	585 0	5 SH:	258 B 0	8 95 0	19 00	NA.	NA.	AV.	
	507	53.1	6.3	. 23 2559	12.15	3.560, 62	2.96.02	2080.00	153(10)	7 (81:13)	8760,01	2.2% (4	3.200, 00	3.77(5.55)	. 27E 50	3.5-4; 10.	37.0,00	NA.	AV	NA.	
	0.00	53.1	10.3	1.3249	13.25	1330, 60	821: 02	1,360, 60	5850, 01 gran	0.08633 656-1	\$460,01 830,00	4.52E.5.	5.300, 00 3.13 0	3.50E ta.	2830.0.	2.826.00	33.1.00	9 . H: 55	1.75E-0. NA	2 (2); 01 NA	-
VW +2-53	016	53.	913	122060	.3.36	28.1.02	100,00	1016.02	3.5 II: 5.	6 150,00	7.27(.5)	25,0,01	2 881: 00	3320, 00	9.721:14	3.250, 101	3.5,1; 10.	AA	NA.	AV.	MWE
V35-65-1	101		-85	5 0 50	1.8	502.02	1000	1.10.2	5.60	831.0	8.5716	-8 8 - 1	5 5 E 00	1 2 101	1.5 [60]	3.21 0	1000	195 101	9 1	1.18 0	BOW P
	102	- 11	.563	4.	10.5	181 1	65E-112	5.02	1.5000	7916 T	K 29 (40)	1.10.0	3.36 11	1511-	21 80 m	5 500 11	3.0 (8)	NA.	NA.	NA.	
	118	- 11	.584	1 10 500	15.55	. 60	5 F 02	55 07	1.550	2,536.1	63 40	18 0	, 13 n	2.086	1.510-00	, ku	2.85 (0)	NA.	NΛ	NA.	
	506	11	58.3 56.3	8 6 2008	1505	353. AL 161. 32	836 FC role FC	2530, 02	3 St. 0.	5.880 of 2.600 of	9 (9), 01 3 (9), 01	826 m. 5 851, til	2.013, 50	3 530 100	5 8,700 196, 0,	2.236.00	3765, 00	I.A	VA VA	AV AV	+
	507	-11	58.3 56.3	10.09.008	12.06	5121, 12 5121, 12	556 (C	2.840, 02	2.54E.0.	280830	5.032,00	2.85., GI	5.970, 00	4 VIII III	3 1: 30	2.24t (C.	7162, 00	NA NA	AV	AV	+
	0.6	-11	58.3	. 23 25.69	12.12	2 900, 12	2176 (0	200,00	2.976.00	7.35[:::]	8.5%, 01	. 921: 10.	3.530, 00	1.251: 1.1.	18 E. O.	3.871; 10.	1220, 000	NA NA	VA.	VA.	1
	0.00	711	58.3	1.52009	1206	1780, 32	858, 10	. 360, 10	2780.00	0.380:03	1,350,01	. 271: 00	6,321, 00	1.211: 14.	1.211: 00	3.181; 00.	1285, 00	3 . 85: 55.	1.881; 0.	2.20: 01	
	510	-11	58.3	1.22.25.69	12.52	3 520, 12	23.1: (2	2,320,00	5.50(0)	1,8115.01	8750,01	100, 00	3 (6), 50	3.75% 000	8.9.155.	3.891, 00.	1500, 000	NA.	ΑV	NA.	
VW +2 10	311	711	58.3 78.8	1,12,306	12 %	166, 10	24: (0	. (0), (0	3 (21: 0)	0.00[3]	7.570.01 5.650.0	2,340, rc. 560-rc.	5 280, 00 4 (34) 00	4 351; 10. 3 300; 100	, 47(c.00 7 (5)(c.01	- 35 : 10.	67,5,00	T.T.Y., (A)	NA NO SI	VA 165°, n	NVv-
1000	101	916	. 15	5 0 2007	12.55	13 1	2.167, 52	1 (81) (2	18 40	9.010.0 3.39% T	195 .01	6 miles I	3 (5 to 1)	1641	8.0	3 127, 101	3.720-10. 4.05-100	NA NA	AV.	NA.	B/99-
	118	916	. 48	1 10 50	1215	1.8	5 - 112	5 02	. 9 .01	3 10 1	6.55 401	6.36.1	188 0	2.116	1.890.00	8  - 11	2.5 (0.0	NA.	AV.	VΛ	1
	- 01	al p	. 88		1.06	301	\$36 m2	96 02	1.58(-0)	5.586 T	9 and	3 5 . 1	201 0	2 201-	93 . 1	5.5 p. m	30, 101	NA.	AV.	AV.	
	160	a l b	. 48	80,16	1 19	105	501-112	1.36 07	1.54(1)	5.786-1	566 40	8.10.00	1.59 0	3.116	> 6b (m)	1500 0	8.85 (0)	NA.	AV.	AV.	
	- 11	916	. 48	1 50 And	121	181	680-005	66 07	-185 405	53.16.1	12.40	64 0	65 0	5116	5 He on	5 331-11	68 1111	NA.	NΛ	NA.	
	16	916	. 48	131.0	1114	616	1.66-111	38 07	- 85 an	5 8514 T	56 40	1304-1	188 0	1 (1)	1 (8) (0) 2011 a)	5 % 51- 11	1 5 000 3 56 101	NA . % I	NA XXI	AV.	-
	10	41.0	-748	0	1 37	2807. 2	2.24-10	5 351 115	3.10(4)2	0.3710-1	K1 1-01	8 13" - 1	3.30" 11	3 >01:	20 171 20	3.1 (- 1)	3.477 (8)	NA.	NA.	NA.	
	- 11	al p	. 48	1.11.206	12.18	188	55E-115	105 105	4.9 (ca)	Sto I	8 5 -01	6 35-1	5.75 0	5.9116	196 - 1	5.58.0	886 (0)	NA.	NA.	NA.	
MV-6 '-1 88	100	1861	4.53	8 0 5 0	1.55	1.85 (02)	1.0%	T 10 2	× 91	816 -0	8 015	1 30	3 P. O.	5 % 101	4.10.0	3.12 0	3.55E	-194 11	41 1	161	MVv 6
	- 03	100	. 54	Juliu Suu	13.55	5 48 1	1 95 01	85 05	8 3 (sa)	5 sto 1 8 t to 1	5 (6 a)] 8 (6 a)]	6.804-1	3.51 0	1:201:	5 46 - 1 - 50 0	3 9 3 h 10 3 1 1 h 11	28 00	AA AA	AV.	AV.	
	- 01	55 55	. 51		13-19 10-05	69	875.00	40.00	\$ 3 (ca)	3 a feet	8.66 201	1995-1	1.66	1881	10 a l	3 1 E 0v	\$9 , 101	AA AA	NA AA	NA NA	-
	- 10	20		20,100	1.1	544 '	201.00	1.76 (0.7	3 4 0	1 80.1	30 40	8 10-1	2.11 0	1.2.1	180 -	23.6.0	12 00	AA	NA.	NA.	1
	- 11		4,25.4	10 29 2008	12.25	2007 2	821-102	160,02	. 21.5 0	5586.1	1.78, 401	.150	60%, 0	71-	2 10:00	8 281-11	86., 00	NA.	NA.	AA.	
	0.6	.76.	. 25 3	. 23 2549	12.5%	626, 12	2.031; 102	2000,00	2 (6), (0)	8.271:04	9 230, 01	1.23(1).	2,00,00	2 (71) (4)	4.970,00	2.245 (6)	2.60, 00	NA.	VΑ	AV	
	509	. % .	.26.3	1.4200	12.38	772, 12	2.86:02	. 321, 102	. "81, 101	870504	593[, 0]	7.13(1).	648), (0	1,26,55	195), 1,	3.25E 00	3.735, 000	1.235, 00	. 831; 5.	2 125, 0.	-
	510	. % .	. 25 3	11.12.2006	16.53	6,310, 10 5,760, 10	2.536.02	2,070,00	2837 (0)	7 836 G	135, 01	180], 10,	3.811, 00	1 50h 55.	3,341,44	3 (3); (C) 7 (2); (C)	87.1,00	NA NA	VA VA	AV	1
JN 40 DC	100,	1821	177-3	5 0 200	1.03	3 1.1. 02	2000, 12	1.746.62	. 221: 1.	181.0.	8701:5.	3.737.00	3.50E-00	3,330, 101	2 (6): 61	3 230, 100	3 591: 12:	116, 50	. 2 E. 61	1.500, 6.	MW-6
	9.0	. 82 .	.49.3	1.29-2007	16.25	1170, 32	23/45/12	. 821, 102	9.5%, (10)	273634	3.240,00	116, 00	3400, 50	3 251: 14.	+ 2.1.5.	2.704: 00	3.150, 00	NA NA	AV.	AV	
	503	. K2 .	,493	1010307	1: 12	1910, 32	831: 10	. 540, 00	. 160, 01	1,008,04	590.01	Aprilent	1.915, 50	. 91E 55	5 150, 50	, 52h (G	2.2%, 00	NA NA	AV	NA.	
	100	**	- 50 s	. 8	1.15	1.00	680-00	0.5	8 Spans	5 86-1	6.34 aut 6.16 aut	- P-	106 11	1-201-	4.55	3 1- 11	133 101	AA AA	AV.	VA.	-
	196	8°	- 59 s	86 108 10 20 200	14.83	198	535 H2	66 07	13 Jun 2	5 5 5 5 1 1 5 1 - 1	9 15 401	8 381-1	61 0	1 XNE 5 47 E	196 .	5836.0	60 00	AA AA	AV	AV.	+
	16	**	- 59 s	17.0	13.16	108	1.50- 01	5113 11.	- 85 40	1 5015 1	6.98 201	-1 91 101	255 0	1081	- sl- 11	2.135.0	255 00	AA AA	VA.	VA.	
	16)	**	- 60 s	1 5 5 0	11.55	46 .	3.5 p. 115	3 07	49.75 441	186-1	9 15 401	* 6l I	6 t * 11	1.916	206.	Laste in	51 00	-6-501-	1.895.0	2 10 01	
	540	. K2 .	1993	1 22 2549	1100	1660, 12	2.131; 02	2,330, 00	2730.00	8 221: 14	57,500	532634	2.9%, (a)	3 (7) <sub>5</sub> (2).	9.125.00	2731:00	2700,000	NA.	NA.	NA.	
W-1 8	:11	. 82 .	1003	11.12.2004	1515	5 100, 42	278.02	1.405.00	1.53(1.0)	5.10(.0)	9.320.01	3 (6), (ii)	7.800, 00 7.00E-00	8 (a); (a) 2 (5) (b)	2.77[: 00]	9 (12) 00.	7,530, 000	NA Tac III	VA.	18" 11	MW
11 25 3	00	119		, s - 11	131	200 2	35.00	86 0	- 18 -01	35 15 1	168 201	98 0	2.05 0	1.00	3 P 0	25 1- 0	223 00	NA.	NA.	- VA	10.00
	113	119	- 0	1 11 500	P 15	1.10	261-112	62.0	4 80-00	6.386.1	12.00	570.0	193 11	1 DI:	4 11 40	25% 0	* 1 100	NA NA	NA.	VA.	1
	- 11	119		0,14	15.89	1.38 . 1	561-112	\$ 112	400 000	a sale. I	88 301	2.89 0	3.29 ()	15%	13 (000	1990	3.5 (0)	NA.	AV.	NA.	
	105	119	- 0	1.25.7.18	14.8	14	251-112	5.18 0.5	5 pars	1586-1	8.67, 201	8 1 - 1	2.38 (0)	5 44	68 - 1	1. 51-11	5 697 1111	\$ 534 0	18)	212.0	$\perp$
	- 16	110		1 5 1 16	1.13	1.9 .	1 NOR -2	9 n2 550002	5.70 o	55 to 1 69mm	1 (68 a) (1 4) a) (	1.41 201	59 6 00	5 5 mm	4 SE 00	5 Sp. 6	5 40 00	AA AA	NA NA	VA.	+
	16	119	0	1.91.0	11.15	131 3	85E-02	250.00	4 Made	6 No. 1	X > 20]	0.8 - 1	201 0	3 11:	1 25 00	3.7 (-0)	3.8 (0)	AA AA	NA.	NA.	+
	500	119	0.7	5.12000	12.25	1.970, 42	121: 12	. 640, 102	1.296.00	9 0.0E 01	930.01	2,370, 000	6.960, 101	1.571; 144	8.330.01	1295.00	195, 00	NA NA	AV	VA.	1
	510	119	0.7	1.45,2539	1124	3 800, 42	831: 10	. 850, 02	2 (7), 01	27964	1750,01	2060, 00	5 121, 100	4 VIII 111	1,321,51	5.94E-06	685, 00	NA.	AV.	NA.	
	:11	119	0.7	11.3.2539	121 -	1.2 E. 42	tol: 02	. 6.1, 02	2,750,00	\$4000	1,310,01	9.2965.	\$ 250, 100	5.781; tit.	1718:00	7.25ds 00.	806), 00	NA.	NA.	AV	1
W +2.21	100,	1, 4	.73	5 8 2007	.313	2.280, 02	1.580, 40	1.551; 1/2	1 (2): 0.	\$ 130,00	7.776.50	1100,01	2.2.1: 00	2.510, 000	3.251; 1.1	27650, 00	2.195.00	1.5% (0)	, 5 H; 5;	1 801: 0.	NVS
	9/0	31.5	17.3	18.26.7	13.28	2,800, 42	77E 02	1,980, 00 1,70, 00	2.600,01	3.30E.0	5.030,01	1.736.64 9.236.64	3.660, 50	3 56E 10.	3.980,00	3 mile (C. 2 mile (C.	3165,00	NA NA	VA VA	AV.	+
	501	31.5	10.3	. 9208	13.25	3 260, 142	15h 10	1,7,5,70	1.29:0.	5.57E (d)	980.0	. 831: 00	3 631, 101	1 1 H; 1.1.	3 530, 61	3 felt (6.	135, 00	NA NA	VA.	VA.	1
	2005	3) 5	17.3	5.43 18	13.54	1907 12	(ed) (12)	2.18, 112	38900	\$ (x0-1)	5.85" (0)	7 to 00	2.051 (2.0	3 781- ***	776.50	3.531- 17	115' 00	3 *** 101	56F-1	* Jo' 11	
	191	4) 5	4.3	5 1 8	1.12	101 2	55h 115	0 0	18 0	18 Io I	5 In add	- 186- 1	0.00	5 % [-	- 91 an	2.62(6.1)	3 (95 101	NA.	AV.	VA.	
	507	31.5	17.3	.1.5.20.08	1, 03	11.0, 10	377E (C	3.85], 02	3.50.	977834	1.780, 01	5.730,01	5 (3), 100	9.701; 55	1.100.00	5 , TE 16.	5.67), 00	NA.	VΔ	VA.	1
	506	31.5	10.3	3.1200	12.22	100, 10	2 221: +0	. 96, 10	2.286.00	987E31	8 13], 01	. LE 06	2.910, 50	3 (5): 14:	260.0.	2.545.00	3237, 00	NA NA	AA AV	VA.	-
	1000		1 17.3	5.1200	12.15	2 - 2 - 2	Tota (C	1 2 5 5 10	2.960.	0.646.61	9.850, 01	6 55, 61	297, 100	1861: 111	1.526.06	3 (2); (6)	1.22, 00	I NA	144	AV.	1

Paper From 2. See Page 2, for Netco

										BUCHANA	3, 31										
Well ID'	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLI, COLI,	EC HOS							,	NALYSIS RESUL	rs							Well ID.
Well ID	ID	depth if below top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC EL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			Ni 63 (pCi4L)		] Well ID
		· ·		Date	Logar	Result	Std Dev.	MDC	Result	Sid. Dev.	AIDC	Result	Std. Dev	MDC	Result	Std Drs.	MDC	Result	Stil Dev.	MDC	
	:10	31.5	17.3	14.25.59	1100	3.371, 42	85E 10	. 880, 00	2.876.00	5.50E.01	9.371, 01 9.8 (1.01	6 (21, 61	5.500, 00 8.311, 00	5 (5): 11.	1.70E 06 8.037.5	\$ 556 HG	6.125, 000	NA NA	AV AV	AV AV	
\W +4.40	311	21.5	31.3	5 5 5 10 7	1.02	3 700, 32	1830, 10	1.736 1.7	5.7516.02	61810	9801 83065	1.337.11	5.28E 0G	5 (01), 000	6 of lead	1237 20	18,1:00	1 (1) (a)	. 211: 5	1.5H; 0.	MW-63-5
	100	ry €	.3" "	- 1,	1500		8 F 10	95' 0"	1.56-0	. 130-11	. 85 40	2 (10) 17	3.181 10	3.901-11	4 58, 10	3 50-17	3.55 (0)	NA.	AV.	N/A	1 111000
	115	10 ~	.4 *	1.11.50	1.1	. 80 .	636.00	\$ 107	-21 -20	S. 16-1	6 40	6.315-1	1.08 0	1 991-	1.56E-00	3 1: 11	486 (0)	NA.	VV	AV.	
	- 01	10 ~	3.1	0,14	15.65	3.46	6 F 105	5 02	1300	3.16.1	8 % 201	33 - 1	166 0	3 15	1.196.0	5 H- 11	8.1 (0)	NA.	AV	VV	
	16	10 ~	3 1	1757 8	1305	1.0	535.00	0 01	12 Jun 6 Jun	5 (5) (-1 1 (2) (-1)	807.00	4 10 00	183 0	1986	300 -	51: 11 51: 11	78 00	* 13 · 111	NA.	. II	
	- 10	10 ×	.3 1	151.8	9.59	31 1	535.00	96 07	55 (9)	5.586-1	5 9 401	9 0	6 % 11	II:	- 11 -00	55700	105 101	AA AA	NA.	VA.	
	16	10 ×	.3 *	8.0	1106	106	2. 35. 112	08 02	55 par	8 16 1	8 5 40	8 80 - 1	3 (6) (1)	1511	1.5 (0.00)	9.5 (0.00	119 101	NA.	AV.	AV.	1
	(4)	10 ~	.3 1	5.1 5.00	1.3	3.40	X  - 11'	65 01	15000	5 86 1	5.59 401	29.0	6' 0	1.86	21 JO 20	5 (80) 11	135 (0)	NA.	NΛ	AV.	
	310 311	19.5 19.5	31.0 31.0	130,009	1, 03	3 350, 10 3 44 0, 10	804; +0 581; +0	. 871, 00 . 631, 00	5 (algo); 5 (31), 100	\$ 8 (E.D) \$ 3 (E.D)	58,1,01	2066 (6.	6271, 10	7 (0); (a). 7 (1); (a).	1 35h 00 35h 50	254: 00	1511,000	NA NA	AV AV	AV AV	
/3E +1 B	100,	100	101	10.2.2006	3.0	\$160.00	1950.02	5 Tole 14	7.816.62	6.730, 0.	7 K2 H Su	5 (6), (0)	(A) (I)	597. HT	1 121, 16	16% 51	2536.00	5 311: 14:	. 231: 1	1.511: 01	NW-63-93
	9.0	93	85. "	5 52557	12 15	2.811, 32	80.0:10	. 750, 102	8 254: 02	7.296.61	5.230,01	1.870.01	1800, 30	1905.00	5.570.01	1.505.00	15.1, 00	AA.	AV.	NA.	1
/3L +1 -0	0.03	13	80 t "	125207	.131	2,370, 02	1820.00	1.578.52	1/3500	1.050	5.296%	1.20: 33	3.3, [; 16.	3500, 000	9/28/: 03	3.750, 00	5,745,16	NA.	ΛΛ	AV.	MW 63.90
	- 11	ds.	*	1.11.50	1.1	118 1	226.115	5 105	8 (8-0)	89 16 1	9.1 -01	-5 986-	10 11	5 DI:	- F 0	5 550- 11	3.74 101	NA.	NΛ	NA.	1
	108	94	8 8	0.18	17.16	*18 *	50k 00 65k 00	10"	1.85(cm)	XI 1	X 15 -01 -35-10	1 - 1	\$ 195 11	1 hol- 1 880:	05 - 1	2.5 (6.0)	5 5% 1111	NA.	NA	AV.	+
	305	92	8	1.25 (2.08)	11:17	2380, 62	256.10	2.65, 02	2.286.03	\$ 500 of 2.2.16 of	3860.00	3.392.50 11.216.5	2010, 50	3 361: 111	3 195, oc	2.506.00	3 230, 00	1 2E 20 NA	, 411; VA	_ lo,, 0, NA	+-
	37.6	99	85. 7	11.5.2538	16.13	3.9(0, 42)	3.73h: 10	3,890, 00	9770.00	, 53E SI	2,340,00	. 531: 10.	\$100, 00	\$10h ta.	2 80 (5 00)	+ 2 Hz + G	140,00	NA.	NA.	NA.	+
	2019	93	85.7	1.25.25.9	11.2%	3 100, 12	23/4: (2	. 930, 00	1.800.	0.33(3)	1.150, 01	5.5 He 5.	3170, 00	3 Ch (4)	8170.00	3 - 31: 10.	3.880, 000	NA.	VA.	AV	
	:40	99	80.7	5 12000	12.06	176, 12	50h 10	, 60, 02	5.14(0)	5,3601	5.530, 01	2004:00	6,720, 500	1.181; 1.1.	, «Alt 100	3 - 31; 10.	3.630, 000	NA.	AV.	NΑ	
	911	99	85.7	11.3.000	11, 3%	3.010, 62	53E (0	. 880, 00	18.1:0.	3 (3) (4)	1150.01	2 151: 00	5.5 E. (0) 1821, (0)	5 511: 00. 5 001: 00.	3.680,04 5.80,04	\$ 5505, 00. \$708, 00.	5 250, 000	NA NA	VA VA	VA VA	
707 63 1 2	100	11 3	20.5	5 5 200	3.11	3700 02	195.10	1.751-1.2	5.27E-02	150,0	5.470-6	2 80 11.	3.504.00	3.597, 181	9 995 01	3.727, 344	1.98.10	\$115.00	317 (3)	135 (	MW-63-11
	112	15	.05	54.5	11.57	.00	831-113	0 0	63950	5 386 T	196 40	6.97% 1	11.1 0	1.0)-	46.55 40	1941	135 00	NA.	AV.	AN.	1 111001
	118	1.5	.03 *	TOTA NO.	13.15	. 8 .	824-112	5 62	2 Oct 247	5 sto 1	8 20]	301 00	× [9 0	1876	65 -	55 F H	118 00	NA.	ΑΛ	AV.	
	- 01	1.5	/0g *	0,10	10.2	160 .	2)- 11,	5 65	* span	5 In I	5.92 (40)	391.1	3.50 0	5.511:	28 + 1	5 hd l- 11	3 5 101	NA.	ΛV	AV.	
	160	15	.00 °	1.75.7 B	1.08	3 1 1	580-02	265 112	atto are	5 9510 T	95 and 866 and	1 ls 1	2.50 0	5 891-	1 55 00	2.80 m	185 00	A A A	1.545 tr	1 381- 01 NA	
	10	13	36	1118	12.1	100	976.00	63 11	1 2500	2.886-1	61 -01	0.5115-1	168 11	5.31	2.86.0	8 1 S O	58 101	AA AA	AV.	AV.	+
	16	18	.00 *	3 . 0	11.49	13 1	3.5 p. 115	9 11.	1.595411	× 15-1	9.15.40	-1.10 00	181 0	, xel-	1 15 00	5 1 E 0	115 101	AA.	NA.	AV.	1
	16)	1.5	10, "	5.12.00	15.3	1122 2	931-112	601 07	1.5000	Saylo I	7.867.00	27.307 (0)	618' 0	5.76	1 381: 00	3 >31: 11	17.7 00	NA.	AV.	NΛ	
	10	15	.46 °	3,0	13.55	161 '	880 02 636 02	6 0	1 S (60)	S 16 I X 1 I6 I	5 8 40 5 % 40	28 23 min 1 881s 1	615 0	5 X61-	13000	5 (80) 11	8.68 (0)	NA NA	AV AV	AV.	
MW-68-121	100	1	-100	13.0	8.17	51 02	184	6 0	3.05	9 20	9 % 201	5 4 401	615 H	5.70 000	119 0	165 11	3 % [- 111	1.40 ti	- 17-	1 1:0	MW 63 121
	107	12	- 8	5,1	1.5	170	X4-10	95 01	4 (84)	54 lo 1	5.91 401	-1.31 00	4.59 0	1.761-	+ 1	3 10 F II	58 101	NA.	AV.	'VA	10 44 - 12 12
	115	- 12	%	1.11.50	13.5	160	.de 115	10.00	, Aglent	6.156-01	3 201	* BD 0	1817.00	19H- 5	150.00	Smilt Oc	181,00	NA.	NA.	NA.	
	- 01	P	- 5	0,14	D. P.	8-10 1	\$16.00°	10.7	* (Flore)	3 To 1	5.09 201	18900	CQ: 0	1.86	1 91-0	3110	102 00	NA.	AV	AV.	
	306	12.	8	1252.8	1.1	15 L/ 2 3 HL/32	444 (C	1,000,00	5 (6) (0) Totals (0)	1 0 0 0 0 1 3 0 3 0 0 1	8.05,301	2.890,04	9.5 pag. 2.080, 500	3.571-10.	1.231: 00	2.356.00	18.5.00	-1.22F	1 5,15 0; NA	2.56E-01 VA	
	90"	12.	138	11 (2008	12 13	195, 42	2396.10	. 980, 00	38.1:0.	* 526.01	8.550, 01	7.578.5	3 120, 00	4 1/7 to 1/4	1.50:06	- 38E 1G	11,5,00	NA.	VA.	VA.	+
	10.00	12.	.18 *	1.30.000	14 L	6230, 12	2 (2): (0	. 970, 00	7.366.00	\$1000.01	4 (5), 01	, 9,1; 16.	3.181, 100	3.10H 555	513041	2895 (6	3 (8), 00	NA.	VΑ	VA.	1
	509	12.	.18	3.12000	11,35	5380, 02	23.45.02	, 68°, 11°	***.E.O.	8 550 01	5230,00	0.036.02	846, 50	5 (H) (d)	2.356.06	1256.00	5.350, 101	NA.	AV	VΑ	
	:11	12.	.181	1 8, 25,59	1, 19	146, 12 501, 12	881: 10 64: 10	. 850, 02	52,100. 5 mlc tt.	\$ 1545 GL	5 600, 01	, 05h (C. 533°, 00)	1891, 10 9381, 10	5 50 to 100 8 5 Hz 100	2 mile (a) 2 mile (a)	0.07E-00.	51%, 00	NA NA	AV AV	AV AV	
XIIV 63 1-3	100,	1/2.5	155.2	5.5207	.138	5 TKL 102	210, 32	1.731: 32	7.136.02	6.5(C, I).	87 II: 5-	8000.01	284: 00	2.5%, 101	9.501:01	2.251, 101	8 TTL 00 2 5 Hz 00	1.5KC, 01	. 11: 5:	1.731: 0.	MVV-63-16:
	10.7	515	- 50.7	14.1	1213	1.9	9 1-10	98 07	4.1 44	3 35E- I	6.76 401	-3 [8 (0)	516 0	1 991-	-181 -0	3 SE 0	4.05 mm	NA.	'VA	'VA	
	118	515	2 NO. 1	1011 500	13.18	3 10 .	65E-02	3 112	Salvaria	986-1	56 40	-1.161-	3101 0	1.781-	4.91.503	199-11	4.4 (0.1	A.A	ΛV	VV	
	101	615	2 50 T	1.9 5.08	10.5	1111	F-105	160 01	4 (float) [3(float)	5.55b I 1.38b I	1 401	215 No. 1	100 0	1 ×01-	5 Np. 101	5 1- 0 31- 0	1.00 (0)	AA U UE	NA L v Tr. 0	* NA * 1501: 01	+
	16	615	2.90.7	51.8	11.56	118	1.00	65 01	18 750	25 (5.1	13 20	2.00 00	1.06 0	×11-	50 - I	19910	1 8 00	NA AA	VA.	VA.	+
	307	.60.4	. 50.2	.1 12:48	12 15	6850, 10	801: 10	. 50.00	. 10.01	5.53(; ).)	1 160 01	17760	5,370, 00	9 (2h ta)	7.780.00	+ 2.1; 16.	7230, 000	NA NA	VA.	AV.	+
	0.6	.10.5	. 50.2	. 25049	1.5	5.810, 40	2.945.02	, 950, 10	28910.	5 + 05 04	× 120, 01	5820, 00	1,230, 60	3 Ch (4)	1.730.00	28.1; (0.	318), 101	NA.	VΑ	AV	
	100	47.4	50.7	4   2   10	11.35	136 12	500-00	667 117	100.00	673671	7 1 7 01	2 880-1	8.871.111	3.7116-77	4 19 40	5 4° E-17	3,600,000	AA AA	AN.	AN.	+
	10	615	- 90.7	11.0	13.15	6.96	636 112	86 0	13 20	8 286 T	5.05 401	2.78 (0)	126 0	5.5%	-1 10 at	5 K (6 10	61 101	AA AA	AV.	VA.	+
MN-63-1-1	100		-16	5 5 5 11	151	5.05 (12)	111	1.30-2	15 05	0, 40	9 10-	-691 - 1	2520.00	2 11 101	8 blass	, 10 11	2.50-0	130 0	80	1500	MW 63 17
	11.5	1.3	- 91	56.5	120	- 18 .	936.03	0 11'	. 8 44	33 [6.1]	5.59 401	6.8 - 1	3.08 0	5.5814	2013 20	5 Sale 11	3 (0)	NA.	AV.	AV.	
	118	1.3	- 61	1.11.50	15.55	3 11 1	65E-02	5 115	- 85 44	96.1	939 40	95 H	190 0	2.00	\$ 50 .00	1561-11	* 101	NA.	NΛ	NA.	_
	101	1.3	- 61	9.568	1038	5.356-113	1 1014 7	260.02	6 61-01	6.95pm	Mison Braid	2. 200 mm	5 (1.56 mm)	5 3 5 (10)	1 18 -01	Arraje (t	5 FOO	NA 21 Ib	NA Lasten	NA Sole of	+
	306	111	.91	1.25-2538	11.15	1190, 52	94: 02	. 921, 102	6.59(102	27963	1865.01	370km	2 230, 100	3 711: 144	. T2E 10	2 -51: 16:	3.75, 00	NA.	VA.	VA.	+
	507	171	.41	11 1 2008	12.11	1771, 12	23.45.02	. 95.10	2.790,00	5.526.03	7.830, 01	2,680, 00	1830, 00	17 He 545	1.36:00	5.15[: 16.	6302, 00	NA NA	AV	AV.	1
	0.6	171	.417	1.25.2539	1.55	1920, 42	2.281: 10	. 970, HC	1276.0.	5 (ed) (d)	9.570,01	1.53(1).	3.810, 00	3 of E 10.	, 305 00	3.256.00	3.321, 00	NA NA	VA.	AV	
	510	171	.41	5 (200) 1 (0.750)	11.28	1570, 40	545 02 865 02	. 630, 00	2150.01	5 205 01	5.870, 01 9.820, 01	1.30, 0	1581, 00 5 521, 00	3 (5); (a) 9 (8); (b)	2 mile (0) 1 221: 00	3 (15 00) 5 THE 00	2.630, 00	NA NA	VA VA	VA VA	+
	:310	173	.41	11.3.349	13.53	1000, 40 1980, 40	80E 02	. 850, 00	. 750,00	5 20E 0	9820.01	30.00	5.521, to	7 801: 14.	5 311: 00	4 THE RE.	82.1.00	NA NA	VA VA	VA.	+
VW +5.28	100.	13.3	26.356	. 1500	.200	2080.02	1830.40	1896 62	10065, 00	2800.0	8500 %	1908.55	3 954 95	3500, 101	\$ 511; 00 \$ 551; 01	3000, 20	3700.00	220,00	900, S0	1300, 00	NVV-65-4
VW 165 801	100	7.3	1 (59	58.306	5.40	372.0	16** **	1.716 - 2	4750	9300.0	100' 00	31511	55E 04	218' 00	23/0/1	1811.00	58E-11	NA.	AV	NA.	N-W-65-8
	112	11	- 609	12.0	12.35	183	8 h m2	\$ 112	15 (60)	8 15 1	8 40	2.5 Fe	5.55 (0.00)	2.50()	- sb - 0	23 (6.0)	19 101	- 901-	66 10 0	50)+ 001	11
VW == 21	90,	.4.	5.	1 50 300° 15.13 300°	16.15	3.37), 63	224: (2	1.766.02	1.7% 00 2.12% 00	7.080, 0, 7.000, 01	2.080, 103 3.360, 01	8 32h ili	3 0.7 (c. oc. 3 0.3) (a)	3.510, 00 2.7 H: 35	22.1.14	3.270, 00 2.756, 06	4.2545.00. 3.180,000	NA 1 St. St.	NA 2006 to	7A 228, 0,	N/V-66-21

<sup>1</sup> to 8 950 L 800 - 8500 VG 2000 - Quarta 3 Lilles Table Signation 3 Ferroarted VVV coss. Macclithas

Fig. 11 et 2. See Page 2, for Note)

						1				BUCHANA											
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER.	SAMPLE COLL	LCHON								NALVSIS RESUL	. rs							
Well III	ID	depth if below top of casing	elevation It mst <sup>2</sup>				TRITIUM ( pC FL	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			NI 63 (pC i/L)		WHITD,
		top or Caring		Date	Loar	Result	Std Drs.	ADC	Result	Std. Dev.	AIDC	Result	Std. Des	ADC	Result	Std Des.	MDC	Result	Std Dev.	ADC	1
	501	111	- 0	12, 2538	1:15	9.530, 12	5.E (C	. 940, 102	.011, 50	23,51,53	2 821, 01	A 50E ST	2,970, 101	137E 35	. 801.42	2.24: 00	375,00	7.28E (G	8.481, 100	1381, 0.	
	0.05	111	- "	11.12558	1. 18	5 3 E. 42	2 (7 h 10	310, 00 60 00	957[60]	3.50(c).1	13%, 01	1011, 00	1885, 50	2 10 h 14 h	1.7H; 00	2 . Th. 10.	3.950, 001 6.170, 001	5 (80) (C	1 (ed) (0)	2786:01	+
	107	1111		1 1 1 2 2 2 2 2	13.55	161	7.91-107	75' 07	15 (4)	7.8 (6.1	8 77 30	8351-0	6 16, 50	3 11: 11	- 87E-10	25/1-16	777 (0)	1.796.1	7 1	193 0	+
	16	1111	- 0	4 . 0	120	1.0 .	5 X  - 115	58 07	4.19(4)	6.586.1	56, 401	150 - 1	6.56 0	3.206	1.25.0	5 X H- 11	165 00	98)- 11	0.1	1.99 0	
	16)	1111		1, , 0	1.0	8.78 1	65E-02	8 07	1.94(4)	sissis I	6.5 401	2.16.0	23 10	130)	9.5 - 1	3 p. o	183 00	. 851- 0	21 1	2.44 (0.00)	
	10	111		24 to 0	13.1	9.11	25/4/102	200 02	In Iso	69 to 1	81 40	-1.5%-	2.0.0	5.5Hz	8.89 . 1	3.656.0	666 00	3 30	650	190.0	
111-66-90		55 6	. 95	1 11 440	13.12	91 10	113	1316.2	b 2 (0)	SI 0	5 96	-981 - 1	26.6.00	5.00	-5 59b I	190 0	5 (9) (1	NA NA	NA.	NA.	MVV 65 36
	11.	44.6	49.5	1 18 500	D 16	8.05 3	56 F 02	02.02	11 1	1.61 0	565 40	0.0	831 0	1.5%	2197 au	5 (5) 11	168 101	1 1	1.880-0	* 91-01	
	113	44.6	49.8	1.7.8	1.1	76 4	J- 115	3.16 0.5	SIE I	* [0 - 0	K 35 and	1.85 (4)	3.4% ()	1.35	. K) 0	5 31: 11	11 (9) 3	9 111	, 80t-	2.1.0	
	501	33.6	15.5	12, 200	13.25	5.00(, 1,3	28/4:02	307.00	. 325, 64 . 200, 64	5.27E.01 1.08C. 00	3760,01	2,8% to 2,6% tol	20%, 50	3 (6); (a); 2 (C); (a);	2596.00	3.50(10)	3161, 00	3,350,01	808h (0.	1.510.01	
	0.05	33.6	19.5	1112008	15 to	5 HE, 13	3.16 (C	. 671, 00	. 200, 61	1 711, 10,	5 230, 01	4 9 E ST	1321, 50	2 80 h 555	1.781; 00	524:00	7423, 00 723, 00	95000	Losts or	1 881: 01	+
	- 11	446	49.8	0	130	365 3	626.00	3.1 02	11 1	1.56 0	5.15 401	4.01.00	188 0	1 bl:	5.45 . 5	5 7 10 11	3 5 (0)	1.38 01	00	18 0	<del>                                     </del>
	0.08	33.6	15.5	1.25.2549	15.2%	1390, 43	134:10	. 871, 02	1070.01	1 120, 00,	5.97(),01	5.5 IE (2	6 HE, 50	1.291: 144	35: 50	11.5]; 10.	1200, 000	8750,00	1,678.30	2.210, 00	
1.11 m Vi	1075	11	.93	28 200	.33	3.05), 113	1100.02	2,06,62	13.0,00	. 2.15 50	3768 %	3 .96 66	0.23E 00	33 (), (0)	9.59(13)	3760, 00	1585 15.	9.227, 111	. 22, 31	216, 0,	NW 68 36
CI = 49	100	48.4	-19.5	1 11 No.	1513	180, 10	1345 oc	508 07 1 GE 32	58° 0 189,, 0]	1.51 o . 89E 50	5 and 3 Alban	1.5 0 1.95., of	6.95 0 2.02E 06	2.1.50	48 (8 % a) + 450 (a)	2 (6.0)	25.40.06	-15H- 5.A	I I I I	, 81- ot	MVV-6:-35
CH = 49	90	38.3	25.8	8 4 201	1.3	5000, 03	3730.02	. 950, 00	2711.34	2.16, 00	9 241 01 9 241 01	. 021. 0.	2.52E 0G	2.0 La 50	3.6%, 5.	2476.00	23%, 00	2.5H: 00	Lost: 0.	1/36/01	R VV-0:135
	501	38.3	25.8	2.25.2548	15.38	1170, 13	8 28E 10	\$ 250, 102	233634	177, 00	9971.01	1.151, 50	3 10, 50	3736 55	1.295.00	13/4:00	3 980, 00	3 LEO.	2.39: 5.	2730, 00	
	0.05	38.3	25.8	1.28.2008	1000	3.8%, 43	721: 10	. 350, 00	. 370, 14	1.111, 06	3.97[], 0]	10%, 00	2.6(0, 0))	3 (2); (a).	1 (1)	2.36.00	346, 00	63E, 00	, 67h 5c	2880.00	1
	507	38.3	25.8	12.18.2008	1, 35	3.180, 43	2 (4) 10	1,1,1,02	. POB 34	1795, 10.	1006.00	. 185, 00	1615, 50	5 tal; (C.	1,330,00	50.00 00.	5811, 00	8.37E G.	. (81: 5)	191, 0,	
	0.00	38.3	25.8	12,249	16.15	3.670, 13	274.6 (C	. 920, 00 . 980, 00	. 120, 01	1.710, rc. 1.560, rc.	5 FG, 01	8 0 Mg 0 0 2 mm 6 m	200,00	2 (5h ta) 1 78h ta)	1.110.00	2000 00 3700 00	12.5, 00	1.20, 01	1 (8): 0.	1.87); 01	+
	510	38.3	258	1.29.2009	1500	2.6%, 13	3.871-102	206, 02	0.377, (0)	1.111.16	3.967.00	1.000.01	3 017, 50	3 (51) (6)	2.337.4	3.29/16	3.757, 000	3 (45, 6)	200E 0	2.250, 0.	+
	11	0.1	.558	1111 509	1506	1500 4	2.136-02	60 01	121: 1	183 0	81 40	4 20 0	80 0	8 8 11	- 93E 0	1- 11	10 1	-184	1.586.0	1 9-01	+
Misselle	101	100.8	-9" 5	8.81 5.01	1.55	86 03	*16 *	3.510	11 00	611.50	2.80%	1.95 (4)	3 p. nc	2001 100	-5 Str. 1	1.68 11	N/41-	NA.	AV	- VA	WW 57 11
	11.5	18	3.459	11 5	1.1	, 91 3	1881-01	95 07	1 160	8 386 I	9 15 401	0.0	611 0	9 P	-18 at	5 (55) 11	30% (0)	1.5 1	1.800.0	1.60:01	
	- 118	18	30° 3	1 % 1 %	15.15	1.18 4	5.33E-02	535 07	5850	9 986 - 1 896 - 1	1 b	432.00	813 0	1.89	-1.9 are	36 5 0	3 (0)	181 01	2.5%	193 0	
	105	1×	37. 1	31.8	13.15	116	2 h 112	2 07	95460	9 % Ho - 1	3 [5 40]	1 19 1	189 0	3 381	10.41	24 6 0	2 8 101	5 00	(65)	198 0	+
	16	18	SP 4	11.8	13.5	194 4	3 79 105	66 01	11 0	36.19.1	165 40	-2.500-	6.56 0	II:	3	5 X 1: 11	56 00	6.1' 0	1.680-0	1.900.01	+
	10"	18	372.3	55.5 0	Te 15	1.06, 3	2.52[102	921 02	1 8(14)	×3 (++1)	9 19" 401	4137 00	3.371 ()	2716	3 10 00	2396.0	2.65, 101	127.01	e III	181' 0	
	16	18	Sh. 5	15.5.0	16.0	1.08 4	5 Sh 115	8K 11,	6 (8)	53%-1	15.40	4 8 00	189 0	1 Yel-	50 -	5 551: 11	50% (0)	1.1.1	13 F 0	2.500.00	
	10	18	36, 3	H111 206	15.5	1111	5 5 1- 11"	206 07	5 5 5 5 cm	5 586 T	168 and 185 and	1635.1	* (45 H	5 TE	2 11 20	5 % SEC. 11	6 101	1 1	1.890-0	1 201 01	
MW-6 -L 5	100	1.34	-1568	8 81 2 11	3.1	105 119	1.36	5 3 15 2	3 31-	3 - 40	3 75	- 100 O	3.56E-16	178 101	1 9500	4.2. 0	1.50	NA.	VA.	VA.	MW 87 17
	- 02	٠,	- 10.8	0.25	113	1.013	3.55-113	95 , 00	1.08(4)	86 %-51	La Fra	431,00	1.9.00	Sulfe or	1871-00	3 SE 15	3 , 101	112 00	TI:	1.96 0	
	- 01	٠,	. 50 s	156.5	150	951 1	55 (6.02)	53.02	-112.00	6 66 1	6.401	6.65% 1	187 0	3 °41-	1661.00	250000	2 000	.5 95 11	13.1	187 0	
	206	. 23	-, 50 st	28.2 8	11.12	912.7.2	2.586-112	. 86,, 02	1 550. 3 18° 00°	2496.1	1855-01 3021-01	41.22,700	20%, 0	4,96	3.63,50,	2,36.0	3 (G) (H)	1.100,000	, 6 III	284,00	
	305		. 97.8	37.50.00	16.33	998, 12	2386.00	. 220, 100	139:0.	2 9 40 M	+ 321, 01	1.00,00	1851, 101	2.501: 10.	705 00	2.580; 10.	273), (0)	1 10, 30	500 S	196, 0,	+
	50.00	153	, 97.8	3 1 2549	1006	6730, 62	1,56.10	38,1,02	500(, 0)	5 126 (4)	995, 01	1.515, 00	5.851, 00	3 901: 55	815,5,	3.1,6.06	100, 00	3 (2), 50	. 10: 5.	200,00	+
	0.09	.72.3	, 97.8	120,2009	15.55	1,110,100	2.286 (0	. 871, 02	233(0)	0.835.01	1841.01	270, 00	7.050, 00	\$ 70f; 555	5,350,50	3 (64) 06.	1245, 00	8 (6), 01	2.086.00	2.0%, 00	
	:30	.72.3	, 97.8	1.28.2539	1829	1.051, 13	2.796, 02	2070,00	1.39(0)	5.580; (3)	9831.01	45 950 13	1.910, 50	3 (51) (4)	6 HL 0.	Stody Oc.	3 175, 000	19966	, 1 Hr. Sc.	198, 0,	
VIW 67 2.9	:11	2188	, 50 g 20+3	11 11 200 8 31 200°	11.55	8 100, 02	2.56, (2.	2000,002	3.27E 52	9.588.03 3.000, 00	8 181, 01 3 471; 5.	2 (78) (1 1 (80) (4	9811, 50 3046 00	9 90h 55	9.526.00 9.626.01	9/58b (G. 3/00), (0)	7.530, 00 3.886, 00	21% (i) NA	. 891: 5. VA	2.1/G, 00 NA	VIVV-67-219
AW 9 219	100,	188	-1.6.1	8 4 200	12.99	9 16	2.256.02	95 07	4.2 1632	5 (6 )	1.36	1.386-1	160 0	1906	9321301	23 8 0	165 (0)	1. 11	16 III	700 0	3199-57-219
	- 01	188	-161	151.8	1 15	1.13 3	58 8 02	53 02	- 6 - 41	1 dalo 1	611 401	-1 33 (0)	3113 11	1.80	1.85.00	3.35.0	3 × 101	1.5 0	811-	203 0	
	108	184	- 1 b 1	26.1.8	1.0	11 3	5E-02	46 0.1	. 19 ard	2346-1	136 401	-19 14	1.98 0	1 541-	-161 -0	54-11	5 [X 101	× 90 n	1769-0	1906-01	
	1161	188	- 1 b 1	1318	1.4	14 4	1995-01	68 11	8 8000	69F1	9 -11	42.0	193 0	5 861-	1.05.00	5 5 F H	\$15 101	190 0	1.650-0	1 (01 - 01	
	10.05	2.88	-1.6 s 266 s	13.349	12.05	9.68	2936.02	. 870, 100	3.27E.0.	53.16.1	15 (40)	-5 500- 2 107 - 101	420, 0	7 OF 1 31-10	N5 - 1	1.254; 00.	180,00	952, 00	* 6F . 8SE 5	2180, 0	+
	309	2.88	256.3	1.28.20.00	1.1.	9 221, 12	25/15/10	2030, 00	18,1:0.	80000	566,01	28%, 66	3.9%, 101	1771: 10	1 (0): 00	3.79(1.00)	1675, 00	1.0.0	Lieft 0.	1.89: 01	+
	210	2.88	2163	1111 506	1 15	1.11" 13	2.888-112	2071.02	357 (0)	0.371011	7.897.00	28, 10	1867 200	5 K*1- **	194" 0	0.250-17	Q.47., 100	603, 70	1.136.0	1.576.01	
VIV-6 -1 6	100	153	-1618	8.81.5.0	2.50	6.9.10	181 .	8.500	3 x Span	3 8 20	1.80%	1.801	5 8 Ye oc	2007 000	-9 SH-1	3 5 11	3 p. n	NA.	- VV	AN.	WW 87.27
	- 02	1 1 1	-761 K	1 5 5 8	1 18	111 3	5.636.00	98 07	Estimate Links	8 3515-1	99 att	28.85 (0)	3 15 0	5.510	3   30	3.5 (0.0)	135 (0)	5 115	(0) 1 Kg) - 0	2.10.01	
	101	**,	- 75 T R	26.7.8	1 18	116 3	56.00	35 (0)	1.5850 2005-201	56 I	5 1 40	- K 9 444	1.98 0	3 80	5.02 -	9 10 10	3 /5 (0)	1.8 1	6%	1 10:01	+
	160	5.5.5	- 76.1 8	15' 8	1 39	1.18 3	3 Sh 113	66 0	25.100 21.5	8 10 1	115 401	3.864.1	5 p3 - 11	5 101-	- 18 -01	5 1-11	6 2 (0)	3 00	30	1.98 0	<del>+</del>
	- 0	5.54	- 76 * 8	1 5 5 100	18.1	1 5 114	8 F 1/4 - 2	2.98(18)	4 5/11-111	> 93pm	5.561-0	1.45 200	5 356 m	5.00 (00)	.) 10p on	4 1 Hr. Ct	3 (6)-101	1.15 -01	68P T	181 01	
	160	* * * *	-761.8	15.5.9	1215	9 16	2.536-02	86 07	Spara	5.885-1	6 5 401	18 0	8.18 0	1641	-181 -0	5 (+5)+ +1	105 00	** of	21.15	1.78 0	
	510	275 3	2/2 8	128 2559	1, 15	9171.32	2 (4): (2	2000, 02	2.23(10)	3/86:01	5 [6], (d)	9.816.51 9.816.51	5 (00), (0)	5 6 H: 555	2.86 00	37.15.0G	1752, 00	1965, 00	. 76b to	196.00	+
NIW 67 323	500	3223	242 8 306 8	11 11 200 8 31 2007	1, 23	1 (6), (3 3 13), (2	885: 10 1.551, 12	1.650, 02 1.676, 02	2.598.00	80/H:01 3067.0	5.5%, 01 37 Helio	9 KH: SI	8 210, 00 3 7 de 00	133, 00	1.295.00	5 , 56 HG	1.170, 01 1.32E to:	1862, 00 NA	, role to.	19E, 0.	WW-67-3
	9.0	322.3	3:58	.01, 2567	1108	1.290, 13	2.94.10	. 940, 00	5 (71) (0)	8 585 13	5.370.00	5.77E.S.	300,00	3.216.00	61%,0,	3 35]; 16.	3.580, 000	5.251: :	. (5): 5.	1920.00	1 200.00
	901	322.3	30.0 8	2.25.2048	1.59	3.720, 42	2.756: 02	2871, 00	30,100,	1,9645.04	8.620, 01	2 586 55	2,970, 50	3.32E-00	1.29: 00	\$ 504: 00	1185, 00	685), 101	. 881: 5.	2.130, 00	
	505	322.3	300.8	1.28.2008	1.24	3.380, 42	5.086.00	. 340, 00	2.380,01	3 (6) [11]	7,250,01	8 295 0	2,300, 40	3.995.55	22%,4.	23.46.06	3 (6), 00	5 781; 144	1.59: 0.	2.891; 01	
	205	327.3	300 8 300 8	.13268	1, 15	68 E. 32	224:10	, 640, 00 Tel: 00	1201:02	3 (0)(0) 0 (3)(0)	1370.01 5850.01	3.560, 00	3.210, 00	5 (81) 100 1 (71) 11	4.2% (A)	5 , 2h + c. 3 380 - cr	5871, 00	381: 1.1.	1.65(1.0)	1.870.01	+
	16	377.3	3.08	11.10	13.5	464	281-11,	8 0	18 01	19.1	8,2 10	-0.23s	3 86° 10	10.15	2 10 0	3 380 17	135 (0)	9985 HI	370	213.0	+
	509	322.3	357.8	28 2548	1. 24	3.9 0, 40	2.96.02	2000.00	53,1:02	3.2,1:01	1000.01	130,00	3.310, 60	3 (5): 144	7,300,00	3 "21: 16-	1350, 00	2101:14	. 191: 5-	200,0	t
	510	322.3	300.8	1111 206	1.34	1010, 40	62E 02	. 68], 112	3025.01	4.895.03	1,250, 01	300,00	8427, 100	8 501; 10.	, 148 50	8,55 00	83%, 00	29.5 m	. 331, 61	110.0.	
7111 2, 330	100,	335.8	327.3	8 31 2507	.231	3.6% 102	1.610, 52	1 (40): 1.2	reals to	2.715.00	30.000	0.525 (d)	1 3 9 15 115	513' 101	1 1537 100	5 (3" (2))	5 Yell 12:	N.A.	VA	VA.	WW-87-340

<sup>1</sup> on 8 969 | 860 | 8699 | VG 3009 (granta 3 I d les Tables quante (Fermania) VVI voic. Vicas (Bass

Pape 18 of 2. See Page 2, for Note)

									15	DIAN POINT ENI BUCHANA											
	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE	SAMPLI, COLI	LCHON							,	NALYSIS RESUL	rs							
Well ID	ID	depth if below	CENTER, elevation ft mst <sup>2</sup>				TRITIUM ( pC FI.	.)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l-L)			N 63 (pCEL)		WHITD,
		top of casing		Date	Loar	Result	Std Drs.	ADC	Result	Sid. Dev.	MDC	Result	Std. Des	AIDC.	Result	Std Des.	MDC	Result	Std Dev.	AIDC	1
	9.0	13y K	12" 1	.01, 25.67	1000	3.9(0, 02	526 (2	. 941, 102	1 (2): 0.	Vilial	1,252, 01	7.295.01	3 (40, 50	3.56h; 55.	. 226: 10	133; 10.	3.502, 000	3.8%, 00	. 511: 5.	176, 0,	
	501	130 K	12" 1	2.25.25.8	12.00	1780, 32 5110, 32	2 82E 02 5 35E 00	2,891, 02	2,170,01	5.5%; (d. 2.28); (d.	990,01 5 PC 01	1.580, 00 3.31(),1	3.990, 00	3.9 Hz 555 3.8 Hz 555	7 (21, 0) 5 (31, 5)	3.745 HG	3.00, 00	5 T21, 100 e/5/He 101	1.83E 0. 1.87E 0.	2 (a)(: 01 2 78(: 01	-
	206	337×	-3*- 3	13718	1 55	660	3 22 112	63 07	8180407	47,1671	5 151 401	2.731.00	675.00	- (4)	3, 9, 101	. 1.1.17	8 F1 00	-x 3 II-	1.551- 0	1 881: 01	-
	- 0	5 957 %	-5' 1	0	12.15	5.14	1.6 (6.00)	1.49 0.1	25 (60)	5.005.1	6.4 201	1.39-1	4 1 0	1 9)-	2 poor 20	3.7 (6.11)	46 101	8 00	780	190 0	
	16	5 50 %	-31 1	11.10	12.5	196	3 F-03	\$6K 11.	135541	5696.1	505.40	118 0	19 0	1 9)-	4 3 40	3.731-11	4365 101	\$115 111	1131-	* *q -11	
	161	5 5/0 st	-51 1	31.11 yes	1.3	1.0 1	5 550 mm	500 00°	2 950	6.396-1 16-1	9 40	5 (\$45 F)	200 11	5.511-	3 B 30	5.636-0	S 45 (m)	20 51 11	1 Kd) - 0 20)	2.60-01	+
Missalm	1005	1,77	11	9 % 100	1.0	VIN 111	18 1	4.2 p. 2	NA.	NA.	VA.	1850 0	116 1	859	NA.	VA.	NA.	AA	NA.	VA.	NVV 10
	- 11	41	101	1.8.	1.15	1.8	5 B 5	191 02	62 11	183.0	1.530	2.55E-0	DI 10	5.50)-	1.1.0	2515-11	KO 101	NA.	AV.	AV.	
	11.5	4.	101	1.8.	1.15	1.	5 p. 02	4.8 (62)	100 0	59 Fo T	5.1 (40)	165 0	91 0	5.6%	1 801-111	5  - 11	9., 101	NA.	NA.	AV.	
	503	32.7	101	9.6.20.6	13.35	1.050, 32 8.975, 31	531; (0)	. 500, 100	2000.01	\$ (3)(1) \$ (3)(1)	5.877.00	7.65°, 10.	8,310, 60	5.2 Hr. Sa.	3.66(, 0,	8 304; 16.	90%, 00	A.A A.A	AV AV	AV AV	₩
	506	32.5	101	1.21.25.68	15 L	1.915, 52	8 Sub- 0	1 150, 00	125,00	22,631	1 (2), (0)	2100, 00	2.781, 101	1 11 12	. 385: 101	2 . 26 . 06	3161, 00	NA NA	AV.	AV	+-
	- 0	- 27	101	53.7.8	15.5	16' 1	9 10 11	58 117	65 9002	55 lo 1	96 40	295.0	188 0	3 30l-	5 8 - 1	3.5 [6.10]	3.5 (0)	NA.	NA.	NA.	+
	16	4.	101	1 *** 0	113	1.96	F-115	86 07	9 4000	3 4 SH - 1	5.82,501	-2 P-	386 0	25.16	LSIE 00	26 E 0	3 [9] (0)	A.A	VV	VV	
VIV 106	003	8.3	4.5	9.29.2016	1239	1.326.02	3.8 E./ (C	134: 02	NV.	ΛV	NA.	1231: 00.	9700, 00	1.30() 0.0	3.2110.00	2 × 35 × C	180,00	A.A	N.A	N.A.	MW 104
717/106	200	8.3		1, 3 206	,200 Di Sa	. 97E 02	12KL 12	1746.02 o8.0	VA n S de H	NA 8 Sec. d	VA RUR III	3.5, E. (C. )	1 (C), (d)	7 QE 10.	2.686.06	* 58E 06	5.3%), 101	A.A A.A	AV.	NA VA	NW 10
VB/ 100	003	8.5	91	9.29.2005	.230	2 8.7 m2 3 545 02	3 810 HZ	136.32	VA 45.0	NA 246 64	8 08., 01 VA	3731:00	1125, 51	8 (51) (4)	3 .96 06	2.57E 00	88., 00	NA NA	AV	VA VA	MWHO
traction.	501	8.5	6.	11.3.254.5	1216	1 011, 12	1236.12	176.10	Ä	AV	VA	3.5%; (6.	1085.33	7 80/1: 144	2 891:06	7 8h (C.	0.202, 101	NA NA	VA.	ÄV	+ ****
	0.0	8.5	h.	5 3 2006	16.15	3.390, 42	858: 02	. 700, 00	2,580:00	8.23534	5,270,01	200.01	5780, 00	5-2 Hr. Sa.	2.50£ 00	14. 2h 10.	70K, 00	NA.	VA.	AV	1
MW 11.	00,	.0.5	2.1	9.29.2016	, (9)	2150:05	2.260, 13	134:12	AV.	VΑ	VA.	1.18]; (0.	1.2 E. G	142H N.	1.811; 00.	5 (2); (0.	5,570,000	NA.	VΑ	AV	NV-1
	501	165	2.1	9.25.253	10.00	2.050, 43	2.50(1.1)	920,00	VA.	VA.	VA.	N.A.	NA.	NA.	VA.	NA.	NA.	NA.	NA.	NA NA	
	9/C	163		15/11/2005	16.06	6810, 13 0810, 13	173[: 13 315]: 111	9 1.0, 00 9 1.0, 00	AV	VA AV	VA VA	NA NA	AV AV	VA VA	VA VA	NA NA	NA NA	NA AN	NA NA	NA NA	+
	- 01	16.5		1 % 505	× 5	118 1	5 10 11 1	0 0	AV.	AV.	AV.	NA.	AV.	NA.	AV.	NA.	NA NA	VA.	NA.	NA.	+
	115	16.5	* 1	11.325.5	9	3107 5	9.51: 1	0.02	- VA	AV.	NA.	NA.	AV.	NA.	AV.	AA .	AA.	- VA	AA.	NA.	<del>                                     </del>
	16	16.5	* 1	1 27 746	D. 0	180 5	5516.3	0.00	NA.	ΑV	NA.	NA.	AV	NA.	AV	NA.	A.A	N/A	NA.	NA.	
	- 11	16.5	* 4	1,11,4	II Is	2	5 50: 5	0.02	NA.	NA.	AV.	NA.	AV	NV.	AV	NA.	NA.	NA.	NA.	M	
	16	16.5	***	1,12,240	16.8	106	× 51- 5	0 02	NA.	AV.	AV AV	NA NA	AV AV	NV NV	AV AV	AA AA	A.A A.A	AV AV	NA NA	NA NA	+
	10	16.5		1219 200	9.55	10" 1	3 61: 4	0.00	NA.	VA.	NA.	NA.	NA.	NA.	NA.	AA	10/1	NV.	NA	0.4	+
	111	16.5	* 1	12.20.346	11.0	212. 4	0.301-3	70.107	NA.	NA.	NA.	NA.	N/A	NA.	NA.	NA.	NA.	NA.	A.A	NA.	
	1.5	16.5	* 1	6,16	D. B	113 5	5 107: 1	0.01	NA.	ΑV	NA.	N.A	AV	AV.	AV	A.A	A.A	NA.	NA.	M	
	13	16.5	* 1	1 3 5 6	H 3	100 -	5 9 F 3	0.00	NA.	NA.	NV.	N.A.	AV.	AV.	AV.	NA.	NA.	NA.	NA NA	NA.	
	111	16.5	11	1, , ,	# 3 H 05	110 5	5 % 10 - 5	0 02	VA.	AV.	AV AV	NA NA	AV.	AV.	AV.	AA AA	A.A A.A	AV.	NA NA	NA NA	-
	16	16.		13.00	12.2	3957.05	3 Sile - 1	6.35 / 00	NA.	VV.	NA.	VA.	AV.	NA.	NA.	NA NA	VA.	AA	NA.	NA.	+
	1	16.5	**	1 106	16.1	1.05	2.80-10	63 02	1 0	6 85 1	63 20	VA.	NA.	NA.	NA.	AV.	NV.	NA	NA.	VA.	
	18	16.5	2.1	2.62.6	14.1	291	4 SH 1	6.36,, 02	- VA	AV.	NA.	NA.	AV	NA.	- AV	NA.	NA.	- VV	NA.	NA.	
	519	163	2.4	3.3.2006	712	2,360,43	7 0.81; 0.3	7,000,00	VA.	VA	VA.	NA.	AV	NA.	VA.	N.A.	NA.	NA.	N.A	NA.	
	120	163	2.1	5 T 2046	5.45 1.5.05	1.150, 13	135]: 13	5 160, 00	2 M. 10	NA 1.100, 10,	1.2 Hz 144	2 32H II.	13.0, 01	. 511: 1.	1.251; 101	- NA - 30E III	NA 1 ISC 01	AA AA	AA AV	NA VA	+
		165		6.23.25.6	5.35	2 621, 13	3.52E-03	2350, 03	6.23(10)	1071.00	1.326.16	1185, 00	1.00, 61	. 301: 5.	1700,00	381: 0.	1.520, 01	NA.	VA.	VA.	+
	122	16.3	2.4	92, 246	16.23	1.590, 43	2576.00	. 121. 103	87960	1.232, 06	1.336.55	9.9832	1.131, 50	. 266: 55	6260,02	51: 15.	125,00	NA.	NA.	NA.	_
	12.1	16.5	2.4	6 5 25.67	1:1"	1.190, 43	1956 01	3,521, 02	974500	0.304:01	\$740.00	7 5 Mg (c.	3.270, 60	3 001: 00	. 2.1.64	279:00	3171, 00	6318 00	1.291; 0.	. 31: 01	
	125	165	2.1	8.3.2007	2.53	9381, 51	2536.03	3,680, 02	97350.	0.736.03	9 270, 01	120.01	2,750, 00	3 (5): 55	3.950,04	2 (64) 00	3025,00	NA.	AV	AV.	
	- '6	16 ^	1.4	1.87.8	1.50	1 1	- 115  - 115	5.1 02	2.86 0	9.5% I	5 18 and 1 1 and	*6 0 -X 5h-	108 0	1 (A) (A)	-6.81 an	755E-11	'65 IIII	L 48t T	1 ost- o NA	NA.	+
	18	16.5	1 1	9 1 7 1 8	1110	661 1	* 1- 115	26 0	9 80-01	9 1 No. 1	9 7 401	-8 M-	3 por 10	1 91-	51 - 1	1.17-11	N/L	AA AA	AV.	VA.	+
	- 19	16.5	* 1	13 1 0	11.46	1 043	100-111	0.5	21 0	83 In 1	6 -01	5 0	101 1	6.6716	45 5 F 0	6 Sale 11	6.15 (0)	AA	VA.	VA.	
	to	16.5	* 1	11 7 7 9	Li K	1.76 1	5.986.00	8 07	8 19140	5, 36, 1	5.55.90	561 - 1	5.01 0	5.41-	J 40 Ju	55% H	65 111	NA.	- VA	AV.	
13 ()	007	25 %	.08	.5.15.2063	,230	3.706.02	1060, 12	1.886.02	VA.	VΑ	VA.	1721: (6.	1.00, 0	, 5H: 5.	3.721; 06	21: 0.	8,500, 000	NA.	VΑ	NA.	U3-4
	116	25.6	10.8	10.21.2005	1206	3960,40	\$76E 52	1,070, 100	AV	VA AV	VA VA	3 (); (C. 35) [1:06]	9310, 00	9 581: 133 8 5 H - 11	2.78E: 06 1.86E: 06	8 7-5]; 10.	9.580, 00	AA AA	AV.	VA VA	+
	12	**0	-1.8	1 18 305	120	1.10	1 100	18 01	AV.	VV.	AV.	1 10 0	913 0	66.1	1 Kill 10	5 1:0	10 (0)	AA AA	VA.	AN AN	+
	13	**0	4.8	1,11,4	120		1.39- 1	161 01	- VA	- VA	- VV	19 10 0	8.00 0	66%	2.0000	5 1:0	515 101	NA.	- VA	NA.	1
	- 01	, . D	-1.8	1215.306	151	100	1.5%	3 02	- VA	ΑN	AV	3 30 0	8.50 0	6.80	1800	850 m	5.65 (0)	NA.	AV	AV.	
	11.5	5.0	4.8	1281310	9.54	1115	1.656	3 07	- AV	- VA	AV	3.53b. 0	100 1	ol:	3.560-0	SE 11	K95 IIII	NA.	VΛ	AV.	_
	101	56	-1.8	1 0	1.0	N. R. (1)	0.40)- 2	5 56F 101	NA.	AV AV	NA AA	y MA	986 u	Tr. NA	R STEEL III	NA NA	AV	AA AA	NA NA	NA NA	+
	100	7.0	-1.8	1.50.0	13.5	5 5 7	3 30 113	8 0°	- 1X -11	5 1-1	9 20	-3  -	8 (8 0	5 H:	-3  - 0	8 ' I- 0	8 00	AA AA	NA NA	VA.	+
	:11	25.6	15.8	+ 22 25.66	16.25	7,000,02	2.36.02	. 480, 10	1.276.00	573E34	5.355.00	2 115, 00	1.151, 34	. 211: 5.	2586.00	8 (2): (6)	834, 00	NA.	VA	VA.	<b>†</b>
	:4.5	25.6	15.8	21.200	12 %	3.750, 42	3ol: 10	. 350, 102	. TKC, 01	7.830.00	5,770,01	2 835 01	2,6%, (a)	3 .06: 55.	1.316.00	3.24: 00	3970,000	NA NA	NA.	AV	
	:16	25.6	15.8	1292008	13.21	3.1%, 42	131: 12	2 221, 102	1.33(0)	2.796.03	190,01	5 (5), (4)	1.910, 50	3.36[; 111.	1.530, 0.	, "N; (c.	29,5,00	NA.	NA.	ΑV	
	117	25.6	15.8	7.28.254.8	To be	166, 12	2.5(4) 02	3,750, 02	3,570,00	170111	58,0.01	2 800:01 3 530:01	2 (80, 10)	3 (2): 10.	1780.5.	2.30(1.00)	3.6%, 00	NA NA	VA.	NA NA	+
	518 510	23.6	10.8	10.00008	12.00	3 680, 40 1 180, 40	1236.42	1,640,00	NA NA	NA NA	1.1E 55	3 531: 01	9315, 50	5 (7); 555 9 (90); 555	3.3 Hz 06	1,35 00 1335 00	150,00	AA AA	VA AV	VA VA	+-
	511	23.6	15.8	1, 10 208	1216	316.30	1,36,52	16.1.00	VA.	AV.	VA.	1.01.00	1030, 61	8 151: 121	2 VIII 06	. 226 0.	5 1.5, 00	NA NA	AV AV	VA.	+
	119	*46	11.8	3 - 5 - 0	1:15	18**	23 1: 102	977 102	12260	\$ 6611	6.1.5.01	3 861 11	166 10	3100.11	7.537.11	3 1 21- 17	3.35" 101	NA.	NA.	NA.	1
	20	, a D	4.8	1 1 0	113	3.81	K31-117	89 0	- 1 -24	35 lo 1	51 20	-9.6 Fe	695 0	1811-	500 - 2	3.5% 11	187 (0)	NA.	- AV	AN.	
	101	23.6	10.8	8.5.2000	1000	1821, 12	881: 10	. 850, 00	.3%.01	5.76.01	130,01	200,00	5 (3), 50	5 (81) (6)	1.531; 000	4 mig 16.	565), 00	A.4 A.4	VΑ	NA.	_
13.11	507	25.6	10.8	.1 5 248 107 248	13.13	1730, 42	281: 02	1.00(1.02	NA NA	S OE SI VA	978[, II] NA	27 1:16	58E, 00 81E, 00	9 TTE 555	3 (35), 5,	+ 25E (C.	9.550, 00	NA NA	VA VA	VA VA	100
+ 5 11	1 90	1 2	-8	100 2555	1 1,000	1 225, 10	1 1 200 52	1 5 . 50 02	144	944	1 444	1 2 30 00	1 8 1 1, 50	90.000 555	1 - 6.06	8 5 8 1 6	9.5%, 100	I INA	344	1 444	1 33

<sup>1 08 8 950 1 800 1 800 5</sup> VG 2003 Quarte 3 Lilles Table 5 Quarter 3 Formatic IVVV 2003 Mac Lithus

IPEC00224899

Paper Proce 2. See Page 2, not Notes

										BUCHANA	N. NI										
	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE	SAMPLI, COLI.	LCHON							1	NALASIS RESUL	.rs							
Well ID	ID	depth it below top of casing	CENTER, elevation ft mst <sup>2</sup>				TRITIUM ( pC ist.	)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC l4.)			NI 63 (pCFL)		WHITD,
		top or canal		Date	loar	Result	Std Drs.	MDC	Result	Std. Dev.	AIDC	Result	Sid. Dev	MDC	Result	Std Dry.	MDC	Result	Std Dev.	MDC	1
	0.00	57	2.K	15.21.2005	1206	3100, 12	3 87E 1.2	4,270, 112	NA.	AV	VA	3.521; (c.	1.180, 64	8 (6): 111	3.876.00	95 . 0.	500, 00	NA.	AV	AV.	=
	510	5"	2.8	10.28.2005	12 (6)	3 100, 32	1256.12	1720, 00	AV AV	VA VA	VA VA	3.55() (c.	106, SI 106, SI	8 0.61; 0.0 8 861; 0.0	5 35E 06 3 30E 06	. 9.15 O.	5130, 00	NA NA	AV AV	VA VA	
	111		- B	1 10 203	1200	4.04. 14	17,1112	16 10	- VA	AV.	AV.	3 1:00	9/321 10	. 801- **	2.671-00	8571.0	. 16" 101	NA AA	AV.	VA.	-
	12	- 5	* ×	1.18.505	120		1.506.5	18 07	NA.	AV.	AV	15 1:0	11 1	× 901-	4 50E-0	76-11		AA.	NA.	NA.	
	14	5	*×	1237.3	120	198	1.596.5	161 01	VA.	AV.	NA.	28 10 0	\$ 40 m	6.346	1916.0	X X 5]+ 11	6.86 (0)	AA .	AA .	VA.	
	- 01	- 5		1215.305	1515	3 (0.1)	1 Ng - 1	5 07	- AV	AV	AV	15ab 0	Brt 11	564	1,980) 11	86 F 0	5.65 (0)	AA .	AV.	AV.	
	115		1.6	1 77 P	0.1	5 '	1.986	5 07	AV.	ΑV	NV.	5 % 0	0.81 0	K 11:	1 10 0	19-11	91 00	AA AA	NΛ	- VA	
	- 01	-	' K	1 2 2 5	95	845	50E 5	6.86 02	AV.	AV	AV	5 I- 0 NA	0.41 0	5 KN1- NA	NA.	N 15H- O	5 IIII	NA NA	VA VA	NA NA	+
	115		· ×	3.5.0	1.5	1.6 3	1 31-111	85 0	6.555-00	K 180-1	8.25.40	161-11	> 19 ii	5.80	-181 -0	5.636.0	615 00	NA AA	NA.	NA.	
	0.05	5"	2.8	5.25246	13.30	7 321, 12	2331: 1.2	. 850, 00	. 275, 50	1000.00	1:41:35	. 2.h (c.	8.345, 50	5 Ch 55	5 96, 06	8785 00	, 15, 01	NA.	VA.	NA.	
	311	4.	5.8	1,2246	12.3%	48 E/32	2.846.02	. 980, 40	3.36(10)	1.36, 0.	1.316.35	, 150, 00	1.135, 54	86 5.	48 50	81: 11.	1.2%, 01	NA.	AV	AV	
	:15	5.7	2.8	8 5200	1.35	1960, 62	2.25h: 5.2	. 740, 102	NA.	AV	NA.	10.45 (0.	9.825, 00	6.330, 00	2 150, 66	6.8 Hz 555	8.2% (6.	NA.	AV	AV	
	16	,	'×	6 11	12.83	5.06	1.56.00	1.49 07	6.25(4)	8 Sto 1	9.85 30]	20 july 1	191 0	5.86	1 - 1	2 6 0	* 33 (0)	- 15h H	Soft- NA	165 11	
	18		· ×	1 22 200	16.13	100 °	3 98E 115	20 07	3.5 (sa)	5 36 I 5 96 P	5 T =01 5 OS =01	-1 18 101	3.11 %	1610-11	186 - 1	\$ 5.25 mm	5 6K 101	AA AA	A.A	NA.	
	519	5.7	2.8	1.22.34.8	161.	100,40	3276.02	296,00	6.29(10)	7.296.01	7,650,01	. 2.1: 00	31.0, 50	3.761; 1.0.	1.76.00	3.5-4; 10.	3935, 00	8.825.00	. 851: 1	20%, 0.	_
13-11	19	4 -	- 0	1 22 2 8	15	0115	3 41- 3	2.6216.02	0.300	1 (150)	7560	10.00	2.757 (0)	3.711- 11	2386-1	2.511:	2.75" (0)	1115 1	1 (5) 0	1.800.01	J3-11
	120	57	2.8	5.2.2006	15.21	7 (60), 12	636 FC	2.220, 00	124:0.	5.74634	8.290,00	2 850 01	1.8 E. 50	3 ,95 55	\$8, 50	. 8°E (C.	2825.00	NA.	VA	NA.	T
	121	4.	2.R	1.23.2538	1, 1%	5.9%, 12	2.586: +0	3,750,00	6.558.00	5.9EG	8.371, 01	2 1.1: 06	2.2 ft. 30	1.86: 55.	9.500,04	2.536.06	10.5, 00	NA.	AV.	NA.	
	1,22	- 5	2.8	10.20208	16.1+	5.9%, 12	5-31:10	5.9.1, 02	75.450c	5.17(5.1)	5,250,01	2.5.1; (0)	A270, 00	7 solt an	1.511; 00	9.24t (C.	7,350, (0)	NA NA	AV	NA.	
	123	5.7	2.8	1.28.200	12.00	6750,40	2.986.02	200,00	, OE, 50	7.578.01	7.150.01	1.530, 00	3.5%, 100	2.75% 000	6.650, 0.	2 30 (6 00)	2 BC, 00	NA.	VΑ	NA.	
	121	41	2.8	1.5.259	15.22	3 080, 40 3 950, 40	1/3/1/102 2/3/1/102	. PG, 02	3.23(10)	0.60E.01	7.6(0.0) 8.99(0.0)	1 (80, 61 2.5 (c. 6)	6031, 00	\$1015 to:	1.2 H; 06	3.35E 00.	115, 00	NA NA	VA AV	VA VA	
	106		2.8	1 13 346	11:34	3.790, 10	81: 10	2,320, 02	367110	5.550.01	5.637.101	2.80 100	50 E, 00 5 331, (a)	4.76E-10.	1 331: 101	- 33 - 16.	7 371, 101	NA NA	VA.	VA.	_
1.5-1.5	12	,	10	10.5	12	118 112	1941	1 No. 112	VA.	AV	VA	16 1: 0	1.10 1	× 61-	1 30 0	100 00	9.49 (8)	NA.	- VA	VA.	J3 12
	13	- 5	16	1 21 Nas	120	11 3	3 (13)	4.5 0.5	VA.	AV.	AV.	3 530 11	100 1	141-	3.00.0	9 1:00	50 101	AA .	AV.	- VA	
	- 11	5	* 6	1.28 500	P90	1.8 3	1.961- 1	5 5 05	- AV	ΑΛ	NA.	\$ 130.00	1.03	6.1-	1.80 0	38)- 11	\$85 mi	AA .	ΑΛ	AV.	
	- 15	5	16	11.5.5.8	P50	110 3	1 hgl- 1	3.5 02	- AV	AV.	AV	\$ 5 p. m	102 1	581-	3 (6) 11	51-11	K\$ 101	NA.	AV.	NA.	
	16	,	16	1 Ju Nos	120	161 3	t high	26 11"	NV.	AV	NV.	5× 1: 0	1111 1	8.511-	3.381-0	SE 0	\$16 101	NA.	NA.	NA.	
	1 18		16	1 18 308	120	113 3	1996	18 01	VA.	AV.	AV.	15 1: 0	119 1	8 00	1.86.0	54- 0 34- 0	\$55 III 51 III	AA AA	AV	VA.	
	- 01	37	7.5	1215.205	13.3	1797 3	1976	10.00	VA.	NA.	VA.	2771.0	8 91 11	5 91	2 851-11	8 55E D	p.477 (m)	AA A	NA.	VA.	_
	102	- 5	16	12 Str 2005	10.8	1.60 4	5 Sp. 5	3 07	NA.	NA.	NA.	5× 1: 0	111 1	× 561-	3 50p. m	56.0	K ( 101	NA.	NA.	NA.	
	115	- 5	16	6,10	× 55	111 1	1995	166 01	NA.	AV.	NA.	1891-0	8.5 0	5.561-	1. 10:0	2 (4.0)	9.68 (0)	A.A	NA.	AV.	
	- 01	- 5	1.6	1 3 6	15.5	1.8 3	3 P 3	1.5.05	AV.	VV	NA.	3 D 0	1.50 1	× 11-	3.316.0	75.00	9.0 (11)	AA	VV	AV.	
	118	- 5	16	1,, 9	1.0	1.5.3	1596	16 01	- AV	ΑΛ	NA.	4.5 (6.0)	102 1	111-	4.2 (6.0)	9×9- 0	95 1111	NA.	AV.	- AV	
	16	3	16	1.55.2.06	1.15	2124	1866	16 .00	AV.	AV.	NA NA	4 991 - 0 4 - 1 - 0	9.51 0	8 15 o	3 1 to 0	Shall to	84 , mi	AA AA	NA AV	NA VA	
	16)		* 6	1 100	4.5	192., 4	25 1: 3	636.02	VA.	AV.	NA.	NA.	W.	NA.	NA.	AA .	NA.	NA AV	NA NA	NA.	
	:10			3 5 5 4 6	1216	166.0	3304.02	200,00	5871:0.	52,631	1000.00	7.136.54	6.360, 101	+ 831; Dis	1.220.00	33E-1G	686, 00	NA NA	VA.	NA.	
	311	4."	2.4	3.54.556	13.14	1500, 53	3.894; 52	2 180, 02	, MJ, 50	1.115, 06	1.016.00	1931:06	1.015, 51	. 221: 5.	5 (0), 06	5.000.00		NA.	VA.	NA.	
	139	4.7	2.4		12.23	1830, 13	378E (C	2.540, 102	12460.	1 75, 10,	1.800, 55	2.581, 16.	6.90(, 50	80.76 00.	1.30(5.00)	9.95E-06	. 250, 01	AA.	VA.	VA.	
	520	4."	2.6	8 5256	16.35	1.580, 10	7.7% 52	72.00	AV	AV	AA.	8.871.13	110,00	TAE, 90	3,290, 64	9.06.55	45 0.	NA.	AV	AV.	
	121	41	2.4	6 2247	3.25	1.150, 13	3.06.00	1360, 02	3,850, 01	1.586.01	53%, 01	2 (3), (4	2.2%, 59	2.516 (4)	10000	2 (2); (6)	275,00	5 88E 10	. 391; 5.	1.5%, 0.	
	122		2.6	81.2007	1515	1 250, 43	179E 02	2,550, 00	1840.00 2.396.00	\$ 37E G \$ 28E G	5 1.1.01 9 081.01	1.750, 00 7. Meta2	3 230, 00	3.20th titl. 3.11th titl.	2.59(1.00	3.50b (C. 3.50b (C.	38.1, 00	NA NA	AV AV	AV AV	
	71	-	- 10	15/22/2007	16.16	133 3	1831:10	20 02	La bar	8 5 3 5 d i	961 -01	90 - 1	2 921, 101	1.10	2 (0) (0)	1.100.00	285 00	1 No. 11	675	189 0	+
	- 14	- 5	16	5.7.5.08	13.13	107 3	1-10	3.15 (1)	65 %-0	3 1 1-1	3 40	5.40 - 1	106 0	1541	9 - 1	5-st- 11	311 101	NA.	NA.	NA.	-
	'6	- 5	16	13.18	111	9.0	2.850-112	364 07	5 d (sa)	5 96 1	8 D 20	45 27	1 2 0	1941	v 96 0	7.5 Sp. 10	4.49 000	AA	NA.	NA.	1
			16	1.50508	11.39	9.8	59 8 02	50 01	1 8000	1956 1	136 401	-1600-	187 0	5.811:	- 5 % 0	5 S S O	616 (0)	AA.	VV	VA.	
	- '8	3.	16	1.8.0	1.1		28 F 102	200,000	6 300	61161	6.5.20	0.41	2.12 0	2.10	106 - 1	23 (6.0)	, 9 mi	AA.	NA.	VA.	
	129	4"	2.4	121349	1, 21	1000, 13	1775.00	\$15,00	, 56, 50	0.50001	\$1,5.01	. 621, 16.	6.650, 00	1.031; 144	\$250.5.	1,95,06	[8%, 00	NA.	VΑ	VA	
	130	5-		1.16.206	13.05	1 1207 13 8 2 1 1 2 2	2746.02	2,340, 00	5.50E 0.	8 % E GI	14580, 01	1.310.01	3.6%, 00	1.231: 10.	6,320, 00 51,58, 510	3.726.00	[105], 00 625°, 00	AA AA	AV.	VA VA	+
. 1-1.55	100	- 1	61	1 91 ' 11	1.35	6 09	Pini ,	5.00-7	195 01	1 60 0	1 11 111	0 20	17-16	10 0	-3 15 I	1.00	5 1: 0	65 01	16.11	100 0	J1 089
	112	- 11		111	1.33	145 4	59 F H2	5 02	9 1	531 0	1.00	1 0	1.05 0	2.01-	0.0	95E-11	** 101	- 5  - 11	***	200 0	
	113	11		6.5	1.39	1 43 3	5 55 115	135 02	15 1	1.91 0	6.25.00	8 50 (0.1)	3 % 11	1.86	1 K2[- (m)	1.50(-0)	105 101	1.326	1.980	2.250.01	
	- 01	- 11	- 6	86.0	13.85	180 3	28 F 102	95 117	1 491	136 0	5 40	189 11	[80 n	1811	7.30 (0)	5.83(-1)	11	AA .	ΑΛ	AV.	
	108	- 11	6	1.55.8	14.84	105	2. 36.002	5 07	3 0	131.0	5.9 arg	185 0	676 11	1 101-	40.88 mg	5 550- 11	3 101	NA.	NA.	NA.	
	160	15	61	1 25 7 08	15.05	6.50 mil	1.968 2	2000°	5 4 (0)	9.01(s) X.63(s, 1	40 au	2. 856 (m) 2.56 (m)	2426 mm	§ 20 (70)	- 6 % I	1000 0 1500 0	5 6F 00	NA -1 XII II	I.A.	NA 11	
	37.00	11	6	18.2008	16.24	1.152, 13	377E (C	1980, 00	183 0	2 (SEC)	5 (30, 0)	. 561, 16	2070.00	3.761: 55	NA	AV.	VA	- 18 · ·	AV.	VA.	$\leftarrow$
	20.00	11	6.	11 - 248	10.18	2 (40), 13	384:10	. 640, 10	97 E. 90	1.200, 00	5 331.00	3.520, 10.	600, 50	201: 144	, 5 dg 100	9 15 E 10	667, 00	1 (2): (c)	. 450, 01	185, 0.	_
	510	11	6.	1, 19 3 08	13.50	2.0(0.13	2336.10	. 620, 00	5000, 00	1.380, 00	5 800, 01	2.350, 16.	100, 30	1781: 144	8.5-0.5.	1 - 31: 10.	5.371, (0)	NA.	VA.	NA.	_
	:11	111	6.	3 8 2 4 8	13.05	1.9%, 13	\$34: (C	38.0.00	. HD 61	2015, 16.	5.230,01	2000,00	5 930, 100	3.16H: 1.0.	2.8%0.5%	33,35,00	3 (2), 00	9 (95,01	1948 %	2 221: 01	<b>T</b>
	142	11	6.	12, 249	1300	3 280, 43	3.871: 02	. 9.1. 02	3,560, 14	260,00	115.01	3.751:04	3.280, 40	3.50 to 100	1.366,000	\$4.26.06	370,00	1.798.30	1 50 to 50	2.16.01	
	113	11	6.	15.26.200	1500	2,910,43	2.8.1: 02	. 890, 00	. 750, SI	1880, 00	5.380, 01	1045 54	5.9 E. 40	97115 SS	\$ 56E DO	47cH; 06	5170,000	0.008-00	2035.00	2.3 H; 01	
1.52	100,			48.208	5.13	5.800, 68	3.190, 10	168, 12	3.970, 00	2.581; (0)	3.57[: 0]	VA.	NA.	NA.	NA.	'VA	VA.	NA.	VA.	VA.	U*-VQ
	107			1: 13 Nos	12.34	6197 13	37 (4.55	6 ' 0"	161	5 80° m	3.33" (0)	NA 165	NA 'NS S	NA 171	NA rc :	'IA	VA.	NA bills 1	NA L I	AV 1 PR 1	
	501	-	-	1.3048	12.15	5010, 63	5.85.02	350,00	3000, 10	\$190 m	8 (2), (1	2.757.00	266, 0	771. 1.	2705.00	1 to 10 to 1	5130,000	5 10 to 12	668; 61	1300, 0,	+
	505			3.552	12.34	246, 13	3.800.00	2080.00	. 3(0, 12)	1980, 10,	\$100,00	. 781, 00	136, 13	391: 5.	2 (4)	37.6.06	136, 00	2.50E-52	2.126.63	2 121, 00	
	306			15.12.2006	44.00	3.111 (.3	2501:02	. 881, 02	837. (4	370, 16	5.727 (1)	327 115	990.12	. 90h 5.	18% 00	0.356.06	7.75 101	- 111 114	20/06/04	2300.00	

Papa Diver 2.

IPEC00224900

To the 8-96 Endow Red Style 2000 - Quarter 3 Falles Table 5 Quarter 3 Format (al VVI 1000) Maccol that

## TABLE 5 HISTORIC GROENDWATER ANALYTICAL RESULTS INDIAN POINT ENERGY CENTER BYTHANAN, NY

										BUCHANA	1. 11										
Well ID	SAMPLE	SAMPLE ZONE CENTER	SAMPLE ZONE CENTER,	SAMPLE COLI	LC HON							V	NALVSIS RESUL	.rs							Well ID.
	l ID	depth if below top of casing	elevation It msl <sup>2</sup>				TRITIUM ( pC id.	.)		Sr 90 (pCVL)			Cs 137 (pC i/L)			Co 60 (pC ld.)			NL63 (pCEL)		1
		top or casing		Date	Lone	Result	Std Des.	MDC	Result	Std. Dev.	AIDC	Result	Sid. Dev	VIDC	Result	Std Dec.	VIDC	Result	Std Dev.	MDC	1
11.8008	00,	i		19.208	8.55	+ 280, 112	1.00.32	1.57E-32	9.980, 111	1860, 0,	1311:55	NA.	NA.	NA.	N.A.	'VA	VA.	NA.	AV	NA.	J1-8706
	9.0			5 8 2008	9.4	8.811, 42	Sd: 10	. 94, 10	. 10, 01	5 . 80: 13	1770,01	NA.	NA.	NA.	NA.	VA.	VA.	NA.	NA.	AV.	
	0.0			15.15.2008	12 15	106, 13	79E 52	. 671, 10	. 850, 14	1.260, 10.	1,5%, 01	VA.	NA.	NA.	NA.	'VA	VA.	NA.	VA.	VA.	
	201			1 5719	9.5	311, 12	871-117	73" 11"	*** -1	16" ir	815'-01	. 39" (7	3 12, 10	2.50	1:35:00	5  - 17	4 444 (8)	- 76F · · ·	1 (2) (0)	1.830-01	
	115			1.51.9	12.4	187 4	1.895.01	4 02	194 [	4114 11	8.15 -01	X (16) (1)	5 B 0	1511-	2.18[00]	5 X  - 11	1.9.00	26 S (6 O	199-1	2.40 0	
	116			5.1.0	× 5	44 1	, N- 11,	1.65 11.	521 1	16 0	1.9.201	9.1 0	H 0	1001	20.04 20.5	1.11(0)	164 00	5.00	1.00-1	2.11 0	
	- 11			1.11.509	9.5	01 2	981-115	\$06117	291 1	* 41 - 0	50 - 20]	27 0	847 0	6.891	5.68 -	58 (-0)	668 111	25 SH- 0	1.695-1	19 0	
111-	- 01	0.2	.3	1 ,2 746	11.5	6.11 1	1.851- 5	85900	8 15 201	19	15% 0	9 244 . [	2.5 (0)	5.584	8 15 1	1619	5 (2.10)	AA .	AV	- VA	RW 1
	112		.30	1 ,2 346	13.15	105 [	2.50-115	585 117	3 par	K 5h I	9.15.401	96 0	5 13 H	5.80	13 .	5 35 00	5.75 (0)	NA.	AV.	AV.	
	118	- 5	.30	1 31 206	12.5	10.5	8 51:115	1 113	24 24	95 to 1	1.06	81 1	1.3 0	3.116	81 .	5 11-11	36 111	NA.	- AA	AV.	
	118	- 5	.30	1 31 206	70.00	189 1	531-116	5 3 115	9 (400	1.18 0	1 10	5 (315-1	181 0	5.316	1.59(-10)	55 (-0)	66 111	NA.	NA.	AV.	
	501	,57.3	311	15.31.200	15.55	2,630, 61	25.95.18	\$ 5.0, 10	1.00E-00	1.150, 16.	1 305 15	2.296.50	3.860, 100	3.996, 55	6 557, 113	2896.00	3.210, 00	NA.	VA	VA.	
	13.84	.57.3	30	.1 . 2556	12.00	180, 51	150 113	1200, 00	3 - 45 0.	1 (00, 10,	1.586.55	3.39(), 000	11.6, 50	\$ 50h; 55	5.250, 0.	15.15.06	11%, 00	NA.	NA.	NA.	
	307	357.5	30	.1.2.2556	12.06	2 100, 64	2.36.03	. 160, 103	1.50(0.0)	9334531	9 Table 01	. 121: 00	2,370, 60	2 901: 10.	8.5(0,0)	2.371; 00.	2362, 00	NA.	NA.	NA.	
	16	- 5	-30	13.0	9	3.06	1 950-119	11 113	18 (m)	2.16-1	8 40	4 08 00	*10 0	1500	8.1	2.5 (6.0)	* 101	NA.	NA.	NA.	
V 145	- 01			6.57.	111 1	1.11 3	1941- 1	8 (6.02)	-3 % att	6.31501	9.1 Jun	-0 5 fs	5   101	1501	5 101- 1	5 41-	5 19 (0)	A.A	NA.	NA.	MH o
	10.5			81	Dib	11 "3	52 1:00	5.86 07	4 (402	8960	9.88 (40)	-5.00%	31 20	1×1- "	Special and	2835-00	7.04 (8)	NA.	NA.	NA.	1
	115			1.76.300	11.5	161 4	2.4 (5.02)	81 07	1.5 160	6 60-1	1 201	2.8 - 1	161 0	1996	46 70 40	19 F 0	\$16 00	NA.	NA.	NA.	
	201			1 5 7 18	12.31	9781 17	2.36.02	*** 0*	167500	8 330-7 1	5 3** 201	3.737.271	2.781.10	3196.11	5,971.7.1	2.55(-17)	20/2 (0)	NA.	NA.	NA.	
At the	118	†	†	53.100	1135	1.50 3	1.9%	5% 02	25.7 201	6 '900	K Khan	5.500.00	V 100	5 II: 0	5.15.1	1831-	5 5 100	NA NA	NA.	NA.	M196
	300			8.212539	10.15	1.900, 53	2.596.02	2160, 02	5.960.	5 - 16 - 11	5.970,00	8 (97,12	5.580, 100	+ 231: 14:	2,701,00	9.5.1: 00	130, 00	NA.	VA.	VA.	
	307			1, 16 306	1, 15	6280, 32	396.10	100,00	35400	0.87[:3]	1390,01	5.30(1).	10% 9	15 5.	2.751: 06	+ 254: 00	1750, 000	NA.	VA.	VA.	<del></del>
LA: 0.0	100		27.3	5 6 200s	12.57	5.206.00	1 10.32	1.835.52	NA.	VA.	VA	NA.	VA	VA.	VA.	NA.	NA.	NA.	NA.	NA.	LAT-CO
15.5. or C	301		22.3	9.6.2006	12.17	3.980, 01	3 - GE 102	1 MC, 10	.390, 00	185, 0.	1795.00	388, 00	1.530, 100	. 9/1: 144	229:10	. 251: 0.	130,01	28 0.01	2.30.0.	2311:01	LA 400
	303		22.3	9 5 2556	13.11	1716.54	53: 10	. 30, 10	5087.01	800E0I	1578 55	6.00,40	205, 30	1,011,00	2798-00	351- 16.	1950, 00	NA AA	VA.	NA.	_
	901		22.3	10 1000	13.36	1.206.5	+2E +02	67.00	1,205,01	7 804 04	8.507.00	NA.	NA.	NA.	State of	5 GH: 16	9.307, 101	2.50-10	7.2541.00	8 01:00	_
	105		.23.8	3 7 10	13.15	4 94	161-117	6 01	8 7 150	1 50 .0	I feet	31100	150 0	5 00	- 1 p. 0	53 1-0	3 101	NA.	NA.	VA.	_
	100		.013	5 10	1518	40.820	M: 112	25 00	3 (0.0)	6 36 1	6.9.40	81 - 1	103 0	1 10	525 - 1	26 8 0	V10 101	NA AA	AV.	VA.	+
	10		.013	103.5	9.55	16 1	130 112	25 112	1.5950	1,986-1	518 40	-5 (5)-	100 0	591-	1.336.0	KI- 11	139 101	NA.	- VA	VA.	_
	16		.014	1111	10.5	900 1	351-112	61 01	18900	62363	562 40	-5 911-	1.0 11	1.5 1	- 2 KM - 11	5 7- 11	8.89 (8)	NA.	NA.	NA.	+
	16)		.014	1 . 8	1111	165 1	8 351: 0	15 02	1 100	3 36 1	1.85 40	9.10.0	211 0	1991	1.511-0	1.351-11	185 00	NA.	VA.	VA.	+
	10		2214	1 1 746	10.32	819 1	301:03	5 02	1 350	9 10 1	50 40	1 Mar - 1	* 6 0	1.00	-308 - 2	1 (0) (1)	1 IS 100	6 h 0	21.11:	2.45 11	-
	10		22.3	11.0	13.75	180	15 112	86 01	I har	3 19 1	5.58 -01	-1 1 100	×91 n	1:201:	35 - 1	1 601 11	5.5 (0)	2.405	27 1	*19 0	
	12		.553	1 19 509	12.85	-7.5116	3 (- 02	65, 02	480.00	5 (3)0-1	7.797.401	1 1'-1	8.91, 0	3 501	6.500.0	95 F H	1 200 00	2.206.0	1376.0	281: 01	+
B-	- 01			0.20	12.50	93		8-20-07	385 40	6 860	48 40	10.0	165 100	3.316	6 SAL 6	3.900	3.1 00	AA	NA.	NA.	B *
100	107			8 1.	1 3	1.00 3	2.56.02	9 11	1.38602	5 9 8 9 1	88 40]	0.10.0	6 1 0	1-941-	994 - 1	3 5 4 10	3.16 000	NA.	NA.	VA.	- "
	103			1 22 300	15.16	1.10 3	1,690-112	50 02	- 36 -01	3 70 1	55 40	681: 0	581 0	1871	1 351-101	3 735 11	4.54 (0)	AA	VA.	VA.	
	91		-	1 22 2 8	1110	110 4	6.15.00	0.0	1.39(4)	3 19 1	612.00	5.5.1	251 0	1811	-9 16 - 3	3 35 11	511 101	AA AA	AV.	47/	$\leftarrow$
	101		-	1.80.08	18.05	11	3 5 02	201 2 00	- 13 an	38 1501	81.00	2011/0	3.05.00	1 1 1 1	-0 B -0	6F 15v	29 , 101	AA AA	NA AA	NA NA	+
	100		-	5 ( 10)	18.3		8 N . 112	401 001	1507	88 Paul		4.716.0		3115	-0.18 pt	5 N U		AA AA	NA.	NA NA	+
			1			881					\$15.20		111 1				~86 mi				100
lev.	90		1	8 1200	8.35	103., 2	1 5 F 2	. 646.02	3.060.01	1.9 1901 9.20E.01	8.320,00	3.940 o	2.970, 00	3 (2): (a)	2885.00	331:00	2.150, 00	AA AA	AV.	VA AV	8.6
	9.0					5 (6), (d 1 (0), (d	58E 02	. 921, 00	3360,00	9 20E M	8.321, 01 5.831, 01	2.351: 16.				2.000.00	305, 00	NA NA	AV AV	AV AV	$\leftarrow$
				19.22.597	1, 35		2536.02	. 550, 00	1530.00	1.3 SE SE	8.831, 01	3 594: 00	2,331, 100	3 (a) (b) (a) 3 (3 (b) (a)	1.5 H; 00 1.20f; 06	3 . 36 . 06	3797, 101	AA AA	VA VA	VA AV	-
	501		1	1 6 2008		1721, 12							1.00, 50								-
	505			123 2538	1:13	5 230 . 61	8 (5); (),	. 130, 00	. 260, 01	2.5% (4)	5.250, 01	28%.5.	195, 50	3.216 (6)	7,500,00	3 (3); (6)	12.5, 00	NA.	NA.	'VA	-
	16	1	1	5 4 5 100	9.5	1.00	351-112	65 117	1 150	XIII I	X [3, a)]	190 - 1	119 1	9.00	1.260-0	5 35 0	5.8 (0)	NA.	- VA	NA.	1

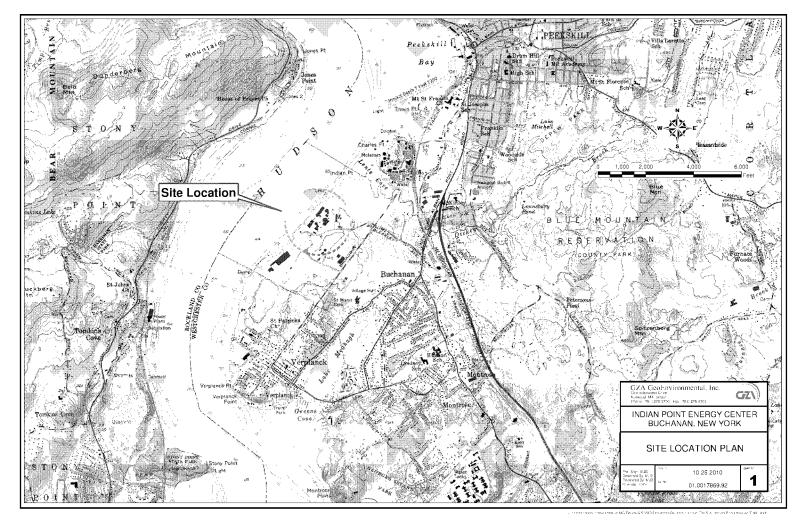
#### Notes

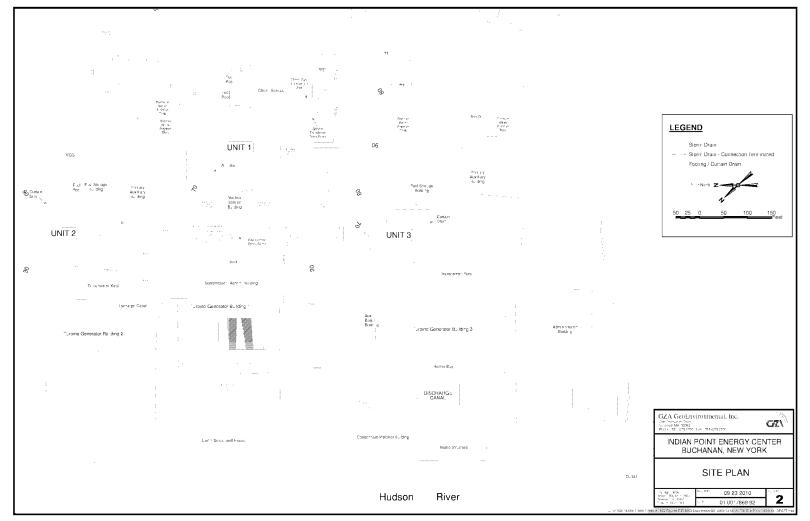
The World Form Rodor Mil Moore quarter of the Tables quarter (Formated W.W. von.).

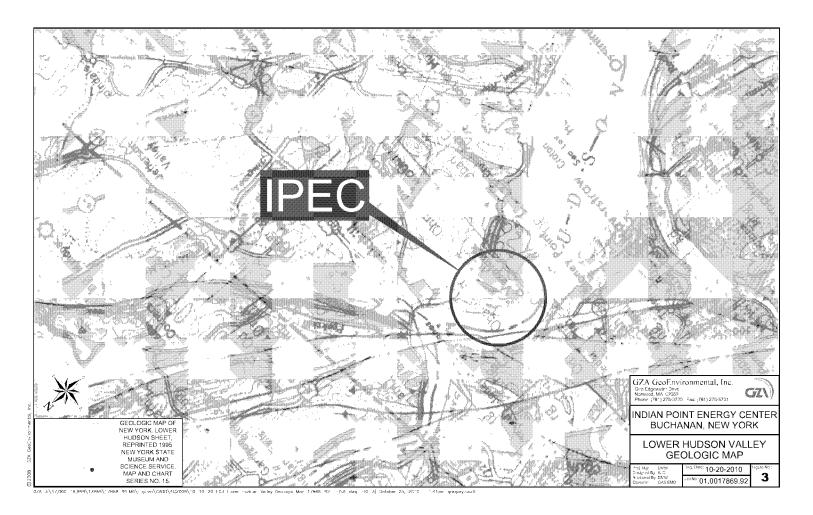
Fq. (1, or 2, See Page 2, for Notes

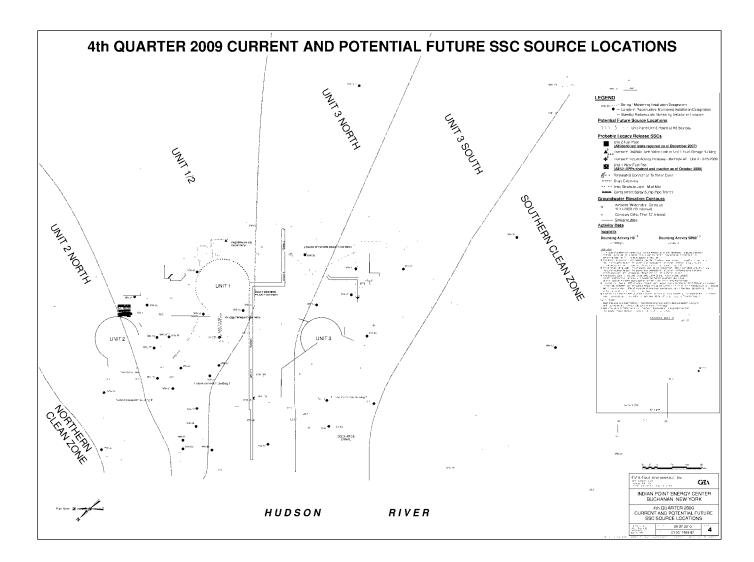
#### **FIGURES**

Figure 1	Site Location Plan
Figure 2	Site Plan
Figure 3	Lower Hudson Valley Geologic Map
Figure 4	Current and Potential Future SSC Source Locations
Figure 5A	Long-Term Transducer Monitoring Evaluation Map
Figure 6	4th Quarter 2009 Average Tritium Activity Map
Figure 6A	Temporal Trends in Unit 2 Rolling Average Tritium Activity Maps
Figure 7	4th Quarter 2009 Average Strontium-90 Activity Map
Figure 7A	Sr-90 Baseline Analysis – Unit 1 Defueling Evaluation
Figure 8	4th Quarter 2009 Average Cesium, Cobalt, and Nickel Activity Map

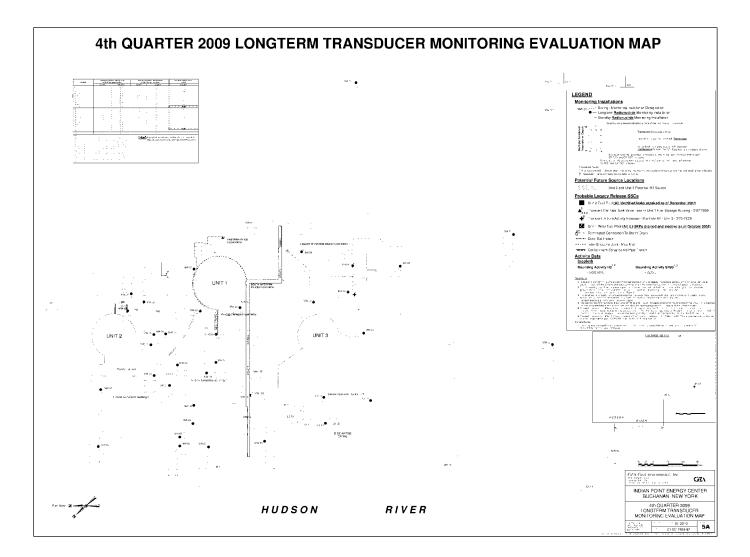




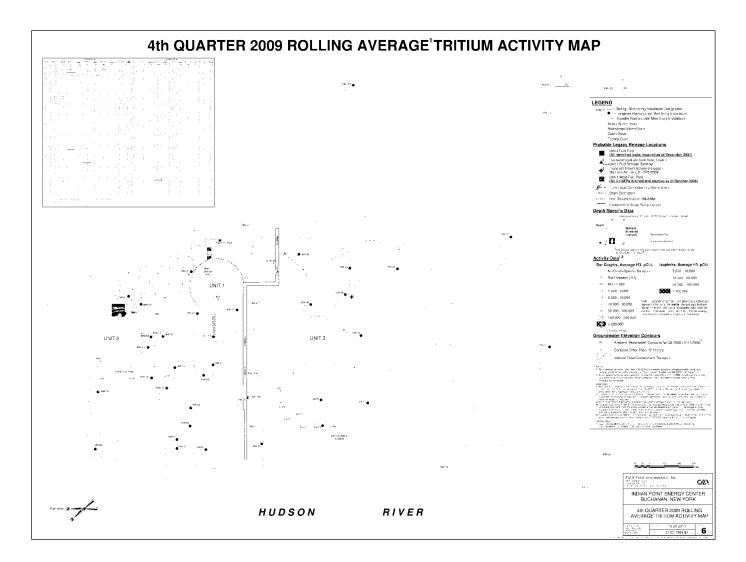




P#000224906

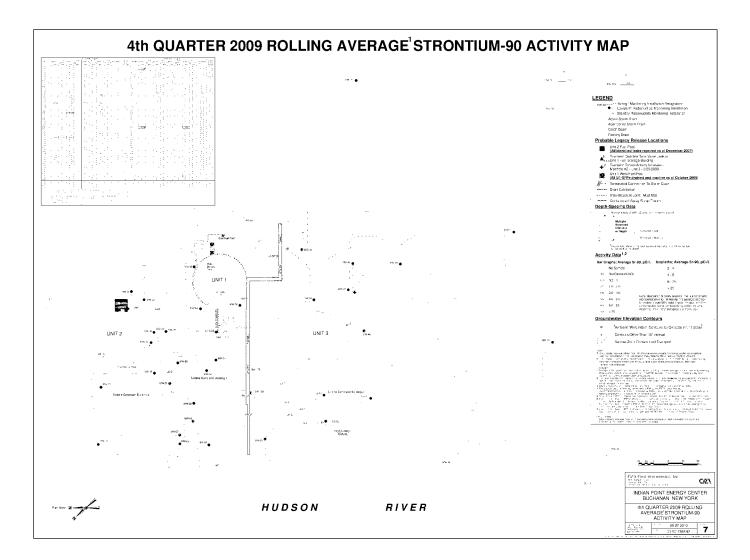


a cocar-as

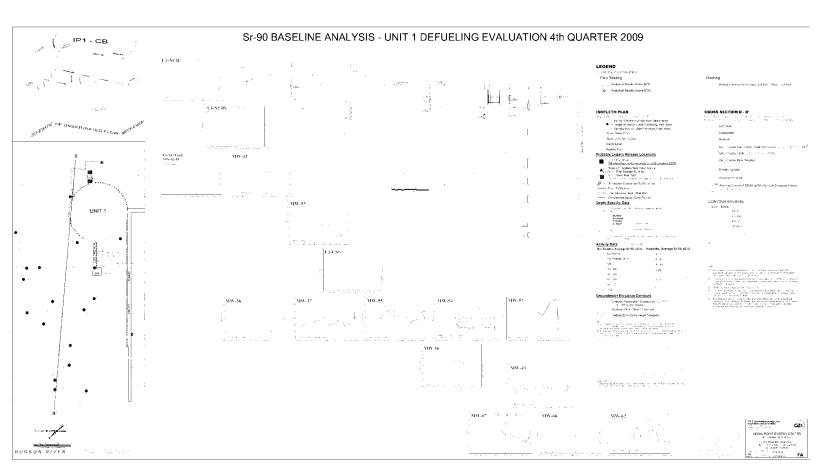


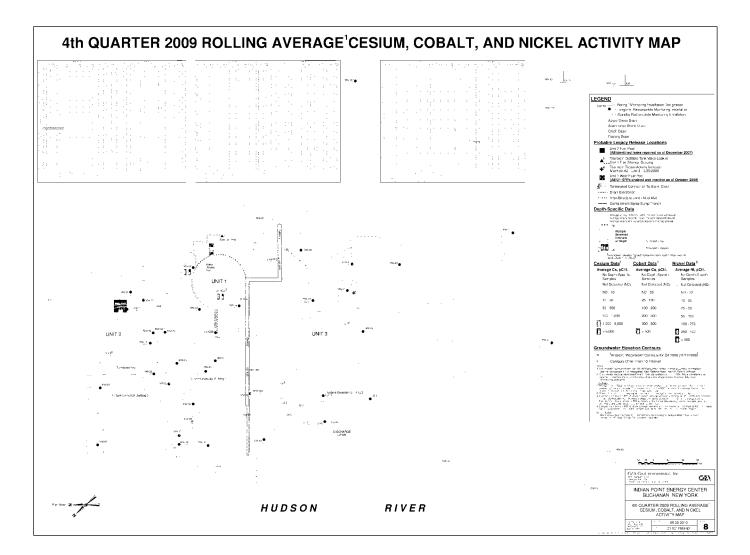
BOUNDING UNIT 2 ACTIVITY ISOPLETHS	Q4 - 2007	Q1 - 2008	Q3 - 2008	. 04	- 2006	Q1 - 2009	: Q2 - 2009		Q3 - 2009	Q4 - 2009	LEGENO	Engelander Dentitier Carracte
			- I	· 🧸 .	. 5			- L	. : 3	5		48 A 1 A
* * * * * * * * * * * * * * * * * * * *	14.		7	2	79 1 7		• •	7.	, , , , , , , , , , , , , , , , , , ,	, .	Printer Legacy Science and am.	1000
			1.00					A 17		. ! ! ?	# # contribution with a contribution of the co	
<b>■</b>	<b>≒</b> ."	<b>5</b>			· · · · · · · · · · · · · · · · · · ·	異			異	展	# 4 # Photograph construction (See 1985)	and the state of the
1 m	gae 1		gave to a Co	3.40	a hara a gi	Company of		566	1 Sept. 1	a system a	or What	
	70.0	1	· inc	17	, cates	`are:	H .				draw a flavor site Date	77 - 17 - 17
						1.4	of the second			4	- ba	
	· .							11			*, *,	
			•				•	•	. ,		Authorytica Bertimber America (CIII) - Martine, menne (CIII)	
							•				19 x _ 11	Z in removals is
20 A		100				2 k			g - 4 - 14 - 4 - 1		. a.	NEASHOR THE HIP! - I
				,	•*							TE DOARLASS
	- resources	· · · · · · · · · · · · · · · · · · ·	wee + x	uppowerser '7	- HIDSON TUNEN	- KOIDINIA	· + no	ECH YOUR	+ according	· · · · · · · · · · · · · · · · · · ·	D D	1.3 25 951 1 1784 2

и полики



PBC00224910





PEC0022-012

## **APPENDIX A: LIMITATIONS**

## HYDROGEOLOGICAL LIMITATIONS

- 1. The conclusions and recommendations submitted in this report are based in part upon the radiological, chemical and physical data from water analyses. These data were obtained from specific sampling locations at specific times. The full nature and extent of variations in the data between these specific locations and times are not known. The conditions existing between these specific locations and times have only been inferred using interpolation and extrapolation based on judgment.
- 2. The subsurface profiles described in the text and presented in the report figures are intended to convey anticipated trends in subsurface conditions. The conditions shown are approximate and generalized and were developed, in part, based on judgment. For specific information at specific locations, refer to the individual subsurface investigation logs.
- 3. Water level readings (piezometric pressures) have been made in the specific borings, monitoring wells, and Waterloo installations at times and under conditions stated. These data have been reviewed and interpretations have been made in the text and on the figures of this report. However, it must be noted that temporal and spatial fluctuations in the level of the groundwater may occur due to variations in rainfall and other factors different from those prevailing at the time and location measurements were made.
- 4. Where quantitative laboratory testing has been conducted by an outside laboratory, GZA has relied upon the validity of the data provided, and has not conducted an independent laboratory evaluation of the reliability of these data.
- 5. Radiological and chemical analyses have been performed for specific parameters during the course of this study, as summarized in the text. Additional constituents not searched for may be present in soil and groundwater at the site.
- 6. Variations in the types and concentrations of contaminants and variations in their flow paths may occur due to seasonal water table fluctuations, past and current plant operational practices, the passage of time, and other factors. Should additional data (water analyses, water elevations, subsurface deposits, plant construction and operation, etc.) become available in the future, these data should be reviewed by GZA, and the conclusions and recommendations presented herein modified accordingly.
- 7. This monitoring report was developed by GZA GeoEnvironmental Inc for the exclusive of Entergy Nuclear Northeast (Entergy) at the Indian Point Energy Center. Any use of data or information provided in the report, by parties other than Entergy, is prohibitated without the prior written permission of Entergy and GZA.

## **APPENDIX B: TRANSDUCER INSTALLATION LOGS**

		ANSDUCER INSTA	LLA HON LOC			
GZA GEOENVIRONMENTAL				WELL ID		IR-1
140 NINTH AVENUE, 18th FL	OOR	Entergy		SHEET	1	of 1
NEW YORK, NEW YORK 100	001 In	dian Point Energy Cente	r	FILE NO.	01.001	17869.91
SCIENTISTS AND ENGINEER	s		PRO	JECT LOCATION	India	n Point
MANUFACTURER In-Situ	FINAL BORI	NG DEPTH (FT)	·	DATUM	NG	VD 29
MAKE MiniTroll			4.99	DATE	11/3	23/09
PSI CAPACITY 30		` ' —	8.50		-	
SERIAL NUMBER 11886		AMETER (INCH)	2			
11000 <u>11000</u>						
		STATIC GROUNDWATE	ER TARLE ELEVATION	J (FT)	0	.81
GZA ENGINEER M. Britos		OTATIO OROGINATION	IN MOLE ELEVATION			.01
ELEVATION OF MEASURING POIN	T - DEPTH TO WATER = REFER	ENCE ELEVATION (WATER	TABLE ELEVATION			
DEPTH TO WATER + ACTUAL DEP	TH = CABLE LENGTH (if transdo	ucer is functioning properly	)			
			C	ABLE		
DEPTH ТО ВОТТОМ:			FT CON	NECTOR	▶ ▼	
GROUND ELEVATION:		14.99 FT	M.S.L.			
CASING ELEVATION:			M.S.L.			
CASING ABOVE (+) OR BELOW (-)	GROUND:	above		4	<b>A</b>	<b>A A</b>
DISTANCE FROM CASING TO GRO		3.50	FT GR			
MEASURED CABLE LENGTH	: s -: P	<del></del>		REACE		
MEROONED OF DEE EE NO 111				W ACE	<b>★</b> ±0	
TIME OF MEASUREMENT:			HRS			
MEASUREMENT TAKEN FROM:		TOC	W.	ATER	<b>√</b> •	
				ABLE	<b> </b>	
DEPTH TO WATER:		17.69	FT			
ACTUAL DEPTH:		<b>+</b> 8.130	FT			
THEORETICAL CABLE LENGTH:		<b>=</b> 25.820	FT			
						4
HAVE CLOCKS BEEN SYNCHRONI S TRANSDUCER SET TO TAKE "S			check check CAI	3LE		ပ <u>မ</u> —
o manosockoch to take o	SKI AGE KEABINGO.	<del>1.7</del>	Sileck CA		AD	6
ELEVATION OF MEASURING POIN	Τ:	18.50 FT	M.S.L.			
DEPTH TO WATER:		<b>—</b> 17.69	FT			
REFERENCE ELEVATION:		<b>=</b> 0.81 FT	M.S.L.			
EST NAME:		HR-1	PRI	ESSURE		
OGGING INTERVAL:		20	MIN TR	ANSDUCER		<u>i</u> i
EST START TIME:		10:05	HRS		▶ 🚨 🔻	▼
			SEI	NSOR		
			l	/ELL		
			ВО	TTOM	******	Ţ
.EGEND: <b>DTW</b> - DEPTH TO WAT	ER				******	▼
DTB - DEPTH TO BOTT						
	F TRANSDUCER UNDER WATE	R				
	ROM SENSOR TO GROUND SUF					
52 3, 522 22,131111						
NOTES:						
ABEND. No connection	ı. Pulled transducer out, cleaned	a, replaced batteries, reset.				
<b>GZA</b>						

	TRANSDUCER INSTALLA		
GZA GEOENVIRONMENTAL OF NEW YORK	Client	WELL ID_	HR-1
440 NINTH AVENUE, 18th FLOOR	Entergy	SHEET_	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy Center	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS		PROJECT LOCATION	Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	DATUM	NGVD 29
MAKE MiniTroll	GROUND ELEVATION (FT) 14.99	DATE	11/23/09
PSI CAPACITY 30	CASING ELEVATION (FT) 18.50		
SERIAL NUMBER 16593	CASING DIAMETER (INCH) 2	<del></del>	
	STATIC GROUNDWATER TA	ABLE ELEVATION (ET)	0.67
GZA ENGINEER M. Britos		-	
	_		
ELEVATION OF MEASURING POINT - DEPTH TO WAT	TER = REFERENCE ELEVATION (WATER TAB	LE ELEVATION)	
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENG	TH (if transducer is functioning properly)		
		CABLE	
DEPTH TO BOTTOM:	FT	CABLE CONNECTOR	·······
GROUND ELEVATION:	14.99 FT M.S.		T
CASING ABOVE (4) OR RELOW (-) CROUND:	18.50 FT M.S.	L	
CASING ABOVE (+) OR BELOW (-) GROUND:	above 3.50	ODOLING /	
DISTANCE FROM CASING TO GROUND (+ OR -):	3.50 FT	GROUND,	
MEASURED CABLE LENGTH	FT	SURFACE	
			<b>                   </b>
	0.47		
TIME OF MEASUREMENT:	9:47 HRS		
MEASUREMENT TAKEN FROM:	TOC	WATER	<del>                                   </del>
		TABLE	[ ]
DEPTH TO WATER:	17.83 FT		
ACTUAL DEPTH:	+ <u>39.052</u> FT		
THEORETICAL CABLE LENGTH:	<b>=</b> <u>56.882</u> FT		
HAVE CLOCKS BEEN SYNCHRONIZED? IS TRANSDUCER SET TO TAKE "SURFACE" READIN:	check		
	<del></del>		T Q O
ELEVATION OF MEASURING POINT:	18.50 FT M.S.		
DEPTH TO WATER:	— 17.83 FT	<u>-</u> .	
REFERENCE ELEVATION:	= 0.67 FT M.S.		
REFERENCE ELEVATION.	<u> </u>	<u>-</u> .	
TEST NAME:	HR-1 #2	PRESSURE	
LOGGING INTERVAL:		TRANSDUCER	
TEST START TIME:	9:47 HRS		
		SENSOR	_
		WELL .	
		воттом	
			<b>*</b>
LEGEND: <b>DTW</b> - DEPTH TO WATER			
DTB - DEPTH TO BOTTOM OF WELL			
<b>AD</b> - ACTUAL DEPTH OF TRANSDUCER U	INDER WATER		
CL - CABLE LENGTH FROM SENSOR TO	GROUND SURFACE/ TOP OF CASING	•	
NOTES:			
Difference -0.757. Reset. Non-vented tran-	sducer. Pulled it out and cleaned it.		
GZA		WELL ID:	HR-1

	TRANSDUCER INS	TALLATIC			
GZA GEOENVIRONMENTAL OF NEW YORK	Client		WELL ID	l <b>-2</b>	
140 NINTH AVENUE, 18th FLOOR	Entergy		SHEET_	1 of 1	
NEW YORK, NEW YORK 10001	Indian Point Energy C	enter	FILE NO.	01.0017869.91	
SCIENTISTS AND ENGINEERS			PROJECT LOCATION	Indian Point	
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	41.00	DATUM	NGVD 29	
MAKE MiniTroll	GROUND ELEVATION (FT)	80.92	DATE	11/23/09	
PSI CAPACITY 30	CASING ELEVATION (FT)	82.23		11,20,00	
SERIAL NUMBER 11998	CASING DIAMETER (INCH)	2			
SERIAL NOWIBER 11990	CAGINO DIAWETER (INCIT)				
	STATIC CROUND		ELEVATION (ET)	51.81	
GZA ENGINEER M. Britos	STATIC GROUND\	WATER TABLE I		31.01	
OZA ENGINEER IVI. BIROS	_				
ELEVATION OF MEASURING POINT - DEPTH TO WA	ER = REFERENCE ELEVATION (WA	TER TABLE EL	EVATION)		
			<i>,</i>		
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENG	TH (if transducer is functioning pro	periv)			
		. ,,			
			CABLE		
DEPTH TO BOTTOM:	41.00	FT	CONNECTOR	▶ ₩	
GROUND ELEVATION:	80.92	FT M.S.L.		I	
CASING ELEVATION:	82.23	FT M.S.L.			
		1 1 IVI.O.L.		<b>A A</b>	
CASING ABOVE (+) OR BELOW (-) GROUND:			CROUND /		
DISTANCE FROM CASING TO GROUND (+ OR -):	1.31	FT	GROUND,		
MEASURED CABLE LENGTH:		FT	SURFACE	<b>  *</b>	
				*	
TIME OF MEASUREMENT:	9:06	HRS			
MEASUREMENT TAKEN FROM:	TOC		WATER	<b>→</b>	
			TABLE	1 1	
DEPTH TO WATER:	30.42	FT			
ACTUAL DEPTH:	+ 8.520	FT			
THEORETICAL CABLE LENGTH:	= 38.940	FT			
	1.6				
HAVE CLOCKS BEEN SYNCHRONIZED?	₩	check		ے ن	
IS TRANSDUCER SET TO TAKE "SURFACE" READIN	3S?	check	CABLE	····	
				A D D	
ELEVATION OF MEASURING POINT:	82.23	FT M.S.L.			
DEPTH TO WATER:	<del>-</del> 30.42	FT			
REFERENCE ELEVATION:	<b>=</b> 51.81	FT M.S.L.			
TEST NAME:	I <b>-</b> 2		PRESSURE		
LOGGING INTERVAL:	20	MIN	TRANSDUCER		
TEST START TIME:	9:06	HRS		▼	
	0.00		SENSOR	F [533]	
			525511		
			WELL		
			BOTTOM		
			DOTTOW "	···········	
LEGEND: DTW - DEPTH TO WATER				**************************************	
DTB - DEPTH TO WATER  DTB - DEPTH TO BOTTOM OF WELL					
	INDED WATER				
AD - ACTUAL DEPTH OF TRANSDUCER U		2			
CL - CABLE LENGTH FROM SENSOR TO	SURFACE/ TOP OF CASING	J			
NOTES:					
NOTES:					
Difference = -0.417					
GZA					
			WELL ID:	I-2	

		TRANSDUCER IN				
	DENVIRONMENTAL OF NEW YORK			WELL ID	MW-41-40	
440 NINTH AVENUE, 18th FLOOR		Entergy		SHEET	1 of 1	
	RK, NEW YORK 10001	Indian Point Energy C	enter	FILE NO.	01.0017869.91	
SCIENTIS	STS AND ENGINEERS			PROJECT LOCATION	Indian Point	
MANUFAC <sup>-</sup>	TURER In-Situ	FINAL BORING DEPTH (FT)	64.00	DATUM	NGVD 29	
MAKE	MiniTroll	GROUND ELEVATION (FT)	54.87	DATE	11/10/09	
-:: :: = PSI CAPAC		CASING ELEVATION (FT)	54.13			
SERIAL NU		CASING DIAMETER (INCH)	2			
OE/(I) (E 110	<u> </u>	o, tollto by the Fert (literily				
		STATIC GROUND	MATER TARLE F	ELEVATION (ET)	31.75	
GZA ENGIN	NEER M. Britos	ON THE SITE OF	WATER INDEED		01.70	
		_				
ELEVATIO	N OF MEASURING POINT - DEPTH TO WA	TER = REFERENCE ELEVATION (W.	ATER TABLE EL	EVATION)		
DEPTH TO	WATER + ACTUAL DEPTH = CABLE LEN	GTH (if transducer is functioning pro	perly)			
				CABLE		
DEPTH TO	воттом:	40.00	FT	CONNECTOR	▶ ₩	
GROUND E	ELEVATION:	54.87	FT M.S.L.			
CASING EL	LEVATION:	54.13	FT M.S.L.			
	BOVE (+) OR BELOW (-) GROUND:	below		4	<b>A A</b>	
	FROM CASING TO GROUND (+ OR -):	-0.74	FT	GROUND./		
	D CABLE LENGTH:		FT	SURFACE		
				331117132	<b>≯</b> 1-0	
					<del> </del>	
TIME OF M	IEASUREMENT:	10:29	HRS			
	MENT TAKEN FROM:	TOC	1110	WATER	$\overline{}$	
	Irachi I Nam.			WATER	<del></del>	
DEPTH TO	WATED.	22.38	[	IADLE		
			FT 			
ACTUAL D	CAL CABLE LENGTH:	+ 15.844 = 38.224	FT			
INCOREIT	CAL CABLE LENGTH:		FT			
HAVE CLO	OCKS BEEN SYNCHRONIZED?	M	check			
	DUCER SET TO TAKE "SURFACE" READIN	ıgs?	check	CABLE		
		7000000			AD d	
	N OF MEASURING POINT:	54.13	FT M.S.L.			
DEPTH TO			FT			
REFERENC	CE ELEVATION:	<b>=</b> 31.75	FT M.S.L.			
TECT MAP	ıE.	RMAL 44 40		PDECOURE		
TEST NAM		MW-41-40		PRESSURE	▶	
	INTERVAL:	20	MIN	TRANSDUCER		
TEST STAF	RT TIME:	10:29	HRS		▶ 🖺 🔻	
				SENSOR		
				WELL		
				воттом	<u>1</u>	
FOELE	DTW DEDTH TOWATER				<b>▼</b>	
LEGEND:	DTW - DEPTH TO WATER					
	DTB - DEPTH TO BOTTOM OF WELL	LINDED MATER				
	AD - ACTUAL DEPTH OF TRANSDUCER		0			
	CL - CABLE LENGTH FROM SENSOR TO	GROUND SURFACE/ TOP OF CASIN	ن			
NOTES:						
IOTES:	Difference = -2.194. reset.					
IOTES:	Difference = -2.194. reset.					

		TRANSDUCER II	ISTALLATIC	ON LOG	
GZA GEOENVIRON	MENTAL OF NEW YORK	Client		WELL ID	MW-44-67
140 NINTH AVENUE	E, 18th FLOOR	Entergy		SHEET	1 of 1
NEW YORK, NEW	YORK 10001	Indian Point Energy	Center	FILE NO.	01.0017869.91
SCIENTISTS AND E	NGINEERS			PROJECT LOCATION	Indian Point
MANUFACTURER	In-Situ	FINAL BORING DEPTH (FT)	105.00	DATUM	NGVD 29
MAKE	MiniTroll	GROUND ELEVATION (FT)	93.52	DATE	11/5/09
PSI CAPACITY	30	CASING ELEVATION (FT)	93.02	DATE	1175765
	16108		2		
SERIAL NUMBER	10100	CASING DIAMETER (INCH)			
		STATIC CROLL	NDWATER TABLE E	ELEVATION (ET)	35.04
OZA ENIONIEED	C.Benmergui	STATIC GROUI	NDWATER TABLE	ELEVATION (FT)	35.04
GZA ENGINEER	C.Derlinergui	=			
		ER = REFERENCE ELEVATION (  I'H (if transducer is functioning )		EVATION)	
				CABLE	
DEPTH TO BOTTOM:		67.00	_ FT	CONNECTOR	·· <b>▶ </b> ▼
GROUND ELEVATION:		93.52	FT M.S.L.		
CASING ELEVATION:		93.02	FT M.S.L.		
CASING ABOVE (+) OR	R BELOW (-) GROUND:	below		4	<b>♠ ♠</b>
DISTANCE FROM CASI	NG TO GROUND (+ OR -):	0.50	FT	GROUND, /	
MEASURED CABLE LE	NGTH:		FT	SURFACE	
			_		<b>≯</b> + + 0
TIME OF MEASUREME	NT:	11:15	HRS		
MEASUREMENT TAKE	N FROM:	TOC		WATER	
			_	TABLE	<u> </u>
DEPTH TO WATER:		57.98	FT		
ACTUAL DEPTH:		+ 6.542	FT		
THEORETICAL CABLE	LENGTH:	<b>=</b> 64.522	FT FT		
			_		
HAVE CLOCKS BEEN S		Ц	check		0 GL
IS TRANSDUCER SET 1	TO TAKE "SURFACE" READING	s?	check	CABLE ······	AD d
ELEVATION OF MEASU	JRING POINT:	93.02	FT M.S.L.		
DEPTH TO WATER:		<del>-</del> 57.98	FT FT		
REFERENCE ELEVATION	ON:	35.04	FT M.S.L.		
CE ENERGE ELEVATION			_		
TEST NAME:		MW-44-67		PRESSURE	
OGGING INTERVAL:		20	MIN	TRANSDUCER	
TEST START TIME:		11:15	HRS		▶
				SENSOR	- النتا
				WELL	
				воттом	
				<u> </u>	······································
.EGEND: <b>DTW</b> - DEP	TH TO WATER		<u> </u>		
DTB - DEP	TH TO BOTTOM OF WELL				
AD - ACTU	AL DEPTH OF TRANSDUCER UI	NDER WATER			
CL - CABLE	ELENGTH FROM SENSOR TO G	ROUND SURFACE! TOP OF CAS	ING	•	
NOTES:					
Transduce	r level off by 0.371. Reset, starte	d new test.			
SZA				WELLID:	MM 44 87
<i></i>				WELL ID :	MW-44-67

		TRANSDUCER II	ISTALLATIO	N LOG		
	DENVIRONMENTAL OF NEW YORK	Client	T	WELL ID_		V-45-61
	TH AVENUE, 18th FLOOR	Entergy		SHEET_		1 of 1
	RK, NEW YORK 10001	Indian Point Energy	Center	FILE NO.		017869.91
SCIENTIS	STS AND ENGINEERS	<u>                                     </u>	I	PROJECT LOCATION	Indi	ian Point
MANUFACT	TURER In-Situ	FINAL BORING DEPTH (FT)	67.00	DATUM	NG	€VD 29
JAKE	MiniTroll	GROUND ELEVATION (FT)	53.662	DATE	1.	1/9/09
SI CAPAC	SITY 30	CASING ELEVATION (FT)	53.217			
BERIAL NU	MBER 16930	CASING DIAMETER (INCH)	1			
		STATIC GROUN	IDWATER TABLE E	ELEVATION (FT)	2	28.33
GZA ENGIN	NEER M. Britos	_				
ELEVATION	N OF MEASURING POINT - DEPTH TO WAT	ER = REFERENCE ELEVATION (	WATER TABLE ELI	EVATION)		
DEDTH TO	WATER + ACTUAL DERTH - CARLE LENG	TH (if transducer is functioning r	ronorly)			
DEPIN IO	WATER + ACTUAL DEPTH = CABLE LENG	rn (ii dansducer is functioning p	поренуј			
				CABLE		
EPTH TO	воттом:	61.00	<b>_</b> FT	CONNECTOR	▶ ₩	
GROUND E	ELEVATION:	53.662	FT M.S.L.			
	LEVATION:	53.217	FT M.S.L.		, l	
	BOVE (+) OR BELOW (-) GROUND:	below	_	. ★	<b> </b>	<b>↑</b>
	FROM CASING TO GROUND (+ OR -):	-0.45	_ FT	GROUND,		
MEASUREI	D CABLE LENGTH:		_ FT	SURFACE		
					<b>★</b> 1 0	
	IEASUREMENT:	11:39	- HRS	14/4		
VIEASURÉI	MENT TAKEN FROM:	TOC	- 1	WATER	<b>X</b>	-
	WATER.	04.000		TABLE		
DEPTH TO		24.890	- FT			
ACTUAL D	EPTH: CAL CABLE LENGTH:	+ 43.790 = 68.680	_ FT			
INEOREIN	CAL CABLE LENGTH:		<b>-</b> FT			
HAVE CLO	CKS BEEN SYNCHRONIZED?	M	check			J
IS TRANSD	DUCER SET TO TAKE "SURFACE" READING	ss? 🔽	check	CABLE	AD A	0 0 T B
					*	
ELEVATION	N OF MEASURING POINT:	53.217	FT M.S.L.			
DEPTH TO	WATER:	<b>-</b> 24.89	FT			
REFERENC	CE ELEVATION:	<b>=</b> 28.327	FT M.S.L.			
			_			
TEST NAM	E:	MW-45-61	_	PRESSURE		
_OGGING I	INTERVAL:	20	MIN	TRANSDUCER		
TEST STAF	RT TIME:	11:39	HRS		🔻 🔻	▼
				SENSOR		
				) A ( = 1 ·		
				WELL		
				воттом	*********	
EGEND:	DTW - DEPTH TO WATER				34.	<u> </u>
	DTB - DEPTH TO BOTTOM OF WELL					
	AD - ACTUAL DEPTH OF TRANSDUCER U	NDER WATER				
	CL - CABLE LENGTH FROM SENSOR TO C	GROUND SURFACE/ TOP OF CAS	ING	•		
NOTES:						
	Transducer off by -2.467. Reset					

	TRANSDUCER IN	ISTALLATIC	N LOG	
GZA GEOENVIRONMENTAL OF NEW YORK			WELL ID	MW-49-26
440 NINTH AVENUE, 18th FLOOR	Entergy		SHEET	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy	Center	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS			PROJECT LOCATION	Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	26.00	DATUM	NGVD 29
MAKE MiniTroll	GROUND ELEVATION (FT)	14.650	DATE	11/25/09
PSI CAPACITY 30	CASING ELEVATION (FT)	14.171		-
BERIAL NUMBER 11948	CASING DIAMETER (INCH)			
	,			
	STATIC GROUN	IDWATER TABLE E	ELEVATION (FT)	1.28
GZA ENGINEER M. Britos				
ELEVATION OF MEASURING POINT - DEPTH TO WAT DEPTH TO WATER + ACTUAL DEPTH = CABLE LENG			EVATION)	
			CARLE	
DEPTH ТО ВОТТОМ:	26.00	FT	CABLE CONNECTOR	·· <b>▶</b> ■
GROUND ELEVATION:	14.650	FT M.S.L.	301111201011	T
CASING ELEVATION:	14.171	FT M.S.L.		
CASING ELEVATION.  CASING ABOVE (+) OR BELOW (-) GROUND:	below	- 1 M.O.L.	4	A A A
DISTANCE FROM CASING TO GROUND (+ OR -):	-0.48	FT FT	GROUND./	
MEASURED CABLE LENGTH:		FT FT	SURFACE	
····		- ''	33.4.7.52	<b>≯</b> 
TIME OF MEASUREMENT:	10:13	HRS		
MEASUREMENT TAKEN FROM:	TOC	-	WATER	abla
***		-	TABLE	<del>*  </del>
DEPTH TO WATER:	12.89	FT	,===	
ACTUAL DEPTH:	+ 11.825	FT FT		
THEORETICAL CABLE LENGTH:	<b>=</b> 24.715	FT FT		
		- ''		
HAVE CLOCKS BEEN SYNCHRONIZED?	¥	check		D C C C C C C C C C C C C C C C C C C C
IS TRANSDUCER SET TO TAKE "SURFACE" READING	3S? 🕌	check	CABLE	AD D
ELEVATION OF MEASURING POINT:	14.17	FT M.S.L.		
DEPTH TO WATER:	<del>-</del> 12.89	FT		
REFERENCE ELEVATION:	1.28	FT M.S.L.		
rest name:	MW-49-26	_	PRESSURE	▶
LOGGING INTERVAL:	20	_ MIN	TRANSDUCER	
TEST START TIME:	10:13	HRS		≯ 🕮 🐧
			SENSOR	
			) A ( = 1 )	
			WELL	
			воттом	
EGEND: DTW - DEPTH TO WATER				· · · · · · · · · · · · · · · · · · ·
LEGEND: DTW - DEPTH TO WATER  DTB - DEPTH TO BOTTOM OF WELL				
AD - ACTUAL DEPTH OF TRANSDUCER U	INDER WATER			
CL - CABLE LENGTH FROM SENSOR TO		ING		
GE - SABLE ELINGTITI ROM SENSOR TO	STOCKE COLL FOR TOP OF CAS			
NOTES:		<u></u>		
No connection. Reset.				
074				
GZA			WELL ID :	MW-49-26

	TRANSDUCER INS	TALLATIC			
	Client		WELL ID	MW-53-82	
440 NINTH AVENUE, 18th FLOOR	Entergy		SHEET	1 of 1	
NEW YORK, NEW YORK 10001	Indian Point Energy C	enter	FILE NO.	01.0017869.91	
SCIENTISTS AND ENGINEERS			PROJECT LOCATION	Indian Point	
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	124.70	DATUM	NGVD 29	
MAKE MiniTroll	GROUND ELEVATION (FT)	70.26	DATE	11/24/09	
PSI CAPACITY 30	CASING ELEVATION (FT)	69.93	_		
SERIAL NUMBER 11897	CASING DIAMETER (INCH)	2			
<u> </u>					
	STATIC GROUND\	MATER TARLE	ELEVATION (ET)	10.45	
GZA ENGINEER M. Britos	37, THE SINES (12)	WATER TABLE		10.10	
<u> </u>	-				
ELEVATION OF MEASURING POINT - DEPTH TO WATI	ER = REFERENCE ELEVATION (WA	TER TABLE EL	EVATION)		
			,		
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGT	TH (if transducer is functioning pro	perly)			
	( (	,			
			CABLE		
DEPTH TO BOTTOM:	82.00	FT	CONNECTOR	▶ ₩	
GROUND ELEVATION:	70.26	FT M.S.L.	55111,261010	T	
	69.93				
CASING ELEVATION:		FT M.S.L.			
CASING ABOVE (+) OR BELOW (-) GROUND:	below		ODCUMP /		
DISTANCE FROM CASING TO GROUND (+ OR -):	-0.33	FT	GROUND.		
MEASURED CABLE LENGTH:		FT	SURFACE		
				<b>≯</b> 1 0	
TIME OF MEASUREMENT:	14:30	HRS			
MEASUREMENT TAKEN FROM:	TOC		WATER		
			TABLE	1	
DEPTH TO WATER:	59.48	FT			
ACTUAL DEPTH:	+ 22.013	FT			
THEORETICAL CABLE LENGTH:	<b>=</b> 81.493	FT			
HAVE CLOCKS BEEN SYNCHRONIZED?	$\square$	check		ပြော	
IS TRANSDUCER SET TO TAKE "SURFACE" READING	s?	check	CABLE		
	7000000			AD O	
ELEVATION OF MEASURING POINT:	69.93	FT M.S.L.			
DEPTH TO WATER:	<del>-</del> 59.48	FT			
REFERENCE ELEVATION:	<b>=</b> 10.45	FT M.S.L.			
TEST NAME:	MW-53-82		PRESSURE		
LOGGING INTERVAL:	20	MIN	TRANSDUCER		
TEST START TIME:	14:30	HRS		→   →	
	14.00		SENSOR		
			OLINOOTO		
			WELL		
			BOTTOM		
			DOTTOW *********		
LEGEND: <b>DTW</b> - DEPTH TO WATER				<b>▼</b>	
DTB - DEPTH TO BOTTOM OF WELL	NDED MATER				
AD - ACTUAL DEPTH OF TRANSDUCER UI					
<b>CL</b> - CABLE LENGTH FROM SENSOR TO G	ROUND SURFACE/ TOP OF CASING	j			
NOTES:					
Low battery power. Replaced batteries and	l reset. Had to pull out bladder pum	p in order to ρι	ıll transducer.		
GZA			WELL ID :	MW-53-82	

	TRANSDUCER IN	ISTALLATIO	N LOG	
GZA GEOENVIRONMENTAL OF NEW YORK			WELL ID	MW-53-120
440 NINTH AVENUE, 18th FLOOR	Entergy	l	SHEET	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy	Center	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS		l	PROJECT LOCATION	Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	124.70	DATUM	NGVD 29
<del> </del>	GROUND ELEVATION (FT)	70.260	DATE	11/24/09
	CASING ELEVATION (FT)	70.190		
	CASING DIAMETER (INCH)	1		
	,			
	STATIC GROUN	IDWATER TABLE E	LEVATION (FT)	9.96
GZA ENGINEER M. Britos				
ELEVATION OF MEASURING POINT - DEPTH TO WATE			EVATION)	
			CABLE	
DEPTH TO BOTTOM:	120.00	_ FT	CONNECTOR	···► <b>Y</b>
GROUND ELEVATION:	70.260	FT M.S.L.		
CASING ELEVATION:	70.190	FT M.S.L.	<del></del>	
CASING ABOVE (+) OR BELOW (-) GROUND:	below	_		
DISTANCE FROM CASING TO GROUND (+ OR -):	-0.07	_ FT	GROUND,/	
MEASURED CABLE LENGTH:		_ FT	SURFACE	≥
				<b>≱</b> 1-0
IME OF MEASUREMENT:	14:18	HRS		
MEASUREMENT TAKEN FROM:	TOC	-	WATER	abla
		- [	TABLE	<del></del>
DEPTH TO WATER:	60.23	FT	1/ /022	
ACTUAL DEPTH:	+ 57.979	FT		
HEORETICAL CABLE LENGTH:	= 118.209	- '.' FT		
		- ''		
HAVE CLOCKS BEEN SYNCHRONIZED?	<u> </u>	check	CARLE	0 CL
IS TRANSDUCER SET TO TAKE "SURFACE" READING	», <del>K.</del>	check	CABLE ·······	AD 0
ELEVATION OF MEASURING POINT:	70.190	FT M.S.L.		
DEPTH TO WATER:	<del>-</del> 60.23	FT FT		
REFERENCE ELEVATION:	9.96	FT M.S.L.		
\ <u>-</u>		- 11 W.O.L.		
rest name:	MW53-120		PRESSURE	
OGGING INTERVAL:	20	MIN	TRANSDUCER	
EST START TIME:	14:19	HRS		→ 🔍 🔻
		_	SENSOR	_
			WELL	
			воттом	
EGEND: <b>DTW</b> - DEPTH TO WATER				······································
DTB - DEPTH TO BOTTOM OF WELL				
AD - ACTUAL DEPTH OF TRANSDUCER UN	IDER WATER			
CL - CABLE LENGTH FROM SENSOR TO GI		ING		
		<del>-</del>		
NOTES:				
Replaced batteries and reset.				
Replaced batteries and reset.				
replaced balleties and reset.				

	TRANSDUCER IN	STALLATIO	ON LOG	
GZA GEOENVIRONMENTAL OF NEW YORK			WELL ID	MW-58-65
440 NINTH AVENUE, 18th FLOOR	Entergy		SHEET	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy	Center	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS			PROJECT LOCATION	Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	72.00	DATUM	NGVD 29
MAKE MiniTroll	GROUND ELEVATION (FT)	14.57	DATE	10/23/09
PSI CAPACITY 30	CASING ELEVATION (FT)	14.25	·	
SERIAL NUMBER 5619	CASING DIAMETER (INCH)	1	=	
33,5			-	
	STATIC GROUNI	OWATER TABLE	ELEVATION (FT)	6.22
GZA ENGINEER A. Altieri			. ,	
	_			
ELEVATION OF MEASURING POINT - DEPTH TO WA	TER = REFERENCE ELEVATION (W	ATER TABLE EL	LEVATION)	
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENG	TH (if transducer is functioning pr	operly)		
			•	
			CABLE	
<b>ДЕРТН ТО ВОТТОМ:</b>	65.00	FT FT	CONNECTOR	··· <b>▶</b> ₩
GROUND ELEVATION:	14.57	FT M.S.L.		
CASING ELEVATION:	14.25	FT M.S.L.		
CASING ABOVE (+) OR BELOW (-) GROUND:	below	_		
DISTANCE FROM CASING TO GROUND (+ OR -):	-0.32	FT FT	GROUND,∕	
MEASURED CABLE LENGTH:		FT •	SURFACE	
				# 10
TIME OF MEASUREMENT:	9:50	- HRS		_,
MEASUREMENT TAKEN FROM:	TOC	_	WATER	<b>∀</b>   <u>*</u>
			TABLE	
DEPTH TO WATER:	8.03	FT -		
ACTUAL DEPTH:	+ 60.934	FT -		
THEORETICAL CABLE LENGTH:	<b>=</b> <u>68.964</u>	FT •		
	1.78			C L
HAVE CLOCKS BEEN SYNCHRONIZED?	···	check	CARLE	_
IS TRANSDUCER SET TO TAKE "SURFACE" READIN	GS7 Y	check	CABLE	AD AD
ELEVATION OF MEASURING POINT:	14.25	FT M.S.L.		
DEPTH TO WATER:	8.03	FT		
REFERENCE ELEVATION:	<b>=</b> 6.22	FT M.S.L.		
		- 1 101.0.2.		
TEST NAME:	MW-58-65		PRESSURE	
LOGGING INTERVAL:	20	MIN	TRANSDUCER	
TEST START TIME:	9:51	HRS		▼   ▼
		-	SENSOR	
			WELL	
			воттом	
				· · · · · · · · · · · · · · · · · · ·
LEGEND: DTW - DEPTH TO WATER	<u> </u>			
DTB - DEPTH TO BOTTOM OF WELL				
AD - ACTUAL DEPTH OF TRANSDUCER U	JNDER WATER			
CL - CABLE LENGTH FROM SENSOR TO	GROUND SURFACE/ TOP OF CASI	NG	•	
NOTES:				
0.74				
C7Δ			M/CLL ID.	MM/ EO CE

	TRANSDUCER INS	TALLATIC	N LOG	
SZA GEOENVIRONMENTAL OF NEW YORK	Client		WELL ID_	MW65-48
440 NINTH AVENUE, 18th FLOOR	Entergy		SHEET	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy Ce	enter	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS			PROJECT LOCATION	Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	48.00	DATUM	NGVD 29
MAKE MiniTroll	GROUND ELEVATION (FT)	69.723	DATE	11/24/09
PSI CAPACITY 30	CASING ELEVATION (FT)	68.856		
SERIAL NUMBER 13993	CASING DIAMETER (INCH)	2		
	STATIC GROUNDV	VATER TABLE (	ELEVATION (FT)	38.25
SZA ENGINEER M. Britos			• • • • • • • • • • • • • • • • • • • •	
	_			
LEVATION OF MEASURING POINT - DEPTH TO WAT	ER = REFERENCE ELEVATION (WA	TER TABLE EL	EVATION)	
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENG	TH (if transducer is functioning prop	erly)		
			CABLE	
ЕРТН ТО ВОТТОМ:	48.00	FT	CONNECTOR	▶ ₩
ROUND ELEVATION:	69.723	FT M.S.L.		
ASING ELEVATION:	68.856	FT M.S.L.		
ASING ABOVE (+) OR BELOW (-) GROUND:	below		•	<b>A A</b>
DISTANCE FROM CASING TO GROUND (+ OR -):	-0.867	FT	GROUND,/	
MEASURED CABLE LENGTH:		FT	SURFACE	
				<b>*</b>
	45.04	LID -		
IME OF MEASUREMENT:	15:31 TOO	HRS		$\leftarrow$
MEASUREMENT TAKEN FROM:	TOC		WATER	<del></del>
NEDTU TO WATER	22.21		TABLE	<b>1</b> 7
DEPTH TO WATER:	30.61	FT 		
ACTUAL DEPTH:	+9.642	FT		
HEORETICAL CABLE LENGTH:	<b>=</b> 40.252	FT		
HAVE CLOCKS BEEN SYNCHRONIZED? S TRANSDUCER SET TO TAKE "SURFACE" READIN	gs?	check check	CABLE	- C - C - C - C - C - C - C - C - C - C
				AD
LEVATION OF MEASURING POINT:	68.856	FT M.S.L.		
DEPTH TO WATER:	<b>-</b> 30.61	FT		
REFERENCE ELEVATION:	38.246	FT M.S.L.		
EST NAME:	MW65-48		PRESSURE	
OGGING INTERVAL:		MIN	TRANSDUCER	
EST START TIME:	15:31	HRS		▶ 🖺 🔻
			SENSOR	
			WELL	
			BOTTOM	
				<b>√</b>
EGEND: DTW - DEPTH TO WATER				
DTB - DEPTH TO BOTTOM OF WELL				
AD - ACTUAL DEPTH OF TRANSDUCER L	INDER WATER			
CL - CABLE LENGTH FROM SENSOR TO	GROUND SURFACE/ TOP OF CASING	à	•	
IOTES:				
No test to download. Reset and start new	test.			
GZA			WELL ID :	MW65-48

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR	TRANSDUCER INSTA		WELL ID	U3-C1
440 NINTH AVENUE 18th FLOOR				00 01
	Entergy		SHEET	1 of 1
NEW YORK, NEW YORK 10001	Indian Point Energy Cente	er	FILE NO.	01.0017869.91
SCIENTISTS AND ENGINEERS		PROJECT L		Indian Point
MANUFACTURER In-Situ	FINAL BORING DEPTH (FT)	NA	DATUM	NGVD 29
MAKE MiniTroll		15.003	DATE	11/24/09
PSI CAPACITY 30	` ' —	18.060		1 112 11 00
SERIAL NUMBER 5548	CASING DIAMETER (INCH)	2		
SENIAL NOWIBER				
	STATIC GROUNDWAT	TER TABLE ELEVATION (FT)		10.15
GZA ENGINEER M. Britos	_			
ELEVATION OF MEASURING POINT - DEPTH TO WAT				
JEFIN TO WATER FACTUAL DEFIN - CABLE LENG	TH (II dansducer is functioning property	CABLE		
DEPTH TO BOTTOM:	NA	FT CONNECTO	R	<b>Y</b>
GROUND ELEVATION:		T M.S.L.		
CASING ELEVATION:		T M.S.L.		
CASING ABOVE (+) OR BELOW (-) GROUND:	above		<b>∮</b>	<b>↑ ↑</b>
DISTANCE FROM CASING TO GROUND (+ OR -):	3.057	FT GROUND,		
MEASURED CABLE LENGTH:	<del></del>	FT SURFACE		*
				<b>★</b> 1 0
TIME OF MEASUREMENT:	11:57	HRS		
MEASUREMENT TAKEN FROM:	TOC			
		TABLE	······································	- <del>                                    </del>
DEPTH TO WATER:	7.91	FT		
ACTUAL DEPTH:	+ 13.830	FT		
THEORETICAL CABLE LENGTH:	= 21.739	FT		
HAVE CLOCKS BEEN SYNCHRONIZED? IS TRANSDUCER SET TO TAKE "SURFACE" READING		check		CL 018
5 TRANSDUCER SET TO TAKE "SURFACE" READING	55? <u>Y.</u>	check CABLE	•	AD 0
ELEVATION OF MEASURING POINT:	18.060 F	T M.S.L.		
DEPTH TO WATER:	7.91	FT		
REFERENCE ELEVATION:		T M.S.L.		
TEST NAME:	U3-C1	PRESSUŖ	E	
LOGGING INTERVAL:	20	MIN TRANSDU		`
TEST START TIME:	11:57	HRS		,
		SENSOR.	**************	4.2.2
		WELL .		
		BOTTOM		
LEGEND: DTW - DEPTH TO WATER			*******	·. <u> </u>
LEGEND: DTW - DEPTH TO WATER  DTB - DEPTH TO BOTTOM OF WELL				
AD - ACTUAL DEPTH OF TRANSDUCER U	NDER WATER			
CL - CABLE LENGTH FROM SENSOR TO C				
SE SABLE LENGTH ROWISENSON TO C	STOCKE SOLL FOL OL OVOLING			
NOTES:				
	set.			
no connection. Replaced batteries and res				
no connection. Replaced batteries and res				

**APPENDIX C: CHAINS OF CUSTODY** 

Project #: Entergy GW Mon Prog GPL Quests # COC Number 11, PO Number: 50013510	**See www.gei.com for GEL's Sam GEL Work Order Number:	**See www.gel.com for GEL's Sample Acceptance Siver:	.com for	S S.TED	ample Acceptance S	ceptani	$\circ$	**			Charl Phon	Charleston, SC 19407 Phone: (843) 556-8171 Fax: (843) 755-1178	9407 9417) 178
Client Name: Entergy	Phone	36	(914) 736-8405	105			Sampie	Analy	Sis &	Sample Analysis Requested <sup>(5)</sup>		number of c	(Fill in the number of communers for each test)
Project/Site Name: Indian Point Energy Center	er Fax#		(914) 734-6247	6247	Ne ter						***************************************		< Priservative Type (6)
Address: 450 Broadway, Suite 3, B	Buchanan, NY 10511				Akont Samp Konsid	tainers		(GS)	Sr90	3)			
Collected by Highe Britos s	Send Results To: Patrick Donahue	hue			ated	1	H3)	Šρευ (	n 90 (	3 (Nic		•••••	Note: extra sample is
mpi	*Date Collected (C) (Mac-44-45)	Splicated CC Code	ode <sup>2</sup> kdu Filhered <sup>12</sup>	Satapie Mauriy ed	ediasetive	iisi aunde	ritium (	iamma !	teontiun	lickel 6			required for sample specific
MW-51-40-(013)	11/18/09/426	126 ×	Z	ପଞ୍ଚ				r					2 Liter Poly
MW-51-40-(013)-B	11/18/09/143	<b>13</b>	Z.	GW	×	(mail			20.00		·^^^		2 Liter Poly
MW-51-40-(013)-D	7 603 11	1449 N	Z.	GW	ベス	;,4	(and		,a	ja madi		~~~~~	2 Liter Poly
MW-51-40-(013)-S	-	438 N	z	GW	≺; 'Z	1000	(a.a.d		,	>			2 Liter Poly
MW-51-79-(013)	O.	Z (CT	z	G₩	≺ Z	~~~	/~_4	,		2		.,,	
MW-51-104-(011)		Λ Ω	Z	୍ର ≨	< Z	~~	~~		^~~			•••••	2 Liter Poly
MW-51-135-(011)	11 10 01	ار ا ا ا	2.	G₩	×			,		*****			2 Liter Poly
MW-51-163-(011)		133 N	2.	GW	Z.		<b>~</b>	, <u>.</u>				**********	2 Liter Poly
MW-51-189-(011)	11 /18 /09 11	<u>u</u>	Z	G%	×	>4							2 Liter Poly
NAT Requested: Normal:   Rush: Spe	Specify: (%b)ject to Sindauge) Pax Besulto	Pax Besulte					irek	le Dehverable	able C	CofA	OC Summary	/ Level ! /	Level 1 / Level 2 / Level 4
known hazards app	able to these samples? If so, p	glease list t	he hazası					o control and				Sumple Co Fastern Central Mountain	le.
Chain Tane	Chain of Custady Signatures  Received by (signed)	Date:	%ink		9	CH. LW	E .	RIN TF	TRENT		Sample Shipping and Delivery Details	d Delivery E	Details
March 2 1 2009 1	200 STOPAGE	11 20	000	12	0	Method of Shipment	Shipm	cnt	XBCB4	XEX	Date	Date Shipped:	
	7				Air	Airbill #:						***************************************	
3				-	Ai	Airbil! #:	-	-			noncon annoncon anno	damment months	
The Chief of the Land Comment of the													Commence of Warrening and American Advanced
. A.	ette, EB v Sajeptoeri Blask, MS-Natou S engle was field Bharod in N-ko seniye wa e Waler, WWWide Wate, Wellinger, MC	ABS Maeru, Spèke Sampte, 483D- Marrix Spike Dyphrate Sample, 65- Grah, Cc Composite for sample was not 5500 filtreet. Browner, M. (Most Line), 380-501, 500-550 firem. M. (Stadio, 585), and Waste, 45-01.	NOVE STORY OF STORY	pike Dephea diment <b>SL</b> eb	z Sample, Gr	Chah, Co	Samposi	estinor.	William (	\$44 P0000	assir I, Polifitar, Polifija, (Iotjina, Polifical, Nobasa	*****************************	Custody Seal hine?

lergy GW Mon Prog	GEL Chain of Custody and Analytical Request **See www.gel.com/for GEL's Sample Acceptance SOP**	hain of Custody and Analytical Re**See www.gol.com for GEL's Sample Acceptance SOP**	ample Accept	ance SOP**	quest	2040 Savaye Road Charleston, SC 29407 Phone, (841) 556-8171	oad 29407 36-8171
COC Number 50013540 G	GEL Work Order Number:					Phone. (843) 556-8171 Fax: (843) 766-1178	56-\$171 -1178
8	Phone #: (914	(914) 736-8405	et visienne	Sample Ana	Analysis Requested 🤲		(Fill in the number of containers for each test)
Project/Site Name: Indian Point Energy Center	Faxe	(934) 734-6247	lete				< Preservative Type (t)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	Johanan, NY 10511	VECTOR AND	Shout somp consid		(Sr90)		Stadistic_3
Collected by M. Britos So	Send Results To: Patrick Donahue		ofrd	H3)	n 90 (		Note: extra sumple is
Sample ID  * for comparies - indicate their and step data-time	*Date Collected (C.C.pde (ABBits)) (C.C.pde (ABBits	ode Field Sample Fiftered <sup>(2)</sup> Matrix <sup>(3)</sup>	Radicactive TSCA Regul	Tritium ( Gamma	Strontiur		required for sample speciation
MW-40-100-(012)	N 464 60 61	N GW		bud bud			2 Liter Poly
MW-40-127-(012)		, N GW	×	100.d 100.d 100.d	;		2 Liter Poly
MW-40-162-(010)		N CW	Z Z	61 64			2 Luer Poly
MW-40-27-(009)	11/19/09/1457 N	i N GW	≺ Z	Annual An			2 Liter Poly
MW-40-46-(010)	<i>            </i>	Z GW	Z Z	 			2 Liter Poly
MW-40-81-(010)	11 17 09 135) N	N GW	re;	inst-	)		2 Liter Poly
Rush	Specify: (Subject to Suppliate) Fax Kessilis:	ď s		Circle Delia	Deliverable: Cof A /	OC Summary / Level	Level 1 / Level 2 / Level 3 / Level 4
known hazards app	ble to these sumples? If so, please list t	the hazards					Sagnole Collection Time Zone Eastern Pacific Ceation Other
Chain Chain	1 m	E is successive.	Me lian	E .	Sampi N TRENT	Sample Shipping and Delivery Details	ry Details
1000 00 00 00 00 00 00 00 00 00 00 00 00	0902 STO (AGE 11 2)	20 09 090	N	f Shipm	FEDEX	Date Shipped	
	14		Airbill #	**			
00000	1,2,1		Aireil #	*			- Announce of the Announce of
<ol> <li>Chair of Custody Number ~ Cliest Beterosteed</li> <li>QC Codes N. A. Norwal Sample, VB ~ Trip Blank, FD~Field Duplion</li> <li>Field Planead. For Hapidenneticus, indicate whith a Y—for yets the sam</li> </ol>	usody Mamber * Clear Determined Nº Normal Sample, 78 ° Trip Blank, PD-Picht Dualouer, 23 ° Equipment Black. M5-Marrx Spike Sample, M80° Marrx Spike Supileate Sample, &> Grait, C. Composite ad For Equid marricus, indicate whith a Y-For yes site sample was field filtered by N·For surrole was out Sand Elecad.	1989- Masse Spike Capile 26.	tate Sumple. 🗗 Grai	), C = Composite			For Lah Receiving Use Only  Custody Sent Inucci
<ol> <li>Main's Codes: DW-Orlobling Water, CW-Groundwater, SW-Gurlage Water, WW-Water Water, Mc-Water Mic-Major System, SE-Scotter on Account of Analysis Requested. Analysis Analysis Requested. Analysis Requested. Analysis Requested. Analysis Requested Analysis Requested. Analysis Requested for Analysis Requested. Analysis Requested for A</li></ol>	e Water, WWe Water Water, We Water All 2006 St. Inglod. St. Bl. (46198/7479)Aed mamber of containing provided for each Sodourn Hydroxods, StA's Sulfains Acid, AA's According Acid	erson, montenences se h (10 a albane A dollanda) 4, UN-dennic AT - Soc	indiange, are done to make, version, et and e. 1774 - E. India Thiospifore, if no preservative is added	o preservative is add	est = leave field blank	Company	Cooler Temps
6.) Plaservative Type: 8.44 Hydrocatore Acid. No = 8888 Acid. 581 State Dyoroxide, 364 - 568	SOCOTIO 13/60/07/600, SIA = SECESTE SOCIE, ACAT ASSECTION OF CONTROL	Control of the contro	Shifteen a Transferration of the Con-	The same of the sa			

1 0.5	OF Chain affinished		GEL Laboratories, LLC
Project #: Entergy GW Man Prog GBL Quete #:	**See www.gel.com for GEL's Sample Acceptance SO	**See www.gel.com for GEL's Sample Acceptance SOP**	2040 Savage Road Charleston, SC 29407
COC Number 50013510 GEI	GEL Work Order Number:		Phone: (843) 556-8171
Client Name: Entergy	Phone #: (914) 736-8405	05 Sample Analysis Requested <sup>(6)</sup>	(F)
Project/Site Name: Indian Point Energy Center	Fax #: (\$14) 734-8247	d state fe to: ered:	< Preservative Type (6)
Address: 450 Broadway, Suite 3, Buci	Buchanan, NY 10511	(GS) Sc90	( ) test were the
Collected by M. Britos Send	Send Results To: Patrick Donahue	ratean (13) Special	Note: extra sample is
Sample ID  *for composing - Indicate som and som datedome	*Date Collected Collected OCTOde Field (State Collected OCTOde Field (State Odfillor) State of State o	SCA Regul intal months (Frithum ( Ganarna ) Strontiur Vicket 6.	required for sample specific
I AFJ02-(012)	N 3E CI PO PI II	- 1	7 Liter Bak
***************************************			
TAT Requested Normal: V Bush Specify	y (Sosjectin Surchage) Fax Results. Ves	(No Circle Deliverable, Clof A. /	OC Summary / Level 1 / Lovel 2 / Level 3 / Level 4
known hazard	te to these samples? If so, please list the hazard		Sample Collection Little Large (Eastern) Pacific Central Other
Chain of	Chain of Custody Signatures	Sample	Sample Shipping and Delivery Details
School Date Tene	Received by (signed) Own Time	GELPM ERINTRENT	
Municipal 18 11 120 09 0900	OPEN STORAGE 11 20 09	2	Date Shipped:
	1-2	Àirbill 4,	
	3	Airbill #:	
<ol> <li>Charrot Cabab, Nomber v Clear Depriment</li> <li>Charrot Cabab, Nomber v Clear Depriment</li> <li>Charrot Cabab, Nomber v Clear Depriment</li> <li>Composite</li> <li>QC Caba. No Nomber v Clear Depriment</li> <li>Charrot Cabab, No Nomber v Clear Depriment</li> <li>Charrot Caba, N</li></ol>	. KB ~ Eupoproest Frlank, 1889: Marris Spake Sjorgbit, MSB* Makris Sp	nke Duplicate Sample, Gr. Grab. Cr. Composite	For Lab Receiving (See Only
<ol> <li>Field Filtered. For dignal macroes, indicate with a Y-fer yearthe sample was field filtered in N-for sumple was not field filtered.</li> <li>Matth Cades. BWell-rinking Water, G.Welfstoundwater, SWelfunface Water, W.Welfunface, W.Welfunface, M.Deffunface, M.Deffunfa</li></ol>	le was freid lithered op N - for supply was ned field filhered fraas N Yo-Waste Water, Yo-Water, ML-Milyo Liquid, SO-field, SO-field	3.) Sield Filtered. For dignid rearrooms, Indicate with a Y- for you the sample was field littlered on N- for standis was not field littlered.  3.) Sield Filtered. For dignid rearrooms, GW-Spanishware, SW-Sanishware Wasser, WW-Waste Wasser, WW-Waste Wasser, WW-Waste Waste, Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldi Waste, O-O-O-Filtered W-Waste Waste, WW-Waste Waste, Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldi Waste, O-O-O-Filtered W-Waste Waste, WW-Waste Waste, Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Waste, WW-Waste Waste, Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Waste, Waste Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Waste, Waste Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Waste, Waste Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Waste, Waste Dignid SO-Saldiment, SU-Saldiment, SU-Saldiment, SS-Saldiware, O-O-O-Filtered W-Waste Dignid SO-Saldiment, SS-Saldiware,	
<ol> <li>Sample Analysis Requested: Analytical method requested if a, \$266H, \$6188/79/79\$25 statisfier of configure type and the exception of a \$15/16 of \$15/16 o</li></ol>	SATERNITATIBALIS INITIDES OF CONSISTED PROVIDED TO SERVE THE STATE IN A STATE A STATE A STATE ASSESSED ACID, BLANK BUSHING ACID, BLANK BUSH BUSH BUSH BUSH BUSH BUSH BUSH BUSH	. \$010/07/2470.4 - 1). ST ~ Sindom Thoughtim: If no preservative is added ~ leave held biank	Gunt senso
= XIJHM	WHITE = LABORATORY YELLOW = FILE	H.E. PINK - CLIENT	

	GEL Chain of Custo	GEL Chain of Custody and Analytical Request	GEL Laboratones, LLC
BY John 4. CHENTRY PAR WON FIND	**See www.gel.com fo	**See www.gel.com for GEL's Sample Acceptance SOP**	Charleston, SC 29407
OCNumber (4): 02 Number (50013510 GF	GEL Work Order Number:		Phone: (843) 556-8)71 Fax: (843) 766-1178
iron Name: Entergy	Phone #: (914) 736-8405	\$405 Sample Analysis Requested (8)	(8113)
າດject/Site Name: indian Point Energy Center	Fax #; (914) 734-6247	d this te by: isred:	~ Pressyvative Type (6)
ddress: 450 Broadway, Suite 3, But	Buchanan, NY 10511	(GS)	Singuists (
ollocted by CS, MB ———————————————————————————————————	Send Results To. Patrick Donahue	H3)	Note: extra sample is
Sample ID  * For composites - indicate vast and stop date time	*Date Collected Collected Of Code Field (man-ad-yy) (McBillart) 0 Feldered Of Code Field	R. C. Radioscoles  FSCA Regul  Tritium (  Gamma   Strontium	Separate Special
U3-T1-(026)		GW Y N	2 Liter Poly
U3-172-(031)	N S S S S S S S S S S S S S S S S S S S	0# Y X	2 Liter Foly
***************************************			
TAT Requested: Normal: Y Rush: Specify:	fy: (Subject is Southerge) Fan Kondin, Yes	s / (No) Our le Deliverable: C of A / QC Summary	_
- 2	de to these samples? If so, please list the have		Sagning Collection Time Zone Lastern Pacific Control Other
	Chain of Custudy Signatures	Şa	Sample Shipping and Delivery Details
Retinaged and Experience ( ) Day ( inne	Received by (signed) (site fine	GELFM ERIN TRENT	
77 Krad of 19 11 16 16 16		ુ 영 4 를 O Method of Shipment FEDEX	X Date Shipped:
	2		
**************************************		Airbill k	
Chair of Cassay Stander - Clear December of the Eight Emphases. I B Standstoner Black - M.S Assoc Souge Sangle, MSD - Matth Shike Database Sangle, W Cash C Cash Cash - Cash	e. \$ B Smoothers Blank. NSW Marks South Sample. MSD: Mari	s Shiker Dupticase Swepter & Craib, C - Composite	Fin Lab Receiving Use Only
Field Filened. For Househous, indicate with a X-far per the sample was field filened on X-far zonaple was not field filened.	ple was held Klassed en K. do: sanghe was not held blitand. The Minister of the Bouwer of a Mark Lind I Winday [8]	Field Filtered For Signif Impaires, include with a Y - far yes the sareple was field filtered on Y - far yes the sareple was field filtered on Y - far Special States of Section of Special Waste Delil, Section, Perform, Fernal, Performing Special States of Special States of Special States of Special Sp	ing, F. Facal, Solitani P. S.
Sample Analysia Requested: Analytical exclude requested to 82668	Water, GW 4 countries of WY buttace water. Www water water water act, with some copies, and some recurrence of a family standard and the standard and standard provided for each ( a 5.0666 5. doi:10.07.0766 5. doi:10.07.0766	\$5.3 of 10 Per 17 (No. 1)	Cooler Temp:
: Progressive Type: HAY Hydroddodd Acad Al o Nobel Acad, Mar Societa (Dydroddo, Acad Section Color of Societa (Dydroddo	WHITE = LABORATORY  WHITE = LABORATORY  YELLOW = FILE	FILE PINK = CLIENT	

WHITE = LABORATORY

*		. !	(H) Laboratories, LLC
Project #: Entergy GW Mon Prog	GEL Chain of Custody and Analytical Ko **See www_gelcom for GEL's Sample Acceptance SOP**	id Analytical Request	2940 Savage Boad Charleston, 50, 29407
50013510	CEL Work Order Number:		Phone (843) 556-817) Pax: (843) 756-1178
	21ame № (914) 736-8405	Sample Analysis Requested 🥯 (Fill	(Fill in the number of containers for each test)
Project/Site Name: Indian Point Energy Center	Fax #: (914) 734-8247	ie tre ered;	<¥reservative Type (b)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	an, NY 10511	(GS)	Substante 3
Collected by: 🎉 🛴 Sand Resi	Sand Results To: Patrick Donahue	r ar con (£13) Spec	Note: extra sample is
outte	*Date Cellautroi Cellautroi Qe Cade Heid Sample (2005) (20	3 7 FSCA Regul FSCA Re	Politica is sample.
MH-5-(007)	WO N CHEST THE	< Z	2 Liter Poly
TAT Requested: Normal: Kush Specify:	(Subject to Seatcheage) Fax Restiles. Yes /	No Circle Deliverable. C of A / QC Summary	
Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards	these samples? If so, please list the hazards		Sayupk Collection I tore Zeen Eastern Pacific Lemma Other
	1 - 1 - 2 1 - 1 1 - 1 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	Sample Shinni	Syante Shianiae and Belivery Belaik
Reginguished By (Signed) Date Time	Received by (aspect) See: Sine	GBLEM ERIN TRENT	7
		f Shipa	Pate Shipped:
	7	Airbil #:	
	Eurit	Airbill #:	· · · · · · · · · · · · · · · · · · ·
1) Chair of Canady Number - Clean Determined  1) Chair of Canady Number - Clean Determined  3) Short State S	e Europeann Bhaic. MS: Meath Spile Sanoyle, MSB: Matrix Spile Dept.	sace Swaphs, Gr. Grab, Co. Composite	For Late Reversing User Only Custody Seed Insect
<ol> <li>Aberta Christ DW Hitching Wass, GW-Grondweler, SW-Sortiner Wars, Wyerwasse Water, We-Waser, MMac Liquid, SO-Soil, SD-Soddwest, Sk-Studga, SS-Soild Wass, Leon.</li> <li>Annedic Analysis Represent. Analysis of represent (i.e. N2608, 4611987/4768and purefor of consultant provided for each (i.e. 87608, 5, 6911087/4704 - 1).</li> </ol>	WW-Wasia Water, We-Water, MtMiae Lispaid, NO-Soil, ND-Stellbucht, S 1747/1860ed mercher eX consultates provided for each U.c. 8256-6-3, 691087	(mSpadys, \$96-Solid Wasse, Certon, Perfeiter, Perwyse, Verbines, Peressat, Neterosa 4704 - 1)	Cooler Temp:
6) Progressive Type Haw Hydrichonic Acid, NY Strike Acid, SH: Souther Hydroxide, SA= Solfistic Acid, AA= According Acid, HX= Hother Howest Hill Hill CLIENT  WHITE = LABORATORY  YELLOW # FILE  PINK = CLIENT	BORATORY PARE AND ASSOCIATION FILE	BINK ~ CLIENT  CHARLES TO DESCRIPTION OF TOWER THE OWNER.	

TO Sumber 50013510	**See www.gel.com for GEL's Sample Acceptance SOP* GEL Work Order Number:	**See www.gel.com for OEL's Sample Acceptance SOP** ber:	w.gel.c	om for (	Sanae	ajdium	Acce;	ytame:	SQE	*	ĕ- :			***************************************	Charleston, 3C 29407 Phone: (843) 556-8171 Fax: (843) 766-1178	ston, 5 (843)	556-8 556-8	× 3 8	
R		Phone #:	(914)	(914) 736-8405	95			565	Sample	Ana	lysis i	Analysis Requested (5)	Eed of		in the	houh	er of	ontai	(Fill in the number of containers for each test)
mjsseSite Name: Indian Point Energy Center		Fax #:	(914	(914) 734-6247	247														< Preservative Type (8)
kddress: 450 Broadway, Suite 3, Buche	Buchanan, NY 10511	AAAAAA				Sheed	cuesid	tainerr		(GS)	(Sr90	53)							K'ramananyo
Allocted by: B, NR Send F	Send Results To: Patrick Donahue	Donahue			AAAMMINING	_	sted	r of con	H3)	Spec (	a 90 (	i (Nit			***********				Note: extra sample is
Sample ID  * For composites - indicate start and stop datestime	*Date CoSected	*Firme (Collected (Millected (Millected)	OC Crade	g Keda Filtered <sup>(A</sup>	Sample Matrix (4)	Badtosesive	ISCA Regul:	Enist nambe	Tritium (	Gamma :	Strontiun	Nickel 63							required for sample specific QC
MW-54-123-(011)		Z.	z	z	GW	×	z			,		~-							2 Liter Foly
MW-54-144-(011)		<u>5</u>	Z	z	GW	~	2	feren		ia.									2 Liter Poly
MW-54-173-(011)		1204	z	Z	GW	~	Z	4.04	had.	jand	~~i								2 Liter Foly
MW-54-190-(011)	•	7	Z	Z	GW	~4	Z	fo.e.d	;e	شمعز	m-i	,							2 Liter Poly
MW-54-37-(011)		135	z	······	GW	*4	Z	(4.1.4	janë	janë.	, mai	,							2 Liter Poly
MW-54-58-(011)	4	<u>-</u>	Z,	~~~~ Z	GW.	~<	Z	tand		inni	proced	·							2 Liter Poly
TAT Reguested: Normal: Y Rush: Specify:	(Subject to Servinage) Fax Rusalts	geo Fax Re	Salts -	žů .		<b>?</b>	V 🔣			Delay.	Circle Deliverable, C	08.2	٠.	QC Summary	mary	- FW	2	\$	vel 3 / Lovel 3 / Lovel 4
кпоwn hazards app	to these samples? I	f so. please	list the	hazard	S												Sample Col Eastern Control		Sample Collection Time Zone  (Enattern) Practific  Control Other  Mountain
Chain of C Relinguished By (Signest) Date Time	Chain of Custody Signatures Rounted by (signed)	gerd) Date		Time			CVEL PM	S.	E	Z	ERIN TRENT		ipie S	hippi	Sample Shipping and Delivery Details	Delf	15.00	etail	E S
	5 DEVENTORES INSIN	\$70846	20		1	7	Method of Shipme	0.0 PM	Shipu	)est	72	EDEX.			Date Shipped:	dading	ă.		
	2						Airbill #	34											
Chain of Custody Number - Chest Determined	3						Caron A	. 3											For Lub Rowering Use Only
) P.C. Lode: W. Manne, Sample, Let ". Displayed and Associated and	ess field filtered of N - fre sa	rryk sas rot del for Mi-Miss Li	el Herred.	Sp.Ko	ingen: SL	A STREET	\$85050 5050 5050 5050 5050 5050 5050 505	Wilkie.	<u></u>										Custody Seal Priace?
PRODUCE LANGE WITH A LINE WAS A STATE OF THE PRODUCE AND A STATE OF THE PRO										Catalan.	No. Action	Sections.	Sec. Sec.	% S-20	ssa.i				YES - MO

Project # Entergy GW Mon Prog	GEL Chair	Chain of Custody and Analytical I	stody	y and	<b>&gt;</b>	2	Y Ti	2	Re	<b>Request</b>	2			इ हैं।	UEL Laboravaries, U.C. 2040 Savage Road	ige R		- 8	
COC Number (1)	CFI Wark Order Number	dibbot	Š	0000	26.3.	2000	200	Ş	,					<u> </u>	Charleston, SC 29407 Phone: (843) 556-8171	#3) S	18-18-18-18-18-18-18-18-18-18-18-18-18-1		
50013510	***************************************									***************************************				To see	Fax: (343) 766-1178	766	1178		energy (A. M.
Client Name: Entergy	Phone #:	1	(914) 735-8405	Gi			20	Sample	ê A 81	Analysis Requested (5)	Requ	ested		E 45	साइ उस	n der	2	ortain	(Fill in the number of containers for each (est)
Project/Site Name: Indian Point Energy Center	9r		(914) 734-6247	14.7															(9) adill adivised firs
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	uchanan, NY 10511				Shool	\$66.6555 \$66.6555	tainers		(GS)	Sr90	*********								C commence of the control of the con
Collected by: CG <sub>I</sub> MB s	Send Results To: Patrick Domanue	ä	000000000000000000000000000000000000000			red	r at con	H3)	spec :	1 90 (	****	~~~~				*******			Note: extra sample is
	*Date Collected *Time				five	iogaite	matees	m (	na S	tiun	******	*****	in alala a ala			*****			required for sample specific
Sample II) *For compaction - indicate north and step distribute	(Accepted (Accep	(Kast)	S, Perence Plots	Manya **	Radione	I SCA 8	Ented see	Tritio	Gaem	Strom		******	********			******	e ererere erere ere i		8
MW-62-18-(011)	285 E2 E2 E2 E2	S Z	Z	OW.	~<	z	<b>~~</b>	,		,									2 Hier Poly
MW-62-37-(011)	527	z IJ	Z	Ω ₹	~4	i- Markan Markan	,	, ma		***		******				.,,,,,,,,,,,	******		2 Liter Poly
MW-62-53-(010)	333	ŠÓ.	Z	Ω₩	×-4	72.		***	,	;									2 Liter Poly
MW-62-71-(011)	1240	Z Z	Z	G₩	~<	Z	***	,	,								~~~		2 Liter Poly
MW-62-92-(011)	1243	ζ Z	Z	Ο₩	×	æ	;		<u>.</u>										2 Liker Paly
MW-62-138-(011)	5)	z	Z	୍ୟ	><;	Z		<b></b>	,i	LA			******						2 Liter Poly
MW-62-182-(011)		N	Z	ୃଷ୍ଟ	بح <sup>ز</sup>	Z			,										2 Liter Poly
														***************************************					
TAT Requested Narmal: 🗡 Rush: Spe	Specify: (Sulped to Surphage) Fax Results:	x Results:	Yes	~	8	$\vee$		Circle I		Merable: Cof A	೧೫	·	OC Summary	1Pusture	٠	Level 1	 	Eovel 2	42 / Lovel 3 / Lovel 4
hazards app	able to these samples!" If so, ple	ease list the	hazards													x 0/-0%			Sample Collection Time Zone (Bastery) Pacific Country Other
Chain	Chain of Custody Signatures			***************************************							80	mp&	Sample Shipping and Delivery Details	ing a	thd E	સીંપ્લ	Ç D	Mails	S
Relangushed By (Nigard) Date Faire	Received by (signed)	Date	X mass			GE	P.K.	ERI		NTRENT	£								
1 500 CH CASAS III 12 150 17	The Same Save		1111207		0	Method of Shipment	94 94	Shipr	TR28	Ξ	XSQBH	×		7	Unto Shipped:	pped	.,		
	7.2					A littery	#			•									
	1.03					Airbil#	*												
1.) Chan of Cuntody Mannior - Clien Determined 2.) CCCodes: No Manual Sangulo II Bor Dig Blank, Fib-Poolet Dupticane, EB or Equipment Blank, MSO Marrix Spike Sangulo, Manual Spike Daphenia Sangulo, Gordina Co-Composida 2.) CCCodes: No Manual Sangulo II Bor Dig Blank, Fib-Poolet Dupticane, EB or Equipment Blank, MSO Marrix Spike Sangulo, MSD of danix Spike Daphenia Sangulo, Gordina Co-Composida	icare. \$33 - Equipment Black, MS-Merrix Spil	ke Sample, MSD	- Watain Spid	kz Dopheda	: Sample	, <b>\$</b>	% C-	Campa	r n										For Lab Reporting Use Chir
4.) Optive Codes DW-Christian Wilder, GW-Control Websiger, SW-Surface, Warrier, White Liquid, 339-Sort, 339-Sort, 389-Sortide Water, Origin, Sw-Striet Water, Dw-Cit, Sw-Striet, Pw-Wipe, Codes, No. No. 1, 1986-1, 19	the Wester, WWW-Wigner Wister, WW-Wester, MS-78.	ing Liquig SEPS atlant for each fit	30 50 - Sodio 31 50 - Sodio	man, 58S	ික්කුද, S	Sex of id	Waste	<b>9</b>	700	i powie	7 (V)	out Sult	Focal, N	Navoj					Cooker Temps
s) Inservative Type: BAs Hydrochoric And, SI - Nove Acid, SIF Sodhen Hydrochie. San Sulfuric Acid, AA: Assemble Acid, BX- Breams, ST - Sodices Throubline, St on prevenentive is noticed in leve field black  WHITE - LABORATORY  YELLOW - FILE  PINK - CLIENT	Acid, SB Section Hydrocide, SA: Sulfuric Acid, AA: A WHITE::::LABORATORY	FFESA. On Year systems	YELLOW - FILE	ST - Solice	e Thesa	Olima II	#NIA	(= C)	PINK = CLIENT	~; ∂. :: :: :: ::	ર ઉદ્ધીર્થ 1	Š.					·		

Project #: Entergy GW Man Prog	GEL Chain of Custody and Analytical Re **See www.gel.com for GEL's Sample Acceptance SOP**	and Analytical L's Sample Acceptance SOI	tical Request		GEL Laboratories, LLC 2040 Savage Road Charleston, SC 29407	
COC Number <sup>(1)</sup> , GEL V PO Number: 50013510	GEL Work Order Number:				Phone: (843) 556-8171 Phx: (843) 766-1178	
	Brone #: (914) 736-8405	•••••	Sample Analysis	Analysis Requested (5) (Fill)	(Fill in the number of containers for each (281)	rs for each (est)
Project/Site Name: Indian Point Energy Center	Fax # (914) 734-6247	al thix de be				< Proservative Type (f)
Address: 450 Broadway, Suite 3, Buchanan,	anan, NY 10511	Shud smp sonsid	(GS)			Company of the second of the s
Collected by: Sond R.	Send Results To: Patrick Donahue	ated	H3) Spec (			Note: extra sample is
a l	*Thate Collected Collected CC Code Field (burn-dd-ty) jhhaun; the Hellored file (burn-dd-ty) jhhaun;	Radioactive FSCA Regul:	Fritium ( Gamma S	Nickel 63	25	required for sample specific QC
MW-67-105-(010)	z	····				2 Liter Poly
MW-67-173-(011)	11 /1 /0"   1450 X X	GW Y N	dand tand	,		2 Liter Poly
MW-67-219-(010)	HINGS INC N	G₩ Y N		<b>,</b>		2 Liter Poly
MW-67-276-(010)	10 10 1 123 N N	GW Y N		<b></b>		2 Liter Poly
MW-67-323-(010)	5	GW Y N	quad	···		2 Liter Poly
MW-67-340-(010)	11 1 123 N N	GW Y N		····		2 Liter Poly
MW-67-39-(011)		GW Y N	hank hank jank	;*		2 Liker Poly
TAT Requested: Normal: Y Rush: Specify:	(Subject to Surcharge) Fax Results: Yes		Circle Deliverabl	Deliverable: C of A / QC Summary	/ Level !	/ Lovel 2 / Lovel 3 / Lovel 4
rds apj	to these samples? If so, please list the bazards				Sample Collection Time /orx.  [Sastem	
	Chain of Custody Signatures				Sample Shipping and Delivery Details	
St. Ed IIII & St. Commention of	~	CCC Method o	EKIN IK	EX.	Date Shipped:	
		Ajrhill #	= #·			
0, 3		Airbill #	TT #:			THE
<ol> <li>Chain of Curtody Nonsber - Clerk Determined</li> <li>Codes: N Marrad Sample, TB - Prij. Black, FD- Sield Daplicate, EB - Englishment Black, MS- Marrix Spike Sample, MS</li> <li>Field Filtered: For Inquid matrices, indicate with a Y - for yet the sample was field Distract of N - for topol own not field Reseat.</li> </ol>	mody Nowber - Chen Decembed  No Morred Sample, TR - Frig Block, FD - Sudd Daplicae, EB - Engigerent Block, MS - Marix Spike Sample, MSD - Marix Spike Deplectu Sample, G - Grab, C - Composite c). For inpud matrices, indicate with a V - for yea the sample was field fibered at N - for complete was not field fibered.	Duplieur Sample, Gr. Gr	yh, C'= C'umposie	fine fiel fram Priferal Now		For Lab Bergeoing Use civily Chaledo Svol Insact!  VEX. NO. NO.
4) Matrix Codes 1999 Prinsing, when, Compositional Commission was a few formal and the control of the principles of the	er (i.e. <b>5260B.</b> 681919/7479And morden of crantifices provided by each (i.e. 5260B. 3, 6916 Acid, SB+ Eodson Bydroxide, SA= Sylfieric Acid, AA= Ascerbic Acid, HX= Baston, ST ×	168674995 - A). Fr Seddan Thewalfabe, S	See preservative is added in le	ave field blank		Capter Frage

Sure: 1 Di	6 81.5 B. ball 1.5		CASTONICA SEGUENTE SE SEGUENTE	(TE) I glavyaveljas ( ) j
Entergy GW	CEL Chain	of Custody ar	GEL Chain of Custody and Analytical Request	2040) Savage Road
OC Number (1)	No.	e onco no upportagion s	DEE www.gendoin for Onch's basiliand Abbaptasiska Storing	Charleston, SC 29407 Phymes (843) 556-8175
50013510	CAST AND SE CANTES IN SECULAR			Fax: (843) 766-1178
Them Name: Entergy	Phone #:	(914) 736-8405	Sample Analysis Requested (%)	(F)
rojecvSite Name Indian Point Energy Center	H Fax#:	(914) 734-6247	de ha kerest:	< Preservative Tyrze (u)
tddress: 450 Broadway, Suite 3, Buchanan, NY 19511	uchanan, NY 10511		(GS) (Sr90	
Collected by:	Send Results To: Patrick Donahue	COCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCO	H3) Spec	Note: extra sample is
Sample ID	*Time *Date Littlement (Aliftene)	1 QC Code Pield Sample	s of subsective sections of the subsection of th	required for sample specific QC
MW-66-21-(011)	241.	Z Z		37 than Bob.
WW-66-36-(010)		Z Z	~	7 I How 2/11
	44			
***************************************				
	~~~			
TAT Requested: Normal: Y Rush: Spe	Specify: (Subject in Surcharge) Fax, 5	Fax Results: Yes /	Circle Deliverable: Cof A / C	OC Summary / Level 1 Level 2 / Level 3 / Level 4
кножн hazards apj	thte to these samples? If so, pleas	se list the hazards		Sample Contra
Chain			Sample!	Sample Shipping and Delivery Details
Relinquixhod By (Signed) Date Fino	(bed)	Date Time	GELFM ERINTRENT	
	OP SEMPE STOOMS	Will Too	Method of Shipment FEDEX	Date Shipped:
		BARRARA BARRARA POPONONO POPONO POPON	Airbill #:	
	int.		Airbill #:	
). Chain of Custody Namber - Claid Determined. ) QC Codes. We Karrod Sangle, US - Frig. Black, FIP. Field Duplicace, ES - Supinared Black, MS- Marix, Spike Sample, MSP- Media Spike Supinared Service Codes, C - Charpoore (A. Field Febred - Ver Kurtod Supple, US - Frig. Black, FIP. Field Duplicace, ES - Supinared Black, MS- Marix, Spike Sample, MSP- Media Spike Supinared Spike Sp	uste, \$8 = Rapisperson Blank, MS- Morrix Spike i imple was Keld Siteration N - On somple was not i	Sumple, MSD+ Metrix Spike Dopli Self Mered	osie Sanjale, Ge Greb. 🗗 « Distribusore	For Lab Receiving Use (Saly Caspulv Seal Intest)
<ol> <li>Mante Codes (1994) Physiciag Ware, CW-Chronolouser, SW-Chronol Well-Well-Well-Ware, Well-Wales And Codes (1995) Serrosines and Codes (1995) Physiciage Ware, Well-Well-Well-Well-Well-Well-Well-Well</li></ol>	e Weiter, WWW.Waste Water, We Water, ML wilder 28, 6010877479, seed paredet of containers provide 6 - Kim Water, Nr. 240 Serfects 2 old 4 20 feet	Liquid, 943-581, 983-589 mem. 98 50 each (Le 82868-3, 69708/7 50 each (Le 828 November 97 × 80	iespiedyk, streinkou w take. Green, z remen, z remen, z menjec procioca, em 2007 - Diometrica, de no sprespessive is galied a jostve field alaeni.	Caster Forge
THE PERMITTER TYPE HAS EXPERIMENTATION OF THE PRINT OF TH	WHITE :: LABORATORY	XELLOW - FILE	PINK CLIENT	

Project #:Entergy GW Mon Prog  3EL Quote #:  "OC Number <sup>(1)</sup> ;  GEL We	**See www.gel.com for GEL's Sample Acceptance SOP**  GEL Work Order Number:	See way	.Hain of Custody and Analytical Re **See www.gel.com for GEL's Sample Acceptance SOP**  ker:	ody an	1 <b>d An</b> Sample A	cceptain	cal I	* Req	nest			2040 Savage Road Clarleston, SC 20407 Phone: (843) 355-8171	2040 Savage Road Charleston, SC 29407 Phone: (843) 556-8171	03d 29407 56-817	<u></u>
?	hai	Phone # (	(914) 736-8405	3405	besolstood		Sample		Analysis Requested (5)	ested		in the	in the number of co	of con	(Fill in the number of comainers for each test)
roject/Site Name Indian Point Energy Center	200		(914) 734-6247	4-6247	le be	oreed:									< Proservative Type (o)
Address: 450 Broadway, Suite 3, Buchana	Buchanan, NY 10511				decourse Strongs Egenes	conside		(GS)	Sr90]						,
Allected by: C[3, MB] Send Resi	Send Results To: Patrick Donahue	nahuse				i.	H3)	Spec (	190 (	*****	********		~~~~		Note: extra sample is
Sample II)	*Date Collected		25.63 BB	Field Sample Sincred <sup>38</sup> Matrix <sup>46</sup>	adiosctive	SCA Reguli	ritium (	Jamma 5	trontiun	~~~~~~	************	******	······································		required for sample specific
MW-43-28-(013)	1 / 2000	Ĭ E	Z.	Z WED		Z									? { itser Brdo
WW. 43-62-1013)		7			<	<u>~</u>	-	-	-					+	7 F. Stran Bode.
								-	ļ	<b></b>	<u> </u>				
					*********										
								-		-				-	
TAT Requested: Normal: V Rush: Specify.	(Subject to Senderted)	Fax Results	-	Ýes /		$\stackrel{\checkmark}{+}$	Citade D	Delivery -	Siverable: Cof A	٠. ا	8	X Summary X	- 1		Terror 1 / Employ 1 (mark)
inown hazards o	hese samples? If s	r, please l	ist the haz	urds											
Chain of Cust	Chain of Custody Signatures								s	ample	Shipp	Sample Shipping and Delivery Details	Delive	ry De	etails
Reliaquished By (Squed) - Date - Fine - S	Recribed by cogneds	) (Jake	Fanz			OET PM:	ERI	$Z_{i}$	TRENT						
and brown Illiplas Ilalia	SECURE STORMOR	το?πα	E ilhedom	1	6	Method of Shipment	f Shipin	ent	FEDEX	×		Date S	Date Shipped:		
	5-a				· h-	A Irbill #							*	0	
	· 2,3				****	Airbill #:									
.), Chair of Ciratoly Norsher v. Client Deformined. 2), OC Coles. No Normal Sumple. Th. v. Lij. Rand. ED- Field Emplicate. EU v. Ecuspacent Blank., MSv. Matrix Spike Sumple. MRD- Matrix Spike Cupiticate Swepte. Go Crab. C. v. Composite. 3.), Field Filterati. For liquid matrices, indicate with a Y-for yea the sample was not Field Chemed.	Bouspean Black, MS+Mat leta filtered o+N - for sample	rix Spiže Sang e was not field	ie, MSD- Mar Dord	as Spēke Doph	icare Sample,	କ ଓଲ୍ଲ ବ	· Congan	S							For Lab Browning Com Only Custody Scal Teams?
a), Mariy Chies, DW-Dinking Water, DW-Goundhaller, SW-Safter, Water, W-Water, Water, ME-Water Lague, A. Exc. SE-Scatter, De-Scotter, De-Scotter, October, SY-State, Mariy Chies, SW-Dinking Water, DW-Goundhaller, SW-Safter, Water, ME-Water, SW-Safter, De-Scotter, De-Scott	W-Wade Water, W-Water, 1479 Aud nomber of contain openids, SA-Solforfe Apol.	Michael suga es provided in AAN Ascerbia	nesch (i.e. flas And, UX-He	resourcer, or Se 3, 60468/7 case SY = So	(Pills - X) Signa Thiosait	ACTURE ASSESSED	Servative :	is added a	outo, x-max. v-totas. Jukied - iczys field hispk	May 8		90,0			Cooler Forty
A STATE OF THE PARTY OF THE PAR			Tarana Carana	!											

Pape 8 98 3			C. 1 ( C.
#Entergy GW	**See www.geloom for GEU's Sample Acceptance SGP**	Kequest	920
COC Number <sup>(b)</sup> PO Number 50013510	GEL Work Order Number:		817) 178
	Phone #: (914) 736-8405	Sample Analysis Requested (Fill in the number of	(Fill in the number of containers for each test)
Project/Site Name: Indian Point Energy Center	ther Fax #: (914)734-6247	f⊭ be	<- Preservative Type (6)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	Buchanan, NY 10511	(GS)	· manual.
Collected by CB , MB	Send Results To: Patrick Donahue	H3) Spec	Note: extra sample s
Sample ID	caveptinum;	officerive  Oral number  ritium (  iomana (  trontium	required for sample specific
> * * * * * * * * * * * * * * * * * * *		7 3 4 1 4 (	3
14. (0)(41).237		+	A. J. (12.7)
MW-41-63-(013)	NO OF BOOK NOW	X	2 Liter Poly
TAT Requested: Normal: Y Rush S	^	No Circle Deliverable: C of A. /. (C Summary. / Level I	/ Level 2 / Havef 3 / Level 4
Remarks: Are there any known hazards appl	Remarks: Are there any known hazards applicable to these samples? If sa, please list the hazards		Simple Collection Line Zone Tracters Pacific Control Other
Сна	Chain of Custody Signatures	Sample Shipping and Delivery Details	ery Details
Resignationed By (Stangel) Trace Trace	ns ns 7	GEL PM ERINTRENT	
Old Bolon 1 4 John Market		Method of Shipment FEDEX Date Shipped:	
	70		
		Airbill #:	
<ol> <li>Chair of Cadady Number - Clear Determinant</li> <li>Chair of Cadady Number - Clear Determinant</li> <li>QC Codes: NNiormal Sample, TB Trip Blook, FD- Field Butticate, EB Egyptyment Stank. MS- Mastrix Spike Sample, MS-</li> <li>Egyld Edgrad: For Educationarizes, indicate with a Y - En-year the sample was field filtered as N - En-sample was not field filtered.</li> </ol>	<ol> <li>Clain of Casady Number - Clear Determined</li> <li>O'Codes, NNormal Sample, TBTrip Block, FD-Field Outsiden, EB Edubrance Stack. MS-Mostic Spike Surspe, MSD- blook Spike Duplicae Surspe, O-Grab, C Composite J.) Seeld Eduard: For Edukid matrices, indicate with a Y-Eu yea the sample was field Oldrech in N-Eu sample was not field Eduard.</li> </ol>	: Sacrophe, On Grade, Cir. Composite	For Lab Rosarving Vos Ciniy  Onytaly fred Ditact/
4) Matrix Codes DW-Chicking Water, GW-Gruendwater, 5W-Sat 5.) Sample Analysis Requested: Analysical method requested (i.e. 8 6.) Preservative Type: HA+ Hydrochlopic Anal, NI = Ninic Anal, NI WHI	4) Matrix Codes DW Chrisking Water GW Chanedwater, 5 West and water, we water, we water, we water, and was a constructed to be consisted to a first the construct of control of the construct of the construction	4 - 8). 11 Thiosolton, Tropessoronte is added a leave field tilmk PINK = CLIENT	COO2
37.35.3			

GEL Chain	of Custody ar	GEL Chain of Custody and Analytical Request	GEL Laboratories, LLC 2040 Savage Road	. C.
**See 9 GEL Work Order Number:	sww.gel.com for GEL's t	**See swww.gel.com for GEL's Sample Acceptance SOP** ##1:		
% spone	s: (914) 736-8405	Sample Analysis Requested (5)	quested <sup>(5)</sup> (Pill in the number of containers for each less)	ntainers for each test)
F4X #;	(914) 734-6247	e he ered:		< Bresnevelike Type (6)
450 Broadway, Suite 3, Buchanan, NY 10511		(GS)		. 7
Send Results To: Patrick Donahue	(3)	H3) Spec (		Note, extra sample is
*Usine Collected	o cei QCCodo Field Sample ry) a Hitored <sup>(1)</sup> Massic <sup>(2)</sup>	z S  Radioscire  CSCA Begulo  Fetal number  Fritium (  Gumma S  Strontium		required for sample specific QC
24412001	MO N N N N N	× × ×		2 Liter Poly
11 69 69 1253	N N CM	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		2 Liter Poly
Specify: (Kubject to Sandrage) FBN	Fan Results: Yes /	No Circle Deliverable, CollA	OC Summary /	Level 3 / Level 3 + Level 4
	ase list the hazards			lketon, Line, Zoos Pacific Other
Chain of Custody Signatures			Sample Shipping and Belivery Details	talls
Secondary (signed)	Date Time	GELPM: ERIN TRENT		
3 DAMES	1000	Method of Shipment:	EX Date Shipped	
3	***************************************	Airfell #:		
salpenent Blank. MS- Matric Spik	e Sample. MKB>> Nasik Spike Supil	usse Sample, Gr. Craft, Cr. Composite		For Lab Receiving 1860 (belo-
nd consection of A one Songer was no P-Wasse Water, W-Water, ML-Mi	ss Viguid, NO-Soil, SD-Sedenson, SI	P. Stodge, 88-Solid Waste, & Oli, P. Silter, P. Wipe, U	Orine, & Peral, & Nasai	SES NO.
d (i.e. \$1688, 60100770)Nood exercises it continues grav Acid, SIP-Sockure Hydroxode, SAP-Sulfaric Acid, AAP-A WHITE == LABORATORY	SOUTH = WOLFEA A WASHINGTON OF THE STANDARD SERVICE STANDARD STAND	Some This said See, if no preservative is saided a leave for PINK = CLIENT	td biank	T. MACHINE DE TOURS AND THE STATE OF THE STA
	TORY  TO ACCOUNT OF THE CONTROL OF T	Chain of Chatody Number - Client Determined  Could of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Client Determined  Of the Second of Chatody Number - Chatody	Airfull #:    Cause of Castedy Number - Closes Determined	Shire, Fowne, Deline, Seecal, See added a leave field blank  (ENT)

WHITE = LABORATORY

CET Chain of Custod		GEL Laboratories, EUC
(		2040 Savage Road Charleston, SC 20497
GEL Work Order Number:		Phane: (843) 556-8171
- 1		15 12 C
13	3468194	A SEED BY AND MILESON OF THE LUMBER BOX CONTROL ON THE SEED OF THE
Indian Point Energy Center Pax #: (914) 734-6	td ctrix ris be derest:	C.—Proservative 3 year (4)
450 Broadway, Suite 3, Buchanan, NY 10513	same considers	\$200 to 0.00 t
Send Results For Patrick Donahue	H3) Spec	Mote: extra sample is
***************************************	tive logali imbe- in ( ma !	required for sample specific
(Nellected OC Code (Nellecter) 15	Sengile Ladinect SCA Re Cotal ave Friction	8
<u>.</u>		T Fine Bah.
127 N N	GW Y N : 1 1 1	2 Liter Poly
pecify: (Subject to Surcharge) Fax Resuits: Yes	/ Crose Deliverable CofA /	QCSummary / Level 1 / Level 2 / Level 3 / Level 4
cable to these samples? If so, please hid the hazara	is a second	Sample Collection Time Zero
		B
Chain of Castody Signatures	Samu	Sample Shipping and Delivery Details
Received by (signed) Date Time	22	
STOPAGE	S (3) Method of Shipm	Date Shipped:
	Airbill #:	
	Airbill #:	77
streme F.R. v. Koschwood Stemb. ANN: March Series Supple. ANN: Nachz S	ooke Duroboore Sample, Griffeatt, Criffeatte	For Lab Breaking (for Chip
3.) Night Edward Fra Hipport manifest, indicate with a Y-fer yes the strople was field filtered by N-fer strople was not fired filtered. Shried.  Shrift Edward France Fra	edineni. MC-734dae XX-866d Waste, OrOT, Friedrich Friedrich, Cribina. I	~ 2
1608, 50 (1907-1479) June autobar of postations provided by each (i.e. A1668-1	3, 6010074704 - 3)	Cooler tener
Avid, SB: Sodrom Hydrovike, SA+ Saffijiic Acid. AA+ Asconitic Avid. BB+ Histore WHITE == LABORATORY YELLOW == F	FILE PINK = CLIEN?	
	CEL Work Order Number:    Phone # (914) 736-84     Phone # (914) 736-84	rem for GEL's Surgiste Acceptance SOP**  Total Marik (a)  Sample Alabytical Request  Sample Analysis Re  Total Marik (a)  Sample Analysis Re  Sample Deliverable of Contributers  Field Marik (a)  N. GW Y Redissoctive Sample Deliverable of Shipment:  Field Service Deliverable of Shipment:  Field Marik (a)  Sample Analysis Re  Sample Deliverable of Contributers  Field N. Tetal minder of contributers  Field Service Deliverable of Shipment:  FED  Nethold of Shipment:  FED  Nethod of Shi

CIC Number 50013510 GH	GEL Work Order Number:		Phone: (843) 556-8171 Pax: (843) 706-1178
15	Phone 4: (914) 736-8405	Sample Analysis Requested	Analysis Requested (*) (Fill in the number of containers for each test)
Project/Site Name. Indian Point Energy Center	r Fax #: (914) 734-6247	g this to he g this	< Preservative Type (b)
Address: 450 Broadway, Suite 3, Buchanan,	uchanao, NY 10511	(6S)	Siromun
Collected by CO, M.A. Ser	Send Results To: Patrick Conahue	(efrac 113) Spec (	Note: extra sampia is
S.	*Date Collegated Collegated DC Code Field Sa Collegated DC Code Field Sa Children 2 Edward Sa	Radinactics  1804 Reput  1804 Reput  Fold annube  Fritium: (  Gamma 5  Strontium	required for sample specific
MW-46-(019)	z z	Z -	2 Liter Poly
***************************************			
TAT Requested: Normal: Y Rush: Specify:	cify: (Salged to Surphage)   Elix Results   Yes	Orde Deliverable CofA / C	U. Summay : Lavel 1   Lavel 3   Lavel 4
marks: Are there any known hazards applicah	Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards		*****
Chain o	Chain of Custody Signatures	Sample ?	Sample Shipping and Delivery Details
Relangiasted By (Nigued)   Date Time	Received by takened) - Date: Those	GELPW: ERIN TRENT	
THEREOF STORE IN CO. ICS	150 150 150 150 150 150 150 150 150 150	)50 Method of Shipmont FEDEX	Date Shipped:
		Airbiil#:	
		Alabili #.	
<ol> <li>Chair of Castady Nourber - Clust Deterroled</li> <li>Killian of Castady Nourber - Clust Deterroled</li> <li>Kill Cales No Marred Sprate TB - Tan Street SD: Field Confeed FB - Exception State.</li> </ol>	are Alexandra (A. V. arta) (A. V. Arta) de la company de l	uphrate Naropic (2) (mat) (2) Coropystee	For Lab Receiving Use Guity
2) Field Fritered. Fire tripinal manusce, findings with a V. for set She stander was field filtered by V. for sample was not field filtered.	2   Field Fritated Face Stranger and state of the second was field district and the sample was not field district for the sample was not field dis	S. A.	of Newhood YES NO
Sample Analysis Regionard Analysis of nested topicstotic a 1898	S) Sumple Analysis Requested. Analysis of method topicostality of \$1000, 600 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100 (600) 100	9,7479.4 ( ) Section Theodolfae, Elicitorescreptive is adulted a loave field Stank	Course Somp.

WHITE = LABORATORY

3713 = MOT1333

**See www.gel.com for GEU's Sam	**See www.gel.com for CEU's Sample Acceptance SOP**	EL's Sample :	ple Acceptance SO	P**		Char	Charleston, SC 29407	107	
Minus Shading Klassic						eocie;	Phone: (\$43) 550-8171	1171	
CLEAN THUS A CAMED THERMOOF.						Fax	(843) 766-117	78	
Fhone #:			Samp		s Requested		e number of o	containers for each te	(252)
Fax #:	(914) 734-62	á thas				**********		ardeaff	Prespirative Type (6)
450 Broadway, Suite 3, Buchanan, NY 10511		Shapl	bisnes					£7	
Send Results For Patrick Domahue				*******				Note: ext	Note: extra sample is
"Fone Cultered Cittered	OC Code Fidd	•••••	жебы	*****		******	*********	required for	required for sample specific
*****	3) Pikered di		Total s	******		****	~~~~~		Š.
	Z Z	G₩ Y		jesen Jesen				2 1.56	2 Later Poly
	z	G₩ Y	, ,	;00000 ;00000 000000000000000000000000		***************************************	*****	2 b.ts	Liter Poly
									***************************************
	esults. Yes	/ (No	) Circk			QC Summary	/ Level   /	Level 1 ( Level ) /	/ Law[4
ta these samples? If xo, pleas	ic list the huzards						S CONTRACTOR S	Collection I inte Zone  Pactic  ther	112
Chain of Custudy Signatures					Sample	Shipping an	d Delivery E	)etails	
igned)				UN TRE					
ACAS STACK	ac illegion	1530	dethod of Shipr		XAGE	Date	Shipped:		
5.0			Carbill #						
			Virbill #:						
88 – Egedymeter Black, MS- Models Spike &	omple, 3850 Marris Spike	: l'Agdience Scomple,	Go Gaste, Cod Compos	1550			~~~	For Lob Receiving Use Only Custock Seel June 3	ing the Only
tor WWW Waste Water, We Wiger, Mc eMisc) HARCI 2700 word reamber of containers of taking	Ligad SO-Sell, SD-Sedin d Corpach (i.e. 82668-3, 88	en. StShalga, 88 909/24/04 - 1)	Solid Waste, O-O3.	Prof. Heer, Brown	ose Building, Pag	Fecal, Nobleat		Cooler Temp:	Pant.
m Nydawiik, SA+ Saffork Acid, AA+ Asaa LABORATORY	THE TANGET SA	F = Sodium Phiosed Æ	PINK = CI	ENTE.	re field black		,		C
gy Center  Send 5 Send 5 Send 6 Send	Photie # Pay #:  the 3, Buchanan, NY 19511  Send Results to Patrick Donahue  "har Collected Cilered Cilered International Collected Cilered International Collected Pay 1921  If the series of the series amples? If so, please applicable to these samples? If so, please applicable to these samples? If so, please Chain of Custudy Signatures  Chain of Custudy Signatures  Specify: Esubject to Suchange: Pay # applicable to these samples? If so, please applicable to these samples of constructions and the sample	Collected by: CB, MA C Sample III  Sample III  Sample III  Sample III  Sample III  **Par contend by: CB, MA C Sample III  **Par contend sont sont sont sont state of sont state of the sample III III III III III III III III III I	Collected by: C.B. AA   Secretary   Secr	Photie # (914) 734-8495   Sample	Collected by: C.B., AA S.   Sendle 3. Buchanne, NY 10511   Sample Analyse   Sendle 3. Buchanne, NY 10511   Sample Analyse   Sendle 3. Buchanne, NY 10511   Sendle 3. Sendle 3. Sendle 3. Buchanne, NY 10511   Sendle 3. S	Sample & Considered:    Sample & Considered:			Exc. (843) 766-1178  ed ** (Fill m the number of contain  The contain of the number of contain  OC Summary / Level / Level  Sample Collie  Eastern  Comrain  Mountain  the Shipping and Belivery Details  Estimpton and Belivery Details

GE Owder: 50013510	**See www.gel.com for GEL's Sample Acceptance SOP**  GEL Work Order Number:	ample Acceptance SOP**	Cherleston, SC 29407 Phone: (843) 556-8171 Fax: (843) 766-1178
	Phone #: (814) 736-8405	Sample Analysis Requested (5) (Fil	(Fill in the mamber of containers for each test)
Project/Site Name: Indian Point Energy Center	Fax # (914) 734-8247	le he ered;	<= ?reservative Jype (6)
Address 450 Broadway, Suite 3, Bud	3, Buchanan, NY 10511	(GS)	Camanage
Collected by CB MB Sen	Send Results To: Patrick Donahue	H3)	Note: extra sample is
Sample II)	*Three *Date Collected Collected QC Code Fixed Sample (Milliarry) # Sheet Agency	E disassive CA Regula tud number ritium ( annma S rontium	required for sample specific
For companies - subjected that they stay and they		ra Ta	
MW-44-102-(015)	1 05 09 1523 N N GW	× × ×	2 Liter Poly
MW-44-66-(014)	11/05/03/1627 N N GW	X X	2 Lifer Poly
V-0			
***			
TAT Requision Normal: Y Rush. Speci	Specify: (Subject as Sureburge) Fers Results. Yes /	(No ) Girde Deliverable Coll A. / GC Summary	mmary / Level 1 / Level 2 / Level 3 / Level 4
sarks: Are there any known hazards opplicab	please fixt the ha		Sample
			Central Other
С'най о	Chain of Custody Signatures	Sample Shipp	Sample Shipping and Delivery Details
auri sergi (pouditorka preumble)	state them	OEL PM ERIN TRENT	
	738 257 2466 308 09 738	Method of Shipment: FEDEX	Date Shipped:
		Airbill #:	
	S. J	Airbill #:	
2.1 Class of Caroly Caroler Clerk Drennings	) ) ( ) See at Consequence of the Constitute of	ate Sauroto, 🚰 Cristo, C. v. Communistic	For Lab Receiving like Only
<ol> <li>Stock Character for Regulations, includes with a X-fit year one complete was fixed filtered for X-fit sample was not fixed filtered.</li> </ol>	pie was field fibered or No. 50 comple was not field fibered.	Second Newtonia Works Oxfold Statistics Sections Sections Sections No.	72. TO
seere ( 1663 - 914 Extexing 1900), appropriate and second of the Saddist.	<ol> <li>Association (Associated Martin Association Composition) in the Property of Conference Section of Conference Composition (Associated Composition) in the Composition (Associated Composition) in the Composition (Associated Composition) in the Composition (Associated Compositi</li></ol>	(2)A-{}	Cooler Temp
regionalise Type: HAo Hydrochlucic Addd. NI - Nitos Add(, SB- Sodium Bydrocida, SA- Sub VPHOTOL HAO HAO HYDROCH TO THE STATE OF THE STA	o i Pressence Type. Has Bydrochinic Acid. XI - Nitro Acid. SB. Sodium Bydrocide, SA- Sodium Acid. AA- Ascebit Acid. UN- Mexico. ST - Sodium Thicacidiae, II no preservative is abide in Said State.	som Takasifate. If no poeservative is added — kase field blank.	

Without the residence of the second s						TO COMPANIES AND
Project 8: Entergy GW Mon Prog	GEL Chain	GEL Chain of Custody and Analytical Ro **See www.gel.com for GEU's Sample Acceptance SOP**	<b>ind Analytical</b> s Sample Acceptance SO	al Request	Charleson St. 794417	tories, EEC Road 37 79407
50013510	GEL Work Order Number:				Phone: (843) 556-8171 Fax: (843) 766-1178	) \$\$6-817) \$6-1178
	Plume #	+ (914) 736-8405	Sar	Sample Analysis Requested <sup>(6)</sup>		(Fill in the number of containers for each test)
Project/Site Name: Indian Point Energy Center	100 100 100 100 100 100 100 100 100 100	(914) 734-6247	e be			< Preservative Type (6)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	n, NY 10511		Should sample consider tainers			Campanie
Collected by: CB MB Send Resu	Send Results For Patrick Donahue	150	s of case	Spec (	**********	Note: extra sample is
Sample II) *For congravition - indicate state and stay state time.	*Fore Collected Collected Collected (Afficiary) (Mitton)	OC Code False	Kedrosetter ISCA Regul Total numbe	Trittem ( Gamma : Strontiur		required for sample specific
		z z	<i>z</i> ,			2 Liter Poly
	10					
***************************************						
TAT Requested Normal: Y Rush: Specify:	Specify: (Subject to Surphoge) Fax	Fax Rosults. Yes /		Circle Deliverable   C.	CoffA / (XC Summary / Lev	Level 1 / Level 2 / Lovel 3 / Lovel 4
snown hazards app	hese samples? If so, plea	ise list the hazards				
Chain of Custo	Chain of Custody Signatures				Sample Shipping and Delivery Details	very Desails
Seign and the test of the seign security of the second sec	Caggred)	Dair Thra	GEL PM	ERIN TRENT		
120 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			SCAMethod of Shipment	sipment FEDEX	X Date Shipped	ed:
			Airbill fo			
The state of the s	*Ju		Airbill #:			,
1 Chan of Canady Number of Case Department. ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Stank Durbscow Sample 435 Ords, Co Composite  2.) QC Codes: An Austral Sample, TB - Cop Black, ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Stank Durbscow Sample 435 Ords, Co Composite  2.) QC Codes: An Austral Sample, TB - Cop Black, ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Stank Durbscow Sample 435 Ords, Co Composite  2.) QC Codes: An Austral Sample, TB - Cop Black, ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Stank Durbscow Sample 435 Ords, Co Composite  2.) QC Codes: An Austral Sample, TB - Cop Black, ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Stank Durbscow Sample 435 Ords, Co Composite  2.) QC Codes: An Austral Sample, TB - Cop Black, ED: Field Emplicate, E8 × Epotporent Stank. 335 March Spilos Shorple, NSD: March Spilos Shorple,	igeigenem Dlank, SD-Marin Spier	Spope, 818D March Spike De	phease Sample -8% Circh, C ^ Co	ospowiec -		For Lab Receiving Use Only  Guandy Stat Institut?
4.1 Marth Cades DW-Drinking Warr. 6/Welcroundwater, SWeStettate Warr. Warr. Water, W. Water, M.). Misc Edgaid, SU-Sci. (SV-Scilage, SS-Scini) Water, D-131, Fe-Fatter, F-Wipe, Undergood Section of States of Computer of Academic Representation in the Computer of Computer of Academic Representation of Computer of Comput	We Waste Woster, We Waster, Mili÷Mila WiDAand outsifter of constitutes provis	c Riquid 1800-Spat, NAP Sederana Jaco Bertandi (Le. 1828-1864), 1849 (I	M. (Shaga, SSCalal Wasa, D. 3,54704 - EE	egii, kedanga kewajaa, to	Ustne, Perfects, Mediasol	Cooler Tetage
a) Property Ban Hydroddonic Acad M. Nibri Acid, SH Sodkan Hydroddo San Sufferic Acid, AAn Azondoc Acid, M. Mexane, NT a Sodkan Prisaeliste C vaperstrution.  **PIK ** CL **Property Ban Hydroddonic Acad M. Nibri Acid, SH Sodkan Hydroddon San Sufferic Acid, AAn Azondoc Acid, M. Mexane, NT a Sodkan Prisaeliste C vaperstrution.  **PIK ** CL **PI	graside San Sufferie Avid AAn Az ORATORY	Onthe Acid HV-Sector, STA  YELLOW = FILE	n XXXX annasian ji sejanenya senyeny	SUNK = CLIENT	t blank	
101 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1) 1 (1	V 357's 5 57'S 7	A SUMMAN OF THE SECOND				

<ol> <li>Choic of Crancity Number of Chem Determined</li> <li>QX Cooks (Not bearing Sunglet The Thin Black, ED+ Eneld Dephosics), Ends Filiaced. Entertails contract, Indiana with a Y or breyon the sample of Nation Chemical Parison, General Parison, Chemical Parison, Parison Chemical Parison, Chemical Parison,</li></ol>				Rejunguphan By (Sugard) Date Inne	Chain of	Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards	TAT Requested: Wormal: 💉 Rush: Specify:		MW-39-195-(007)	MW-39-183-(007)	MW-39-124-(007)	MW-39-102-(007)	MW-39-84-(007)	MW-39-67-(007)	Sample II) * For compositing - indicate sourt and step slatestimes	College (19. C.S. , M.B. Sen	Address: 450 Broadway, Suite 3, Buc	Project/Site Name: Indian Point Energy Center	Chem.Name: Entergy	(OC Number 50013510 GE	Page: Enlergy GW Mon Prog
1) Chain of Catholy Number — Chem Determined  2) (X. Codes 19 — Pectrual Sumple, 18 — Trip Black, ED—Card Deplease, EB — September Mark. MS—Marix Spike Beyond, MSD—Marix Spike Bephante Simple, G—Grab, C—Composite  2) (X. Codes 19 — Pectrual Sumple, 18 — Trip Black, ED—Card Deplease, EB — September Spike Sporte, MSD—Marix Spike Bephante Simple, G—Grab, C—Composite  2) (X. Codes 19 — Pectrual Sumple, 18 — Child Deplease, EB — September Composite No. Card Deplease, Spike Spike Bephante, Spike Spike Spike Bephante, Spike Bep	}	7	138 X 75 X E 100 0 1 17	<i>ي.</i> يو	Chain of Custady Signatures	te to these samples? If so, please list the hazards	fit: (Subject to Surchage) Fax Results: Yos /		NOW DE BOOK N OW	17/04/24 1257 N N GW	= 1040 1256 N N GW	SIN N CM	S C C C C C C C C C C C C C C C C C C C	S OS OS ISSIN N N OW	*Yane Collected Collected QC (note: Field Sample (Military) on Schemel Matrix (Military)	Send Reselts To: Patrick Donaitue	Buchanan, NY 10511	Fax #: (914) 734-6247	Phone #: (914) 736-8405	GEL Work Order Number:	GEL Chain of Custody and Analytical Re **See www.gel.com for GEL's Sample Acceptance SOP**
te Surgit, G. Grah, C. Composite Shrige, \$8-Sold Waste, O. Git, Peffice, PeWys, Deffice, FeFred, NeNassi The 31 PINK & CLIENT PINK & CLIENT	Athil #:	Airbill #:	38 Method of Shipment FEDEX Da	GELPM ERIN TRENT	Sample Shipping a		No Ciule Deliverable: C of A / QC Summary /		Z	Z	 			Z	Radioscire TSCA Regul Total combe Tritium ( Gamma Strontium	H3)	(GS)	le be ere <b>s</b> :	Sample Analysis Requested (5) (Fill in t	Pao Fax	Analytical Request ple Acceptance SOP**
For Lab Receiving Use Only  Custody Soul Intact?  YES  Cooler Very  C			Date Shipped:		Sample Shipping and Delivery Details	Sample Collection Time Zone (Eastern) Pacific Central Other Mountain	15		2 Liter Poly	2 Liter Poly	2 Liter Poly	2 Liter Poly	2 Liter Poly	2 Liter Poly	required for sample specific QC	Note: extra sample is	C Description of the Control of the	< Preservative Type (6)	(Fill in the number of containers for each test)	Phone: (843) 556-8171 Fax: (843) 766-1178	GEL Laboratories, LLC 2049 Savage Road Charleston, SC 29407

	- Capazanouson	3000	N.E.	PINK = CLIENT	(2) (2) (2) (3) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	Alexander de la companya de la compa	m Palou	TE Sodiu	YELLOW - FILE	ITAA Teev squess	kold. /s.k∼/	ATORY	Acid, SE-Sedion: Bydicalde, SE-Sull WHITE = LABORATORY	6.) Passer and Joja, H.Y. Hydrichtek Acid, N. e Nink Acid, She Sadon Rydmick, She Sulfane Acid, She Asorbia Acid, She Asorbia Acid, She Asorbia Acid, She Sadon Rydmick, I to posteristic it acides acide acide acide.  WHITE = LABORATORY  YELLOW = FILE  PINK = CLIENT	b.) Praservance Type. I
Conter Temp:	1710005	Controller, programmer t		12\$	30 X 00	Session &	7. P. S.	60108747	Son, SD-Sed it 83nox-3,	ase Eliquid, SO vidad for each t	oud sueurinu WarTPV von	ste Water, Wolf 21d number of 20	00 W300, <b>WW</b> -W	4) Magic Cour. 840-Decking Water, CW-Countinater, SWeStefact Water, WW-Waste Water, WeWater, ML-vides Edguid, 860-Son, SD-Sectional, McCountinater, WeSteface, SWeSteface, Water Counting For Counting F	1) Matrix Cours: 844-1 1) Matrix Cours: 844-1
Castody Seal Indust:	<b>Y</b>	No. Person Bellowell P		e serve	, Q		e Sanapia	ke Dapiical	II- Matria So	er Sample, MN ex Dold fältered	March, Seel	end Black, MSP	icum 88 – Bipapi zmple uns held fi	<ol> <li>Color S. S. Schmad Sample, 18 - Phy Black PD-Field Suplicate. 83 - Engigerant Black, MS-March Starple, MSD-March Spike Duplicate Sample, Go State, Co-Composite</li> <li>Sold States. For Equid matrices, indicate with a Y - Cor yes the attribe was field Bitmed by No. Constant and field Bitmed.</li> </ol>	<ul> <li>Color of Codes (No Sept.)</li> <li>Post Filterad (For I.)</li> </ul>
					****	Airbill #									
					35.	Aurbill #							12		
	Date Shipped	FEDEX		pmen	(of Sh	Method of Shipment		1630	- T				38	100 100 1000 1000 1000 1000 1000 1000	
			N TRENT	ERIN		GEL FM:			Nauc			Received by the		Date	Resignated by (Signed)
HS	Sample Shipping and Belivery Details	Sample Ship										Signatures	Chain of Custody Signatures	Ciri	
Pacific Other	Eastern) Control Mountain														
n I ime Zone					•	611111111111111111111111111111111111111		- 1	e hazard	ase list th	y so, ple	samples?	able to thesi	known hazards	emarks: Are th
vel 2 / Level 3 / Level 4	OC Summary / Level 1 / Lovel 2	C 4 A / (XC 8	Deliverable: 4	Circle Del	Ω Ω	<u> </u>	Z \		Χes	Fax Results:		Subject to Statch	Specify: (Subject to Statcharge)	< Rush:	TAT Requested: Noneal:
												***************************************			
		•••••			~~~~~	~~~~					******				
						ļ			******		<b></b>		1		
								***********							
					-						<b></b>				
		-							<b></b>					**************************************	
												energy and the contract of the		OCONOCIONADA ANALAS ANA	
												***		000000000000000000000000000000000000000	
2 Liter Poly			}A			Z	-4	GW	z	ري ح		Ç.		-(009)	MW-56-83-(009)
2 Liter Puly			>·· <b>^</b>	,		z		GW	z	£ z	ż	Ç Ç		-(807)	MW-56-53-(807)
CO			Strontin	Gamma	Tritium	TSCA Regu	Kudioactive	Sample Marrix <sup>sq</sup>	Filerod 14	my CC Code	*Time Chilemed (Military) (Shreen)	*Date Colleges (mm-dd-yy)	TOTAL PROPERTY OF THE PROPERTY	Sample {}} * for contente: - indicate sum and auja data) inte	destable of
Note: extra sample is	•				····	tased				ie	Donahu	o: Patrick	Send Results Te: Patrick Donahue	S S	Cullected by: 💍
Comments				(GS)	ntsiners	consid	Saort somp					lY 10511	luchanan, f	450 Broadway, Suite 3, Buchanan, NY 10511	Address
< Preservative Type (6)					nhaanahaan			247	(914) 734-6247		F3X #:		92	Indian Point Energy Center	Project/Sate Name
niters for each test)	(Bill in the number of containers for each test)	Analysis Requested (8) (8)	alysis R		Sample			Ġ	(914) 736-8405	3	Phone #:			Entergy	Chert Name:
	Phone: (843) 556-8171 Fax: (843) 766-1178										ber:	Order Nun	GEL Work Order Number:	50013510	COC Number 15
	2040 Savage Road Charleston, St. 29407	<del>(**</del>	Kequest		mee S	Anderst And	mpie	Y and EE's Sa	om for C	HAIN OF CHSTORY AND ARAPTECAL KI* ***See www.gel.com for GEL's Sample Acceptance SQP**	**See	GEL CHAIN OF CISCORY AND ANALYTICAL  **See www.gel.com for GEL's Sample Acceptance SO		Entergy GW Mon Prog	Project #: <u>Ente</u> l GEL Owek #:
LAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	GBL Laboratories, LLC	۴.				••	4				<b>F</b>		*********************************	e*	Page 3

inger is	GBL Chain of Custody and Analytical R  **See www.gel.com for GEL's Sample Acceptance SOP* GEL Work Order Number:	M.gel.es	istod Marter S	y and		Analytical Request	ica1	¥ 70	die	Š.			GEL Laboratories, LLC 2040 Savuge Road Churlestan, SC 29407 Phone: (843) 556-8173 Fax: (843) 766-1178	ooratori vaye &c an, SC 843) 55	es. 11. 29407 6-817	# 7 K
hent Name Enlergy	Р <sub>ино</sub> #:	(914) 7	(914) 736-8405	cn			Samp	the Am	atysis	Sample Analysis Requested (5)	Steal (5	FIII	in the n	unsber	of cor	(Fill in the number of contamers for each test)
roja.มีSire Name: Indian Point Energy Center	Fax#:	(914)	(914) 734-6247	247	le be	prex;				-						Preservative Type (6)
ddress 450 Broadway, Suite 3, Buci	Buchanan, NY 10511	OVV FOR CONTROL OF CON			Shaok sampi canshi	***********		(GS)	Sr90							
officeract by MARA CPA Sound	Send Results To: Patrick Donahue	***************************************				1	H3)	•••••	 1 90 (	******			********	******	********	Note: extra sample is
Sample ID	*Date Culturies Culturies Culturies	OC Code	F&8.0		Restina	A Reguly	tium (	oma S	ontim	***************************************				•••••	*********	required for sample specific QC
osaisasos dos pus paris ampares engranas especias	(marky) (K. f.pco.us)	3	Friberco	Marri, "			Tri		Sto			la stotata .			*****	
MW-63-112-(OH)		 Z	Z	GW	Υ.	Z.		}	····							2 Liter Poly
MW-63-121-(011)		Z	z	GW	~	Z.	,,,,									2 Liter Poly
MW-03-163-(011)		z	Z	GW	۲	Z 	****	<b>~~</b>	(and							2 Liter Poly
MW-63-174-(011)	11 05 05 05 3	Z	z	G₩	~<	Z 			,							2 Liter Poly
MW-63-18-(011)	11/02/01/12/19	z	Z	େ₩	<	Z 			ya							2 Liter Poly
MW-63-34-(011)	11 63 CM 1102	z	z	GW	Υ	 Z		·	,							2 Liter Poly
MW-63-50-(011)	11 S c 1 1 C 42	Z	Z	G₩	~	Z.		,		******						2 Liter Poly
MW-63-93-(012)	1160 CG 1055	z	Z	GW	~	Z.			~~	******						2 Liter Poly
	, i								***************************************							
1A3 Requested Normal: X Rush: Specify	Specify: (Subject to Strekwige) Fax Results:	Sugre:	Yes (		\{\bar{\bar{\bar{\bar{\bar{\bar{\ba		Circ	Circle Delia	detable:	citvenable: C of A	~	OC Summary	mary /	Level	, ,	Level ) / Level 2 / Level 3 / Level 4
known hazards app	e to these samples? If so, pleuse	list the	hazards											z o/∂\§		Santalis Collection line dans  [Sastan Fractic Central Other  Manualis
Chain of Reliagations discovering the Page 1997 Chain of Page 1997 Chain of	Chain of Castody Signatures  Received by (signed) Dan		Ease	***************************************	<u> </u>	GEL PM		ERN TRENT	Res		ngie S	hippin	Sample Shipping and Delivery Details	)eliver	y Det	dails
	24 SECURE STOPACE	1	11/3/200	1424	<u> </u>	Method of Shipment	if Ship	ment.	E	FEDEX			Date Shipped:	baddi		
					>>	Airbill #										
	<u></u>				 خخ	Airbill #:										un ou une de la composition della composition de
Ones of Crassey Namber Clear Determined GC Codes: N. Sarrond Sample, VM of tip Mank, ED- itself Digitizate, EB of Equipment Blank, MS, Marth, Spike Sample, MS, Cold Flatered: For Highth matrices, adduted with a V-for yearing compile was field filtered on N-for sample was not field illusted.	EB - Equipment Blank, MS, Marth, Spiter Sarspia, MMD: Marine Spike Displante Sample, Ge-Grab, Cir-Composite t was field district on Ni-Corsample was and dead illusted	ngaig MSD	Materic Spek	ж Эпрасах	Sangle, D		Conge				; ;		Į.			For Lab Receiving Use Only  Custody Seal Indact!  VPC
Sample Arshyin Regarded Andydood method represent it e 1860. 60160070706and member of constincts poweded for such it e. 18600. 5. 60160070704 - 13  Crossvatile Type BAS Bydrochiene Acad, N. Samoe Acad. SB. Sadam (Acad. SAS Satiscia Acid. AAS Acade) Acid. ANS Beame, ST. Saddam (Biosadiate, If no preservative a added "Saw field blood Crossvative Type BAS Bydrochiene Acad, N. Samoe Acid. SB. Sadam (Biosadiate, If no preservative a added "Saw field blood Crossvative Type BAS Bydrochiene Acad, N. Samoe Acid. SB. Sadam (Biosadiate, If no preservative a added "Saw field blood Crossvative Type BAS Bydrochiene Acad, N. Samoe Acid. SB. Sadam (Biosadiate, If no preservative a added "Saw field blood Crossvative Type Bas Bydrochiene Acad. Samoe Acid. SB. Sadam (Biosadiate, If no preservative a added "Saw field blood Crossvative Type Bas Bydrochiene Type Bas Bydrochiene Type Bas Bydrochiene Type Bydrochiene	in 1980/1976 Sand monther of populations poweded um Eydroxide, S.A.º Santucia Acid. A.A.º Ascort	Torruch it s pic Acid, BX	. 8.3600 5. o	.e108/7179. 3 - Sodium	( - 3) Thiosalia	A King	essevati Terrores	N 63 45 5 N 63 45 5 N 63 45 5	vest in to	idded ~ have field blonk	2.					Cooler Comp:
" A. Sten	AGCEVECTOR F " ALITINA	A 1 3 4 1 4	$X \times X = A \times Y \times X = X \times X \times X = X \times X \times X = X \times X \times X$	*		~	TOTAL NAME	S. S.	;							

THE REAL PROPERTY OF THE PROPE		***************************************		Print Laboration 117	
Project * Entergy GW Man Prog	GEL Chain o	GEL Chain of Custody and Analytical Ri  **See www.gel.com for CEU's Sample Acceptance SOF**	Analytical Request ple Acceptance SOP**	264) Savage Road Charlesion, SC 29467	
COC Number 97.	GEL Work Order Number:			Phone: (843) 556-8171 Pax: (843) 766-1178	
E	9hone #:	(914) 736-8405	Sample Analysis Requested ®	(3)	each test)
Project Site Name: Indian Point Energy Center	€r Fax#.	(914) 734-6247	to be	^	< Preservative Type (b)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	Suchanan, NY 10511		(GS)		Comments
Collected by:	Send Results Fo. Patrick Donahue		refem 143) Spec	. <u>X</u>	Note: extra sample is
Sample (I)	*Date Collected Collected Collected (Milkory)	QC Code Filested to Massic to	disection SCA Regulated must stat must iritium ( iamma )	icinii	required for sample specific
additional fire tast unit auchous - crossologia val.			1		
MW-111-(030)	11 2 10 C 15 K	N N GW	X		2 Liter Poly
					***************************************
PROPORTION CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPORTY OF THE PROPERTY OF THE P					
20000000000000000000000000000000000000					
**************************************					
(A) Requested Normal: Y Rush: Sp	Specify: (Subject to Surchage) Fax Results:	ř.	No Circle Deliverable Cof A	/ OC Summary / Level 3 / Level 2 / Level 3	evel 3 / Level 4
known hazurds app	cable to these samples? If so, please	list the hazards		Sample Collection, Lime Zone  Eastern Pacific	me.Zone
				Mountain	
	Chain of Custody Signatures		H. E. C.	Sample Shipping and Delivery Details	
Relixabished By (Suprod) Date Tune	Reneived by (signed) Date	ax Tiene	GELPM: ERIN TRENT		
	3995 SECULE STORES (500)		Method of Shipment: FEDEX	Date Shipped:	
	2				
			Airbill #:		
1) Chan of Control Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Doplical Sample, CV Cottoride  2) OC Codos: No Normal Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Doplical Sample, CV Cottoride  2) OC Codos: No Normal Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Doplical Sample, CV Cottoride  2) OC Codos: No Normal Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Doplical Sample, CV Cottoride  3) OC Codos: No Normal Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Doplical Sample, CV Cottoride  3) OC Codos: No Normal Sample, 18 w Yelp Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Sample, MSD: Marti Spike Black, FD: Field Supicate, EB w Eqdpress Black, MS: MSD: Marti Spike Black, FD: Field Supicate, EB w Eqdpress Black, MS: Marti Spike Black, MSD: Marti Spike Black, FD: Field Supicate, EB w Eqdpress Black, MS: MSD: Marti Spike Black, M	vicate. EB = Egolpment Blank, MS-Mariti Spike St	mple, MSD- Mairix Spike Deplicate S	Bangke, & Crob, C' v Composite	Por Lab	Par Lab Receiving Use Only  Owneds Seed Intant?
<ol> <li>First Editors: The Expectionated Many, Indicate with a 1 - Fix yest are supplied was trite and the Property of the Many of the Expect Many, Indicate with a 1 - Fix yest are supplied was trite and the Many of t</li></ol>	ton topics materies, tradicale with a 1 - the year are sample was retreated and the strength was not from convenient. See "DW-Theorems Water, Water, Worden, Mew Mater, Mil to Mater Liquid, SD-	iquid, SD-Sedt, SD-Sediment, SL-Ski	adge. SA SCAA Wasse. O-CH, Foliuter, Politics, Voltéae, Politics, Novasi		ES SO
Majors Code DWE Processing Water Commissional Commissional Commission of containing provided for each (Co. 8,000). A 50/08-74-704 - (L. 5.) Springly Analysis Requisited — Analysis rathest agreement of the Commissional Com	608. 60108/1479/send number of containers provide	For each (i.e. 82608-1, 50708,74704	. E). This was the Mark movement with the standard of leave fitting them?		Cooler Temp:
6) Preservative Pyte HA: Hydrochlurie Acid, N) - Mitte Avid, SH: Sockion Hydrichiec SA: Stelluri Acid, AX: Aspecie Kool, BX: Howard, N: A Social Coloradad, ax: is preservative to the coloradad, ax: is preservative to the coloradad, ax: is preservative to the coloradad, ax: is preserved to the color of the coloradad, ax: is preserved to the coloradad to the	Acid, SB+ Acidium Hydrichide, SA+ Subfuric Acid, BAY Asido WHITE == LABORATORY	AETTOM = LTTE  AETTOM = LTTE  Pre year House of the second	PINK ~ CLIENT	,	

age: 1 of 3 mject ≠: Entergy GW Mon Prog iii. Quete ≠:	GEL (	GEL Chain of Custody and Analytical Re **See www.gel.com for GEL's Sample Acceptance SOP**	f Cu	istod m for C	y an	d A	nal)	/tic:	್ಫ್ರ್ <b>=</b>	*eq	equest			<u> </u>	GBL Laboratories, U.C 2040 Savage Road Charleston, SC 29407	aborat svage ton 5	ories, Read C 294	S E	
50013510	GEL Work Order Numbers	berr												~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	Phone: (843) 556-8171 Fax: (843) 766-1178	(\$43) 43) 76	556-4	2 2	
55		Phone #:	(914)	(914) 736-8405	36			Sai	Sample A	naly	Analysis Requested (S)	arsaul		Fill H	the	gum	ध	2000	(Fill in the number of containers for each test)
ന്വാഗങ്ങൾ Name Indian Point Energy Center		Fax#	(914	(914) 734-6247	247														< Preservative Type (b)
ddress: 450 Broadway, Suite 3, Buchanan, NY 10511	lanan, NY 10511	***************************************				dimenti Stronti	Konsida	toiners	(0.0)			(3)							7
bifected by: Send	Send Results To: Patrick Donahue	Donahue					red	**********				(Ni6			******				Note: extra sample is
Sample ID	*Date Collected (seco-dri-yy)	(Addinty)	100 Code	ic paratis	Sample Marrix "e	adbonetisse	SCA Regula	eial number	fritium (	Jaanna S	Strontian	Vickel 63			***************************************	************			required for sample specific QC
The state of the s	TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	( neconnectivity			1	2	T	-			4	4	- -	_	-	_			
WW.27.07.24.403.23		1223	2	2	CV	~	2	-	-			ļ	ļ	ļ	_	_			2 1.307 Pay
MW-55-35-(011)		15 15 15	Z	z	WB	~~ <del>;</del>	Z		hank	huah	~~~	~~			*****				2 Liter Poly
MW-55-54-(012)	*	1733	z	Z	GW.	~<	Z	,	h-ab	****	,	~~			******				2 Liter Poly
**************************************																			
														•••••					
								_				-							
TAT kequested Normal: Y Rush: Specify.	Specify. (Subject to Surcharge)	rge) Fax Results	in its	Yes	`		4		Circle Deliverable: C of A	elivera		S. A	ĝ.	OC Summary /	NO.		~ [	9	Level / Level 2 / Level 3 / Level 4
enown hazurds app	to these samples? }	f so, please	list the	be hazard	ક્ર		Services										Committe Co		an Time Zone south: when
Chain of 6	Chain of Custody Signatures						-	***************************************				Sample Shipping and Delivery Details	le Sh	pping	and	Deli	CL3	ery Defa	ails
Relinquished By (Signed)   Date Taise	Received by (signed)	med) Onto		3000			GEL PM:	*	ERIN	N. L.	ERIN TRENT	***************************************							
	805 Seals 37206	579236			<u> </u>	X	Method of Shipment	å of %	ipme	at:	FEDEX	×		[	Date Shipped	aippe	డ		
	2						Airbill #	*											MANAGAMANAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
							Airbill #	184: 1								ı			
) Chaire of Chorele Standon - Chorel Debrimina. ) OC Code: N. Normal Standon - Chorel Debrimina.  Fig. Field Displace, EB - Explanated Blank, W. W. Marris, Spike Sangle, MSD - Mordy, Spike Displace Sangle, Co-Code, Co-Code, Co-Composite	88 - Equipment Black, 383-	Mars Spike San	opte. MSO	~ Marix So	yihe Dupkic	ate Sangelo	R (20 C)	% & ~ (°	niposite										For Eath Receiving Use Chip  Controls Sent Interc
March Codes DV-Driving Water, GW-Corondwater, SW-Sarbase Wests, WW-Water Wests, W-Water, MC-Miss Limited, SD-Soul, SD-Scalinger, SE-Studger, SE-Studger, SC-Oil, F-Filter, P-Wipe, U-China, E-Frenk, W-Nasc	io, WW-Ware Ward, W-86	Act. Mil. "Mise Lie	996, SO-S	oit, SD-Sa	duncest, Sa.	Studyo S	A Pijos-el	vale, O	(A) \$-6	iller p	Wige, 6	Chine,	f-feat	* 22	Ÿ.			T	YES NO
Supple Analysis Requested. Analysis include analysis represent to a superior of the superior o	an Elphodde, SA: Salfanc A	rainas provietos vid. A.A Ascorb	ic Asid, Ho	Ko Resona.	. 58 - Sod	sen ( bios	R s≴t'ombyn	rassad o		added =	iesve ik	ld black							Announce of the state of the st
= 3LHA	WHITE - LABORATORY		13.7	etie = motes	E ST			MNK - CLIENT	C	Z									

[286]						- 5			- Character Constant	Po 1 test.	N 72 PLATE AND	F 1 1	
* Entergy GW	GEL Chain of Custody and Analytical  **See www.gel.com for GEL's Sample Acceptance SC	hain of Custody and Analytical Re*See www.gel.com for GEL's Sample Acceptance SOP**	dy and	Analy	tical	200	Request	<b>*</b>		2040 Savage Road Charleston SC 29407	vage 80	29407	
PO Number: 50013516	GEL Work Order Number:									Phone: (843) 556-8171 Pax. (843) 766-1178	843) S 3) 7(6-	1178 1178	
Cless Name: Entergy	Phone #:	(914) 736-8405	105		Sample	de Ana	lysis R	Analysis Requested (*)		n the m	umber	of con	(Fill in the number of containers for each test)
Project/Site Name: Indian Point Energy Center	f Fax *	(914) 734-6247	6247	le Se	•••••			*******	~~~~~			********	c Preservative Type (6)
Address 450 Broadway, Suite 3, Buchanan, NY 10511	uchanan, NY 10511	在	H H H H H H H H H H H H H H H H H H H	Skoul samp consid	tainers	(GS)	Sr90						3) American fo
Collected by: Micon C Dailes Se	Send Results To: Patrick Donahue			tred		Spec (	a 90 (		**********		*****	***,* ** * *,* * *,*	Note: extra sample is
ಜ್ಞ ಚಿ	*Date Collected Collected Collected (Millery) (busin-de-jy) (Millery)	QC Code Steld	Sample Matrix '*	Esdioactive	rout sumbe Tritium (	Gamma S	Strontiun	••••••			*******	**************************************	required for sample specific
MW-60-135-(011)	0 8 0 0 0 0 0 0	z	GW.	z z	4 (4	~~	>4						2 Liter Poly
MW-60-154-(011)		Z Z	Ω ¥	≺ Z	, 	ind	prot	~~~~	******		******		2 Liter Poly
MW-60-176-(011)		z Z	GW.	z	****		****						2 Liter Poly
MW-60-35-(011)		Z Z	GW	Z Z	h	lood	pa		******				2 Liter Poly
MW-60-53-(011)	1419 Solos	z	GW.	Z Z	pro 	ind			******				2 Liter Poly
MW-60-72-(011)	~**	z z	GW	Z Z	; ;e	·~-	, mi						2 Liter Poly
***************************************													
TAT Requested: Normal: V Rush: Spec	Specify: (Subject to Swedunge) Fax Results:	sahs: Yes	· Δ	ð	Circle		Dehverable: ₹ of A	٠.,	QC Summary	Mary /	Level	. 1 .	Level 4
пожн hazards app	tble to these samples? If so, please	fixt the hazar									< 0/Ω\€	ample Col Eastern Central	. IS
Chain	Chain of Custody Signatures							Sample	Sample Shipping and Delivery Details	g and I	3elive	y Deta	tails
Responsibled By (Signed) Fram: Time	Received by (signer) Onto			GEL PM:	M: ER		IN TRENT						
1 50 08 10 A A A A A A A A A A A A A A A A A A		3000	620	1	Method of Shipm	ment:	33.5	XEDEX		Date Shipped	ipped		
	tu.			Airbill #:	3±								
***				Airbill #:	**								
15 Chair al Custady Norther - Chian Lebecolined  2.1 OC Custar No Northal Sample, 18 - Chip Bugak, ED: Fool Duplicate, EB o Equipment Stark, MS Magna Spike Sample, MSD Magnix Spike Cupitware Sample, Do Grob, Co Composite	are, 88 – Equipment Stark, MS-Marry Spike San	apie. MSD- Menia i	ριδες Ουρόσοιε έ	ample, 6~ Grø	, C∞ Coκρ	asies						1	For Lob Reveiving Use Only
2) Marrix Codes DWDrinking Water, GW-Groundwater, SW-Surfaxe Water, WW-Water Water, W-Water, Mi-Miss Liquid, 30-508, SP-Siddonom, M-Sludge, SP-Siddo Water, GW-Dill, 2) Marrix Codes DWDrinking Water, GW-Groundwater, SW-Surfaxe Water, WW-Water Water, W-Water, Mi-Miss Liquid, 30-508, SP-Siddonom, M-Sludge, SP-Siddo Water, GW-Dill, 2)	Water, WW-Waste Water, W-Water, MiMsz. Lis	und. 80-Soil, 80-S	edenen, <b>Sl</b> ~Slu 3. <i>K</i> 01.08/72/02	dge, 88-Salud N	ase, Oros		Briffich.	ferfilter, PrWipe, U-Chine, Frifetal, N-Nasal	Social, A-No	8			Cooler Fimp
o.) Preservative Type BA: Bydoxolitova Acid. M.: Ninje Acid. SH: Sodana Hydracide, SA: Sufferio Acid. AA: Ascurbin Acid. BX: Meane, ST: Sodian Thomastae, If on prezervative is added is have field blank  WHITE: T.ABORATORY  VELLOW: FILE  PINK: CLIENT	Sodium Hudrovith, SA: Sufferts Acid, A6:: Ascurb	YELLOW = FILE	«ST – Sudium	d. Bernanger	PINK = CLIENT	LIEN.	i ~ kerve i F	heid blank					0
HINW	WHITE - LABORATORY	AETFOM = 1	2	~~	N. C	1.33.7	,						

OEL (wate #: COC Number **) PO Number: 50013510 CEL \	**S GEL Work Order Number:	**See www.gel.com for GEL's Sample Acceptance St	.gel.com	for GE	U's Sam	ple Acc	epiano	<u>آب</u> ا	**				Charlesson, 3C 29407 Phone: (843) 555-8171 Fax: (843) 766-1178	Charlesson, 34, 29- Phone: (843) 555-5 Fax: (843) 766-11	2940 18-45	71	
Client Name: Entergy		Phone #: {	(914) 736-8405	6-8405			<b>36</b>	Sample :	ple Analysis Requested (5)	s Regu	ested :		in the	न्यास	rofo	ntain	(Fill in the number of containers for each test)
ProjecuSite Name Indian Point Energy Center		Fax#:	(914) 7	(914) 734-6247	7	la be											6 Preservative Type (6)
Address: 450 Broadway, Suite 3, Bucha	Buchanan, NY 10511					Should kampl conside	triners										8" oznamova te
Collected by: Sand 8	Send Results To: Patrick Donahue	nahue				sted	rafeຍກ		·		******	~~~~~			*******	*******	Note: extra sample is
	persello) atsta-						smber				*****				*****		required for sample appealso
Sample III  * For composites - milieure num und non dutenime	(yyantadd-yyy)	(Totalected (Totalected (Middenty)	QC Code	Filtrand <sup>(b)</sup> b	Mania w	Badiose YSCA B	Latel ac	Tritin	Gamr Stron	Suon Nicke	*****		*******	*****	**********		×
MW-49-26-(018)	10/24/29	7.2	z	Z	GW	ベ Z		,i	F	}****							2 Liter Poly
MW-49-42-(018)	10/29/04	\$	z	z	GW	× z			e	p							2 Liter Poly
MW-49-65-(018)	5 2 2	7. V.	2	z	GW	X X	~~		re-1	,						ļ	2 Liter Poly
															ļ		
		.,															
TAT Requested: Normal: Y Rush: Specify:	(Subject to Surchage) Fax Results.	) Fax Rose	ufes.	Yes				Circle Deliverable: C of A / OC Summary /	eliveral:	ile: Cod	A /	X Sun	mary	183	3 5	Level	Level 2 / Love(3 / (ave) 6
Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards	o these samples? If:	o, please l	list the h	azards											Sentral Co.		Na <u>male (</u> Collection Jone 2-on Castern Pocific Control Other
	Chain of Custody Signatures									*	Sample Shipping and Delivery Details	ddigs	अंध विष	Della	ery D	erails	~
Relinquished By (Signod) Date Tene	Reveised by (signed)	d) Use	Tiene.	370		E	GEL PM	ERI	RIN TRENT	LNE			7				***************************************
	3 S22500	DESTRUCTION OF THE PROPERTY OF		chedoa	1572		Method of Shi	Shipment:		FEDEX	X		Data Shipped:	hippe	٠٠٠		
ing from wholes 152	12					Air	Airbill #:										
) 10/16/04 15						Á	Airbill #										
) 10/16/100, 15															***	٠.	For Lab Reserving Over Oak
Clien Determined applicate the Sample, TB · Fry Hank Y · Cor yes the sample	as beld likerad op N - for som	ntiv Sprike Sian	ple MSD- N	Aarrix Spöre	Duplowe i	Sample, Gr	Seat Co	Composite	2000 Sec. 2000	856 153	Ĩ	2 7					Capady Sed Invest

Project #: Entergy GW Mon Prog	GELC	Chain of Custody and Analytical R **See www.gelcom for GEU's Sample Acceptance SOP**	T Cu	istod	y an	d Ar	<b>12] y</b> 1	ical	min .	Request			ন <del>ডু ত</del>	GEL Laboratories, LLC 2040 Savage Road Charleston, SC 29407	on SC Age R		, j	
OX: Number (1):   GF   GF   GF   GF   GF   GF   GF   G	GEL Work Order Number:	er:											T 19	Phone: (843) 556-8171 Fax: (843) 766-1178	843) S 34 766	1178 1178 1178		
11		Phone #:	(914) ]	(914) 736-8405	Ğ	******		Sample		Analysis Requested (S)	equesi		(Fill tr	the m	Suppo	of co	taine	(Fill in the number of containers for each test)
Project/Stie Name. Indian Point Energy Center		.≉ xe₃	(914	(914) 734-6247	247		ered;											< Preservative Type (6)
Address: 450 Broadway, Suite 3, Buchanan, NY 10513	chanan, NY 10513					Skonl Sacop	consid	······	G8)	Sr90								
Collected by:	Send Results To-Patrick Donahue	onahue							pec (	190 (				******				Comments Note: extra sample is
Sample ID *For composites - indicate account stop directime	*Exec Collected (2014): dd-yy)	Nine Codested (Milliary)	01 02 Code	Sidered 108	Sample Matrix 191	Radioactive	TSCA Regula	Tritiani (i	Gamma S	Strontium		·····		*************	***********	***************************************		required for sample specific QC
MW-37-22-(016)	50 Sty	S	Z	z	C#	×	Z								•••••			2 Liter Poly
MW-37-32-(016)		Ē	*****	Z.	GW.	≺,	Z	,d	••••									2 Liter Poly
MW-37-40-(016)		348	Z	Z	GW	~<	z		<b></b>									2 Liter Poly
MW-37-57-(016)	•	1200	Z	Z	G₩	~	Z	<b>,</b>	4									2 Liter Poly
VAT Requested: Normal: Y Rush: Specify:	(γ) (Suβject to Serokarge)	po Fax Results	artrs	¥4\$	-			Circle E	c Delive	beliverable ColtA / QC Summary / Level ) /	O M. A	8	Summ	857	1.evel		Level 2	2 / Level 3 / Level a
known hazards apj	de to these samples? If	so, please	list the	huzards	•				***************************************						~ 0/m\s.		i offices	n Juma Zona wific wher
	Chain of Custody Signatures										Sam	de Sh	Sample Shipping and Delivery Details	and I	elive	r. De	aits	
Relinquished By (Signed) Uses Time	Received by (signed)	ed) (see		.X00; 3,			We TO	ERI	în T	NTRENT								
TO BOX - PORSION	700 SEVE	STORAGE		NS 2/0	<u> </u>	Š,	Method of Shipment	of Ship	ment	33	FEDEX			Date Shipped:	podd			
7 3	[23						Airbill#											
) Chan of Custody Murden's Client Determined	100			*****			Alitein #										37	For Lah Receiving Use Only
3 (X. Clodes, N. Normal Marties, 196 - Frey Hast, 199 - Fred Deplotant, Et Septembert Hatte, New Popies, Space Supper, 19822 - Super Supper, Super Supper, 19822 - Super, 1	e, f.B. o separatem static, Moo me the was field silvered on N - for some	des and the season and	gote, on son distanced	San Color	es Supplies	s value		i Anna		E.W.	Ī.	2	Z	÷				Custody Soul Interce
Mates Codes Diverbishing Wass. Checkensel was the System was wear, we waste not proved the second meters of the Control of the System of the	Water, We Was was a water. We Walke, 60 10 RE-13 70 Manual mumber of contra	eners provided	(1) (C.C. 40)	(1), 300 (1) (1), 8260 (B. 3)	CECHBEDS CECHBEDS	13 - File	ST TENT	ie o o o o				^		4		·····		Cooler Tonp
). Progressive Type, II Av Hedrochieric Aud. Ni v. Niere Arid. SH. Sudana Hydexide, SA - Salinix And. AA - Assansia And. III N. Sevana, Sa - Sasania i inspectation in assansiance in a superior in a superior in assansiance in assansiance in assansiance in a superior in assansiance in assansi	xbaro Hydroxide, SA+ Selfaric Acc	of AA+ Ascorb	K Appl. 180	Autol. 15X - Nevade, 53 -	24 - 5000	100 CONST.	300 :: 300	to Jacobs Kathan Sanda .	C 10 00000	20000	1000 0000	,				ſ		

				AND THE RESIDENCE OF THE PROPERTY OF THE PROPE
Project * Entergy GW Mon Prog	GEL Chain of	GEL Chain of Custody and Analytical R.  **See www.gel.com for GEUs Sample Acceptance SOP**	\nalytical Request s Acceptance SOP**	GFL Laboratories, LLC 2040 Savage Road Physicator &C 7940?
50013510	GEL Work Order Number:			Phone: (843) 55(-817)
	Phone #. (	(914) 736-8405	Sample Analysis Requested <sup>(8)</sup>	#43)
Project/Site Name: Indian Point Energy Center	er Fax #:	(914) 734-6247	le ire	< Preservative Type (6)
Address: 450 Broadway, Suite 3, Buchanan, NY 10511	uchanan, NY 10511	Shoaf	consideration (GS)	
Collected by:	Send Results To: Patrick Donahue	**************************************	HII)	Note: extra sample is
Sample ID  * For contrastive state and state determine		OC Code Field Sample  ** Filtered *** Matrix ***  tadioactive	Fisca Regoli Fritium ( Gamma S	required for sample specific
MW-36-24-(016)	10/24/31 PLE	N N CW Y		2 Liter Poly
MW-36-41-(010)	5	N N OW A	7.	2 Liter Poly
MW-36-52-(015)	1539	N N OW A	Z.	2 Liter Poly
TAT Requested: Normal: Y Rush: Spe	Specify (Subject to Sunchange) Fax Results	ilts: Yes / Cilo	Ciscle Deliverable: Cof A	/ QC Summary /
known hazards app	able to these samples? If so, please l	ist the hazards		Sample Collection Time 2-ms (Sastern Pacific Central Other Mountain
Chain			S	Sample Shipping and Delivery Details
Reliaquished by (Signed) Date Time	Received by assueds — Date	Since	GEL PM BRIN TRENT	
	TOD ISSUARS STORES	Colomba Toc	Mediad of Shipment: FEDEX	X Date Shipped:
	2 4		Airbil *.	
	*200		Airbill #:	
1) Chain of Conady Number - Cited Decrisions 2) QC Codes No Normal Sample, 18 - Top Blank, FB- Field Dapilicate, EB - Squimmen Blank, MS- Marrix Spike Bample, MSD- Mema Spike Dapilicat-Sample, G- Code, C- Conavelet- 2) QC Codes No Normal Sample, 18 - Top Blank, FB- Field Dapilicate, EB - Squimmen Blank, MS- Marrix Spike Bample, MSD- Mema Spike Dapilicate Samule, G- Code, C- Conavelet- 2) QC Codes No Normal Sample, 18 - Top Blank, FB- Field Dapilicate, EB - Squimmen Blank, MS- Marrix Spike Bample, MSD- Mema Spike Dapilicate Samule, G- Code, C- Conavelet- 2) POC Codes No Normal Sample, 18 - Top Blank, FB- Field Dapilicate, EB - Squimmen Blank, MS- Marrix Spike Bample, MSD- Mema Spike Dapilicate Samule, G- Code, C- C	uate, KB ~ Squipment Black, MS> Matrix Spike Burn	ele MSB- Maera Spike Daplicas: Sam	ole. Or Godi. Cr Composite	Enr Lah Receiving Use Only  Checody Stat January
3.) Field Febrer: For injust state-oct, metade in 1822 for surprise was new interview of the control few to the first See Selforent. St. Scholage. See Solid Waste. De Od. 4.) March Creas: DW Dritting Waste, GWelloundwater, SWeSolid Waste. De Od.	erijke 408 seem meers, ee is "na samme was ee naar de Wister, WWAWASSE Water, We Water, Miljowies, Lidg	nd, SO-Soll, SO-Sollment, SL-Sludge		Prédie Prwys, Dilline, Stiech Nebrod YES NO
5) Simple Analysis Requested Analysis of the desire between types and analysis of a second of the se	es netre a repair concer a common por men a Sadum Hydroxide, SAN Schlert Acid, AAN Ascadio A A MAN A TENNES A TENNES A	Acid Six Heaven Six Salism this	esulfair, % no preservató e is added ~ teave field	
WHITE	WHITE - LAHORATORY	YELLOW - FILE		

4) Mater Claise DW Breiding Mater, GW (countrieder SW Sindage Water, WW Water Mill May Lagua Me 2001 30 Sections, 38 Sample Section of Countries C	1. Local Science Science and describes institute with a Notice of States of States and States an	1 Fact of Code by Norther - Chest Detectioned		۵	: 	Reduce that the Property of States Same	o men )		Patriarks: Are there and known becards madicable to these samples? If so, please list the hazards	4 11 11	20 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -		N 1000 CT 1000 CO		19 11 to the second and company and company to the second and the	AND THE REAL PROPERTY OF THE P	MW-42-78-(014)	MW-+2-49-{019}	Sample ID	Collected by Son	Addres: 450 Broadway, Suite 3, Buo	Pojast Sala Name: Indian Point Energy Center	Chust Nansa. Entergy	(Of Norther 12 20013510 GE	Probate: Entergy GW Mon Prog
Water, WW-Waste Water, W-Water WATER TO CONTROL OF STREET	<ul> <li>S.B. Compagned States. MSC Matter, Note: Buildings matter was a construction of an array of the control of the co</li></ul>			2.7		Novel Neurolet By Laigner)	Chain of Custody Signatures		le to these sumples! H'so	***************************************							1012709	10/27/69	*Oose ( related (mm-dn-ys)	Send Results To: Patrick Donehue	Buchanan, NY 10513			GEL Work Order Number:	GEL Chain of Custudy and  "See www.gel.com for GEL's Sam
men needlee	tel or state of			Sin	9	্রা			so, please list	- 8							AON.	534	*Cina Collegad (Millacy) (bhann)	orrahue		Fex #.	Phone #:	5	hain of Custody and Analytical Re**See www.gelcon for GEL's Sample Acceptance SOP**
igua agalan	ogas stra			1					Bet the			1					z	Z	Q 10%			(914)	(914) ?		i Cu
6 8 30 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Mark Section					3003			hazards	<							z	z	Field Filestop de			(914) 734-6247	(914) 736-8405		study
SOLOGOVANA					* (2)				, ,	· ·							QW.	ुद्ध	Særgvio Matou (**)			<i>₹</i> 2			and
edinger, som	Suden Se		~~~	>	7	To T				1		-					,<	Α.	Radiosciive	****	Shout some	ંદ છા∗			ipic Ac
3000	Xi		Aidyll #	Aishili #	Stethad of Shipment	OEL PM			-	~~~~		-	-				Z	Z	Total numb	****	L				Analytical being Analytical by
, S	F 0-04	· ·			elites it				27166	3			-	-			>		Tritium	(H3)			Sample		% SO:
,	recording.	<u>.</u>			chent.	N.S.			C TOCH ACT STOLE										Gamma	Spec	(GS)				** £6
	P Stiller &				X3G34	ERIN TRENT			- },	~- <u>.</u>							-	-	Strontan	m 90	(8790	***********	Analysis Requested (5)	************	equesi
a American	~Linion, F				×	***************************************	Sample Shipping and Delivery Details					+	-	-			-	╂	<u> </u>				uestes		
	Z.						Ship		K	8				-			-	<b> </b>	<b>_</b>				(F3)		
:	Z.				Date	-	Ring an		Co. Management	mmary			-										in the	Fax: (	2040 Savage Kond Charleston, SC 19407
					Date Shipped:		d Desi										_						нить	Fax: (\$43) 766-1178	2040 Savage Kond Charleston, SC 19407
		,,,,,,,,,,			18.		ery D	Central Mountain	Sample	(### 		-	-			_		-	-		*************		roteo	6-3378	Cond 129405
		7					rtaits	B C	Cullecti	Elevel 2 /		-	-				-	<u> </u>	;				BRIESE	-	•
Cooler Temp:	SES '80' Cristody Soal fataet)	For Lab Receiving Use Only					***************************************	Pacetic	Tune Zone	2 / Level 3 / Level 4							2 Liter Poly	2 Liter Puly	8	Note: extra sample is required for sample specific	Comments	< Freservative Type (6)	(Fill in the number of committees for each test)		

a.) Provinder Type RA: Helwebkire Add AF Seria As Seria Astronomyddiad SA: Selfiria Ard, AA: Asonbi And, RX: Hermy, ST Sefind Francikae, if in prestraise i'i aiddol aces fidd blash PAR = CLENT	<ol> <li>First Priced To to to the Control with a Y-lot per for surger was food flaved to &amp; -lot entitle was not red blaced.</li> <li>Approximate Day Training Wass, DW Control and SW States Wass, WW Wass, WW Wass, Mp. Major, M. Streichen, Streichen, Streichen, Swischen, Streichen, Swischen, Streichen, Swischen, Streichen, Swischen, Streichen, Streichen,</li></ol>				100 SEC 100			CONTRACTOR OF CANADASTA	(N. Rejudici Norma: Y. Rush. Specify (Subset to Sachberge). Fax Results: Yes.  Remarks: Are there any known hazardy annificable to three summing? If we choose for the hornards.			**************************************		MW-53-120-(017)	MW-53-82-(013)	Sample II)  For congressive - indicate nor and sup that time	Collected by Send Res	Addhass: 450 Broadway, Suite 3, Buchanan, NY 10511	Project/Site Number Indian Point Energy Center	Ciliant Name: Entergy	PO Namebon 500 13510 GEL W	Project #EINOEGY GVV Mon Prog OEL Quote # OFG No	**************************************
AMITE) = LABORATORA 	terd filered of 8 of transfer was not to Woward Water, Woward, \$3,500,00 i 7479 Aud Journey of Crestation provides	Bhaipeann Clauk, M.S. Madan Spike K		~	375 TO 10 Cap	Reculied by (signed)		estant to the conditions acres	(Subject to Sauberge) Fax Results:					3		*Fine Colleged Colleged (Silbertos) (Silbertos) (Silbertos)	Send Results To. Patrick Donahue	an, NY 10511	Fax #	Phone #;	GEL Work Order Number:	م	CFI Chain
risk Aced. HX= Hereor, ST = Sections YELLOW = \$11.K	eta bilareal Apado, SCP Sert, SCP Sedimano, SC - Sia d for each (* v. 1876)3-3, voltab/24704	ompie, 31800- Maaris Syde Dopticas i		A NA	2251 2016C(0)	Data lime		e alse ence su garns						Z Z	Z Z	Of Code (field Sample)			(914) 734-6247	(914) 736-8405		**See www.gel.com for GEU's Sample Acceptance SOP**	of Custade and
Phospittas, if no preservative is added a tease field blank  PINK = CLEENT	adga, SibiSohd Wasse, Orthi, Erffilm, ErWipe, Orthus, Friend, M. 1- ti.	Sample: Sim Orab, Eim Collepsaide	Airbill #:	Airbill a.	Method of Shipawat: FEDEX	GEL PM. ERIN TRENT	Sample Shipp	WATER TO THE TOTAL THE TOTAL TO THE TOTAL TOTAL TO THE TO	No Cick Deliverable, Cof A / OC Sa					12/.	Z	Escioactive TSCA Regut Total numbe Trituum ( Gazuma ! Strontiur Nickel 6.	H3) Spec	(GS) (Sr90	le he lerad:	Sample Analysis Requested (8) (Fi		opie Acceptance SOP**	
	chand YES NO Chaler Temp	For Lab Receiving (to Only		TOPOTOTOTOTOTOTOTOTOTOTOTOTOTOTOTOTOTOT	Date Shipped.		Sample Shipping and Delivery Details	Lastern Pacific Central Other  Mountain	OC Summary 1 Lovel 1 / Lovel 2 / Lovel 3 / Lovel 4    Sample Collection Time 2 our					2 Liter Poly	2 Liter Poly	required for sample specific QC	Note: extra sample is	To receive the	· Prosecustive Type (5)	(Fill in the number of containers for each test)	Phone: (843) 556-8171 Fax: (843) 766-1178	2040 Savage Bond Charleston, SC 19407	GEL Laboratories, LLC

WHITE = LABORATORY

FIES = MOTESA

Project : Entergy GW Mon Prog GEL Wark Order Number:  CHO Number: 50013510 GEL Wark Order Number:  Physical : Entergy GW Mon Prog GEL Wark Order Number:  Physical : Entergy GW Mon Prog GEL Wark Order Number:  Physical : GEL Wark Order Number:  Physical : Factor of the College with the College w	#See www.gel.com for GE  #See www.gel.com for GE  Order Number:    Phone #: (914) 736-8405   Phone #: (914) 734-524  NY 10511   Patrick Donathue   Phone   Pho	**See www.gol.com for GEU's Sample: Acceptance SOP**  ***  **See www.gol.com for GEU's Sample: Acceptance SOP**  ***  ***  ***  ***  ***  ***  ***	(914) 736-8405 (914) 736-8405 (914) 734-62 (914) 734-62	Custody ; gel.com for GEL (914) 736-8405 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-5247 (914) 734-	Sample Sa	Z Z TSCA Regulates consistence C Z Z TSCA Regulates consistence C Z Z TSCA Regulates C C C Z Z TSCA Regulates C C C Z Z Z TSCA Regulates C C C Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	- First member of consciones	Tritium (H3)	Gamma Spec (GS)	-   -   Gramma Spec (GS)	Gramma Spec (GS) Strontium 90 (Sr90 Requested 3		the same (841)	(1011. Laborationnes, 14. (2041) Savage Rocci (1018/covage Rocci (1018	2043 Savage Road 2043 Savage Road Churleston, SC 29407 Phone: (843) 556-8171 Fax: (843) 766-1178 in the number of conta	Charlesona. SC 29407  Phane: (843) 556-8171  Pha: (843) 756-1178  (Fill in the number of containers for each test)  Comments  Note: extra sample is required for sample is pecific.  QC  2 Liter Poly  2 Liter Poly
		2	Z	-			<b>,</b>	ļ		·				-		2 Liter Poly
		Z	Z				y		3			-				
											-					Second 1 1 Lacol 3 1 Lacol 3
Remarks: Are there any known bazards applicable to these samples? If so, please list the bazards	samples? If s	so, please list	iss the h	zarás				Cacia	Copyrigation	line con A	1	Car continues		\$ 0/W	Control Control	oilectuen Time Zanz ) Pastir ) Pastir ) Deber
Chain of Custody Signatures	gnatures										Sample Shipping and Delivery Details	Smiddig	2818	eliver	y Det	(ails
Reliaguistica By Chipped - Buer Bure - Bur	Required to (signed)	s) Dute	, inc. j.	7		6	CH PA		Z	IN TRENT						
	74 (E.		1216		1402	Med	Method of Shipment	Shipro	38	XEGER	×	9	Date Shipped	pped		
Z. V.: .		stine				Aidi	Andrill #:					-				
						Arribili #	3:		000							
1. Clare Proced. Manter John Estamment. 2. A. Crobe, N. Award Steph Th. Page Steph, PD. Page Department M. Jac., MNS Mobile Stander, MSD-Motors Spike Daybeare Survey. Co. Composite 2. A. Crobe, N. Award Steph Th. Page Steph, PD. Page Department M. Jac., MNS Mobile Stander, MSD-Motors Spike Daybeare Survey. Composite Composite Manter Composite M	of Super Sup	dota Spile Sam	de MSD- K	izan e Signika	Dagobrate S	angie, Or 0	B (*)	oscapero)	r.							For Lab Beautylag Use Only  Curredy Seal Imac?
<ol> <li>James Cara, 1990 prince Cartering and Sweather Sweat New Water Webson, M. Alice Lepen, SO-Sale, So-Sale Sweat Water Deski.</li> <li>Amort Card Deskind. Audithor method concentrative Nation. W.W. Water Works of consumers provided for each tile of 5008-3, 601007-5004 - 8.</li> </ol>	e Water We West	, MD -Allier Exp ners provided t	and MONSON.	\$20-Selime Trial 3, 600	81. St. 1844	18 S9 648 18	West.	9		13 POSSES	Printed Printed States F-Food, or name	(8), 24-3486			T	Cooler Temp
4. Preservities Figs. BA: Bydarddoir Aeid, 88 w Nard Acid, 88 Sadam Bridanida, 8A: Addidi Abd, Ab: Abovos Acid, 88. Board, 87. Sadam Bricadina, From preservitor	SAT Sulfrice 200	LAAN Asombe	o Arid MX+ Hexand XX+ VXX 1 FYAV — XXI V	Sexane Sy	v Sodien i	3 coultino.	on preservative is added	20136.435	s added o	is added in house fight blook	: Maak				ſ	

				The state of the s
Pour Entergy GW Mon Prog	GEL Ch	SEL Chain of Custody and Analytical Re **See www.geleam for GEL's Sample Acceptance SOP**	1 Analytical Request mple Acceptance SOP**	C.E.I. Laboratornes, I.L.C. 2340 Savage Road Charleston, SC 29487
610-75-10 11-11-11-11-11-11-11-11-11-11-11-11-11-	GEL Work Order Number:			Phone: (843) 556-8171 Fax. (843) 556-178
Chen Name: Entergy	şd.	Phone # (914) 736-8405	Sample Analysis Requested (8)	(Fill
Project Site Hame: Indian Point Energy Center	200	Fax #: (914) 734-6247	અં અંદ	C., Pjejervacive Type (e)
Address: 450 Broadway, Suite 3. Buchanan	Buchanan, NY 10511		(GS)	Свинск
Collected by: Send Result	Send Results To: Patrick Donahue	ahue	e of em H3) Spec	Note: extra sample is
Sample II)	*Dale Critectol	QC Cook Field	a Regul A Regul I sumbe fism ( frama )	OC OCCUPATION OF THE CONTRACT
A first confidence of a property of a second	(84-99-660)	(Missing) 12 Filtered 10 March	Ten Tri Ga	
U1-CSS-(013)	0.00	WON N CW	Z	2 Liter Poly
TAT Requested: Normat. Y Rush. Specify:	(Sebject to durawage) Fan Kosults	Fax Results Yes - (	Par Circle Deliverable: Cal A / O	/ QX Summary / Sevel   - Sevel 2 / Level 3 / Lovel 4
enown huzards applicable to the	ese samples? If so	, please list the hazards		7582
				Mountain
Chain of Custody Signatures	ty Signatures		Sample S	Sample Shipping and Delivery Details
Eulenquistra By Sugassifi - Data - Year	Kacerwood by (segment)	(न्द्रक् १ अप्र	GELPM ERIN TRENT	
		N. 1. 1. 1. 2. 20.00.	Method of Shipment FEDEX	Daw Shippod
		~	Airbill 9:	
	w.		Airbill #:	-
13 Chart of Chatalib Neutrin - Chart Determined			Supports (C. Carrier C. Carrier Str.	For Lab Receiving One Only
<ol> <li>C.C. Color. We channel the part of the 10th Materials. Edit and District. Edit of Superior display of the superior of the superior of the 10th Materials. Edit of the 10th Materials of the 10th Materials of the 10th Materials. Edit of the 10th Materials of the 10th Materials of the 10th Materials.</li> </ol>	Enhanced Law In The Security of	is appearable. Another control plane independence to the field (Metric)	to the control War. Addition Private Individual Private Privat	
<ol> <li>Cordy Codes (New Control Control Control Western New Years) WW Waster water with a water and a control of the con</li></ol>	Whate water, within a	ay, peopleided for each film 2000000 3, 60100 No	SAMPLE OF LICENSE PERSONS OF SECTION S	Custor Femp:
e) Paudronous Type RA: Bydechlaid Ard M. Steith Asid, SB redline Rystinude No. Saithow And AA: Anothe And. BX: Became NF - redline Tossediae, il to preservative is saided blank.  WHITE = LABORATORY YELLOW = FILE  PINK = CLIENT	RAYORY	3.164 = AOTHAA Waxayayayayayayayayaya	m Thoselfast. If we preserve we is added a leave field Floor.  PINK as CLIENT	

5 of		5	3					- 1				NA N		node.	GEL Laboratories, LLC	CH C	
Project #		_	**See www gelcom for GEL's Sample Acceptance SOP**	m for GE	and L's Sam	<b>Ana!</b> the Acces	ync.	- F	* cq	Kequest	• 1		Charle	Thrass Arang	Joho Savage Road Chudestan, SC 29407	<del>1</del> 07	
50013510	GEL Work Order Number:	sumber:											. १९५ सन्दर्भ	843) :	Phane: (843) 556-817) Pax: (843) 766-1178	33.7	
are a re-		Phone 4.	- 1	(914) 736-8405			<i>5</i> %	Sample /	\naiv	is Re	Analysis Requested (8)		l in the	tems :	er of	contai	(Fill in the number of containers for each test)
Projecte Site Numer - Indian Point Energy Center	eg.	Pak #t	(914	(914) 734-8247	<b>‡</b> 7	te be						***********	************				< Freservative Type (b)
Address: 450 Broadway, Suite 3, B	Buchanan, NY 10511					Sibrasi Recep rocesio	tainers				53)	*****					( Marangara) e
Chillacted by: AA	Send Results To: Patrick Donahue	ick Donahue	,,			sted	ef cor			******	3 (Ni)	****					Note: extra sample is
Sample II)	*Course Calviolad		- Š	Test.		A Regul	el aumbe	itium (	mma i	ontiur	ckei 6	~~~					required for sample specific
* For pargoing - independent and sognifications	(3.5-199-198m)	ye) (himou)	- X	Folkaced 179	Majorik di	<b></b>	Total	<del> </del>	<del> </del>		Nic	<b></b>	-				
AAA'			Z	Z	େଞ	>< ~~~ ~<	3										2 Liter Poly
MW-59-66-(024)	6		\{; Æ	Z	C#	>< -<	)e>	,ee	~~	(~~	innd						2 Liter Poly
	**************************************																
								-	-	-	-	<b>-</b>					
			-							-		-					
***************************************																	
[A] Requested: Normal: 💉 Rash: Spi	Kush: Specify: (Sagget to Succhage)		Fux Results:	É	- A	3	~	Civie	क्षा <b>भर</b> ाइ	Deliverable: Cof A	8 A /	OC Summary	nemary.	/ 14	vel t	e tav	Level ( Levei 2 / Level 3 / Level 3
agons	able to these sample	s? If so, plea	se list the	huzarás											人	1/2	Time Zone fiv
																Central Central	(Ather
( hair	Chain of Custody Signatures	res									Sample Shipping and Delivery Details	Shipp	ing ar	d De	Sery	Detail	N (E)
Pelitequished By (54gaed) Base Your	Received	gned)	Dane	Fane		WH 1313	WH.	55 XI	IN TRENT	ENT							
						Mess	Method of Shipment	hipme	<del>2</del>	XEGES	ĒΧ		Oasc	Date Shipped	cd		
	2	***				Aibill #	25 24										
,	Ser .					Airbill #.	⊞ 3*										
1) Club, J. Dobredy Number - Ellera Parameted			Y AND THE REAL PROPERTY OF THE	24				aria constitue									For Lab Becaving Use Only
S. Cold Photoci. Extrapol colorest, Holicide with a V-decyclate completes and the colorest control of the colorest colorest control of the colorest colorest colorest control of the colorest color	sample was field thereof or X	previous sections and	Highly followed.	The Carlotter of the Ca					₹ <b>2</b>		Red Follows - Productions - (1991) trigger - Section (1997) (Sections)	* ** **	Ž 2850.				Custody Seat Imacci SCS SCI
11 March Color (W. Dreking Water, G.W. Grondwater, S.W. Surfan Water, W.W. Water, W. Water, M. Surfan Society, Society Society, Society Society, So	en Taka Patawa da San da S	of containers provin	e cogana social ded for such (s	e <i>\$2508</i> 3, 66	HURCACUR.	Sec. Securior	2			j.							Cooler Temps
64 Prisaryanya Uga. 1600 Hydradsind Acid, M.: Nind Acid. 819 Sodium Rydramide, Swel Suduric Acid, AA: Asmolike Acid, 818 - Honore, ST.: Sodium Universities at Addition was stadd thank WHITE LABORATORY YELLOW FILE PINK CLIENT	AUG SIF Kodiam Hyarmids, Saffikalı Augustus Karamanı	(veic Avid, AA- Au	FFT3A 38 Past made	XXIIS = WOTIBA	F-Swkom T	missuituse, d	FINK ~ CLIENT	TO S	ENT.	lease the	Sa blank						William Commence of the Commen

Project # Entergy GW Mon Prog	GEL Chain of	hain of Custody and Analytical R	Custody and A	Analytical	Request	GEL Laboratories. 2040 Savage Road Charleston SC 90	GH, Laboratories, ELC 2040 Savage Road Charlester, SC 70407	
50013510	GEL Work Order Number:	er:				Fine (84)	Phone: (843) 556-8171 Fax: (843) 766-1178	··· octoccccc
7		Phone #: (914) 736-8405	-8405	San	Sample Analysis Requested (5)		(Fill in the number of containers for each lest)	(354)
Projectivite Name: Indian Point Energy Center	*	Fax s: (914) 734-6247		is by eved:			10634g ~;>	Preservative Type (6)
Address 450 Broadway, Suite 3, Bu	Buchanan, NY 10511		Showin	stempi crosisi				5) 65 69 fC
alloand by:	Send Results To: Patrick Donahue	onahue		r of con	Spec i		Note: cx	Note: extra sample is
Sample (I) Same some some some some some some some so	*Date Collected (rem-dif-ry)	(a) to (a) (a) (b) (b) (b) (b) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	Field Stongle States and Matter and Stongle	TSCA Regula Fotel combe Tritium (	Gamma S Strontiun		required for	required for sample specific
MW-32-59-(014)		Z Z	Z GW Y	~~			2	2 Liter Poly
MW-32-85-(017)		3 \$ x	N CW K	Z			2 Li	2 Liter Poly
MW. 154.154.WW		Z	A MO N	* + +			213	2 Triter Holy
MW-32-149-(015)		Z	N CW A	Z.			21.	2 Liter Poly
MW-32-173-(013)	\$ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	S36 N	A MO N	2			22	Liter Poly
MW-32-190-(016)	(3) (5) (5)	N OCS	N GW Y	Z			2 Lú	Liter Poly
TATE Boom and Normal Control	2			<i>J</i>	Code Deliverskie	A Communication of the Communi	Could be bound of the could be	··.
кножи huzards app	licable to these samples! If so	so, please list the ha			MODOL CONTRACTOR CONTR		Sample Collection Time Core (Eastern) Pacific (Control Other	38
Chain	Chain of Custody Signatures	*****	the desired the second		S	Sample Shipping and Delivery Details	elivery Details	
Reforming the Year Same	Raceined by (signed)	ed) Osac Yane		GEL PM B	RIN TRENT			
ころかんなからまでも	 Ω	in the state of	% 3°	Method of Shipment	pment FEDEX	X Date Shipped:	pped:	
3				Airbill \$:				
}	CO.			Airbill#			COCCOOCIONATION CONTRACTOR OF THE COCCOOCION	
3 C. Salo J. Casado Dander - Clieft Decembro. 3 G. Cado - N. Koosad Sungle, TB o Frip Black, 8D. Field Duploute, 8B o Equipment Slank, MSc March Spake Sumple. MSR o Matrix Spike Duploute Sample. Gr Class, Co Convente	ote, BB – Equipment Slank, MS- M	laris Spike Sample, MSIn. Ma	am Spike Duphoste San	gle Gristati, fin Can	ye saide		For Lab Receiving Use Oak	ving Use Oute
:	ngle was beld filtered to N+for sam o Wases, <b>WW</b> -Waste Water, <b>W</b> -Wate	n. MijoMise Lionic, SC-Suil, S	Medicalment Sloddings	SS-Solid Wate, D-O	ii, Pafritor, Palkijot, ii i	Pige, 31 Fenal, WeNesel	NAS Specify de	THE WOOD CHINEST
5) Saugu Analysi Kujinasul. Asalytud mehad mepasted (i.e. 1860), 1600). 1788and similar provided for each (i.e. 1768) 3, 2600). 17470. 13)  S. Groom min was 13. A. Halvadaline A. M. W. Wire Acti. SIF Nodom Hydrimid. SA+ Suffusa A. M. Anantie Real. BN+ Brosse, SF+ Suffusa Thiometriae, If to preservative a added 8 base feeld flowly.	<mark>)8., 50108/7478Xe</mark> nd number of conta Nodiam Hydrinkik, SA+ Suffuse AU	itners provided for each (1 e. 82) id. AAT Ascorbic Acid. 81X× 8	668-3, 50108/14714-11 Responsible ST = Sodium Thi	enifer If to preserve	ive a advict v jegve tield	Mark	\$ \$400.00 A	(ha)
XHIX	WHITE - LABORATORY	FIB - WOTIGA	EILE	PHNK T	FINK - CLIENT			

WHITE "LABORATORY

FILS - WOTTEA

	GEL Chain of Custody and Analytical Re **See www.gel.com for GEL's Sample Acceptance SOF** GEL Work Order Number:	d Analytical Request	GBL Laborstones, LLC 2040 Savage Road Charleston, SC 79407 Phone: (843) 550-8171
	Phone #: (914) 736-8405	Sample Analysis Requested 6:	94
rgy Center	er ::ax #: (914) 734-5247	e te ored:	<>\$\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\square\text{\psi}\squar
, Suite 3, B	, Suite 3, Buchanaa, NY 10511	Should see apply consider a see apply consider a see a	
Collected by	Send Results To: Patrick Donahue	H3)	Note: extra sample is
27	OC Code Fedd	Kezois Bumba SIII (	required for sample specific
Sample 11.) * For composites - indicate start and step described	20	Badies ESCA Fonts Triti Ciam	
MW-31-49-(020)	MONN SSETT STOLL	N	2 Liter Poly
MW-31-63-(020)	WD N N OCE   50,0000	Z Z	2 Liter Boly
MW-31-85-(020)	WO N N N N N N N N N N N N N N N N N N N	< Z	t-J
No. Neuronaea Peanas: Act 2000 No.	Specify: (Subject to Servinge)   Fire Kendle: Fes	No Care Deliverante Cot A / Q	CK SUMMARY / LOVE! / LOVE! / LOVE! / LOVE!
temarks: Are there any known hazards applic	r, please list the ha		Sample Collection (Eastern) Pac (Central Off Mountain
		Sample S	Sample Shipping and Delivery Betails
KoSinjaciled By (Signed) - Date - Tune	Reactives for case and Since Time	GELPM: ERIN TRENT	Octobra - Andre Administrator de la composiçõe de la comp
21 50KK 101 - COS (200)	30 1 20/10/01 may 10/23 16 38	Method of Shipment FEDEX	Date Shipped:
The state of the s			
	3	A::bill #:	o a s s em mindopalmanha a green mahkoographaa a s estimodoographaa a serimodoographa
1) A Solar of Colored Northern Chiefe December 2) Of Colored No Schould Northern Title Trip Blank, Fth. Evold Dugit	n Norsker - Chien Decemined  Norsker - Chien Decemined  Norsker - Chien Decemined  Norsker - Chien Decemined	te Sample, SA Chats, Chi Campada	For Eath Receiving Clac Only
<ol> <li>Field Fliered. For topid markets, indicate with a V - for yea then.</li> <li>Mobile Cales, SW-Diricking Water, CW-Groundwater, SW-Saction.</li> </ol>	3) Birli Fibreri. For topic matrics, indicate with a Y- Co., so the sample was field filtered by N- Co. sample was no field filtered. 4) Main a Code, BW-Oxinking Water, CW-Commissioner, SW-Souther Water, WW-Waste Water, W-Waste, W-Waste, W-Waste, M-Waste, M-Waste, Lipid, SD-Soit, SD-Sadonent, St. Sindige, SW-Soiti Waste, O-OA, 9-8 Fibrer, P-Water, E-Code, N-Water, W-Waste, W-Water, W-Waste, W-Waste, W-Waste, W-Waste, M-Waste, M-Was	Sindigo, 1890-senii Rasse, OrOA, Institus, Institus, Institus, Institus, Institus, Institus, Institus, Institus	K no
<ul> <li>Suraptic Analysis Requested - Analytical method requested (i.e. 826)</li> </ul>	S) Surger Analysis Requested Analytical method inquisated for \$1,000, 603000 (400000000000000000000000000000000	764 - () von Thiomediae - View orthographye is added - have field black	Cooler 7 cmp.

WHITE = LABORATORY

3313 = MOTIBA

# APPENDIX D: 4TH QUARTER 2009 SAMPLING DATA SHEETS

WELL ID: MW 30 . 69

SAMPLE ID: \_\_\_\_\_\_\_\_

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Emergy - IPEC Buchanan, NY SULWAY	, 61°F			PROJECT NO: DATE: SAMPLER(S):		01.9017869.92 101.727 275/10	11/	9/09
SAMPLING I	NTERVAL (depth		of casing)		PURGE RATE PURGE METE	:	al/min) Double Valve l		80404(colds), colors - 10000(colds)
VATER QUA	Purged Visiamo (gal)	P.COP	1.312	Dissolved Oxygen (g/l)	pH (80)	ORP	Turbidity (NTU)	Orive/Vent Cycle (seconds)	Dirve Pression (psi)
10 3 3 10 3 10 10 3 10 10 3 2 10 3 2 10 3 2	2,25 2,15 1,05 1,15	24.30 24.35 24.35 24.35 24.35 24.35 24.35	1.232 1.233 1.203 1.203 1.203 1.312 1.314	4.725 4.33 4.40 4.42	3.54 3.54 3.54 3.54 3.53	1887 1887 1897 1807 1807 1807 1807			
162	1,30 3,1621 5,1xD S Punns	24.72 3430.64 4346.45 65.5	1315 2212 2212	11623 1103 1122213	\$.92 C. 1763	3.73,5		*	*
YSI 556 MPS	S Reader and \$553.5	····	iquipment Us	ed				ment Identific	ation #

WELL ID: MW 30 . 94

SAMPLE ID: OF

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	, 67°F			PROJECT NO: DATE: SAMPLER(S):		01.0017869.92	terer 1110	ગાંગ
SAMPLING IN	77.3 ORT		of casing) 항의식		TOTAL VOLU PURGE RATE PURGE METE	: \nishl <b>e</b> (	1.65		
WATER QUA	LITY:								
Time	Perged Volume	Fern <b>p</b> ( <sup>®</sup> C)	Specific Conductivity (SAm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbiday (NTC)	Dove/Vent Cycle (secouds)	Bove Pressun (ps.)
C  5   C  42   C  42   C  12   C  12	1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42			7.03 7.03 1.95 1.88 0.83 1.77 1.78 3.03 3.02 8.02 8.02 7.02 7.02 7.02 7.02	6.79 6.24 7.20 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30	23.71 26.42 32.33 35.71 71.35 43.71 94.71 94.71 94.71 94.71 94.71 94.71 94.71 94.71 94.71 94.71			
		Ε	quipment Use	ed			Equip	ment (dentific	ation#
S SI 556 MPS	Reader and 5563 S	ioni <b>se</b>					5		

WELL ID:	MW	道.	11
SAMPLE D	D:	$\cup \partial$	0

7 7 83 VX ROV 376	CONTA PACCETARE A DOCUMENT A CONTACT A
CLIENT: Energy IPEC SITE: Buchanan, NY WEATHER: Signify 10°S	PROJECT NO: 01.0017869.92  DATE: (12.1/0%  SAMPLER(S): (2.1/1/1)
SAMPLING INTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURGED: 3.95 gas
	PURGE RATE: variable (sal / min)
0.070	
SAMPLING PORT	PURGE SIETHOD: Double Valve Pump
<u> </u>	, , , , , , , , , , , , , , , , , , , ,

#### WATER QUALITY:

Tine	Parged Volume	Temp (°C)	Specidic Conductivity (S/cm)	Dissolved Oxygen (g/l)	pΗ (SU)	ORP	Turbidity (NTU)	Drive/Vera Cycle (seconds)	<u>{</u>
nii.	70m20	J						W.Z	2.2
11.12.22	2.4	19.12	1.33%	2.34.3	6.24	191.3	1.32		
N. L. G	1 2.4	13.15	1.834		2.15	1:20:8	5.79	<b>.</b>	
1182	ि तर्	13.02	1.856		2.51	101.0	L.5:32		
	140	19.24	1.974	1.54	12.65	_iQO:3	9:44		
1150	1,44	13.11	1:354		(#***)* <b>4</b>	29.9	122		
k.bk.%	**********			74	2.7.7	7.2.62	1		
361	125			نتششن		1.4.1			
no	1215	La composition de la composition della compositi	( - 40) i .				المنابقة المسلم		
12.12	i &	19.25	1.708	1.76	4:32		5.46		
1218	1.45	(** ?.)	1.909	<u></u>	6.83	32.2cm	13.72		
236	3.35	1942	Lilit.		\$.\$3 <u>.</u>	2.1.2	3.72		
12.321	3.35	19.20	1.413	1.75		بالمنات		***************************************	
2 42	315	12:17	1:013	ulu				•	
1246	7.15				<u>\</u> \\		3.79		
17.47	Trace 2	27.2	ķ	****					
1749	T 3 344 5		Lidat Kiritika da			***************************************	<b>_</b>		
125X	TENINS	9442446. C	amak na	di INC.		•••••			
				***************************************		****			
***************************************						********************			~~~
				**************************************			<b></b>		
							ļ		
	- defendance							-	

Equipment Used	Equipment Identification #
Con Ser Ame Danks and Sight Sopular	2
whichty meter	2.20703.293

WEIL (D: N	ww.	· \$ 63
SAMPLE ID	. (	1,76

7 7 44 5 C 4 C C 5 7 C C	xxx factorist remem frances				
CLIENT: Entergy - IPEC SITE: Buchanan, NY WEATHER: SAMPY, 70'S °F	PROJECT NO: OATE: SAMPLER(S):	01.0017859.92 (5/22/09) 			
10-10-10-10-10-10-10-10-10-10-10-10-10-1					
SAMPLING INTERVAL idepth in ft below top of casing)  55.8  03.8	TOTAL VOLUME PURGEO: [1-10 gal				
43	PURGE RATE: variable (gal/min)				
SAMPLING PORT  B  G  S	PURGE METHOD:	Double Valve Pump			
WATER QUALITY:					

Time	Purged Volume (gul)	Temp (°C)	Specific Conductivity (Sven)	Dissolved Oxygen (g/t)	pH (SU)	ORP	Turbidity (NTU)	DriverVess Cycle (secunds)	Drive Pressure (psi)
1116	TRUMP							4/3	29
433	223	13:35	1.517	<u> 840</u>	7.01	-/130-2	5.35		
14.40	0.4	MO.	1.533	2.862	7.24	11.5	7:01		
\$1.555	0.5	12.21	<u> </u>	1-12	1.01	22:1	bull		
	0.55	19.01			2.2.7.		37 کر رہی		
233	10.6	19.42	11165		1.10	28.8	2.5	·	
	1.20	11221	1.427	1.10		11211	6-69		
12.17.	1 0: 1	20:15	11438			42.4	6.1		
1215	0.76	24.34	1451		1	45.4	S. 22		
	0.3	10 46					5-13	ļ	
23	l ol	10.38	1.493		7.10		5.14		
17.40	0:2m2	ore		<b> </b> 	<b>*</b>				***********************
1241	S. TARK	Same & Co	i shillini			واد و دادادادادادادادادادادادادادادادادا			
1370	600 S	meri oc	Lucia Tieni	21966 2	k root		<b>\$</b>		
				·	} •		<b>_</b>		
								***************************************	
*********************									
},					***************************************	<u> </u>			
							·		
						deres e e e e e e e e e e e e e e e e e e			
<u></u>		[							
<b></b>									
		-				***************************************	***************************************		_

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidny meter	2200 1213

WELL ID:	MW	. <u>=</u> 35
SAMPLE I	D:	30

CLIENT: SITE: WEATHER:	Entergy PEC Buchanan, NY	, 70°s E			PROJECT NO:         01.0017869.92           DATE:         10/23/09           SAMPLER(S):         CAIAA				-		
SAMPLING IN	iTERVAL (depti	in ft helow top	of casing)	8 85.4	TOTAL VOLUME PURGED:						
SAMPLING PO	ORT		<u> </u>	. ,,	PURGE RATE	ë: <u>variable</u> (g HOD:	ał / min) Doubłe Valve I	Pump			
WATER QUA	LITY:	3 J.			***************************************	<del>(((((((((((((((((((((((((((((((((((((</del>		***************************************	874444444444444444444444444444444444444		
Time	Purgest Volume (gal)	Temp +°C)	Specific Conductivity (Sign)	Dissolved Oxygen (g/l)	pH (8U)	OKP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Orive Fressus (psi)		
11.161	71.AND 2							¥ 1 7	20		
11 310	1.0.2	LiáiQ	1.514	244	1 4 Si	-104.3					
1137	<u> </u>	12.12			<u> </u>	النقليسا	9.05	•••••••	<b></b>		
14-40	10.4	11:22	L.i.a.11.7	3.05	L. 2.2.2	- 77.X		· <del> </del>	ļ		
1150	1 0.5		1.425	201	<u> </u>	-34.8	3.79	·	<u> </u>		
5.7	1 1.62	1,21,06		<u> </u>			-1.35	-			
1.202	کہ ڈ		المردميا		1 7.01	21.3	3 63				
2/22	25	13.53	14430	3.09	1 2.02.	35.0	3.53				
12.12	0.15	133	623	ă, is		71.7	3.35	~ <del>}</del>			
		19.39	11,27	3.12	1-00	45.3	3.44	•			
1111	V.S Pume	L	Andreas de Santonio de Companyo			·		•	•		
17.32		1000 PLE	7820500	O a./		1	*****	***************************************	f		
1231	TOAMS S	holfi 6		W: IP	EC 2.4	19064			****		
	.ii.i.i.i.i.i.i					,	**************************************				
**************************************		Ì									
					**********						
Aurenaunaunaun								<b></b>			
			<u> </u>								
				A							

C = 0	The state of the s		
kliguig	oment Used	Eq	pipment Identification #
AAA-TITOTO AAAAA AAAAA AAAAA AAAAA AAAAA AAAAA AAAA	**************************************		1
YST 556 MPS Relider and 5561 Sonde			A second
turbidity meter	**************************************	<u>12CO</u> _	104/45

WELL ID: M	w <u>10</u> - <u>10</u> w	
SAMPLE ID:	1014	

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	F.SC.		-	PROJECT NO: DATE: SAMPLER(S):	enagenemos na magazis stanios d	01.0017869.92	3162 1997 12	-
SAMPLING E			of casing)	~	TOTAL VOLE PURGE RATE PURGE METE	: <u>vanable</u> n			
SVATER QUA	LITY:			(				······································	***************************************
Time	Paiged Volume	Temp (°C)	Specific Conductivity (S/cm)	Dissolvat Oxygen (g/l)	giff (SU)	ORP	Torbidity (N <b>T</b> 11)	Drive/Vens Cycle (seconds)	Orave Pressus (psi)
					2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			4772	
			्वशंpment Us	ed			Egoip	men <b>t Id</b> entific	ation #
YSI 556 MPS turnship meter	Render and 5563 S	ionde		ad a particular particular de la compansión de la compans	المراجعة ال المراجعة المراجعة ال				

well id: ww32.55
sample id: 017

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CEIENT: SITE: WEATHER:	Entergy - IPEC Biscipanan, NY				PROJECT NO: DATE: SAMPLER(S):	ATE: <u>131234163</u>			- -	
Sampling E	VTERVAL (depth		of casing)	-		ME PURGED: :: <u>vanable</u> (g	1. C gal			
SAMPLING P	ORT SS				PURGE METI		Daniste Va <b>lve</b> i	Pump	······································	
WATER QUA	LITY:									
Fine	Perged Volume	Feering (°C)	Specific Conductivity (S/cm)	Disselved Oxygen (g/l)	рН (SU)	ORP	Turbidity (NTU)	Dave/Vent Cycle (seconds)	Drive Pressue (psi)	
	77.25	(*)						3.73	$\mathcal{A}_{G}$	
					-t	1053 9	1 1.15		<b></b>	
				125	<b>*</b> .		Q. , & F		<u> </u>	
12.5		(-9) 142	Lists			1			<b></b>	
25.63	2.3	. 3 V J		2 2 7 1				-17		
				1	. <u> </u>	- 1 10x X			<b>,</b>	
	1						7 S.		<b></b>	
		1 (2) (2) (3)	1.666				7 3 7 3			
		14.5	1664	1			3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	···		
20				6.83	ــــــــــــــــــــــــــــــــــــــ		3 15	<u></u>		
				l Mai A Alya	1 - 2 6				ļ	
		<u></u>		ļ						
			<b></b>				<b></b>		<b></b>	
				<b></b>						
phiningshippingshippe			<del> </del>	<u> </u>			<b></b>	<del>-</del>		
}		<u> </u>	<u>i</u>	,]		.!	1		ξ,	
			quipment Us	ed			Equip	ment Identific	ation #	
							<b>-</b>		***************************************	
YSLSS6 MPS	S Reader and 5563 S	onde				······		<u> </u>	<u>1.6</u>	

NOTES AND OBSERVATIONS: 1/2 A 1/2 CC 2012 TO LONG TO THE TOTAL OF THE CONTRACT OF THE CONTRACT

WELL ID: MW 2 - 131
SAMPLE ID: 107

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CUENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	<u> , 200</u>		-	PROJECT NO: DATE: SAMPLER(S):		91,001/869.92 / 9.1.2 / 224.	) (8 <sup>6</sup> )	
SAMPLING	NTERVAL (depth		of casing)	<u></u>	TOTAL VOLU		//*	_gal	
SAMPLING	PORT	- 		4	PURGE METH		Double Valve	Pump	
WATER QU	ALSTY:								
Course	Porged Volume (gai)	Temp (°C)	Specific Conductivity (S/cm)	Ossoived Oxyges (g/l)	p <b>H</b> (SU)	(87	furbidity (NTU)	DriverYent Cycle (seconds)	Orive Pressur (psi)
			Equipment Us	sed			Equi	oment Identific.	ation #
YS1 556 MF	S Reader and 5563	Soute				***************************************	<del>\</del> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1701389	

WELL ID: A	WN		· 16467
SAMPLE ID	·	Ò١	S

CLEST SITE: WEATHER:	Entergy - IPEC Buchanan, NY	<u> </u>		•	PROJECT NO: DATE: SAMPLER(S):		01.0017869.92	<u> </u>	~
SAMPLING I	NIERVAL (depth		of casing)	- .3	TOTAL VOLU PURGE RATE PURGE METE	: <u>Fariable</u> (g	al / min) (Nontrible Valve I		
WATER QUA	ALITY: Purped Volume (gab)	Temp (*C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Furbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
13.3 14.3 14.3 14.3 14.3 14.3 14.3 14.3	- 7AS/C		2.123 2.123 2.123 2.123 2.123 7.123 7.123 7.123 7.123 7.123		\$ 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6				
YSI 336 SIP:	S Reader and 3363 S		quipment Use	ed ed			Equip	ment Identifica	sišon #

IPEC00224971

WELL ID: MW	32.123
SAMPLE (D:	0/3

				8.	(a)	•			
CLIENT: SITE: WEATHER:	Entergy - (PEC Buchanan, NY	<u> </u>	1		PROJECT NO: DATE: SAMPLER(S):		01.0017869.92 	<u>G</u>	
Sampling P	(TERVAL (depti	ı in ít below top	of cusing)		TOTAL VOLU	ME PURGED:	1.90	gal	
	<u> </u>	to	1/13		PURGE RATE	: mainhle (g	al / mun)		
SAMPLING P	ORT 173			2	PURGE METE	IOD:	Double Valve F	unp	
WATER QUA	LITY:								
Times	Purged Volume	Temp (°C)	Specials Conductivity (S/cm)	Dissolved Oxygen (g/h)	pH (SL/)	082	fiotelisty (STO)	Drive/Vent Cycle (seconds)	Drive Pressure
	7. 7.	(2 <b>%</b> )							
			7,403	10.74 %	l in the	11111	2.29	and the second	

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Disselved Oxygen (g/h	pM (SM)	088	furbidity (NTO)	Cycle (seconds)	Drive Pressum qeai)
1325	Pose	2.30					••••••	<u> </u>	
V ( )				11.77.6			-4-27	<b></b>	
	0.75	\$ 310 PG &						<b></b>	
A STATE OF THE STA		11115			<u> </u>	11.2761.54			
		1.3.39		0.36.		72,042,5			
1420		I 1911	1 995		لث شا		442		
1131	1		<u> </u>	Cara	سنبت شس				
1442	131		1 996	( ) ( <b>)%</b>	<u>                                    </u>	للانتك			
	130	I 10.13	1.795		0.15		3.34		
	130			4.09		- 341, 2	242		
	1 45	L M. 35					0.08		
	1 40	Landing to the same	1449	- 3.22 - 3.64			Q.::::::::::::::::::::::::::::::::		
	1 1000	1 173-12		L.C.GV	897		0.07		
A CONTRACTOR OF THE PARTY OF TH		110.23			1X	29 9	000		
C. P.S.	142.	Anna a sa	de la company de la company de la contraction de la contraction de la contraction de la contraction de la cont						
1674					266	•			
	The said		•				***************************************		
	}						,		
			ļ			····		<u> </u>	
						******			
							~~~	***********	
							•		
	***************************************						ann ann an an an an an ann an an an an a		
	-						*****		

Equipment Used	Equipment (dentification #
YSLSS6 MPS Reader and 3563 Sonde	Ų.
Surbidity meter	S 34 - 2 C 4 C 2 3 3

WELL ID: MW 32 . 10	<u>i</u>
SAMPLE ID: 15	

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY				PROJECT NO: DATE: SAMPLER(S):		01.0017869.92   \rightarrow 22] 		-
SAMPLING D	CIRRYAL (depth		of casing)	,	TOTAL VOLU PURGE RATE PURGE METH	: <u>Yuriab<b>le</b></u> (go	1.5 al / min) Double Valve I		
WATER QUA	LITY:								
Time	Purged Volume (gal)	Temp ("C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/i)	pH (SU)	ORP	Turbiday (NTU)	Drive/Veat Cycle (seconds)	Drive Pressure (psi)
	2.2.3. 2.2.3. 2.2.3. 2.2.3. 3.3.3. 7.1.3.2.		1.0000 1.0000						
			qsipment Usi	ed .	W.Tavasur Comm		Equip	ment Identific	ation #
YSI 556 MPS turbidity mete	Reader and 5563 S	onde		***************************************			18 W.		

# GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WEATHER	Entergy - IPEC  Buchanan, NY  Gan So 15F	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 10.7287.05 2017.05
		A 15 15 15 15 15 15 15 15 15 15 15 15 15	

WATER Q	UALITY:	otw=		└{ ¹ Transd		i Depth	44; L	60)	
Time	DTW or Acidal Depth	Temp (°C)	Canductivity	Dissolved Oxygen (g/l)	p <b>H</b> +S <b>U</b> )	ORP	Tarbidity (NTU)	Flow Rate (gai/hr)	Notes
1232	444 400	******	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<b></b>		<u></u>			·
1237	iii.yol			<b></b>		}		•••••	******
1335	130012	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		<b></b>					~~~
1340	44.00	244.000.	LATIS			1-190-2.	11.93	2	~~~~
1592	44.400				1.13		7, 7 <u>5</u> 7	•••••	************
Lund						347	الإدتيد		*********
1-3-165		14.10					*****		***************************************
1202	44.4,22	121.00	بەكىلىك	2.15	7.74	لنكشنا	****		**********************
1 1 2/3	14430	27.10	2.12.1X	129		-073	. Ya ba		·
1440	48.402			235			222		************************
* * * *	Grant Hits		2023 2023				1.24		***************************************
TUST.	1 44 472	21/90	Laux 5	231		- S2_x		***************************************	************
I Wasa			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			v G o - 2		***************************************	
<b>3</b>		Setthic	1200 31		*********				*****
1 < 4.5		ستبشيش		<u> </u>					
		.,,	*************************		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				
				<b></b>					
			****						
			••••						
			**********						
, , , , , , , , , , , , , , , , , , , ,						····			
			••••						

Equipment Used	Equipment Identification #
YSL556 MPS Reader and 5563 Sonde	15
Now moter	2
turbulity merer	20010101

NOTES AND OBSERVATIONS:

Total volume purgest 1. TQ gai

Depth and Depth to Water (DTW) measurements are given in feet from top of casing,

Commitwater Elevation measurements are given in feet and

WELL ID: M436-4 SAMPLE ID: 010

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

P916F2

CLIENT: SITE: WEATHER	Entergy - IPEC Buchagan, NY	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	61.0017869.92 

vater Q	CALITY:	DTW =	Transducer Actual Depth								
Time	DIW or Actual Depth	Temp i <sup>d</sup> C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes		
1333	3 4 1								~~~~		
.125222			**********	<b></b>		·			~~~		
	Punt.	0.0							***************************************		
	[2.0]	110.79	1.7.42	1.00	1.15		15.00	<u></u>	Y		
13.92	TV8.23				1.72	-173	25.25	2	·		
1.00	<u> </u>	Mw.XI.		0.261			22.24		Y		
1415	1.2.1.4	20.14		22.2			21.15		***********		
100	1.2.34	22.14	LLYZZ	1.5%	2.43.	53.2			·		
	12000				*****************						
			***************************************	*******		***********			******		
				**********					·		
									************		
			****	********			***************		~~~		
				***********					·····		
									**************		
		<b></b>		<b></b>		*******************	····		~~~		
		<b></b>			********	******************	***************************************				
		<b></b>			****		·····				
		<b></b>		····			***************************************	<del></del>			
		<b></b>			******						
		<b></b>	<b>Marine Marine State</b>		******		adronal contract of the state o				
			*****						····		
									***************************************		
						********					

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	77
flow meter	1
turbidity meter	202 1012 S-1

		e purgedgo
Clepph and Orpit to Water (DAW) measurements are given in feet from top	लें हततील्युः	
Commission Elevation measurements are given in feet and		
DAMAGERIA PROGRAM DOLLAR PART BOLL OF TO MEN	Aleman Armania	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MAD SUP 11 >> SAMPLE ID: OLO

MARFZ

CLIENT: Entergy - IPEC SITE: Bachanan, NY WEATHER: LAND, QUAF						PROJECT NO: DATE: SAMPLER(S):			01.9017869,92 	
WATER COL	UMN HEIG	HT (N)	0 2.2	1	4.7	L AR	Well Diam	er(er:		in
	40 nrs	,	orw	, as	****	o. (3) lumn t <b>icight</b>	្តា	Diameter	Multipliers 0.041	0
GALLONS @	F WATER P	ER WELL VO	LUME:						11.163	
		36-03	, <b>x</b>	0.241 Mattiplier	*	Well Vi		<u>4</u> _gal	0.853	1
1 :- (	Ŷ <sub>x</sub>	1.5	22	2,23	The second district of the second district of the second	_gal	V. W. Z.			
***************************************	_			Designed Pur	ge Volume	TOTAL VOI	.UME PUR	rged: 2.3 g		
WATER QU	ALITY:	DIW =		fransdace	r Actual Dep	oth				
Time	Volume Purped (gal)	DIW or Actual Depth		Specific Conductivity ( (S/cm)	Dissolved Oxygen (g/i)	pH (SU)	ORP	Tarbidity (NTU)	Notes	,,,,,,,,,,,
	0.4		523	\$ ·					********************	
			علامك للمالي	(49)		L <u>. 2</u> 5	49.2	eller er e	*************	Was a supplication
	ļ					7.21		74.4	Manager Co. C.	**********
1527					Q.::134	7.53	4.60	73.3	*****	w
	1435			1. 719		7.51	72.3 74.8		Anno conserva a qua no conservação e que	(AAAAAAAAA
	1 1 4 5			4 (10)			an halidain haana		<b>(***************</b>	
				***************************************		***************************************			Marian Marian Caranta Caran	(***********
	l Yasasa	<u>i Scenie</u>			***************************************	• • • • • • • • • • • • • • • • • • • •			Ver-eq. (1,000,000,000,000,000,000,000,000,000,0	**********
	كنششنشش		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			·····	***************************************		************	, e e e e e e e e e e e e e e e e e e e
AND THE RESIDENCE OF THE PARTY			***************************************		1000000 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		rica e a para la processió de la composició de la composi		Here of the book of the state o	22222 <b>2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 </b>
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				(A)AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA		00000000000000000000000000000000000000	***********
	·								***************************************	
		3								
					**************		***************************************		\$2000000000000000000000000000000000000	17711122000
\$00.000.000000000000000000000000000000					and the second second second					
Consession of the Property of the Consession of	************************						0	<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>	<del></del>	Andria e e e e e e e e e e e e e e e e e e e
			Equipn	ient Used				3	uipment ification #	
YS1 536 MP	S Reader at	d 5563 Sonde	-	**************************************				7		to de la mana espa
turbidity met			and the state of t				**************************************	20710	357	

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MULL 52 SAMPLE ID: 015

	Entergy - Il Buchanan.	PEC NY 2/5 (2/3)/	1	•		PROJECT N DATE: SAMPLER(		01.00±786 	
WATER COL	25	HT (ħ)	EL GO	-	//7	ि lumn Height	Well Diam ft	eter: //	in in
	DTB			:	** (1) **	um izeign			Multipliers 0.041
		ER WELL VO				استعدادات		4	0.163 0.953
Water Co	damn Height	476	(6 x	C. C.L.	, 22.	1 US	lumr	gal	
1.95	. ×	1.5	<b>::</b>	Designed Pur		_gal TOTAL VOI		rGFD:	3. D. gat
WATER QU	ALITY:	piw=		Transdace	r Actual Dep			***************************************	<u> </u>
Time	Volume Purged (gai)	DTW or Actual Depob	Temp PC1	Specific Conductivity (\$/cm)	Dissolved Oxygen (g/i)	pki (SU)	ORP	Terbidity (NTU)	Notes
					•••••				***************************************
i i i i i i i i i i i i i i i i i i i									***************************************
1401		114414	25.22						***************************************
		Line book and		*********************	Period and analysis of the second		***************************************		************************
						· · · · · · ·	ender was ender ende		***************************************
1-317						0.31			**********************************
	<b>Q</b> 5		40 20						******************************
1132			35.85				(1 7		MANAGER
									*******************************
			7(24)		andolesia di dela	7. X		21.5.3	**************************
	<b></b>	August and a second	7.11		makan darih.				•• • • • • • • • • • • • • • • • • • • •
		45774	the state of the s						·
		- X 3 - X ( 5)		1.1777	A A		- 64-3		**************************************
	<b></b>		VV. VV. 144. 144. 144. 144. 144. 144. 14	production of the state of the		africanisminini kanadanisming			
		Market and the second contract of the second		<u> </u>					
1539	13	V. C. V.	Equipa	ient Used				1	uipment ification #
YSI 556 MF: turbidits met	********	d 3563 Sende						<b>)</b>	61254

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet rist.

turbidity meter

WELL ID UST SAMPLE ID: OHO

### GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy-IPEC SITE: Buchsnan, NY WEATHER: FARM, SO'S F	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01 0017869.92 2 12 15 17 ft
---	--	-----------------------------------

WATER Q	CALITY:	prw	1 1 10 2		ocer Actua	l Depth	3.34	1	
Time	(DTW) or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen izd)	gH (SU)	ORP	Turbidity (NTU)	Flow Rate (gat/br)	Nutes
	7.0.1				<b></b>	<b></b>			
11125					<b>_</b>	<b></b>			••••••
10.28	<u>lrume</u>	<u></u>				<b></b>			***************************************
1222	1.4.03		2.293	لينتين	7.00	£	-5.4K		*******************************
1043		27.41	a	_a.sia	7.45	1_35_7_	4.41		**************
10492		2155	<b>2</b> .301		1.2.20	LSUS	2 - 1.100 APO **	8	************
1092	g de	<u> </u>				<b></b>			*****
	g								***************************************
<u> 053</u>	<u>l 1 ci </u>	2111	<u> 212 213 </u>						***************************************
1255	,,,,,,,	24/12	·	ં ્રે ઢે	L.D. 241	322	9:33		***********************
1103	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	27.73			227	31.4	3:13	Managanananananan	***************************************
110%			2.22.2		7.23	13/3	<u> Quy</u>		ląsi
uil		**********		0.25	3.33	77.41	<u> </u>		·
1113		2745	2.3.3.2.		************	***************	2.22		•••••
1173		27.987	2.343	0.23	******************	73.5			11544
1125	GIARI		iiiiii.i			<b>,</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
1134	LEWD S		224242	TICAL	LLX ()	<u> </u>			·····
	<u>L Pame</u>	er-	***********	******		<b></b>			********
			************	********	***				
			·····						**********************
			y						******************
			<b></b>		****				*********
			May'r i'a						····
			•		***************************************				
					*********				

Equipment Used	Equipment
Equipment Csed	Identification #
y SI 556 MPS Reader and 5563 Sonde	2
flow meter	2
ulificity meter	2027011113

NOTES AND OBSERVATIONS:

Total volume purged 1,415 gal

Doubh and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Edevation measurements are given in feet risk.

WELL ID: 016 SAMPLE ID: 016

### GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: SITE: WEATHER	Entergy - IPEC Buchanan, NY	7 1 yr F	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 
101 <del>1111111111111111111111111111</del>				
				print of the second of the sec

Time	DTW ox Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (s/l)	ρ <b>Η</b> (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
750	Sixil						M		****
023	5.477								••••••
0 135	Punc	<i>⊘</i> ∧	****		( <b>***</b>		************		***************************************
032	61.11.21	handii <b>200</b> 0 ka a mada a ma			***************************************	-48.1		2,0	
1042	5,004	21.12		<u>O.S</u>					******************
1048_	9.032	240.383	<u> </u>	0.43.		الناهد			****
10.20	Burne	ce.							***************************************
1002	Punc	27V					*********		***
10523	7.434		2544			الأعالات	1:41		***************************************
(0.525	15.950		2_355	O. The	7.42	-727	2.:29		***************************************
122	12.02.1	20.50	1362	S 36	t.i.		****		******
1123	\$	216.97	<i>2-35</i> 01	0.71	7:45		***********		لنصلشلس
	5 335	21221			Kanaga da	-42.7			~~~ ~~~
سوَّ لِنِن	Lance Harry State and States	26.71		1050	145	162.3	10.02		
122			re tom						······································
131	CN2 SAL	APLE L	Chassian		LI POY				****************
~	<u> </u>	ŒĒ	***************************************						
	*****************						***************************************		~~~
									~~~
									V-//
				***************************************				,	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
			/						
							*************		**********
***********	5	1	₹	•	}	2			

	Equipment Used	Equipment Identification #
1	SESS6 MPS Reader and 5563 Sonde	- 53
1	how meter	
tı	arbidity meter	

NOTES AND OBSERVATIONS:

Total volume purged 1445 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Translation of a series of the contraction of the c

erru.	Entergy - IPEC Buchanan, NY		F					017869.92 1081.69 11766 11		
NATER QUALITY: DTW = 7, 3°7 Transducer Actual Depth 30. 277										
Tiose	DTW or Actual Depth	Temp (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen 18/1)	р <b>Н</b> :SU)	OR <b>I</b> P	Turbulity (NTU)	Flow Rate (gabbu)	Notes	
Ours.	32.222					ļ	ļ			
	72411	5			<b>_</b>	<b></b>	ļ		<b></b>	
	12/2020	<u> </u>	************		<b></b>		<b></b>		******************	
						<u> </u>	<b></b>			
	】 ギ とかたんさ N		*************************			<b></b>	<b></b>			
		J4.38	N 116	^ory	7 7.7	366	174 .15	, i	72	
1456	31.746		2,110		forker en bereke en ber	***************************************		<u> </u>	<u> </u>	
	3/3/2					46.	12.5			
	2.421			1, 1477		- 17.9	Barr	***************************************		
	12122		harris Arghreil		<b></b>	<del>franciska</del> } }				
	3	lo l	**************************************					***************************************	<b>****</b>	
11700	31427	37.22	2465	2.2	7.2	35	7.53		******************************	
11/5	121.315	23.418	2.167	0.1 <b>.</b> )	43	34. 3				
1.20		2.5 49	3 166	3,00	731	36.7	2.28			
1, 5	NZ-186	23.47	2.112.	: 3,44	2.31	1.34.3	$1 \times 10^{\circ}$	***************************************		
Land	152.166	125.44			1.21	41.7	<u> </u>	****	***************************************	
325	32.101	12:43		2	2.32	122.3	162		*****************	
201										
	4.025			COwa.				*****		
			**********************		****************	*************			************	
	<b></b>		***************************************					A	•••••••	
								***************************************	***************************************	
<u></u>	<u></u>		••••••••••••••••••••••••••••••••••••••	L			L		****	
			Equipment	Used					oment cation #	
YSI 556 NO	PS Reader and :	5563 Sonde				high and construction		Į.		
thow meter			**************************************		· · · · · · · · · · · · · · · · · · ·					
turbidity ma	ter							5 5,500	21.277	

Groundwater Elevation measurements are given in feet and.

Of the first of the state of the stat

Total volume purged \_\_\_\_\_\_gal

IPEC00224980

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.



LIENT: ITE: /EATHER	Buchanan, NY		7	•	DATE: SAMPLE: PUMP DE		01.001780		ft
VATER Q	CALITY:	prw=	7.40			l Depth	43 6	7	
Tune	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Oxygen		ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
<u> </u>	41.099					•			************
1828							<b></b>		***************************************
	<u> </u>		**************************************				<b></b>		***************************************
		······································	, , , , , , , , , , , , , , , , , , , ,		************		<b></b>	, ,	*******
		<b>**</b>	2.166	100	1.03	201.14	14.54	4344 )	
	11232		194	1.51	7.1.3	1920			•••••••
		2 to 01	2.193	7.335		12:22	5.70	***************************************	***************************************
71110	177 461			7.449	7.24				***************************************
TIDS.	42961	24 %		17,32	7.33	1357			
1111	112.945				_7.35.	lle			
	Skit	X	لتلبلنك						
للمشك			<u>Caucib</u>		************				*************
	L BLUE		***************************************					······································	
~~~	<b></b>				~~~~				***********
	<b></b>		***************************************		***************************************				
****			••••						
	<b></b>		••••		••••••		***************************************		······································
******	<b></b>			***************************************					******************
*************	<b></b>		•••••					····	
			•••••	······			····	····	•••••
·····	<b>†</b>					*************			
***********		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						·	
•••••							Ì		*****************
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		***************************************				
			Equipmen <b>t</b>	Used				Equip Identific	
51 556 M	28 Reader and 5	563 Sonde						1	
ow meter					**************************************		I	5	
anidity me	irr							20070	>54

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater blevalion measurements are given in feet uist.

SAMPLE ID: OC7

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	14 40	<u> </u>	~	PROJECT NO: DATE: SAMPLER(S):		01.001786 <b>9.92</b> 1 ( ) 5	109 9B	<del>-</del>
SAMPLING INTERVAL (depth in R below top of casing)  SAMPLING PORT					TOTAL VOLUME PURGED:  2 S5 sal  PURGE RATE: Antigble (gal / min)  PURGE METHOD: Double Valve Pump				
Time 1345	Purged Vulume igal)	Temp (C) 1° - 74 P 160 - 18	Specific Conductivity (SiGM) (CAS)	Dissolved Oxygen (g/l)	ря (SU) Д. УЧ	082	Turbiday (NTU)	Drive/Vent Cycle (seconds)	Drive Pres (psi)
1402 1401 1425 1431 1436 1450 1459		16 01 15 99 15 67 15 54 15 16 15 16	2 235 2 235 2 225 2 223 2 223 2 223 2 221	6 1 5 64 5 44 5 46 5 39 5 39 5 24 5 24	\$ \$9 6 93 6 93 6 92 6 92 6 92	35 3 62 1 62 1 72 7 74 6 76 1	11.44 4.63 5.16 4.92 3.06 4.17		
1500		247\ 30MPU 10HP	in/xe	LE TES	111857	ICEC			
YSI 516 MPS Surbaidly group	Reader and \$562 Se		quipment Use	d				ment identifica	ition #

NRITES AND URSERVATIONS:

WELL ID MW 31 - 34	
SAMPLE ID: CC	•

CLIENT: SITE: WEATHER:	Entergy IPEC Buchanan, NY	4 405		-	PROJECT NO: DATE: SAMPLER(S):		01.001;869.92	0 <sup>9</sup> 1 11 <b>5</b>	~
SAMPLING E	NTERVAL (depth		of casing)		ME PURGED;	2.35 al/min) Double Vaive P			
WATER QUA	LITY:		Specific				\$555550 1551 1551 1551 1551 1551 1551 15		
13415 1351 1402 1402 1425 1439 1439 1439 1439 1459 1459 1459 1514	Purped Volume (gil)  CCCI CCI CCI CCI CCI CCI CCI CCI CCI	16.15.15.15.15.15.15.15.15.15.15.15.15.15.	Captuctisity  Skew)  COAS  3 C12  2 179  2 179  2 157  2 157  2 157  CCC	Dissolved Orogen g/1) 4 G 9 4 32 4 32 4 23 4 23 4 31 4 31 4 31	7 0 3 7 0 4 7 0 6 7 0 6 7 0 5 7 0 5 7 0 9 7 0 9	33 7 - 3 3 - 1 2 - 1 2 - 2 3 4 - 2 9 6 - 3 C 4 - 3 C 4 - 3 C 4	Turbidity (NTD)  J.J. 528 44.95 44.29 44.38 44.38	Oriver Vent Cycle (secretals)	Drive Pres (psi)
YM D6 MPS	Render and 156.1 S		38ipment Use	xi				nent Identifica	

STREET COORSERVERINGS

WELL ID:	MW	1.	<u> 192</u>
CARINEES	ь	00	7

200701254

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

Time	
Time Purged Volume Temp (°C) Conductivity Oxygen (g/h) pH (SU) ORP Turbidity Oxive/Veel Oxygen (g/h) pH (SU) ORP (NTU) Cycle (seconds) (SCm) Oxygen (g/h) pH (SU) ORP (NTU) Oxive/Veel (NTU) Oxive/Veel (NTU) Oxygen (g/h) pH (SU) ORP (NTU) Oxive/Veel (NTU) Oxive/V	
1345 COM CA CA 1986 5/8 1986 1986 1998 1998 1998 1998 1998 199	(ne Pressu (psi)
1433 1 2 15 93 2 722 3 73 1 1	
Equipment Used Equipment Identificati  1556 MPS Reader and \$563 Sonde	)H #

TTES AND OBSERVATIONS:

bidity meter

WELL ID: MW	<u> 194</u>
SAMPLE ID:	CMOIL

LIENT: TE: EATHER:	Energy - IPEC Buchanan, NY	<u> * 0344</u>	\$25 3		PROJECT NO: DATE: SAMPLER(S):	~~~	01.0017869.92 13.1.42 2.13.4	0 <sup>9</sup> 4.3	
AMPLING E	NTERVAL (dept)	in ft below top	of casing)		TOTAL VOLU	ME PURGED:	7,45	_8.8l	
AMPLING P	a partie de la cidade de la companya de la cidade de la companya de la cidade del cidade de la cidade del cidade del cidade del cidade de la cidade de la cidade del c			·	PURGE RATE PURGE METH		al / min) Double Valve P	ump	
ATER QUA					**************************************	***************************************		***************************************	
Time	Parged Volume (gal)	Temp ( <sup>5</sup> C)	Specific Cardoctivity (S/09)	Disadved Oxygen (#8)	pH (\$81)	(RP	Turbelis (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
11226						1774		3,32	7.2
105	2.5	13 13 15 15 15 15 15 15 15 15 15 15 15 15 15	4:66 6:3 7:733	<i>1</i> .5.1	Q: 11 T	-7477.7	3.41		

Time	Parged Volume (gal)	Temp (°C)	Caratocivity (5/cm)	Oxygen (#3)	pH (\$\fi)	(RP	(NTO)	Cycle (seconds)	(psi)
	()	TAME.						15.28	<u> </u>
	() 3:4							3,32	
1014		Colar.	<u> </u>		****				
11325		COMP.	200		ana a sanan andan andan andan andan a				
1120	7. 5	15.62	2933	4.5.1	. <u> </u>		ــ المناسبة	<del> </del>	
1134	2,.12	152144	2.047	1.73			32. 524	<u> </u>	
3335	3.7			7:00				•	
1150		- 3.3.}-	<u> Aga</u>	<u>, 4</u>			<u> </u>	<u> </u>	<del></del>
1124	1 1 1 1 1 1 1 1 1 1	19.94			7.07		14,23		
llci	9.12		7,153	2.17	7.04 7.06		<i>12.00</i>		
	13.35	15.43	2.051	2.28	1.00	184.1	31.16(2 3.25		
12.02		15.34	7.75.1 1.444	2. 76				<del></del>	***************************************
_1239	3.15	15 3 3	1.541	2.56	7.04	-13/25	16.32	· •	
1172		15,12	7, 14 1	7.47.	7.04	-1764	10 94 10 94	•	
	3.3		130	\$	7. 05	\$1.000000000000000000000000000000000000	5:45	<b></b>	······································
1239	13	15.23	341	2,30	7.06	-175.V -179.2	9.03		
13.40		19.30	2 713	7.355	7. 043	-172 3	1 m	der en en de en	
1.45	1.12	15.12		·	1				
12715	Linki	L Senson La			1276			<u> </u>	***************************************
	Light Line	OFF	<u> Salahan Balaban Balaban</u>	- Washington Construction (Section )					
		2						<del> </del>	
			<b></b>				<del></del>		•
Accordance and the second seco								•	
	,								
			<u> </u>			L	bararan da mananan da manan d		

Equipment Used	Equipment lilentification #
3 SSo MPS Reader and 5563 Soude	
E .	24 - 13 - 25 it 1

ITES AND OBSERVATIONS:

WELL ID: M	w <u>}</u> `	
SAMPLE ID:	63 Co J	

CLENT: SITE: WEATHER:		PROJECT NO: DATE: SAMPLER(S):	91.0017869.92 <u>11 54 じ当</u> <u>ご名,料 乃</u>
***************************************		WATER A THAT TAKEN THE	incep.
SAMPLING !	NTERVAL (depth in ft below top of casing)	TOTAL VOLUME PU	3.45 gal
	1605 to 1800	PURGE RATE: yar	iable (gal/min)
SAMPLING	PORT	and the state of t	
	183	PURGE METHOD:	Double Valve Pump

#### WATER QUALITY:

Fine	Paggot Volume (gal)	Temp (C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	ρθ (SU)	ORP	Forbiday (NTU)	Drawe/Vess Cycle (seconds)	Drive Pressure (psn)
84 / 34:			(*				*******		7
	0.05		1 1 7	101	3 47 S	- (13 X)			
10514		CUNSY .	C ( )						***************************************
1103		CHAIL	<u> </u>				*************************		
112.11	1.25	iu.ct	1/11/2	C 3.2		WELL	1.23	ļ	****
1125	175	112.0%	1 1164	0.1.0	?5	173.4	5:48	ļ	
1145	2.00	10773	1.10	<u> </u>	7:10		ــــــــــــــــــــــــــــــــــــــ		
15512	2.23	(5.97)	1,09 *5	<u>?                                </u>	7.10		7.13	<u> </u>	
(155	1.32	15.11	[ , 0 () <b>I</b>	2:10	7.10	. Litte	1.15	<u> </u>	
1301	2 350	75.50	1.089	2118	7.00	157.4	5.77		
1204	1.419	19.83	1.051	0.17	7.0 <b>8</b>		4.05	<u> </u>	
12.10	122.55	15.35	1,010	Qi	11	~ /54s_1	3.35	ļ	
13.152	2, 636	12.34	0.013	3.42	1:13:		3:11		
1218	1,75	15,54	1.052	, <u>, , , , , , , , , , , , , , , , , , </u>	2.13	-/5 <b>X</b> -G	3.74	ļ	
12%	12,35	[345b]	1.0.18		7:11	-1400	3.77		<u> </u>
1236	3.3	19.53	1.031	<u> </u>	7:11	- 144.4	1.3.23	<u>*</u>	7
1234	THEX	2.(1m2).c	ككفششتك						
1131	CAYD SA	halli E Ci	Landing all	1. J. J. 2.E.	<u> </u>	***************************************		ļ	
	T Zaadade	CFE					<del></del>	<del> </del>	
				************					
					************		<u> </u>		
		1						<del> </del>	
		ļ						<u> </u>	L
			<u></u>	L	<u> </u>			<u></u>	

Equipment Used	Equipment Identification #
SSI SSA SSBS Reader and 5563 Scade	1
nahidity meter	23.30.33.25.25.24

NOTES AND OBSERVATIONS:

WELL ID: MW	<u> 31. 19</u> 5
SAMPLE ID:	OOT

		* **	
CLIENT: STE: WEATHER:	Entergy (PEC Buchanan, NY Sevil A.C. Courts St. S.	PROJECT NO: 01.0017866-92  OATE: 11.32 C.3  SAMPLER(S): 52.53 14.63	
SAMPLING)	INTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURGED: 1.15 gal	
	377.0	PURGE RATE: yasable (gal / min)	
SAMPLING	(M)RT	IN THE PART OF PROJECT CASE.	
	<u></u>	FURGE METHOD: Double Valve Pump	
			730000000

#### WATER QUALITY:

T.190	Furged Volume (gal)	Femp (°C)	Specific Conductivity (S/cm)	Disudvat Oxygen (g/l)	ρΗ (SU)	ONF	Pubiday (NTU)	Drive/Vent Cycle (secondo	
10.36	()	Co. M.			<u></u>			12	: 2
		14		2.3	<u> </u>				3.3
1123.4			CCE		<b>-</b>	***************************************	***		
1105		RUMC	C) (4)		ļ		**********		
1112	0.15	17.21	148		165	2816		2/10	6.4
11114	10.01	17.2.4	1.919	ــــــــــــــــــــــــــــــــــــــ	1.4.93	294 0	145 201	<u> </u>	
11.32	T 15	(-1.87)	1.412	9.13	¥.15	2018	3,17	<u>.</u>	
1145	n 55	li wy	1.40k	<u> </u>	L. \$2. 18	274.42	34,74	<u> </u>	
1150		1735	1540 Z	6.35	4:13	221.4	7.62		
1135	0.16	_i7.74	12421	Q::(3	4.29	242.5	adia di bana	4	<u> </u>
ilgi	1031	13.52	1.402-		1.01	2775	2.46	ļ	
17.09	0.90			وبابا	3.40		2.49		<b>.</b>
1210	<u> 1095</u>			0.13	771	212:5		4	X
1214	31421	السمادك			ļ				
3.0 2	· · · · · · · · · · · · · · · · · · ·		LACATIO		3166			·	
	Pump	EP			<b>_</b>	ļ	********************	<u> </u>	
					<b></b>	<u></u>		- <del></del>	
					ļ	<b></b>		•	
					<b></b>	***************************************			
							****		
		<b></b>		****************					
					<b>_</b>			<b></b>	
							***************************************		
	}				Ł			1	

	Equipment Used	Equipment Identification #
VS	SI 556 MPS Reader and 5563 Sonde	
	Paskty meter	20070-254

NOTES AND OBSERVATIONS:

WELL ID: (1) (1) (1) (2) (1) (1) SAMPLE ID: (2) (1)

### GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy-IPEC SITE: Buchunan, NY WEATHER: (10 4 60 5	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 -11/10/09 -B, MB ft
-------------------------------------------------------------	----------------------------------------------------	-----------------------------------------

WATER Q	CALITY:	DTW=	. 22.380		ucer Actua	Depth	5844	Terroria Terroria	3000 3100 - 3107
Time	DTW or (Actual Depth	Temp } (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	рН (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/lar)	Notes
; 0 33.	15.73C	£.	MC ON					(danada o o o o o o o o o o o o o o o o o o	
1 53	15.137								
i > 1 3	(5.70)	18.14	1.150		7.62	115C ->	.,,,	*************	
	15.683	12.20	2 252 3	6.6.0	7.04	129.3	633.77		
1 1 2 4	15.420	18.46	2.2.24	506	1.03		6.53	w	0.01
7127	15 wil	12.64	Lacroscope and a superior of the superior of t	1076	7.13	832	8.62		
andreden die eerste verden van die eerste verden van die eerste verden verden van die eerste verden verden verd Lieuwen verden verd	15 603	2 34	2.284	A 80Z	1.17	182 2	7.24		C + 24
1 1 24 O	15-6-26	8 44		4.23	2.13	194 3	. Z. (:: C.)	***************	4.242
1150	14 645	18 M.I	2 292	(a. 5 x.	7.20	1350	7 67		C i _ i
	15 6.52	18 MM	2.293	4.60	3.22	35.3	7.50		0.34
1 1 2 4			I SAM	CLL	Sala Sala				
1302		223840	1	hCLE I	20		ICEC	***********	
363		POM			***************				
eggi e e e e e e e e e e e e e e e e e e			****		*****************		***		
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,									
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,									
								-	
					***				
***************************************								***************************************	
**********************									
***************************************									
***********									
***************************************									

	Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 So	nde	,
flow meter		200 101254
turhidity meter		K 1 7 1

NOTES AND OBSERVATIONS:

Total volume purged Q 44 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing

Groundwater Elevation measurements are given in feet and,

### GZA GeoEnvironmental of New York **Modified Traditional Purge** Sampling Data Sheet

WELL ID: MANY 63 SAMPLE ID: 013

CLIENT: SITE: WEATHER:	Entergy - II Buchanan.	NY				PROJECT N DATE: SAMPLER(		01:017869 <u>Wie/i</u> 	7/)	-
WATER COI	UMN HEIG	HT (ft)	25 32 DIW	22	37 C Water Col	े डे uma Height	Well Diam ft	eter: Diameter	Multipliers	in
	F WATER P	er weel vo 37. o∀		<u>), (() ()</u> Multiplier	. 2	Well V	olume	2 4 gal	0.163 0.163 0.653	
1 52	_ x	1.5	æ	2 28 Designed Pur	ge Volume	gal TOTAL VOI	LUME PUR	GED:	2.5	gal
WATER QI	BALITY:	DTW =		Transdace	r Actual Dep	th				
Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (5U)	orp	Turbidity (NTU)	Condition (S	] }e\
IALL		PAA		financia i i i i i i i i i i i i i i i i i i					************	~~~
	***********		غميد	1340	6.50	17.25	112.1	Accession of the Contract of t		**********
فينقينا	and the second second second		17.21	<u> </u>	5.26	17.08. 17.05	104 X	garacana a calabarana a		~~~~
ين في المالية	40.32		17.5	*****************	43	1303	1	5 6 6	Alabania (1900) di Romando (1900) di R	••••
H320			17.02	2 8 4 3	4 24	17.07		2339	*********************	***********
1322 1322	2. 52		16 38		74 i 2	17.08	los c	22.23		**********
1 3 2 24	223622222222222	May year o	646	2 3/43	3.9.2	7.69	ligy i	2.1.09		*******
11325		1	(°C (*1)	e ore						
1322			STAR			****************				
11336			LAM		LLETE	12 2	i. 1		******************************	
13.30			RUM	C OFF	<b></b>	***************************************	<b></b>			~~~
						***************************************	<b></b>		***************	~~~~
(*************************************			<b></b>			***************************************			***********************	*********
			<u> </u>							********
			l		<u></u>			<u> </u>		
	angen a papalaga a maganista a magana		Equipn	nent Used				8	uipment tification #	
VEL CEL II	DC Dander or	id 5563 Sonde		······································	····	55	A-4-1	7	}	
131320 M		the delivery of the				***************************************	***************************************	1200	10125	

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

turbidity meter

SITE: Buch	ergy - IPEC hunan, NY RALW - (2) E	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 1012.169 
------------	------------------------------------------	----------------------------------------------------	-------------------------------

ATER Q	DTW or Actual Depth	Temp	Specific Conductivity		pH (SU)	orp	Turbidity (NTU)	Dose/Veni Cycle	Drive Pressure	Notes
	***************************************		(S/cm)	(¥!)				(seconds)	1051 <u>1</u> 2.44	Hagai
135K	rume		/ 1003	135	~3,12,	26.9	· · · · · · · · · · · · · · · · · · ·	<u> </u>		,
1407	13.42)	15.45	//105	1.62	7.50	19. C	W.K	<b></b>		<u>                                     </u>
4447	13.516	142. 14	0.951		7/54		3,70	······		<b></b>
1477	13.510		0.364	7.72		-0.7	3.20	<b></b>	***************************************	· · · · · · · · · · · · · · · · · · ·
T-1.24	13.7V1	17.14		i i i i i i i i i i i i i i i i i i i	7.62 131	(m	3,14	<b></b>	************	1.1:0
1420	13.498	15.14	0.714	1.53	7, 14	<u> </u>	3.51	ļ		<b>!</b>
14155	12,511	بليتيا		<b>1</b> .23		Landonino Correrens	A M M M M M M M M M M M M M M M M M M M			<b></b>
1300	13451	للكوا	1.121.2	A CONTRACTOR OF THE PARTY OF TH	7.82	3.5	3 10 2.12		**************************************	1.5
120,2	13.400	15.70	1.013		1332	24	2.06		******************	
1500	19.419	15.11	3	garanian make si e e					**************************************	1.75
1915	13413	19.00		<u> </u>			2,5 <b>k</b>			
1514	STAPLE	Samo		K. Talax		T PEY				
1524	Section 199		E Can	CC(2/33).					*************	
*****	<u> Post</u>	LLEE.							******************	
************				<b></b>					***************************************	<b>.</b>
		ļ		<b></b>					~~~~	
					*******		****************	<b></b>		
						***************************************	••••	······		} }
					***************************************	••••				
					**********				~~~~	
							***************************************		~~~	
econtribution (Advisor		***************************************								
		ļ	<b></b>			***************************************				
***********			<b></b>						***************************************	

Equipment Used	Equipment fdentification #
YSL556 MP8 Reader and 5563 Sonde	5
arhidity meter	200161199

VOTES A	ND 088E81	ફે. ર ૅૅ	1() / A:
---------	-----------	----------	----------

Total volume purged 1.35 gal

Depth and Depth to Witter (DTW) measurements are given in feel from top of casing.

Greendwater Elevation measurements are given in feet and

 CLIENT:
 Entergy - IPEC
 PROJECT NO:
 01.0017869.92

 SITE:
 Buchanan, NY
 DATE:
 11/10/0\*1

 WEATHER:
 AGS(LY CLOUD!), 10/3
 SAMPLER(S):
 GB, AIR

 PUMP DEPTH:
 D.3

WATER Q	UALITY:	DTW =	15.73			Depth il.	<b>इ</b> न्ली			
.,,	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	рН (SU)	ORP	Tarbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (DSi)	Notes 60s
1209	11.200							0/1	1.2	
1222	11.192	านใ	4.944	3.02	602	1915		6/9	14	<u> </u>
1230	11,00%	10.52	4.4224	1.21	12 SS	1428		619	15	10.03
1240	11.001	17.66		0.54		12.7.4				00
1250	11.029	13.32	4.675	0.31	U-58	130 7	3.4/2			1.0.18
1300	10.921	17.27	4.475	0.13	V:38	112.1	2.99			0.23
1302	10 419	17.23	4.1/50	2.15	62.57	114.0	3.25			0.25
13112	10 964	17.22	9.657	0.10		1122	3.04			0.28
1315	10.95%	17.27	4.425	دين ۵		110.1	3.17	*	*	C.40
1311	57821	Silmi	LE COLLE	Kili Chi.					***************************************	
1410	CND SA	mplc	COLLEL	Was is	4 186		*************		***************************************	
	Phase 3	E.C.								<b></b>
									***************************************	
					•••••	***************************************			977777 1 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	<b>6</b>
			~~~~		~~~	~~~			***************************************	
									<b>A</b>	
					**********************				****	
					<b></b>			***************		
							***************************************			
									****************	
			and the state of t							
		ļ							**********	
			MANAGEMENT						ennonno - es es expensión con con	
			**********************		\$-#500mmar-c-c					
					harden de de la companie de la comp				************	

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	-5
turbidity meter	2001042:3

#### NOTES AND OBSERVATIONS:

Total volume purged 2. 2 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing. Circumdwater Elevation measurements are given in feet nisl.

WELL	ID:		
SAMPL	E ID:	013	

CLIENT: Entergy (PEC SITE: Buchanan, NY

WEATHER MONCO (LOUDY, 605

PROJECT NO: OATE:

OATE: SAMPLER(S): PUMP DEPTH: 01.0017869.92

WATER QU	JALITY:	DTW =	16-13		cer Actual	Depth 3	5. 136			egoverna naconomica de la canada
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen 15/l)	<b>рН</b> (SU)	ORP	Turbidity (NTU)	Drive/Vens Cycle (seconds)	Drive Pressure (psi)	Notes Cycl.)
1003	35 851	PUMP	<u>. 20</u>	~~~~				V13	20	<u> </u>
1006	35/101	14.68	2.780	<u> Palici</u>	6.32	1403				<u> </u>
1015	3/5.127	16.46	2.994	2.41	10.16	1334	(21.37)			015
10 25	35.112	ાઇ ેંડે	3000	2.90	W 75	1532	34.76			1025
10.35	3/910/95	10.30	3106	2-26	V-14	1677	30 22	*		LØ.50
1045	35 199	16.33	3 (12	2.00	provide the second of the second section in	****	20.55	62/12	23	0.75
1055	35.507	10.54	3.433	i. Ic	12.13	1974	17:15			1.
1105	39.943	ાહ⊹ે\	3107	1.88	¥.13	2245	17.32			1.25
1110	3-9.5041	112 95	3 105	190	<b>v</b> .73	217.0	development francisco			1.3
1115	30 00		_الاستادات	1.94	6/13	1245	9.83			1.4
1120	33,943	16.99	<u> 3.191</u>	1.93	0.74	224.0	10:22	*	<b>.</b>	1.35
1123	\$7#£1		ELIZZES	Silver S. A. Sent Sales		<b>,</b>			***********************	••
1102	ENDS	AMIPLO		ILDAL.	22 11					
Andread Control	Pump.								***************************************	
}										
y.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,									****************	
·										
				***************************************		<b>\$</b>			*********************	
					***************************************				******************************	
										***************************************
				***********				······	***********	
									**********	
	***************************************								******	
									************************	
					***************************************					
			**********		A. 1/1/1/17 - M. M. 1/1/17 - 1 - 1 - 1 - 1					

Equipment Used	Equipment Identification #
YSL556 MPS Reader and 5563 Sonde	4
turbiday meter	20014293

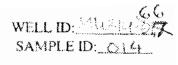
NOTES AND OBSERVATIONS:

Total volume purged 1. 1 gal

Depth and Dupth to Water (DTW) measurements are given in feet from top of casing.

Groundwater filevation incasurements are given in feet inst.

### GZA GeoEnvironmental of New York **Modified Traditional Purge** Sampling Data Sheet



CLIENT: SITE: WEATHER:	Entergy - IF Buchanan, I	NY ,	3 \$			PROJECT N DATE: SAMPLER(		01.0017869 11/5 CO, N	101	
WATER COL	UMN HEIG	HT (ft)	57.93	) =	7.0	7	Weit Diam ti	eter:		in
	DTB		DTW	<u> </u>		unuo Heig <b>ht</b>	, 11	Diameter	Multipliers	
CALLONS O	F WATER P	ER WELL VO	LUME:					2	0.0 <b>41</b> 0.163	
				0-163	-	1,47		<u> </u>	0.653	
Water Co	dimo Haght	-1.02	. ×	Meltiplier	,	Well V	olume	gal		
: with		£.5	120	2, 2	9	gal				
1,241	_ *	1.2	••	Designed Pur		'Sar				
						TOTAL VOI	JUNIE PUR	GED:		ដូររ}
WATER OF	MATTY	DIW =	<b>,</b> 1.4 <i>3</i> 0	Transduce	г Асныі Эер	dr 6.54	L			
10.41.00	Vislamo	DTW or	Temp	Specific	Disastred			Larbidity	P. E 550	5 C
Time	Parged	Actual Depth	3	Conductivity (S/cmi)	Oxygen (g/l)	pH (SU)	ORP	(MTU)	Notes	
1130		EVIA	6 00	· · · · · · · · · · · · · · · · · · ·	3371	-				<del></del>
1135	1001	6 5 8	1 (37)	3 110	S 2 8	6 55	229.0		6/6 (8/2	, C.
1140	0.05	3.944	6.60	3 (11)	14 13	7.34	2351	***************************************	harring and the same and	Samoran
1145	10 10	5 58%	16.31	2 16 3	4-67	6 51	2317	10.13		
1153	0.20	5.711	10:51	2.491	5.21	10.10	251.1	7.412		
115%	10.25	4.512	14.25	2.450	5.13	<u> </u>	2349	3.20	L	
12:201	0.30	4.594	16.32	2.394	5.53	<u> </u>	2347	2.74		
1111	T ø-50.	1.18%	16.37	2.36.1	2,51	691	234-7	2.11		
ilia	0.15	3.351	10 M	2.339	5.76		<b>23</b> 55	2.3.7	ļ	AMAZONIA A B. B. B. B.
1224	10.95	3 30	14.53		<u> </u>	7.01	23:14		<b></b>	
1234	1.051	3,000	. لايتانيا	2.30	422	ZuH	2347	210	<b></b>	~~~
1245	1.15	12.017	10.48	2, 2,65	<u> </u>	7.07	23/22	4.70	<b></b>	***********
17.55	11,17	2.112	<u> </u>			3.68	235.4	**********	<u> </u>	······································
1305		-1.149	الإربارا	2.265	<u> </u>	1.12	235.5			
1315	1.46		116.19	2 202	5.95	7:41		10:52		**********
1325	11.425	i digi a mang ang ang ang ang ang ang ang ang ang		2.350		1 1 1 2		540		
1535	1.8-5	1.712	18:25	2,251	5.35	2.44	748.3			
			Equipa	nent Used		·····		,	uipment tification #	
YSI 556 MI	PS Reader an	d 5563 Sonde			***************************************		· · · · · · · · · · · · · · · · · · ·			
mebidity me	ter							2000	264293	3

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (OTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet mst.

1335 Audically College Dick Grouped Published. 76 Audical Occus to Scientification of S

# GZA GeoEnvironmental of New York WELL ID: 14044 15 **Modified Traditional Purge** Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IF Buchanan, I					PROJECT N DATE: SAMPLER(		01.001786 	).9? <u> //                                   </u>	··
WATER COL	CMN HEIG	HT (ft)	(24 S) DIW	126	Water Col	ି () umn Height	Well Diam n	eter: Dianwter	Multipliers 0.041	in
GALLONS O	F WATER P	ER WELL VO	LUME:					2	9.363	
Water Co	siumu Height	37.01	, x	A. Collinson	. =	1252 Weil Vo	dume	gal	0.653	organia Company
	× X	1.5	<b>2</b> 3	Orsigned Pur		.gal TOTAL VO	£00.48° \$98 \$8	ero 2	. <del>45</del> 0	ટ્રઢાં
WATER QI		DIW::	·		r Actual Dep			ş		adino <b>a</b>
Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTC)	Notes	~~~~
44.2				~~~	********		***************************************		0000000	
	262					and the same of th			************	~~~
	1	<b></b>	11/2/11		442		1723.1 173.3	2704		
		<b></b>	100 400			4			**************	Market e e e,
	1.1.2		1244				111111	1625	*******************************	******
						7.41		laran	***********************	
	32									******
			-			<b>7</b> 23			******************	*******
									***************************************	*****
				***************************************	************************	<u> </u>	******************		VIII. 1. (1. (1. (1. (1. (1. (1. (1. (1. (1.	*******
vvvv						***************************************				********
*************		<b></b>	4	***************************************			******************		Win and the control of the control o	
· · · · · · · · · · · · · · · · · · ·					***************************************					
									***************************************	ANALONI-
***************************************										
			Equipa	nent Used				lden	uipment tification #	1
YSI 586 M	***************************************	d 5563 Sonde	***************************************		· · · · · · · · · · · · · · · · · · ·			7	· 12 2	

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet mil.

# GZA GeoEnvironmental of New York WELL ID: A (1045-40) SAMPLE ID: 018 **Modified Traditional Purge** Sampling Data Sheet

	Emergy - 11 Bachanan, 1 Pagaray	NΥ	<u>wo</u> śF			PROJECT N DATE: SAMPLER(		01.0017869 11/15/2	<u> </u>	•••
WATER COL	UMN HEIG / / // DTB	HT (ft)	24411 DTW	=	Water Col	्र umn Height	Well Diam ft	eter: Diameter	Z Multipliers	-in
GALLONS O	F WATER P	ER WELL VO	LUME:					2	0.163 0.653	1
Water Co	luma Height	<u> 17. Si</u>	. ×	Mudtiplier	: <u>:</u> :	2, 9; wai v		āul		.3
2.412	•	1.5		니 3 S Designed Par		gal TOTAL VOI	LUME PUR	GED:	3.5	gai
WATER QU	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	prw = {				di /6.97	2.2			
Trave	Volume Purged (gat)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen (gd)	pH (51.)	ORP	Turbulity (NTU)	Notes	
0854		(1000)							5.2.7.	234
12231	10.5					111.75			} ************************************	~~~
			الإندارا		بتبيي		<u> </u>	52 SX	***************************************	***********
10412			12.14	4.1	034	1116	19.3		*************	*******
	120.	<b></b>	17 14	0 480	garantan da kanan ka	1	1 <u>2 6</u> 23 0		***********************	***********
<u> </u>	123		13 94 13 93	6 444	059	11 22	23 C 25 C	753 263	*************	********
122.2.3.	<u> </u>	<b></b>	Trick Control Control		<u> </u>		25	374		*****
<u>  12 X</u>			18.35		<u> </u>		26 7	44.77	W 4, 4 4, 4 6, 6 6, 6 7, 7 7, 7 7, 7 7, 7	
0111					2 2 5	11070		5333	***************************************	
0436	<u> </u>			Aass	4,1,3	Strategers of	· · · · · ·		·····	6 1 5
154.3	·		Vac Vo			******************************			jania della esta especialista de la composicio de la composicio della comp	.3
144	***************************************	***************************************	LIAL	C SAMPL	E COC	ECTION	2		VV-1.444.00000	
1449		***************************************	CAMO			1 2 4	INE		*************************	~~~
12.44			CLAN						******************	N0000000000000000000000000000000000000
	1	1	}			L	L			
		12012 2 3	Equipn	nent Used					uipment ification f	<i>‡</i>
TYS1 556 MF	S Reader at	d 5563 Sonde					***************************************		>	

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing Groundwater Elevation measurements are given in feet msl.

turbidity meter

# GZA GeoEnvironmental of New York WELL ID: MINGS-GO Modified Traditional Purge Sampling Data Sheet

SAMPLE ID: 018

CLIENT: Entergy- SITE: Buchanan WEATHER:	.NY 🚬 🤟		-		PROJECT NO: DATE: SAMPLER(S):		192 10°1 ИВ
WATER COLUMN HEI	GHT (N) 	4.90	×	36.10		Diameter:	in
DIB	<del></del>	DTW	• ~~	***************************************	umn Height	Diameter	Multipliers 0.041
GALLONS OF WATER	PER WELL VOL	UME:				2	0.163 0,653
Water Column Heigh	21.25	x	Multiplier	æ	ا زو ۶ Well Volume		0,12,03
1. 23 Y x	1.5	<del>#</del>	2 2 2 Designed Purg	e Volume	<sup>*</sup> fal		
				***************	TOTAL VOLUME	PURGED:	gal

VATER QI	ALITY:	DIW:		Transduce	r Actual Dep	th			
Time	Volume Purged (gai)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (5U)	ORP	Turndity (NTU)	Notes
1261	0			erra a a a a a a a a a a a a a a a a a a	******************	***************************************	AAAAAAAAA	***************************************	en e
1207	0.04		11223	0.212		13.53		1113.	<u> </u>
1210	0.25		12.11		23	7.35.	212.1.	Property and the second se	وروروا والمالية والمتحدد والمتحدد والمتحدد
1213	63.70		2.2	1.024	- 3 J.	7.73	1112	157.2	**************
1. 1. 6	0.70		3				2446	346 8	0000000 a a a a a a a a a a a a a a a a
	090		: <u>9.21</u>	116	3.65.		2 3 8 3	3.62 3	***************************************
223	1.20	New	\$ 30	1.143		766	296 9	352.4	
	1 50		13.44		3.23		2416	4980	•••••
2.33	11.30	,	18 53		3.23	1764	230.8	<u> [4718]</u>	
2 39	2.0		18.51	1.233	100	7.64	2203	5927	
3243	12.2	20.0	18.54	1241	2. 23	7.69	2114	537.4	
1 2 2 4			STAR	T SAM	V.E. 1323	LEC No	ed.		
de discondinamento									
20000000000000000000000000000000000000	***************************************								
	1								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	.3
	206704293

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing. Groundwater Elevation measurements are given in feet msf.

			***************************************
ZA GEOENVIRONMENTAL OF NEW YORK	Client	WHEEP MAD 45 -	\$2.1
40 MINTH AVENUE, 18th FLOOR	* Entergy	399997 133198	
EW YORK, NEW YORK 10001	Indian Point Energy Center	FILE NO. 93 001798	8.92
CIENTISTS AND ENGINEERS		PROJECT LOCATEIN TRÉMIN P	(A) N
**************************************	PSICAFACHY ~ (	DATUM , MSE,	***************************************
engracionen in Situ			
Roy, Frank 3 8 8 8	SERIAL NUMBER	C OATE MA ON	***************************************
	CASING DIAMETER (INCH)	····	
un enomiem <u>CB MB</u>			
ELEVATION OF MEASURING POINT - DEPTH TO WATE	R = REFERENCE ELEVATION (WATER TABLE	ELEVATION)	
DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGT	H (It trænsducer is functioning properly)		
	3	CABLE	
Casing above (+) of Below (-) Ground:		CONNECTOR	
DISTANCE FROM CASING TO GROUND (+ OR -):	) <u>~ i</u>	1	
MEASURED CABLE LENGTH:	**************************************		
	and the state of the state of	* <b>!</b> * !	<b>* *</b>
elevation of measuring point:	55211 Frast	GROUNQ/	
DEPTH TO WATER:	- 14 590 9	SURFACE 2	
REPERENCE ELEVATION:	= <u>28 32 1</u> FTASL		
	\; 3 € нев	WATER V	
TIME OF MEASUREMENT:	TOC	TASLE	
Measurement Taken From:			
DEPTH TO WATER:	24.310 F		1
ACTUAL DEPTH:	+ 4.3740 #		الس
THEORETICAL CABLE LENGTH:	FY		Cia estea
Chicone		CABLE	O 50
	check	1 15	
HAVE CLOCKS SEEN SYNCHRONIZED?	5222222 /		
IS TRANSDUCER SET TO TAKE "SURFACE" READING	E CONTRACTOR CONTRACTO		
TEST NAME:	Miller 45 45	PRESSURE.	
LOGGING INTERVAL:	<u> </u>	THANSOUNER	1
TEST START TIME:	<u>il 3°4</u> HAS	* *	¥
		SENSOR	
		WEI3.	1
		SOSTOM	ĺ
			*
EGENU OTW DEF TO WATER			
DTB - DEPSH TO SOTTOM OF WELL			
AD - ACTUAL DEPTH OF TRANSOUGER U	DER WATER		
CL - CABLE LENGTH FROM SENSOR TO C	ACUNO SURPACE TOP OF CASING	•	
PROSESS: NO.	1. 2 2.2 2 3		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
MOTES: Tromphones of)	2 - 2 4×1 L	South 1	
1			
GZA		WELL O ENGLY 45 4	

### GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MILLE (F

CLIENT: SITE: WEATHER:	Entergy - II Buchanan,	NY				PROJECT N DATE: SAMPLER(		01.0017869 	2	<u>.</u>
WATER COL	UMIN HEIG 24 1 DTB	HT (ft)	<u>4.05</u> ptw		2.5.6 Water Col	⊃ umn Height	Well Diam fi	Diameter	Abltipliers	in ]
		25.65	LUME:	0 653 Modiplier		16,75 Well V	olume	4 gul	9.163 9.853	the state of the state of
14:15	. x	1.5	=	2.5.12 Designed Por	***************************************	gal TOTAL VOI	.UME PUR	GED: 2	5.45	gal
WATER QI	ALITY:	DTW = 4	1.65	Transdace	c Actual Dep	sh 23.76	K			
Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Disselved Oxygen (g/l)			Turbiday (NTO)	Notes	
Ilai		23:131	Lawi							POTTE CANADA
حثهنا	ــــــــــــــــــــــــــــــــــــــ	123.125	4.2	0 000	0.429	1126	- <u>24.1</u> -199.7	3 . cv	erricus escaparatorio de la escap	***************************************
1114	13.15	10.091	<u> </u>	0.1413	(1.3,2		-177.0	9.43		**********
1130	7.2	14,450	4.3	***************************************	0.21	1778	187.6	herenness and the second		***********
1142	115	111, 721	(1.510	6237	044	7. 31	-1460		********************************	
1215	150	13.246	24.3	0440	1:1:15	7.75	-47.7	4/3)		• • • • • • • • • • • • • • • • • • • •
1233	18.8	19,015	1132	4.114	3.60	7,746	-1.0.1	1.53		
1249	12.00	7.043	1173	làua	4.15	17.13	-:4.7		errandonos este errandonos	********
1300	24 0	12040	19.31	WWW. CONTRACTOR CO. C.	440	17.72	- 36 2			
1314	125.74	12.015	19.75	L. Curi	4.74	7.72	* 22.2	3.43		
1775	<u> Statë</u>		LE.L.	LL XX III			•••••		***************************************	***********
1324	***************************************	<u>Dinul'e</u>	خنتك	t C Cox	14135	<u> </u>		**********************	(A SANDONO CONTREBANÇAÇÃO CON	
	<u> Print</u>	lore				<b>}</b>				**********
					******************		******************		erene er er og af hande er er er	Y********
	1	.1	<b></b>		<u>.</u>	1		L		***************************************
	110-10-1		Equipo	nent Used				,	uipment ification f	<b>‡</b>
YSI 556 MI turbidity me		id 5563 Sonde					Mark Myster (Charles Control of the	74076	71293	

#### NOTES AND OBSERVATIONS:

Depth and Depth to Woter (DTW) measurements are given in feet from top of casing.

Unroundwater Elevation measurements are given in feet mst.

# GZA GeoEnvironmental of New York WELL ID AND 192-78 Modified Traditional Purge Sampling Data Sheet

SAMPLE ID: DIH

CLIENT: SITE: WEATHER:	Entergy - IP Buchanan, i	٧Y				PROJECT N DATE: SAMPLERO		01,0017869 101.27 278-14	<u> 2109                                     </u>	
WATER COI	UMN HEIG	ዘፐ (ስ)	39.98	22	45.	ζb	Well Diam ft	der:		រព
	ртв		DTW		Water Cole	ımıı Height		Diameter	Muitipliers 0.041	
GALLONS O	F WATER P	er well vo	LUME:						6,163	
Water C	olumn Height	45.62	*	Multiplier	<b>\$</b>	1.75 	dema	gal .	(),653	
(.85	X	1.5	=	Designed Pur		gal TOTAL VOI		sged: 2		gal
WATER Q	HALITY:	prw=¥	162	.48 5 Transduce		n 13-51	***************************************			8
Time	Volume Purged (gai)	DTW or Actual Depth	Temp ("C)	***********	Dissolved	***************************************	ORP	Turbidity (NTU)	Notes	**************************************
1312	Dump		********	······		-2 -2 43	:2 *		************************	**********
1343.	ļ Çil	igaava.	- 14. N.	2100	4.32	1,39 7,23	323	20151	Carante de la composition della composition dell	~~
1348	44.20		110.00 10.00	2.173 2.165	4.38	7,2-1	351. 950	***************************************	errorran e e e e e e e e e e e e e e e e e e e	
	<u></u>		.132:25. }{}};}	<u> </u>	3.33	7.21	X93			~~~
1.57	2.5	A A A A A A A A A A A A A A A A A A A	10.00	2.15.3	3.00	7,20	35/4	301.5	***************************************	*********
13,5%	سردددددونون وروال و و و و و و و و و و و و و	42-44	1(2.00		2.30	7.14		3245.60	*********************	********
	12.35	Sanvî.		. (2. 11.28.)						*******
140%		1 28 0 1 P 1 C		ekanaazika. Ekai kom	11 12	<i>d</i>	************			
	1 END	3			estidone estado.	3	8000-11 BBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBB			*********
	Throng	<u> </u>		····	*************	******************	( <u>0,000,000,000,000,000,000,000,000,000,</u>	************	de de la composition della com	
·						***************************************	\$\$\$\$\$\$\\ \tag{\tag{\tag{\tag{\tag{\tag{\tag{		***************************************	******
				***************************************			************	<b></b>	MACCOCCUS - 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	
							*****************		0.000.000.000	*******
							\$0000000000000000000000000000000000000	<b> </b>	************************	,000000000
<b></b>		ļ		parentes						********
L		.k	3	<u> </u>	h	doe		5		
		A SSET Canda	Equipa	nent Used				} -	nipment ification #	
tarbidity m	2222200	d 5563 Sonde					·			

#### NOTES AND OBSERVATIONS:

Depth and Dopth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet rost.

CLIENT: Entergy - IPEC SITE: Buchanan, NY WEATHER: SKIN NY - 500 SF	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.00)7869.92 <u>お行行で</u> <u>さられいる</u> <u></u> 作
---	--	---

VATER Q	UALITY:	prw =	10 69	Transdu	cer Acmal	Depth				
45.5	DTW or Actual Depth	Temp ("C)	Specific Conductivity (SA:m)	Dissolved Oxygen iz/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vegt Cycle (seconds)	Drive Pressure (1951)	Notes
1117	10.77	***************************************	2 0 v						•	<b></b>
117.3	10.39	<u> </u>		1.32.	1.25	425.2.			*************	<b>}</b>
11 3/2	11.02	13.03	<u> </u>	LLYW.	7:12	4010			***************************************	<b></b>
<u>una</u>	11. 15	12.37		4.35.	2::11	3994	(***************			ļ
168	111/1	17.17	_2.001 <u>.</u>	18	245	3:12:11		······································	*********************	
1203.	11.2.1	القائلا		1.33	145		<u> </u>		****************************	
12.0%	11.21	<u>ile l-T</u>	2 - 414	1.44	Tillia		(44)			<b></b>
1213	11023	#3T		<u></u>	.7.L.k	3333			VIII.	
1716	11.242	15.53			1.11		0.00		~~~	
1113	11.20	19.64		2.13	3.16				·//**	
1775	11.34	isili	2.11.5	0:34		_3_234			*****	D. 75.
1235	11.35	19.00		0.972	241	3703			~~~	0.75. J. 150
1234	TSTART	SAN			<u> </u>				*************	
1114	[6x.D.5x	mille		IIIN	25.52	53			*****************	***************************************
n fan i Badereen en in oan	Marie Company	OFF.	***			***************************************			******************	
AND BEEFER OF CONTROL CONTROL CONTROL					********		*********			<b></b>
******************				<b></b>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	*****		****	******	
***************							***************************************		·	
	-								~~~	
handa al- e el e a a d'altre de la estada de la elementa del elementa de la elementa de la elementa del elementa de la elementa del elementa de la elementa de la elementa del elementa de la elementa del elementa del elementa de la elementa de la elementa del elementa del elementa de la elementa del elem										
	·••••••••••									
									**********************	
		\$						*****		•

Equipment Used	Equipment Identification #
YSL556 MPS Reader and 5563 Sonde	5
turhidity meter	200704293

NOTES AND OBSERVATIONS:

Francisco ACTEP A Total volume purged <u>0.75</u> gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing. Groundwater Elevation measurements are given in feet uss!

CLIENT: SITE: WEATHER	Entergy - IPEC Buchanan, NY Santon 4, Shora F	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 10.125.165 65.168
		1 1/2/24 1/2/24 2 1 1 2	***************************************

WATER QI	ALITY:	DTW ::	10.90			Depth /(	o. 239	(3.50 Z	in)	~~
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (5/cm)	Dissolved Oxygen (g/l)	p <b>H</b> (SU)	OSP	Turbidity (NTU)	Flow Rate (gat/hr)	Notes	
3175	1 <i>n</i> 90		*************************************						***************************************	
1117	16.254	Phison				<u>.</u>				J
1128	IO-14X	15.24	2.003	1.71	1.22	1515	2.99		<b></b>	
1138	14.10.2	18.98	2.052		1.13	1981	<u> </u>		······································	
1143	10.141)	13.32	20011	0.66	1.30	139.3	3	****************		
11 58	14.00	19.30	2267	12.0	1.31	/35.3	42.20		***************************************	
1203	153.4980	19.20		0 & 5	130	135	10. QV			1
1704	15.742	<u> 19. C</u>	<u> 1 oun</u>	L O.WA	يشيد	132.4.		••••	***************************************	
1213	15.923		<u> </u>	<u>                                     </u>	130	1345	2:00		***************************************	
1218	15.942	13:30			? <u>;</u>	<b>**************</b>	التوكيدية		~~~	4
1223	<u> </u>	15.21	*************	1	1.30	<del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>				1
12.1%	13570	13.18		0.02		132°X	<u></u>			1.45
1233	Diagr	y	الكالمالية الكالمالية	4	***************************************	<b></b>	***************		~~~	1 .
12024		HWILL	ELLSTLLE	L.T.I.Zi.,		IFE			·····	
	Tung :	LE		ļ					*************************	,
	<u></u>								*****************************	1
	<b></b>			<b></b>				************************	*************************	1
	<b></b>					<b></b>		~~	******************************	
			<b></b>							1
			******						Managanananananan	Ì
							••••••	**********		
	<b>.</b>									
								*************************		
			***************************************					************		
		<b></b>								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
New inster	3
turbidity meter	200701263

NOTES AND OBSERVATIONS:

Total volume purged 1.35 gal

Daprh and Depth to Water (DTW) incosurements are given in feet from top of casing

Coundwater Elevatara measurements are given in feet aid,

CLIENT:	Entergy - IPEC	PROJECT NO:	01.00 <b>17869.92</b>
SITE:	Buchanan, NY	DATE:	
WEATHER	: <u> </u>	SAMPLER(S): PUMP DEPTH:	<u>a a la </u>

WATER Q	CALITY:	DTW =	11 05			Depth 1	SOIS	(2,062	V.a.)
Time	DTW or Actual Depth	Temp ('C)	Specific Conductivity (S/og)	Disselved Oxygen (g/l)	p <b>H</b> (SU)	ORP	Turbidity (NTU)	Flow Rate (gab/hr)	Notes
1112	16015	****							
	, , , , 000	DUND	Paal		***************************************			******	****************
117.2	14.712	14.44	0.34¥		1.24	1.266.1		*******	*******************
1128	4 9 44	<u> 15.71</u>	<u> </u>	2.15	1.14	1224.2	4.57		
2FIL	14.752	14.13.	1.240	3.13	121	ilu 1	2.98		
153	19.02	1302,	1.323		1:20				***************************************
7003	19736	13.84	11931	سلتمثي	7.27	7.51	~~~~~~		*******************************
1108	14,730	342	1.334	3.72	121	عندتينا	<u> </u>		******
77.3	14.736	y	1.233	3.33	7.7.1	210 u		***************************************	*********
1218	5	1316	1132	<u> </u>	1.33		<i>Q-0</i> 22		
1222	13422		1.138	7.43	7.29	2435	Vigia		المهجتنكت
1124		Same					····		.,,
12315	<u>Lavos</u> n	14111LG	<u> </u>	MAYAA	24 L. L. S.		po		*****************
	<b></b>								******************************
		<b>.</b>							***************************************
			*************	*******************		<b></b>			***
						****	***************************************		***************************************
<b></b>									**************
<b></b>		<b></b>							***************************************
<b></b>	<b></b>						***********		
<b></b>									
<b></b>	<b>.</b>								
<b></b>			****************						*******
					****				********
		L		L					

Equipment Food	Equipment
Equipment Used	Identification #
YSI 556 MPS Reader and 5563 Sonde	
flow meter	
(groidity meter	200764243

NOTES AND OBSERVATIONS:

Total volume purged (2/10) gal

Depth and Depth in Water (DTW) measurements are given in feet from top of carsing.

Caromidwater lifes atten measurements are given in feet insl.

		3 M.			DATE: SAMPLE: PUMP DE				ñ
vater qu	ALITY:	DTW =	743			l Depth 💍	3 674		
Time	DTW or Actival Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen te/f)	p <b>H</b> (SU)	(RIP	Farbidity (NTU)	Flow Rate (gal/hr)	Notes
1001	7 63 7								******
		Δ	***************************************	<b></b>	<b></b>	<b></b>			Maria de la compansión de
		200			1				00000000000000000000000000000000000000
	7 4 5	المنشانين	3 3 542	L.i26		1:36.2.	71 14 41 14		**********
T) > 1		21.61	3211	1.44		<b></b>		*****	
0.10					سمسس				
242		21.3		3.3.1				~~~~	
		11.12	1 12 1	2 23	2.23	33.	11 Y 12		*****
2.4.4	100 Higgs	.v 4 - 23		0.44	7.32	-25.6			
	7 45	0.00	2 75%	7.71	2. 14.	- 2, 3	7 Y		
	ana daga maghatha a sa				2.47	(- ). Y			
			3.366	1.114	i i i i	<	4.01.		
	7 7 7				147	9.)	(f. a 1		
	7 (2 7 7 (2 7 7 ) 2	21.43	3.250	350	2.10				
/ 2 1 7	7.45		> 350	1.79	7.53	50.57	. A 74		************
	7.19	77.35	1 7 74	0.4	350	<i>A</i>			************
	1,637	73 5 d <b>§</b>	3 397	). TY	7 73	jg	A Special		
	7.332			3.25	:	7.3	3	***************************************	\$60000000000000000000000000000
	Can in S	, j (j	422640	20,70	21, 13				A0000000000000000000000000000000000000
	7 / J	:5 <u>0</u> 2						***************************************	A ANDRONOS CONTRACTOR AND A SERVICE OF THE SERVICE
	i dali minda mada m		······································	gender vilke eksemmen och	******			***************************************	, in the property of the state of the second
					***************************************		***********	**************************************	
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		*********			***************************************	
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						· ·	Lancock Color of the Color of the Color
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			errolen de la		******		×		entre el el deserve en en el entre el estado.
	<u></u>	l	<del>liken er er it blike forse</del> n och för och före er er	te e e e e e e e e e e e e e e e e e e		hamana ay	ha a a a construence de la construence		
		THE WALL STREET	Equipment	Used		nganaganan and madaphin y y y y y y ganganan		Equip Identific	ment ation #
VCI SEC VIX	S Reader and S	S63 Sonde			· · · · · · · · · · · · · · · · · · ·				
*********	S M.S. SERVER WELLS.	ANALYS OF THE PROPERTY OF THE						4	
flow meter arbidity me						***************************************			N. j. cr.;

Dogah and Depth in Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet nist.

IPEC00225003

WELL ID: 1445 CG SAMPLE ID: 144

### GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IP: SITE: Bachanan N WEATHER: 2003		DAT SAM	TE: !PLER(S):	1.0017869.92 	řt
			**************************************		<del>2000-00-00-00-00-00-00-00-00-00-00-00-00</del>
WATER QUALITY:	orw ≈ 1	( ) Transducer	Actual Depth 👙 🦠	r.Jor	***************************************
,	1 3200	the Costolned	1	1	

WATER O	UALITY:	OTW =	14.08	Transd	ucer Actua	Depth [			
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	p <b>€1</b> +SU)	ORP	Turbidity (NTU)	Flow Rate (gai/hr)	Notes
	\$ 1 5 A		*******************					····	
7755	8 (47-12)	31						***************************************	L
7710	48.722	19.32	2.22				33.32	V****************************	
	2142	147.12			671	430	***************************************	**************	
234			2.26		<u> </u>	73.2			
1044	18.053	11.672	************	1.0	2.2	947.44	2.)	***************************************	
	8 5 24	17 14	2. 202			7.17 9	<u> 49a</u>	***********	
11.57								*********	
	A STATE	11/4/2		4.62	242	476.0			
	1 33 22	17.53	<b>********</b>		2.44			**************	
135	1727 F X		ulks. Obj	2				~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	****
72.74			Lilland					·····	*******
				į				*************	
								***************************************	*****************
					***********			***********	
						****		,	
								*********************	
								and the second s	
								*******************************	·
								*******************	
								~~~~	*********************
			******************************					******************	·
									***********
					***************************************				

Equipment Used	Equipment Identification #
YSE 556 MPS Reader and 5563 Soude	1.3
flow meter	
turbidity meter	2005-27

X3333	833	DRSERY	ATRONS:
-------	-----	--------	---------

Total volume purged 4 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Organization inclision measurements are given in feet in d.

Consider the value measurements are given in feet in d.

Consider the value of the consideration of the consideratio

WELL	ID:		0 s 30 s d
SAMPI	EID:_	13	

CLIENT:	Entergy - IPEC
SITE:	Buchanan, NY
WEATHER	Sycken Law Lasset

PROJECT NO: DATE:

SAMPLER(S): PUMP DEPTH: 01.0017869.9**2** 7~72.376 **9** 

fotal volume purged 🖖 💆 gal

\_\_\_\_\_n

Tinse	DTW or Achial Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Terbiday (NTU)	Derve/Vænt Cycle Lsecopds)	Drive Pressure <u>(psi)</u>	Notes (GAC)
12.22	Parnt			<b></b>		ļ		L:13	3.1	
C.C.L.L.L.	2000		Aich Link	licar EE		Çirin Z.	X		VVVVV = = = = = = = = = = = = = = = = =	
1112	Manne.	2.04					<b></b>			<b></b>
Li	22.10 13		4.433	3.32	سلامك تكلسا		12.33		******************	<u> </u>
11:11	DZ 443	16.4.	2:2:43	L.Z.::45	<u> </u>	54.2	6.27		********************	
1113				***************************************			ļ		************************	
1113	Pani	<u> </u>				<b>.</b>				
11.20	1224633	16-64	1.741	لكنتك	120	NZ 12			habaaaaaaa	······································
1128	13. Sa.2	10.02	LNOL	8.15	7:48.	<u> </u>			***************************************	Q.2.35
115.	111/2	17:12:	LLLL	3.34	1.25	32	441		************	
U AZ	[37. 20]	17.12	1.410			124	\$243		*******************	
142	.1.52.1.552.	17.3	1.464	229	7.427	227	033			~~~~~
11077	2.2 1. Sec. 2	1212		2.35		XX.2	10 X3		Print Control Administration Control Control	****************
1.52	I de la companya della companya dell	12.19		124		23.1	<b></b>		***********	
₩3°.	Lial	''ميدهد			h					***************************************
DOL					Ž	han a salah sa		**************	National Control of the second state of the second	,
						***************************************			*******	-
	<u> </u>					*********			***************************************	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,										***************************************
					·····	******************				
		*********			****************		***************************************			
			***************							
	<u> </u>									******************************
viere										

Equipment <b>Used</b>	Espsipment Identification #
YSI 556 MPS Reader and 5563 Scade	2
narhidity meter	800 1 ct 2554

1.233CO	VID ORNERV	VIIONS:
---------	------------	---------

Depth and Depth to Water (DTW) measurements are given in feet from top of casing,

Groundwater Elevation measurements are given in feet oist.

## GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: 1/1/153-100 SAMPLE ID: 011

SITE: WEATHER:		* <u>8 a 191 - 191</u> AA	79 'F	-		PROJECT N DATE: SAMPLERI		01.0017869 	1
WATER COL	120 DTB	-	5¶,5° orw	<u>=</u>	190.4 Water Col	umn Height	Well Diam	Dismeter	Multipliers 0.041
GALLONS O	f wate <b>r p</b>	ER WELL VO	LUME:					3	0.163
Water Co	iuma Height	100 4	х	Multiplier	, <u>=</u>	2.47 wei v	dume	Lui t	0.653
241_	- ×	1.5	=	3 .72 Designed Pur	ge Volume	_ <sup>gal</sup> TOTAL VOI	UME PUR	GED:	4.0 gat
AA: 4 10/2/19/6 5/10/5	BIITV.	DIW =		Fronstate	r Actual Dep	th			
WATER QU	Volume Purged (gal)	DIW or Actual Depth	Temp ( <sup>6</sup> C)	Specific Conductivity (S/Cm)	Disselved	pH (SU)	URF	Tarbidity (NTU)	Notes
1110									
	15.35						223 &	24.6S	
117.0	10.15		14.47	1.10%	3.22			Ļŝava	~~~~~
1128	1122		1121	1:587		<u>                                    </u>	262.S.	182 4	
11.22	122		17.12		1.4.5	<u> </u>	1977	ليبينا	***************************************
	1.2.5		60.36	1.651			٨٤٢٠٠	***************************************	
		10.100.	10 11	1 663	<u></u>		114.3	7355. <b>X</b> 139.1	
111111111111111111111111111111111111111	3		17.52		12 <b>S</b>	639	135.4		
سيكتلسا	1 4 2			1.45.7.3					
1125	1200				LIPES		***********		
1157	<u>LENG</u>	SANITIE.					***************************************		00000000000000000000000000000000000000
127	Phieni	LVLL		***************************************	****	<b></b>			
	-	<u></u>						h	
<b></b>		<u> </u>		********************	***************************************				
				• • • • • • • • • • • • • • • • • • • •		<b>.</b>			***************************************
<b></b>	managan	A	far: errer er er en fariable er er er	***************************************	Processor (1991) - 1991 - 1992 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 - 1993 -	the accessor and a second and a second		30000000000000000000000000000000000000	and and a second se
VSI 556 MI	Equipment Used  YSI 556 MPS Reader and 5563 Sonde							, -	ipment ification #

#### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

turbidity meter

WELL ID: MW	54-37
SAMPLE ID:	OH

LIENT: HTE: VEATHER:	Entergy - IPEC Buchanan, NY	. Lanal.	10.	-	PROJECT NO: DATE: SAMPLER(S):		01.0017369.92 1.1/1.5/c	Z1	÷
Sampling P	VTERVAL (depth		of casing)	•	TOTAL VOLU		3.1.135	gal	
Sampling P	ORT		**************************************	Comments of the Comments of th	PURGE RATE		gal / min) ()casble Valve I	Pung	nakkanakakkakkakkanakanakanak
WATER QUA	Pagest Volume	Temp (Č)	Specific Conductivity (Second	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1339		Fladin	<u> </u>					4.74	200
	0.45			<u> </u>	7 - 5 ;	~ Q · 3		<b></b>	
	1,15			مهال المسلم			1,21,		1
	1.00		43.081	1 0 . > 2	1		1.257		ļ
14 (V	1.25		23,03,99 23,586,51			1.2.27			ļ <u>.</u>
**************************************	2.35		γ		1.19	19.5 77.6	<u>.                                     </u>	<b>.</b>	<b>-</b>
1420	2.5				1748	<u> </u>	<u> </u>	·	ļ
	12:02		6336666					· <b></b>	
19.41	Linit		<u>l i idebbe</u> Policio (n.)		<b>b</b> ec	<b></b>		+	<del></del>
	28		L. Situlutuuliine		<b>*</b>	*****			<b></b>
				·		***************************************	1	•	<b></b>
				<b>*</b>				1	
				•	***************************************	<b>****</b>	•	***************************************	
<u></u>			1	1	***************************************	İ	1	***************************************	

	Equipment Used	Equipment Identification #
,	r SI 536 MPS Reader and 5561 Sande	4
- 5	whilety meter	12 12 20 12 12 2 2 2 2 2 2 2 2 2 2 2 2 2

NOTES AND OBSERVACIONS:

WELL	Ю.	MW	59	53

SAMPLE ID: 011

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT. SITE: WEATHER:	Energy IPEC Buchanan, NY		~	PROJECT NO: DATE: SAMPLER(S):	01.0017869.92
	######################################				
SAMPLING !	INTERVAL (depth in ft b	relow top of casing)		TOTAL VOLUME PURG	ED: 2.95 gai
		10° 10° 10°	-	PURGE RATE: <u>yariabie</u>	madayama dalaharan
SAMPLING	PORT			PURGE METHOD:	Double Valve Pump
	<u> 53</u>		5		•
***************************************	#300.0000000000000000000000000000000000	######################################			
*** * ****** ****	11 1TY+				

Time	Purged Volume	Temp ("C)	Specific Conductivity (\$\s/cm)	Dissolved Oxygen (g/l)	p# (\$U)	ORP.	Turbidity (NTU)	Orive/Vent Cycle (seconds)	<u> </u>
12 3 13	0	e time?						1977	2.0
13.364		2.147				. 76 4	2.000	1	<u> </u>
		23.0.0	1.071551						
			3.303	0.26		- 77 <u>- 8</u> - 627, 77	1.985		
	LA	Q., (3.)	1.301	0 : 2. 2 <u>.</u>	7. 24		0.00		
	1 A Landing	71.13	1.0675	0 646	7.26	- <u>6×2.</u> s			
	1	24.15		4.25	7.2.1	- 627.03	000		
	7.2.5	71.17	1.36340	1.2.0	77.28		Cica		
	2		1.240	<u> </u>	1.3%		1.000		
		21.13	1.305.7		7.25		1000		<u></u>
	1.74				1.2.2.1		12 012		1
	(. (. et al)	I Salakudi		laeai	<b></b>		<u>į</u>		
			ka dalah dalah			***************************************			
Land Control of the C		1940 E.				•			
				[ 					
				<u>.</u>	<b></b>	<b></b>		<b></b>	<b></b>
					<b>.</b>				
A			<b></b>	<b>_</b>		*****		<u> </u>	<u> </u>
			<u></u>	<b>}</b>					} \$
				<u></u>	<b></b>				
				<u> </u>	<b></b>				
	and an area of the second					ļ			
	1								
	•								

	Equipment Used	Equipment Identification *
h	r SF 556 MPS Reader and 5563 Sonde	3
- în	urbality meter	15 (1) 1 (1) (1)

NOTES AND OBSERVATIONS:

WELL	ID:	MW	54	-	(23_
------	-----	----	----	---	------

SAMPLE ID:	OH

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY CLOUD - DV INDY - 4D-5	PROJECT NO:       01.0017869.92         DATE:       1/13/69         SAMPLER(S):       6/2, p. 13	
350000000000000000000000000000000000000			2000000
SAMPLING E	NTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURGED:	
	160 10 1260	PURGE RATE: <u>variable</u> (gal/min)	
SAMPLING 8	CRT	PURGE METHOD: Double Valve Pump	
	A CONTRACTOR OF THE PROPERTY O	4	
200000000000000000000000000000000000000			00000

#### WATER QUALITY:

Time	Parged Volume	Temp (°C)	Specific Conductionty (Section)	(Pissolved Gaygen (g/l)	pH (54)	ORP	fwhelig (MTU)	Drive/Vent Cycle (seconds)	
		Thirth?	i i n					4/A	<u> </u>
		13.10	7 n. 1. 925	1.770	4.4 1. L	22.0			
		21-312	4. 483.2	d:71	<u> </u>	-95.7		į	
		2:31		0:30	(5.69)	- 1000	21.0		
1410		Bas 83	1.354	0.20	44.74				
	0.85	2.11.15.0	1.357	0.30					
			1377	0:142	12. 31 12. 37.3 11. 32.2	<u> </u>			
	17.75	73. 2.2	<u>  18841                                 </u>	0.18	10.96		1.2.00		<b></b>
	1. 2.			0.11					
\$   \qua	1.25				7.6.5		0.00	<u>.</u>	
3.3				Karanaan.	<u></u>	ļ	<b>,</b>		
			سلملك والتلافية	11. 2sc. IE.	<u> </u>	<b></b>			
	(7644 P. A			·			*****		
			<b>}</b>			<b></b>			
			<b></b>	<u></u>				<u></u>	
		<u></u>	<b></b>		*************	ļ		·	
			L			<u>{</u>			
						<u></u>	,,,,,		
								<u> </u>	
			<b></b>					<del></del>	
				<u></u>					
		<u></u>			<b></b>			-	
					<u></u>				
				ļ	<u> </u>				
			1	<u> </u>					

Equipment Used	Equipment Identification #
YSLSS6 MPS Reader and 5563 Soude	
Purple Day and and	2003/04/03

NOTES AND OBSERVATIONS:

WELL ID: MW <u>54</u> - 1424 SAMPLE ID: <u>011</u>

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	<u> </u>	· · · · · · · · · · · · · · · · · · ·	PROJECT NO: DATE: SAMPLER(S):	01.90 <b>17869.92</b> <u>비술(공주)</u> 준공권으로	
CONTRACTOR	·*************************************					
SAMPLING !	NTERVAL (depth in fl	below top of casing)		TOTAL VOLUME PURGED:		
	1350	to <u>155.5</u>		PURGE RATE: SKINDLE	· · · · · · · · · · · · · · · · · · ·	
SAMPLING	PORT					
	144		3	PURGE METHOD:	Double Valve Pomp	
200000000000000000000000000000000000000						
WATEROU	ALITY:					

Time	Purged Volume (gal)	Temp (E)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/1)	р <b>Н</b> (SU)	୍ୟନ	furbidity (NTU)	Drive/Yent Cycle (seconds)	Drive Pressure (psi)
38:3		MARK C						3/4	33
	0.01	20.25	2-046.5		41.15	sel : 1			
		1.1.0.1			625Hå	10.2	9.03		
	1:00		nanata	0.33			4424		
	1115		2.000	0.30	0.31				
		70.03		2.3.3	12-11-1	202	0.020		
	1,75				4153	25.4			
hh.b.sh.	1 2.0	20.42	7			200	0 3 6		
11111	2.3.5	20-54	[2:34]		7.07	30	<u> </u>	38	*
	7.74 C.L.	Sakok film	1.2244.62.1	10AL					
2.130	1600	Mark E							
<u></u>	Post	3							
			<u></u>						***************************************
<u> </u>				ļ					
<u> </u>	A-1								***************************************
									***
							*******************		*********************
						41.57.144.14.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		•	*******************
***************************************		T							
		T			•				
1					***************************************				
		T		1					
	~~	1							

 Equipment Used	Equipment Identification #
SI 556 MPS Reader and 5563 Sonde	<u> </u>
whidity meter	

NOTES AND OBSERVACIONS:

WELL ID: MW	<u>51.113</u>
SAMPLE ID:	Ои

CLIENT: SITE: WEATHER:	Entergy IPEC Buchanan, NY CONDY INDIVIDATIONS	PROJECT NO: 01 0017869.92  DATE: 1
	(NTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURGED:
	13C-5 6 182.0	PURGE RATE: \ankle (ga) / min)
SAMPLING	7.	PURGE METHOD: Double Valve Pump
WATER QU		

Time	Purged Volume (gail	Temp + C)	Specific Conductivity (Sácmi	Oisselves <b>i</b> Oxygen 1 <b>9</b> /0	pH (SU)	ORF	Furbidity (NTC)	Drive/Verst Cycle (seconds)	Drive Pressure (psi)
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<b>†</b>	I WAR						1 27.4	38
		23:22	1.983	2- 64:	L 5.0				t t
	0.5	2.31 037	U430		12:13	4.243.2	5.342		Ì
	1 (1/1/)	245 SA 265 SA	N. 954	Cald	6.95				1
100		20 4046	1.930	0.41	1111		05:042		
	1.3	77147	I 1. 0.26	0.2.0	Laus	L =5-27 / I	I Chara		
	1 2.0	76.475	1.773.0	ಾಯಿ	1.1.2.2.	5.0			- AP
	START			N.				· ·	
1 1201	160000	Millia	. <b></b>		De C				
	Park	022							
***************************************									
***************************************									
and a common statement of the state of the s									
			I						
	A		T						
<b></b>								Ī	
			1						
		<u> </u>	<b>\$</b>	***********************		****			
			***************************************	•		***************************************	<u> </u>		***************************************
					1				
		1		L	<b>&amp;</b>	L	<u> </u>	L	

Equipment Used	Equipment Identification #
YSI 356 MPS Reader and 3563 Sonde	3
swbwity meter	

NOTES AND OBSERVATIONS:

WELL ID: MW	24-120
SAMPLE ID:	011

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	104, 40s	PROJECT NO: DATE: SAMPLER(S):	01.0017869.92 
50000000000000000000000000000000000000	#2000000000000000000000000000000000000	**************************************		
SAMPLING !	INTERVAL (depth in fi	ticken top of casing)	TOTAL VOLUME PURG	ED: 2.05 est
	1350	w <u>2036</u>	PURGE RATE: <u>Variable</u>	
SAMPLING	PORT		PURGE METHOD:	Double Valve Pump
	142	ì	• • • • • • • • • • • • • • • • • • • •	·
30000000000000000000000000000000000000	**********************************			

39.ATE#	QUAL.	Ţ¥:
---------	-------	-----

Time	Purgred Volumer (gal)	Temp (*C)	Specific Conductivity (\$400)	Dassived Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Cycle (seconds)	Drive Pressure (psi)
		23344	Z ANJ					\$74	537
		71.25	1.200	4.30		10 1.5		1	i
	2.23				0.79	<i>532-1</i>	2.73		
3 33	115		6.032		W. 183	346-3	UrOsk		
L	0 12	10	1.330		1977 KS 4 1777 G 50	39.2	$Q_{i}Q_{i}$		
	112	1000		0.21		37.8	12.2.2.2		Ĺ
114.5	1 1 2 2 5					1.31.3			
			Liroz	0.11	7.12	132.2			
	1135		1. 44 2.	0 29			<u> </u>	4	39
12.02.2		CARNESS		MOV		<u>.</u>	<u>.</u>	*	
12.1		Maria	611.00	120 24	I I I C		<u>.</u>		
	-didiriiiiiiiiiiii								
								<u> </u>	
									5
		-							
<u> </u>	****								
<u> </u>									
				***************************************	I	I			
		<del> </del>	***************************************	1	<b>†</b>	***************************************			
<b></b>			•••••	***************************************	<b>*</b>	<b>†</b>			
1	1	1		<b></b>	<del></del>	Ammoonoonoonoonoonoonoonoonoonoonoonoonoo	b	in a second	hammannan

	Equipment Used	Equipment Identification #
	¥SI 556 MPS Reader and 5563 Sorale	7 - 1 - 1 - 1 - 2 - 1 - 1 - 2 - 1 - 1 - 1
- 1	turbulity meter	

NOTES AND OBSERVATIONS:

CLIENT: Entergy - IPEC SITE: Bucharas, NY WEATHER: DYEC (AST, SD'S F	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017 <b>869.92</b> 11 / 2.10 <sup>6</sup> 1 
--	--	---

WATER Q	UALITY:	() <b>TW</b> =	9-20		ver Aussai	Depth (:	641			
Time	DIW or Actual Depth	Temp ("C)	Specific Constactivity (SAcm)	Dissolved Oxygea 12/D	ρ <b>Η</b> (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle Gesonds)	Orive Pressure (psi)	Notes 4 - 4
1033	7.643					***************************************				
1335	W-300	14-24	9 11/41	3.00	134	~1. T	<u> </u>		*********	
1055	G 450	15.40	Q-3118	1.00	1.91				***************************************	
1105	10.508	18:14	Q 612.5	LΩ			<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>		••••••	10. <u>1</u>
	0.423	18:31	0.8is		1.45	-94.3		**************	<del>and and and and and and and and and and </del>	·
1123	6.423		ــــــــــــــــــــــــــــــــــــــ			- 202			***********	2.35
11(35)		13:17		£12.Q	1.73	L30.1.	C-CD		***************************************	0.4
11112		18.20	0.875	0.30	1.74		0.25		*****	1-2-5-6
11:45		12.11	.0.315	\$ 17 Z	<u>Jak</u>		<i>0</i> 4.630.		********	12.75
HOND.		13000	0316	្រាំ	7.77		<u> </u>		••••••	
115/6		18007		<i>Q</i> 33	7.77	* <b>(</b>			*******	
12.02			0.315	0.31	7.11		<u>                                     </u>			
126		13.31		یال ک	1.31		LC CID		••••••	. Obs. 1177
12.10		1330			7.81	- XX	0.02		••••••	22 <b>22</b> 7
2-1-4	Singl		L.C. Lilled		<u></u>				***************************************	***************************************
			L (Q.L.L)	ستستند		IPCC			**************************************	
	Pulvie	LOSE								
									~~~···································	
		<b></b>								***************************************
									***************************************	
			***************************************						***************************************	
	AN MERCO DE CONTRACTO DE CONTRA							<b></b>	······	
	,.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,								······································	
			<b></b> , population						******************	
			<b></b>					ļ	***************************************	<del></del>
					L	<u> </u>	<u> </u>	<u> </u>	think think the construction of the construction	

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	
turbulity meter	222700059

4-1-4-25-61	5.5014	BRCFRV	ATIONS:

Total volume purged 👉 🚫 gal

Depth and Depth to Water (DTW) measurements are given in feet from up of easing. Cheantwater Elevation measurements are given in feet msl.

CLIENT: Entergy - IPEC SITE: Buchanan, NY WEATHER: NOCCAST, SOLF	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 
------------------------------------------------------------------------	----------------------------------------------------	-------------------

			73 1 7							
WATER Q	UALITY	= WYC	4.62			Depth /	4.08		***************************************	
Time	DTW or Actual Depth	Temp } (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen (g/l)	p <b>H</b> (SU)	ORP	Turbidity (NTU)	Orive/Vent Cycle (securals)	Drive Pressure	Notes 501
1023	24.092				<u>.</u>					
1235	23 941	10.01	<u> </u>	L.13	1.50	لنشنا	<b>14</b> 55		·	laci
1003	23. III	3.4	0.757	0.48	1	757	3.74		***********	<b></b>
1105	23, 233	1345	_1_9_w	Liukă	LL	ستستقشا	\$00.500.000.000		***************************************	2.4
1115	23 959	181710	1.50	<u> </u>	253.	324	1.000		** ** ** ** ***************************	<u> </u>
1125	13 45 2		1.023	للانفا		112.0			******	4.0
11 72 42	232140	LETT.	1.103		7.83 7.83	-4351	2:00			115
1140	133 1412	18.61	ــــــــــــــــــــــــــــــــــــــ	Q 38			C.C.C.		·	
11:15	135 Jud	13.41	1/130	التسنا	2.33		<i></i>		<del>//</del>	1.5
Tu :: 522	123 122	السندنا		ــدـــــــــــــــــــــــــــــــــــ	283.	-48.7	Q. 1212.		<del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>	<b>}</b>
1.55	123 740	18.73	1:151	0.43	7.32		4.00		***************	<b></b>
1202	123 115.	1371	1.196	0.34	3.82	-517	A RANGE AND A STATE OF THE STAT		~~~~	<b></b>
1205	133 122	18.80	1.202	9.30	1:32	-49.2	0.420			
12.112	23 922		1,172	0.30		-517	<u>. Q. QQ.</u>			
12.12	STARL		LE CELL	is not		MARKENER ENTER STORY	**********	······································		
12.34	ENDS	amill		011261	44II	<u> </u>	~~			
	PWAR	occ.			*****************	******************				***************************************
									*/**********	
				***************************************		w	***************************************		**************	
					A CONTRACTOR OF THE PROPERTY O	MANAGE			***************************************	**********************
									······································	
				**************						
						*****			***************************************	
	<u></u>	<b></b>							***************************************	
		<b></b>				***				
	<u></u>	<u> </u>								

Equipment Used	Equipment Identification #
ever 556 NDS Reader and 5563 Sonde	Ø
rurhidity meter	200701154

SOTES.	3 3 83	OBSER	1.	3	ioss:
--------	--------	-------	----	---	-------

fotal volume purged 2 2 gal

Depth and Depth to Water (DTW) measurements are given in feet from 6-p of casing. Groundwater Blesation measurements are given in feet msl.

CLIENT: Energy - IPEC SITE: Buchaban, NY WEATHER: OVERLAS I	<u> </u>	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 
-------------------------------------------------------------------	----------	----------------------------------------------------	-------------------

WATERQ	UALITY:	DTW=	9 34		icer Actual	Depth Z	41.64	3		
Time	DTW or Actual Depth	Temp ) (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen (2/1)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vest Cycle (seconds)	Orive Pressure iøsi)	Notes
1028	71.213					······································		~~~~	***************	<b></b>
1045	المتنابي			بكتعلنكسإ	6.17	<i>[</i>	<u> </u>		***************	
0.95	41183	13.21	2.253	12:31	<u>Jui 35</u>	<u> </u>	5.42		****************	
11,25	91.191	LLALA.		2.43	<u> </u>	<u> 45 3 .</u>	<u> </u>		MANAGARAN POR COLUMN SAN SAN SAN SAN SAN SAN SAN SAN SAN SA	0.25
1115	41178	<u> </u>	2.217	2.31	122	38.0			**************	
1125		. 13.21	2.35	Lings	2.01		1.41.		****************	10.75
132	الالالاللا	<u>raus</u>	2.243	4143			1.44			115
THE	المالك المالك المالك المالك	15.35	$\frac{2.311}{2.214}$	2.51	100	52.1 55.1	2-24 2-54		······································	1,25
11772	191175	18.31	2 - 1-13	2.44 2.55		57.2	2 . 33		Military Control of the state o	1,23
1150	i i i i i i i i i i i i i i i i i i i	13.43	{ <b>~</b> ,*******************	2.63	<b></b>	57.1	2.03			
165	41 102	15.52	1-212 2-21 <b>3</b>	2.61	7.12	and the second second	132		**************************************	
	111155	13.40	2.218	7.0		**************************************	1.11		***************************************	3
- چندرنا	<u>,,</u>		.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	3	}	سنعصد شاساس	<u> </u>		*****************************	
Lil <u>uş</u>	STACT END S								**************************************	
1233	71. MAD			11.10				~~~~		~~~~
						***************************************			*************	
				***************************************	•••••••				*************************	
	<b></b>					***************************************			***************************************	***************************************
						***************************************				******************************
					***************************************	<b>*</b>				
				***************************************		***************************************			***************************************	******
									***************************************	
										***************************************
			y,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			······				
										***************************************

Equipment Used	Equi <b>pment</b> Identification #
Vot 556 MPS Reuler and 5563 Soude	5
subjective meter	200161254

Total volume pargod 2.2 gal

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet risk

CLIENT: Entergy - IPEC SITE: Buchanan, NY WEATHER Sand Courts Sons	PROBECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 11 / & 1 & 9 
--------------------------------------------------------------------	----------------------------------------------------	-----------------------------------

WATER Q	CALITY:	ptw :	46,000	Transdu	cer Actual	Depth 🚣	4 435	,		
	OTW or Actual Depth	Temp ) (°C)	Speedic Conductivity (S/cm)	Dissolved Oxygen 18/0	9 <b>H</b> (SU)	ORP	Turbidity (NTU)	Drive/Vem Cycle (seconds)	Drave Pressure (psi)	Notes
	Za 27 24 25	:	My ay					6 - 3		
	74790	17.54	1.6.6.3		6.42.				22	***************************************
13.0.3	2014 15	17.2%	1.72		( 5/2)	2322			**************	
	44.133	17 21	1 9777	. V		234.2				
	1. (4. )	77 3.1	2 14.0	3.63	$C \otimes X$	224.5	2.55			
	72 A 13 Y	7 3:		1.59	6.25	2346	417			00
	44.0	77.28		1.533		23 7.0	14 4 7 7.			
1333	44 176	1 7 %.1	2.302.	157		234 2	4.12.	<u> </u>		G 753
		2004		Andrews	241.1.5	17322	******			***************************************
		1,72454	lić co	<u> </u>		2				
			1.086						NAMES AND	
					*****************				AANANANAN OO	
					****				M NANANANANANANANANANANANANA	
									*******************	
						***************			**********	
									************	
					<b>.</b>				MARROCERO COCCO CO LA PARRE DE LA CO	
						~~~		<b>****</b> ********************************	<b>Marian marian</b> de construir de la construir d	FEF Salabation and a second and a second
									**************************************	
									<b>**********</b> **************************	
					**********	,				
						***************************************			***********	
									******************	

	Equipment Used	Equipment fdentification #
YSU556 31PS Reader und		
ambiglity meter		3.40 Pulk file d

22376	S 85 8 2	acres.	5 8 3	SNS:

Dispth and Depth to Water (DTW) measurements are given in feet from top of casing,

Commissator Elevation measurements are given in feet and

Total volume purged <u>J. 1912</u> gal

### GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: Mid-56 33

GALLONS OF WATER PER WELL VOLUME:	043 163 553
Water Coloma Height 67.33 A C C 4 gal Well Volume  Well Volume  1.5 = 2.23 gal  Designed Purge Volume  TOTAL VOLUME PURGED: 2.55	3
Designed Purge Volume  TOTAL VOLUME PURGED: 2 55	
	ç3
TT , 0 8 20 83 10 10 10 10 10 10 10 10 10 10 10 10 10	
Time Purged Same a Community Consequencial put (SU) ORP (NTU) Cy	of Vent Orive yole Pressure Notes ands) (psi)
thought and the contract of th	
<u> </u>	
- CT - TO - 1	
TT X Y 1 X 1 16 30 1 1 20 12 44 12 20 12 13 14 27 12 3	
[17] [17] [17] [17] [17] [17] [17] [17]	
TERT I LAW LE CANTRE TRO LE CLECTE L	
Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	
turbidity meter	

Mass. 3	
WELL ID	
SAMPLE ID:	

LIENT: ITE: /EATHER:	Entergy - IPEC Bachanan, NY	: : <u>: : : : : : : : : : : : : : : : : :</u>	<u> </u>		PROJECT DATE: SAMPLE: PLMP DE	R(\$):	01.001786	- 3/ <u>- 3</u>	ft
VATER Q	UALITY:	DIW::	7.63	Transd	ucer Actua	l Depth			
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen in/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Bair (gal/br)	Notes
	7.63								
40, 5	1/2 3 - 3 / 3							f	
	103	11 -18				7. 6			
1.00					1	-13.0			······································
						1510	<u> </u>		*******
	77.227						1 2 KI		
	2.5		1.1.1.15	1.03	1,230				***********
	1.12.6						16.35		***
			1300				10:10		*************
							1041		*************
		بالسسية.	1115	<u> </u>	1.00	24.32	1 :	···	***************
aldi.	1.0.1						Q 45		V-44,444,0000000000000000000000000000000
			********				paration and all a series		Order of the Control of the State of the Sta
سنسس		13.41)	<u> </u>		7 7 3	<u> </u>	9 ( )		****************
				<u> </u>	·	III.A			*****************
	5127 ( )				<u> </u>				*******************
Substantia	2		Leinen	**********					*************
				######################################					
				**************************************	****	**************		· · · · · · · · · · · · · · · · · · ·	
				***************************************	*************				
			************************		***************************************	***************************************			-
والاستان والمعاوض الباران الماران والموارد الماران الموارد الماران الموارد الم	ļ							•••••••••••••••••••••••••••••••••••••••	
**********	<b></b>							***************************************	
					***************************************	(1,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0	***************************************		
	\$		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		h	******************	barra and		
	****		Facianant			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Equip	ment

Equipment Used	Equipment  Identification #
YSI 556 MPS Reader and 3560 Soude	si si
flow meter	
ourbality meter	

	L KITS	OBSERVATIONS:	
V 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 / 11	1335 KV 4 130 13.	

Total volume parged \_\_\_\_\_ gat

Highth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Edevation measurements are given in feet nisk.

WELL	ID( <u>~u~</u> )	<u> </u>
SAMPI	.E ID:	

CLIENT: SITE: WEATHER	Entergy - IPEC  Buchanan, NY  SECULAR	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	03.0017869.97 10179 31 ( ) 10179 31 ( )

Time	DTW of Actual Depth	Temp ('C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	p <b>iłł</b> (ŠU)	08JP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
430	60 452								
1024	/ 5/4/2003		<	<b></b>					
TOMA.	الالملايع					***************************************	5.34:		
	o u a a i i i i i	112.23				سليد فستسل			***********
	404.4	13.92		<b></b>	4.95.	\$1.000000000000000000000000000000000000	4.50		
104	AO SEK	13.36					4		
114	453		( .		7.02	-3520			/460.000.000
				1					
N Add	Z. 11. 24.5	22.52	1.534	1.01	7.4.7	SALES CHEST STREET, SALES CO.			******************
7739	60.932		1. 1. 1. 1. 1.			عبين عب			~~~~
3.5	100.190	. Maritim				·	کانت	···	**********
11.40		and the second				74			***************************************
	<u> </u>		1.6.2.)	1. 2. 2. 3.	سؤلسان			******	
11.52	Andrews Company	1023	***************************************	144.7.2.	1.18	52.2		····	***********
115.2		سنبشلسا							
and the state of t	161.025			l.a.a.a.	11.26	-61.2			
	Charles A				<u> </u>				**************
					ja	************************			****************
		************************			*************				er er er eggyadalakkelekkelek er er
	<b></b>		***************************************		*****			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	****************		***************		V*************************************	*******************			***************
	<b></b>		*****************		w d = = = = = = = = = = = = = = = = = =				PPRAKA PROGRAMA CONTRACTOR
					-				na n

Equipment Used	Equipment Identification #
YSL556 MPS Reader and 1563 Somle	·-
iliyw meter	.)
carbidity meter	Are / Fire 27 t

SOTES	AND.	OBSERVA	TIONS:
N( !   Y	.A. V.	1,243,75,45 7 ()	

200	,	,	1 3	
10131	volume	DUE GOOD		3,01

Depth and Depth to Water (DTW) measurements are given in feet from top of casing

Groundwater blevation measurements are given in feet and,

WELL ID:	MW	69_	-	35
SAMPLE U	D:	01	1	#18th temporous

CLIENT: SITE: WEATHER:	Entergy IPEC Buchanan, NY		PROJECT NO: DATE: SAMPLER(S):	01.0017369.92 10 30 03 M DESTUS
200000000000000000000000000000000000000				
SAMPLING I	NTERVAL (depth in ft below top of casing)		PURGE RATE: Sadiable.	(gal / min)
SAMPLING	PORT			
		***************************************	PURGE METROD;	Double Valve Pump

#### WATER QUALITY:

Time	Porged Volume	Temp (*E)	Specific Conductivity (S/Cm)	Onygen (g/l)	pH (3D)	ORP	Turbidity (NTU)	Drive/Yess Cycle (seconds)	Drive Pressure (psi)
		PALME						140.41.177	2.0
300		141.3	2.756.	12010					1.62
13 0	( ) (3						<u> </u>		
			212		1.26	<u> </u>		<b>.</b>	
1325	0.40	17.41	332.)	کسنیکسلسی		la Sio li		<b></b>	••••
1 2 3 3 3	Q. 5Q.	14. 4.2.	4.224	0.93	2.35	<u> 3.62</u>		<b>ļ</b>	
17.61	0 55	146.664			<b></b> 2		LLULIO		·
	0.60	<u> </u>						<b></b>	
3 24 55 2			<u> Alsoi</u>					<u> </u>	
1 3 60 1			تعشك بيك			هنگسنشله	9.37	ļ <u>ļ</u>	
171014	TO 25	1.63 82	فينكتبدستناسا					ļļ	
17409		ككدينيا	بعكالم فيكسد أوسا		7. 54	L			
1412			24 - <u>Q</u> x 64 2	12.2	LZa.54	<u></u>	SL SAG		300
				<u></u>					
1416			لفميسيا						
1810		المشخصي			<u> </u>		<u>C</u>		************
			006			<b></b>			***
							***************************************	***********	
			-		**********	<b></b>		•	
		******************		**************************************					
			***						
				*******					
									All and the second of the seco
				***************************************		<u></u>			

Equipment Used	Equipment (dentificat <b>ion #</b>
YSI 556 MPS Render and 5563 Sonde	
lurbidity meter	

WELL ID:	MW	S.A.	 	. "	23
SAMPLE	D:	0	ţ		

CLIENT: SHE: WEATHER:	Entergy - IPEC Buchanan, NY	PROJECT NO: DATE: SAMPLER(S):	01 337869.92 16 13 c   6 9 18 18 18 18 18 18 18 18 18 18 18 18 18 1			
200700000000000000000000000000000000000		OOO OO				
SASIPLING I	NTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURGE	Dt gal			
	<u> 454</u> 10 <u>514</u>	PURGE RATE: Katishle (gal/min)				
SAMPLING E	PORT	PURGE METHOD:	Double Valve Pump			
	<u> </u>	<i>G.</i>	·			
WOODS OF THE PROPERTY OF THE P		xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx	000142000000000000000000000000000000000			

#### WATER QUALITY:

Fixte	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/3m)	Dissilved Oxygen (g/f)	p <b>H</b> (SU)	082	Torbidity (NTU)	Orive/Vent Cycle (seconds)	
	<u> </u>	<u>Para</u>			and a supplemental and a superior of the super	and the second s			
17362.53	f 5 + 3	344/	[3.53]	1.3%	666	. <b>1</b>			
1312								*************	
	1. 2		<u> </u>	0.444					
	3 532							·	
			33.31.)		Laus	1.132.5	41.114	<u> </u>	and the second s
			2.600		ļ?\ <del>k</del> .6a	1.24.8			
1867	10.864	Link			1-4.27			<b>_</b>	
				62-4-2	<u>                                     </u>	<u> </u>	<u> </u>	3.9	¥
1343		Pant.	<>** \$ *********************************			<b></b>			
130			L LAME L		مكتالكما			ļ	***************************************
1411	Ĩ	Laaatt	CASA (		1 2 1				*******
	T	I i a mai	Z-94				***************************************		*************************
		<b>.</b>	 	••••				•	
		<b></b>				-	****		*****************************
		<b>.</b>							**********
							<b>alleleles a seguence</b> de la la del de la del		********
					ş	ļ			
									•••••
									·
			•		<b>.</b>		• • • • • • • • • • • • • • • • • • • •		
			ļ			***********	***	****	
						***************************************			

Equipment Used	Equipment Identification #
	7,
YSI 556 MPS Reader and 5363 Sonds	<u> </u>
trubultry conter	l Academical pries i

WELL ID: M	w <u>60 . 12</u>
SAMPLE ID:	CIL

CLIENT: SITE: WEATHER:	Entergy - 1PEC Bushayan, NY	<u> </u>	`		PROJECT NO: DATE: SAMPLER(S):		01 <b>0017869.92</b>		
SAMPLING IN	ORT		of casing)	4	TOTAL VOLUME PURGED:    Company of the control of t				
WATER QL'A	Furged Volume	Temp (C)	Specific Conductivity	Dissolved Oxygen (w1)	pH (SU)	ORF	TurbicSty (NTU)	Drive/veat	Drive Pressure
09450 0006 1006 1016 1036 1036 1036 1055		(20M) 19.57 15.74 16.60 14.97 14.97 14.97 14.97 14.97	18491 2333 2333 2462 2463 2463 2463 2463 2463		7.03 7.03 7.04 7.04 7.06 7.06 7.06 7.03 7.03 7.03	-14.9.1 217.1.7 24.3.4 -52.4 -52.4 -51.4 -50.4	3 1 3 2 5 4 2 3 4 2 3 4 2 3 4		
1057 1057 116 <b>8</b> 1162		Part 5703 i 5049014 19440 i	SEE SEE SEE		ECROA 2 C T	<b>2</b>			
					I				

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u> </u>
furndity acter	

WELL ID: MW 🔾	$\Omega \cdot 139$
---------------	--------------------

SAMPLEID: CIL

Equipment Identification #

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	<u> </u>			PROJECT NO: DATE: SAMPLER(S):				-	
SAMPLING INTERVAL (depth in ft below top of casing)  to 1/4 4  SAMPLING PORT					TOTAL VOLUME PURGED:  2 15 gal  PURGE RATE: YELLER (gal/min)					
WATER QUA	XXY:									
Fisne	Purgest Visione (gal)	Yевир (°С)	Specific Conductivity Lifemi	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Orive/Vent Cycle (Seconds)	Orive Pressure (pst)	
1 1 4 3 7 5 7		<u> </u>			*		*****	1	3 2	
		1.924.4			<u> </u>					
Lick	1	<u> </u>						·		
سفيد داد				<u> </u>	245	11211		~ <del>}</del>	<b></b>	
L. C. A. Sa.				2.42	7 40	1-1800cm	3 41 <b>X</b>	•		
					<u> </u>	. Lakaliilii kii			<b>T</b>	
1044		narias	SAMO	E 62 68	Do Tates	***************************************	**************************************			
10.55			C.63.843		1 32 1	To the contract of the contrac				
1055	man 1	TO CARC	C 6- C							
					<b></b>					
		<b></b>		***************************************	<b></b>		************			
			<b></b>	•	•		**********	<b></b>		
				<b>,</b>		***************************************		···	***************************************	
						***********		••••••••	······································	
					*************	***************************************	***************************************	***	•	
				************	***************************************	***************************************		***************************************		
**************************************	,									
						<b></b>				
			<b>4</b>	*************	t and the state of		ر در			
				***************************************		<b></b>	•••••		**************************************	
				······································						
		<u></u>	<u> </u>		1					

Equipment Used

NOTES AND OBSERVATIONS:

YSI 556 MPS Reader and 5563 Sande

turindity meter

WELL ID: 5	ΜW	<u>60</u>	-	154
CAMBIE IE	١.	52 2 1	ş	

SITE:	Entergy - IPEC Buchanan, NY	<u>( 50`&gt;</u>			PROJECT NO: DATE: SAMPLER(S):		01.0017869.92 101.103 101.103		-	
SAMPLING INTERVAL (depth in ft below top of casing)					TOTAL VOLUME PURGED:    15   5   6     PURGE RATE:   Variable   (gal / man)					
Sampling PC	)RT	000000000000000000000000000000000000000	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2	PURGE METH	(( <b>)D</b> :	Souble Valve I	Pump	***************************************	
SVATER QUAL	Purged Volume	C) quest	Specific Conductivity (\$/cm)	Elissilved Oxygen (g/l)	ρΗ (SU)	ORP	Turbidity (NTU)	Drive/Vens Cycle (seconds)	Drive Pressure	
				109 252 252 4 45	7 3 6 7 3 7 7 3 7 7 3 7 7 3 9 7 3 9	34 3 34 3 34 3 34 3 34 3 34 3 34 3 34 3	3 75 3 77 3 77 2			
						-				

Equipment Used	Equipment Identification #
	4.
YS! 536 VIPS Reader and 5563 Sonde	Our six right to a said
turbality meter	the contract of the contract o

WELL ID: MW	Ga-176
SAMPLE ID:	Oil

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	Scis			PROJECT NO: DATE: SAMPLER(S):		01.0017869.92 1013c M 233	log Tes	-
SAMPLING IN	TERVAL (depth		of casing)	***		MEPURGED: : vanable (8	23/ min) Double Valve	_	********************************
WATER QUA	LITY:								
Yime	Purged Volume	Temp (°C)	Specific Conductivity State)	Ossolved Oxygen (g/f)	pH (SU)	ORP	Turbidity (NTC)	Drave/Vent Cycle (seconds)	Orive Pressure
16.34 16.34 16.34 16.34 16.34 16.34 16.34 10.34			C N 133 1	2 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				35.75	
			quipment Us	ed	***************************************		Equip	ment Identific	ation #
YSI 556 MP3 corbidity meter	Resiler and 1563 S	mile			***************************************		26.0	<u> 1900-2009</u>	

IPEC00225025

WELL ID: 41/62 12	
SAMPLE ID:	

CLIENT: Entergy IPEC SITE: Buchanan. Y WEATHER: Oudy, windy 40's	PROJECT NO: DATE: SAMPLER(S): PUNIP DEPTH:	01.0017869.92 11/12/09 CB, MB
--	---	-------------------------------------

WATER Q	CALITY:	DTW =	9.55			l Depth	5.957	trans	ques -
Time	DTW or Actual Depth	Temp ;°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Motes
1057	6.372			<b></b>		<b></b>	ļ		<b></b>
1105	6.293					ļ	<b></b>		<b>,</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
<u> </u>	6.181	14.31	1.744	6.04	7.85	And the Parker William Contract of the Parker of the Parke		***************************************	
1124	6.141	14.26	1.726	5.90	136	1638	13.34	***************************************	
1141	6.024	13.72	1.102	5.61		11560	12.78		0.1
1156	<b>5</b> .824	13.06	1.699	6.2	7.92	1530	14.00	***************************************	
1203	5.822	12.83	1.700	5.96	7.7.2	152.0	13.43		0.15
12.10	5.757	12.57	1.687	5.97	7.44	150,9	12.61	***************************************	******
1218	5.704	12.48	1.679	594	7.93	149.8	11.58	*********	0.20
1228	5.608	12.36	1.679	5.98	7.93	147.5	11.09		***************************************
1233	5.556	12.28	1.681	6.06	7.93	146.1	10.39	*******************************	0.23
1240	5.532	12.20	Andrew Standson Standson	6.11	7.93	145.2	8.97		*****************
1243		STAC			<b>DLLE</b>				************************************
	Fow	cate	<u>v tre</u>	2.1	طيرسه	and the same of a water of concession and	ecter.	Level	Keeps
	droppi	28	deading	25		ACCOUNT OF THE PARTY OF THE PAR		anstu	<u></u>
	Keeps	daner	منستممنا		CLLS	bece	<u> </u>	Lean	<u> </u>
	an z	Luci	sir d.	*		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		<i>y</i>	
	Host	لاعملنا	\$\$\$\$\$\$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		arianda	. tecsed		AANAANAA COO COO COO AAAAAAAAAAAAAA	NAMES OF STREET STREET, STREET STREET,
153U	GAID SAN	irle d	opuscen	N 219	TOPLO!				anna ann ann ann ann ann ann ann ann an
	PUMP D	EC.					AAA00000000000000000000000000000000000		
***************************************				***********					***************************************
							I		
					1				

Equipment Used	Equipment Identification #
YS1 356 MP5 Reader and 5563 Sonde	4
flow meter	Ki # 1
surbidity meter	200701254

NOTES AND OBSERVATIONS:

Total volume purged Q.4 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet insl.

WELL	ID: 1106)	27
SAMPL		

CLIENT:	Entergy - IPEC	
SITE:	Buchanan, NY	11
WEATHER	Cloudy, windy	405

PROJECT NO: DATE:

11/12/09 CB MB

SAMPLER(S): PUMP DEPTH:

WATER Q	UALITY:	oTW =			ucer Actua	I Depth	***************************************	p.(	
Time	DTW or Actual Depub	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	ρ <b>Η</b> ⊹S <b>U</b> )	ORP	Turbidity (NTU)	Flow Rate (gal/fu)	14.0(9ad
1057	15.140								
1105	15.242		~ ~ ~ ~	<b>_</b>	***				
1119	74.461	13.82	1.370	2.14	7.01	-104			
1124	14,968	13.82	1.373	1.21	1.97	- 99.3	***************************************		
11 41	14.824	13.54	1.385	1.53	7.20	-1040	*********		0.10
1156	14.780	1354	1.408	1.22	7.28	-107.9	hammer and the second	****	0.15
1203	14.717	13.49	1.426	1.15	7.31	- 1047	19.08	***************************************	0.20
1210	14.676	13.38	1.434	1.15	7.33	-100.	17.71	***************************************	
1218	14.632	13.26	1.437	1.09	7.35	- 97.8	16.15		0.25
1 2 28	14.578	13.11	1.434	1.08	7.37	-100.1	15.80		
7 33	4 539	13.07	1.433	1.09	7.38	- 98.7	15.18		0.27
1240	14.513	2.96	1.434	1.10	7.39	-96.6	14.39		
243	Carlo carde caixes caixed the car	STAR	T SAMP	re ce	LLEC	TION		Α	
	Flow	ata	sat ve	u Co	1. <sup>L</sup> zw	t wot	ea le	ed ka	26.2
***************************************	1		Ladins	محرة لأع		Q. T	eno ex	2.72.4.00	
ļ	1 1 1 1 1 1 1	2	ALC UN	ال مال	282	becom	100 824	cold.	
	1	+031	n. 0				Z)		***************************************
	Most	. le	tide is	د قد ت	C 6~4	Ŧ.			
1200	Secretary and a second contract of the second	ample	***************************************		3	<b></b>			~~~~~
1521	Pump 0			1.8c.13.c			***************************************		
<u></u>	I WILL						····		***************************************
						·····			
***************************************			•••••••••••••••••••••••••••••••••••••••				<del></del>		
MANAGERE CONTRACTOR							······································		
		l		l	ii				

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	Ki #2
turbidity meter	200701254

VOIES.	123	OBSER	V.	$\odot$	ONS:
--------	-----	-------	----	---------	------

Total solume purged 0.4 gal

Depth and Depth to Water (DFW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet hist.

WELL II	): MW	alah -	3
SAMPLE	E fD:	MI	)

CLIENT: SITE: WEATHER:	Energy - IPEC Buchanan, NY	1,40.	00000000000000000000000000000000000000	-	PROJECT NO: DATE: SAMPLER(S):		01.0017869.92 31.4.12.7 51.4.13	04	~~ ~~
SAMPLING I	NTERVAL (depth		of casing)	•		IME PURGED:	217	gal	
SAMPLING I	PORT S		22/07/04/04/05/05/05/05/05/05/05/05/05/05/05/05/05/	42	PURG <b>E</b> METI		Double Valve	Pump	
WATER QUA	ALITY:								
Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (Skora)	Orsoived Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
105.19 105.19 12.10 12.1						7/// 3 902.6 902.6 12.3 12.3 42.7	2002 2002 2002 2002		
YSI 556 MPS turbiday meter	Reader and 5563 Si		quipment Use	d				ment Identifies	

WELL (D:	MW	6)	. 1
SAMPLE II	D:	On	

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY	*******************************	PROJECT NO: DATE: SAMPLER(S):	01 0017869.92 11/12/04 28/40713
SAMPLING R	NTERVAL (depth in ft below top of casing)		TOTAL VOLUME PURGED	): 1145 gal
	61.1 to 07.6		PURGE RATE: \mishig.	(gal / min)
SAMPLING P	<b>⊙RT</b>		DESTRUCTED A SECOND LOCAL.	0. 11. 11. 6
	~11	5	PURGE METHOD:	Double Valve Fump
200000000000000000000000000000000000000	**************************************	20000000000000000000000000000000000000		**************************************
WATED OHA	EITY:			

Faint	Purged Volume (gai)	Temp (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen (g/1)	pět (SU)	ORP	Turbidity (NTU)	Orive/Vent Cycle (sea inds)	Dave Pressur (psi)
	.:	. (11111)						14/14	20
11341	[ V.Oi	15.41	1.111		42 4 1	25.3			
1144	[ , <b>L</b> S	1422	4421	Quill	3.52		2.22		
11-7-4	0.3	12.74			1.45	44244	L. &. C.Z		
1123	1. 2.75	12575	1:11.731		7.7.		<u>Ç.</u> Q		·
12.10	117	13.2.1			1.77		2.63	· · · · · · · · · · · · · · · · · · ·	*******************************
1212	1.15	145.15	1:42.	2.3.3	1.73.	21:2			
1277	1.25	16.14	1.12.2		1.12				
		Solder	11111	ST W					
	TOWN	aluta? 4.50	4. 3. 3. 3. 5. 5.	100//1	LIES	****			
	1 1000000			*************	************************	MANAGES   FEFER   MANAGES   FOR STORE			and the state of the
	1						****	1	**************************************
		***************************************			***************************************				
	T								
				••••			****		
			<b>.</b>		/····		-		
	1				******************	~~~~			****
\$					***************************************				
					***************************************				***********
***************************************					************				
							,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		*************
							Million & Angeles and Control of the State o		
						***************************************			
ļ	1								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5363 Sonde	
furbality meter	

WELL ID: MW 2 - 9)
SAMPLE ID:

CLIENT: SITE: WEATHER:	Entergy - IPEC Suchanan, NY	***************************************	PROJECT NO: 01 0017869.92  DATE: 1(1) 2 1(2) 2  SAMPLER(S): (C) 4 1(2) 2
SAMPLING)	INTERVAL (depth in ft below top of casing)		TOTAL VOLUME PURGED:  /-45 gal  PURGE RATE: Satisfable (gal/onlin)
SAMPLING		4	PURGE METHOD: Double Valve Pump
***************************************			
WATER QU	ALITY:		

Time	Purged Valuanc (gal)	Temp ( <sup>9</sup> C)	Specific Conductivity (Sátra)	Disselved Oxygen (g/I)	pH (SU)	ORP	Turbidaty (NTU)	Cycle (seconds)	Drive Pressur (psi)
1, 2 3	(5)	2						2/4	4
4.24		1.1.1.1.3	Littii	1.31		- 102.51			
11-11	3		11112		4.32	42.444	3,73		
121	2.5	Like D.I.	سننتنا	1 5 34 L	7.65		<u> </u>		
1201									
11.11.	لــكـناـــــــــــــــــــــــــــــــــ	15.43	1122	226	<u>lli</u>		<u> </u>		
1712	1.15	XĽ	Litti	1.25	1, 2, 2	13.1.5		·	
1110	11112	12:14	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.2.	lsb		71.00		****
12.77	المعاللة				22 3 3 3 3	<u> </u>		·	
			<u> </u>	and hall die	des	***************************************		·	
*************************						**********************			
**********				•					
				************************	***************************************	****	***************************************		***************************************
			\$\rightarrow\tag{\tag{\tag{\tag{\tag{\tag{\tag{			************************	-	<u> </u>	#00000000000
	<u> </u>	~~~		***************************************					*************
									*****************************
***									
************									
***************************************	, , , , , , , , , , , , , , , , , , , ,								
	-	<u> </u>				, , , , , , , , , , , , , , , , , , , ,			

	Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sur parhidity meter		7.7.7.2777

WELL ID: MW 62 15 SAMPLE ID: O 1 1

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE; WEATHER:	Entergy IPEC Buchapan, NY	4. wad	y 403	-	PROJECT NO: DATE: SAMPLER(S):		01.0017869.92	2 0 <sup>1</sup> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
SAMPLING IN	TERVAL (depti		of casing)	_		ME PURGED:	2.0	gal	
SAMPLING P	0RT   138	-		3	PURGE METE	: widde (8 100:	ar <i>r</i> min) Double Valve P	чтр	
WATER QUA	LITY:								
Time	Purged Volume	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (5U)	ORP	Tarbidity (NTU)	Drive/Year Cycle (seconds)	Drive Pressur (psi)
1105		POMI	C/3					162 143	30
1113	0.1	133	1629		1 2 3	1021			
1421	10.4	16217	1164	Q: 2k.	<u> </u>	115211	<u> </u>		
1421	06	11617	1 111	0,40	121	310	ŢŢŢ	<b></b>	
14 35	Luc		يكيا إلىا	ļ2.2 <u>c</u>	1 226			•	
<u> </u>	<u></u>			1 047	7,25				
1945	1,25	Like like		2223	7.24	774.3	2.6		
1,450,				2.26	7,2,1	13.0	800		
1155	5.708.1	Anikit	111111	mil	1				
122	ENDI	risi C	Lichtel	10. J: 24	J 126				and the second s
	7 7 11 11 11	FF							
****									****************************
				<b></b>					
					<u> </u>				
					<del> </del>				
		ļ	and a superior of the superior	***************************************					partie e e e e e e e e e e e e e e e e e e
		<u></u>				·	Andready and the second		Name apply control of the second of the seco
	<u> </u>						***************************************		A0000000000000000000000000000000000000
		•	***************************************						A COLOR
							**************************************		***************************************
			***************************************	-	***************************************		-	************	**************************************

Equipment Used	Equipment Identification #
VSESS6 MPS Reader and 5563 Sande	<u> </u>
surfiedity meter	400704243

WELL ID:	MW	<u>l</u> .	18.2
----------	----	------------	------

SAMPLE ID: \_\_\_\_C 1 1

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy IPEC Buchanan, NY	y win	14 403		PROJECT NO: DATE: SAMPLER(S):		01.0017869.92	12 07 M B	~
SAMPLING IN	TERVAL (depti		of casing)	-		ME PURGED:	1.45	_gal	
SAMPLING P	ORT			***************************************	PURGE METI		Double Valve P	ump	***************************************
WATER QUA	LITY: Purged Volume (gal)	(roup (°C)	Specific Conductivity (Sem)	Dissolved Oxygen (g/l)	ρΗ (SU)	ORP	Turbidity (NTU)	Drive/Vens Cycle (seconds)	Drive Pressun
1455	01	70.M7 15.51	1 311	039 C 11	433	-165	3, 4. 1	43	30
142	<u>0</u> 4	16.52	1 214		7.24		8.85		
115		6.00	1.316	0.53 3.33	1.33	14.7	0.00		
135		\$20114121 \$41221 \$565			16 3 GE				
		ļ		************	***************************************				***************************************

Equipment Used	Equipment Identification #
YSI 586 MPS Reader and 3563 Sonde	Q.
in bulity meter	200104243

CLIENT: SITE: WEATHER	Entergy - BEC Buchanan NY C NAME 50 S	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 111/3/ごら ことがいる 14.9 「
-----------------------------	---------------------------------------	--	--

Time	OTW or Actual Depth	Tengo (°C)	Specific Conductivity (\$70m)	Dissolved Oxygen (s/l)	ρ <b>Η</b> (SU)	ORP	Turbidity (NTU)	Phrw Rate (gai/hr)	Notes
636.2	1.457.0	7×1111					~~~~	Z.	<b></b>
<u> </u>	7.733	್ಷಗ ಭಬ	2.60 32.	5 47	7.54	54.2			6.010
Till	7.80	17.24	1000	5.71	7.77	41.3	7.2.4		0 150
1120	7.967	17.18	1.352	·5.12.	797	484z	7.11	į	2.17
1934A	8.85	(7.25	1.30	5.30	1.45	340. %	7.40	6. [	10 15 1
7 J.Hu.	X.234	lik on	1.788	5.25	7.94	232	6.15	***************************************	0.2.
1514	3350	1-1-1-6	1.744	L vara	7.71	-113 4	Ų ĮI	***************************************	2.39
ستبكلنك	8.412	14.25	1.712	6.30	7.5%	33	2.92		2
2.15	8.533	13.91	1.70%	6.10	7.87	330	3.94		U
	3.948	13-32	1.710	k:349	7.34	: 2 - 2	3.23	•	2 34.
0.25	3.010	13.44	<u>1: 701</u>	12:11	7.36	13.1.	2.05	***************************************	J
\$ (-)	8.616	1312	1 443	V-30	7.925	243 .5	41.2.7	•••••	
3.5	5 610	13.11	1.432	7.3:	7.81	-16. ]	3,721		2 15 <sub>4</sub> ;
0.12	5.016	14.17	i viiv	1.13	7. 37	-18.5	1 34		J
046	3.747	14.49	1-12-08	7.74	3.01	37.9	5.05		
050	5.151	14.70	/ 933	1.51	3127	74.0	4.97	*******	0 23
095	8.772	14.14	1.22.2.1	TKO	3 64	-18 2	4.88	****	C.L.Car
00	8.760	14.35	1.380	7.83		70.0	4.1%		C. C.
u.U.	STAILT	Semi	LE LOLI	ii aa					
		$m_1$ $\sim$ $\sigma$	(2346%)	347V					
	Tzukilu		*******			********	~~~	•••••	
									************************

Equipment Used	Equipment Identification #
YSL556 MPS Reader and 5563 Sonde	3
thus meter	
nut hiddty meter	2007/12/4

NOTES AND OBSERVATIONS:

Total volume purged 0 3 gal

Ocpile and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in teet inst.

CLIENT: Entergy - IPEC SITE: Buchanan, NY WEATHER: SWAM; SV 5	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 11 <i>124年</i> ころいち 31.5 f
---	--	---

WATER Q	UALITY:	DTW =	(10.41)	Transd	ucer Actua	i Depih 🦸	5.834		
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (\$/cm)	Dissolved Oxygen (g/l)	pH (SU)	orp	Turbidity (MTU)	Flow Rate (gal/hr)	Notes
12.1	16.215	Pane							
903		Pains2		LAGGLI	سمندسا	Litiza C	***************************************		*****
000		PWM	<u> </u>				***************************************		
910	110 553	112:52	1.22	2.12	12:30	39.7	SP2 7		2544
6,50	10.534	11:221	1:3:21		18.07	28.12	15 4 7	*****	. a <u>S</u> .
2136	110.6/12	110.59	1. 3/24	2.43	1:22	312	11.35		kar a
0946	100.50.3	110.10.	1.301			39.4	1.54		Cuida
00512	112 916	110.13	1.391		122	43.3	242		
19 02	170. <u>uzi</u>	116.115	221		17.2.1	111.3	132	******	1.02/2
1015	17.108	10.01	1.308	2.37	7.30	20.5	3.26	**************	
10.10	111.153	15.16	1.344	6.31		_علاقــــا	0.63		344
10 6/2	Trudz	115.13	1394	LC31	7.34	L22.g.	1.10	AAAAAAAAAAAA	.3
1030	11.2.35	15 26	1.4.20	021	7.74	-31	222		******
10.54	17,249	15/13	1700	071	1.34	535	000		ئېنگىل
10 4	STAGLE		LE COUL						£.
1102	I (NO )	hould	232-50	112.04	122.12	C.C.			***********
A	17 <u>00 mil 2</u>		***********					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	*************
41									*********
		<b></b>	***********************				*************		
~~~~			AAAAAAAAAAAAAAAAAAAA					*****************	
			***************************************			<b></b>	***************************************		
									******************
MARINE S SERVICE CONTROL CONTR									*************
									***************************************

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
tion mater	3
turbidity meter	200 201259

NOTES AND OBSERVATIONS:

Total volume purged 1.76 gal

Depth and Depth to Water (DTW) measurements are given in feer from top of casing.

Groundwater filevation measurements are given in feet msl.

WELL ID:	MW	(23	-	<u> </u>
----------	----	-----	---	----------

SAMPLE ID:	
------------	--

SITE:	Entergy IPEC Buchanan, NY	<u> </u>	200	-	PROJECT NO: DATE: SAMPLER(S):	<del>(1100,000,000,000,000,000,000,000,000,00</del>	01.0017869.92 11/3/04 63/416		-
AMPLING IN	TERVAL (depth	in A below top	of casing)		TOTAL VOLU	ME PURGED:	265	ea)	
	41.5	to .	53.0		PURGE RATE	: <u>yariable</u> (g		• •	
SAMPLING PO	рят <u>50</u>				PERGE METH	HOD:	Double Valve P	nuib	
WATER QUAL	LITY:								
Time	Parged Valume (gal)	Temp (°C)	Specific Conductivity (\$/cm)	Disselved Oxygen (g/l)	pH (SE)	ORP	Turbidity (NTU)	Drive/Vent Cycle (veconds)	Orise Pressure (psi)
		30.31		•				IICIII.	24
71345		2.2	342	<u> </u>	<u> </u>	1 22 2 2	<b>_</b>	ļ	
7 4 49 5	1 1		<u></u>	<u> </u>		1:39 4	1249		<b>_</b>
3 (2 (2 )2	12			<u> </u>		ļ2:1::3	13.12	<b>.</b>	ļļ
-01L	1		3:4	1. 4. 4.		<u> </u>	14.73	<b></b>	<b>.</b>
	J			,			10.00	<b>}</b>	<b></b>
	1 2 2			<u> </u>	7.3.2			····	<b>_</b>
	123			<u> </u>	<b></b>	<u> </u>		<b></b>	ļ
and the second				<b>.</b>	1.20 780	<u> </u>	<b>}</b>	<b></b>	<del> </del>
				<b>h</b> eris		**************************************	***************************************	•	<b>†</b>
1 1 1 1 1 1					<b>†</b>	<u> </u>	<b>†</b>	·	•
		<u> </u>		<del> </del>	<b>†</b>	***********************	***************************************		<b>****</b>
,				***************************************	***************************************		<u> </u>	•	<b></b>
			**************************************			\$00000000000000000000000000000000000000		***************************************	
	\$	A STATE OF THE PARTY OF THE PAR	>	· · · · · · · · · · · · · · · · · · ·	· y · · · · · · · · · · · · · · · · · ·		4	A	A

	Equipment Used	Equipment Identification #
	St 556 MPS Reader and 5563 Some	/·×
1	thulary meter	2000 76 92 93

WELLID: MW 63 . 93

SAMPLE ID: 012

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY		PROJECT NO: 81.0017869.92 DATE: 11/2/0억 SAMPLER(S): ビデジャルプ				
SAMPLING	NTERVAL (depth in ft listow t	op of casing)	TOTAL VOLUME PURGED:				
	<u>81.5</u> w	100.5	PURGE RATE: ** ** ** ** *** ********************				
SAMPLING	PORT		PURGE METHOD: Double Valve Pump				
	<u> </u>	5					
200000000000000000000000000000000000000	**************************************						
CACCOMODES PARS	. የ የ <b>ም</b> ህ ,						

#### WATER QUALITY:

Time	Purged Volume (gail)	Contract Con	Specific Conductivity (Sector)	Dissolved Oxygen (g/l)	p <b>H</b> (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psr)
0425									
	3.1.2					. 47.5			
0455		75.49	1.302	() 1112	7 34	22.9	3 19	ļi	
.10.12		35 75	1 274	030	13.2	222	1.52		
1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	1 5 4	5.13				. 2 0	0.00		
10.8				22.2.3			000	<b></b>	<b></b>
2073	3 (	15.4.3	1 247			<u> </u>		<b></b>	
10.3.0		15 43				<u>32</u>		<u> </u>	- Y
120.2.1		<u> </u>		<b></b>		<b></b>	•	•	
1.2.2.2.					ಚಲ್ಟ್	<b> </b>	<b></b>	<b></b>	
1055			كتنسيط	48 DE N	***************************************	<b></b>		<b></b>	
112512		<u>llyma</u>	<u> </u>				; <b>;</b>		
				·	<b></b>	<b></b>	<b></b>		**************************************
		***							*****
				***************************************	***************************************	**********************	\$ \$4 \$		****
				<u>.</u>		***************************************		***************************************	
							<u> </u>	***	***************************************
			: 5			<b></b>	<b></b>	<b></b>	
						<u>.</u>		<u>.</u>	
			, , , , , , , , , , , , , , , , , , , ,				<u></u>		
			<u>.</u>	•	***************************************				
		ļ		•	·····	<b></b>	<u> </u>		That there exist a translate communication,
								<del> </del>	
		}					(	L	

Equipment Used	Equipment Identification #
VICLASA AIDE Duraber and 5563 Suitale	
Surbolity meter	1007104743

WELL ID: MW	63.112
SAMPLE ID:	011

CLIENT: SITE: WEATHER:	Entergy (PEC Buchanan, NY			PROJECT NO: DATE: SAMPLER(S):	•	01.0017869.92 11.13.10 6.63.101	9	•	
SAMPLING IN	TERVAL (depth	in ft below top	of casing)		TOTAL VOCE PURGE RATE	ME PURGED:	2 05	_gal	
Sampling P	08T 	ussessania issuotaanna ouroccion	4	222222000000000000000000000000000000000	PURGE METI	(OD:	Ocubie Vaive Pr	ыяр	
WATER QUA	LITY:		,,,,,,,,			<b>y</b>		***************************************	·
Time	Purged Volume (gal)	Femp (°C)	Specialic Conductivity (Scott)	Dissolved Oxygen (g/l)	ρΗ :SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	}
0925	(,)			***************************************				12.24	
2345				ļ	1	<u></u>		<u></u>	·
2922	्रिय			ليقتناكم	1 2 3 9	- 4 <u>4</u> -4	2.30	<u> </u>	
0.85	A B		1244	<u>ļ. ņ </u>	ļ2			<b></b>	<b></b>
1011	LIL B				1 2 3 1	<u> </u>	12.33	<b></b>	<b>.</b>
1015				18 27	<u> </u>	1-14-6-	000	<b>}</b>	<b>-</b>
1023	<u></u>		<u> </u>	8 24	7.34	4 5	000	<b></b>	<b>*</b>
<u> </u>		15.22						<b></b>	<b></b>
	1.2.			102	7 3 4		000	†	· · · · · · · · · · · · · · · · · · ·
		, s. s.is. stálico dirección es 			<b>4</b>	<b>*</b>			
				Tie co	NECHO				
		SAMEL	C CADAMA?						
		PUNC.		<b></b>		<b></b>			
**************************************				ļ	<b></b>			ļ	
200000000000000000000000000000000000000				-	<u> </u>		<u> </u>	<b>}</b>	
				<b></b>	<b></b>		<u> </u>	<b>\$</b>	
				<del> </del>	<b></b>	<b></b>	<b></b>	<b></b>	
			<b></b>	<b></b>	<b>,</b>				****
				<b></b>	<b>†</b>			<b></b>	

Equi <b>pment Used</b>	Equipment Identification #
YSLSS6 MPS Reader and SS63 Sonde	
turbulary moter	20/01/20/4/25/5

WELL ID:	MW	63	121
SAMPLE II	D:	OΚ	

CLIENT: SITE: WEATHER:	Entergy (PEC Buchanan, NY	Classis	<u> 50.5.</u>		PROJECT NO: DATE: SAMPLER(S):	000000000000000000000000000000000000000	01.0017 <b>869.92</b> 11] 3 [c 		
	TERVAL (depth	in ft below top	of casing) 127.5			ME PURGED:	1.45 (al/min)	gał	
Sampling P	121		3		PURGE METI	IOD:	Double Valve P	nwb	
WATER QUA	LITY:								
Prise	Purged Volume (gai)	Temp ( <sup>3</sup> C)	Sponsie Conductivity (Szem)	Onsolved Oxygen (g/b	pH (SU)	ORP	Turbidity (NTU)	Drive/Vieta Cycle (seconds)	Drive Pressuo (psi)
								17574	25.3
0432		35222	1 5 1 3			<u> [.:557/4</u>	****		
5355			1 247			<u> </u>		1	
1. 1. (11)			1144			كمعتششا	1131		<u> </u>
10033			1952			30.7	1150	<del> </del>	ļ
10 S			23.3	1043	<u> </u>	. 347 7	ئينا	<del>}</del>	ļ
3			1.3.5.2	1949	<u> </u>		<u> </u>	ļļ	<b></b>
1		1.5.5.1						<u> </u>	
11131	<u>G</u>		344		7 3 3		<u> </u>	·	
1 11 12 12 12			ka ka kalendara da kalendara da				123	<u> </u>	<b> </b>
] 11 12 1			4.13.35 1.53.5	0.20	7 : 5	1.934	2 2 5	<del> </del>	
110%					<u> </u>			•	<u> </u>
<u> </u>				Par co		<u> </u>	. <del> </del>	<b>†</b>	
		S I AND						<u> </u>	
			C V F			AMMONDA ASS	. 62		
		1 Mainin		***************************************		***************************************			
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				***************************************			•		
		***************************************	60204						
· · · · · · · · · · · · · · · · · · ·									
a dia philiphopophical graph of the St. 1.									
	Significan coccosticitisticitis								
\	Ada, No Congression of the		.,,	······································					
		8.	quipment Use	ed			Equip	nent Identifica	ation #
V 10 48 1108	Reader and 5563 S	mile						3	

NOTES AND OBSERVATIONS:

turbidity meter

WELL	ID;	MW	63	-	163
WELL.	Ю;	MW	<u>. د ک</u>	-	165

SAMPLE ID:	

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY Sign and Si	PROJECT NO: DATE: SAM <b>PLER(S)</b> :	01.0017969.92 11/2/21 ESIME
SAMPLING !	NIFRVAL (depth in ft below top of casing)	TOTAL VOLUME PURGED	e gal
	150.5 to 165	PURGE RATE: Yanishie	(gal / min)
SAMPLING 3	<b>₹)RT</b>	PURGE METHOD:	Double Valve Pump
	163 2		
		000000000000000000000000000000000000000	

#### WATER QUALITY:

Tipae	Purged Volume	Oʻi qarsi	Specific Conductivity (Sicm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drise/Vens Cycle (seconds)	Orise Pressure (psi)
	~	€ CME	DALLE.			***************************************		122/40	
and a substantial and		17,45 A				- 340			<u>X</u>
and the second	0.5	17.7.0							and the state of t
		17.22	0413	0.62	7 3			<b></b>	
		17.81	11 2 2 1 1 1 1	0.15	7				<u>}</u>
2.60			0 000 <b>1</b>		7.16	- 1669 S	1.03		·
		11.13		2.35	7.16	Likk 1	1.77		<u> </u>
11.45	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.			<u> </u>			2.17	<u> </u>	<del></del>
							000	ļ	
		11111					0.00	ļ	<u> </u>
132							1.00		
17,000	1 1.150				2.15				
1/4/2	1 7.75	. 81				کا انتخابات		<b></b>	
1915		10.85	2.231		7.4.				
	7.44	6	سلتلاسكسك		1		<u> </u>		
	Ininit	Samula			<b>[</b>	***************************************			<b>.</b>
		<u> </u>		<u> </u>	X ( 2 C				
	T I WAY		<u>.</u>	<u> </u>	<b>.</b>				•••••
				} }	<del>[</del>		•••••••		
					<b>,</b>			•••••••••••••••••••••••••••••••••••••••	************************************
				ļ					
					<u> </u>				
					ļ				

Equipment Used	Equipment Identification #
YSLSS6 MPS Reader and 5363 Sonde	.35
turhidity motes	

WELL ID: MW	<u>63</u> .174
SAMPLE ID:	Oil

LENT: SITE: WEATHER:	Emergy - IPEC Busharan, NY Son a Cloud to SD 3				PROJECT NO: DAYE; SAMPLER(S):		01.0017869.92 11173.04 645.64	à	-
SAMPLING IN	TERVAL (depth	in N below top	of casing)		TOTAL VOLU	ME PURGED:	240	gal	
	1650	to	1911	,	PURGE RATE	: variable is		** &	
SAMPLING P	⊖RT				PURGE METH	wh.	Double Valve P	h	
	1774				FURGE MEAR	N./L/;	DOGGIC A SIAC L	amp	*******************************
WATER QUA	LITY:								
l'iss <b>u:</b>	Parged Volume	Yesip (°C)	Specific Conductivity (Sem)	Dissolved Oxygen (g/l)	pM (SU)	OKP	Tentuciny (NTU)	Drive/Vent Cycle (seconds)	Onve Pressure (psi)
1156		FUM					<b>4</b>	<u> </u>	1 244
k						1 2 2 2 1		<u> </u>	
	10.15	11		0.4.2	<u> </u>	Lalle S.			<b></b>
	TO 350				42	L 42 11		<b></b>	<b></b>
1222		123		Landon Maria	1 1, 21	<u>L. 10</u> i	L.J. 44.4	<b></b>	<b></b>
1130		7. *** 3	4.37.4					<b>ļ</b>	
	1.12		4.333		1 2 2 2 2 2 -		4.25	<b></b>	
			<u> </u>	0.17		<u> </u>	3,75	·	<b></b>
.,, 0			2.323	\$1,0,000 000 000 000 000 000 000 000 000		_ :	1	•	<b>,</b>
1755					4		<b></b>	<b>.</b>	<b></b>
	1 50		4. 3.13	2 34	131		7.3	<b>†</b>	<b>†</b>
			F 15 12 19 57		<u> </u>	\$ 2.00g B		<u> </u>	<b>†</b>
للمالينسي		10.08			<u> </u>		1027		<b>†</b>
	1	112:11	0.35	0.16	1.22	5.7	0.00		
			L 0.334.		1				
and the second second	والمنازع والمنافق والمناف والمناف والمنافظ والمنافذ والمن	Arrest Manager Land	14 12 3 19	1	119 19 2	1	ł	3.	3

000000000000000000000000000000000000000	Equipment Used	Equipment Identification #
	YSF 556 MPS Reader and 5563 Sonde	4
ĺ	(urhality meter	1007=4243

WW	
WELLID: WELLI	
SAMPLE ID: DR	

CLIENT: Entergy-IPEC SITE: Buchanan, NY WEATHER: (LOSED 1 , SU:	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.8017869.92 (1.111/077 
-----------------------------------------------------------------	----------------------------------------------------	---------------------------------

WATER QU	ALITY	DTW=	11.860			Depth 3	, some		
Time	OTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen ug/D	p <b>H</b> (SU)	ORP	Turbidity (NTU)	Flow Rate (gat/hr)	Notes Aud
J 1965 3	3.520	Pari	<u> </u>					Z	
1000	2-309		1.832	ll L	7.50	111.3.	. 20002	****	
ibili	8.235	בני בני בני	1.697	and and a	100 16	***************************************		*****	
1010	5 HZ	17.35	1.579	S. 314	& 1S	1954	0 18		
1014	PUMP	orr	****	*****	***********			ing new new contract to the second of the se	
1030	POMP.	<u></u>	***************************************						
1032	3135	17.35	1512	0.39	641	174.3			
1046	5 238	16.12	) <u>569</u>	0.26	700	: 1915	3.4.7		C
1045	8 75	1231	1.011	10.15	12:21	1758	1.30	*******************************	1225
1125	3.177	141.16	1:452	1.49	1.04	1120			415
11112	8 37	14.76	1.045	سيقيما	7.62	<b>*</b>	8.66		1:25
1115	8.110	14.17		0.49	202	178.5	7.12		***************************************
1120	2.127	14.40	huduummir	2.52.	2.63	1919	3.18	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
1175	5 254	MUY		0.52		11111	3.54		<b></b>
	141 241 L	1331	1 650	2.22		41124	S. V. I		
	L ALL	L. MINE	Andreas				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
1 242					Ladri		*****		····
	TYMES.	L. C.		************					www.
		<b></b>							•••••
		<u></u>				****	<b>,</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	p. 40, 40, 40, 40, 40, 40, 40, 40, 40, 40,	
has an annual to the second se							w		······
									***************************************
			Addresis					*****	
									***************************************

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	3.
nurhidity meter	202701234

SOTES		n.	ORS	FR	V.A	TH	388:
VOTES	11	13	OBS	L.K.	٠,٦	. 1 13	<i>3,</i> 33

Total volume purged 1: 2 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Coundwater Elevation measurements are given in feet msl.

WELL	ID:	M	إنكأ	ي) ي	2.0	À.,
SAMPI	E I	D:	0	; (1)		

CLIENT: SITE: WEATHER	Entergy - IPEC Buchanan, NY				PROJECT DATE: SAMPLE: PUMP DE	R(S):	01.001786 11/11/2 	e-{	ft
WATER Q	CALITY:	DTW =	แนวอ	Transd	icer Actua	Depth [6]	5.ŭeD		
Time	OTW or Actual Depth	Temp (°C)	Specific Conductivity (Szcm)	Dissolved Oxygen (g/l)	р <b>Н</b> (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
0003	147300	Plint				<b>3</b>		2	J.,
1000	1153	/5/11	2.318.	1.75	12:21	235.8	,,,,,,,,,	****	001
1010	14470	16.14	2.308	0.91	7:11	233.3.	3.03	*****	*******
1020	14423	22.22	1.12>	1.42.22	7.22	2363	Q.X.2-	<b></b>	**************
1024	PLLEYIP	CFF	1.72me 0	علسمت	1.2. No	Laudee	hi.		******
1030	<u>fons</u>	200							
1046	14.278						$S \cdot 2$	~~~~	1.15
10-5-5	14.77.1	5 60%	3-353	0.35	1.41	23154	3.1.1		1.25
11052	14 252	13:42	_2_331	4.55	2.34	233.5	1.51	~~~~	***************************************
1112	111111	12.21	2.334	£.33	7.3%	2341	4.74		***************************************
LLL12	17.274	12.47	2-381	1,40	3.39	2.3±	254	***************************************	***************************************
1120	14.142	14.32	2-334	231	7.39	234.3	3.47		Y
1115	14.244	17.60		0 45	7.34	234.4	3.36		
	سنشلش للسنسال	***************************************			<i>.</i>	•		*****	~~~~~
<u> Zi</u>						<u> </u>			***************************************
	r William	22.7			***************************************			******************	***********
				*****					M
		<b></b>	<b></b>			***************			••••••
<b></b>	<b></b>	<b></b>			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	····		***************************************	
	-				*************				
				***************************************		**************		***************************************	***************************************
			••••		*****************				
					*******				
					************	***************************************			************************
	<u> </u>	<u> </u>		i			L		
:			Equipment	Used	***********	***************************************		Equip Identifi	
7107 556 14	PS Reader and .	563 Sanda	· · · · · · · · · · · · · · · · · · ·	7.555				. ?	rativit n
	ro Reader and .	DIE TRANCE	· ••••••••••••••••••••••••••••••••••••				· · · · · · · · · · · · · · · · · · ·		***************************************
flow meter					*****************	· · · · · · · · · · · · · · · · · · ·		200 101	
harbidity me	SIEL					~~~~			4-2-1

NOTES AND OBSERVATIONS:

Total volume purged 1 52 gat

Depth and Depth to Water (DTW) indissirements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 67 . 39

SAMPLE ID: Oll

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

SITE: WEATRER:	Entergy - IPEC Buchanan, NY Cloudy, windy 50's		PROJECT NO: DATE: SAMPLER(S):	01 0017869.92 11/11/09 Cb, MB
SAMPLING I	NTERVAL (depth in ft below top of casing)		TOTAL VOLUME PURGED	<sup>1</sup> 2.05 84
	28.8 % 54.3		PURGE RATE: variable	and finish
			PURGE RATE: STIANS	gal / min)
SAMPLING I	PORT		PURGE METHOD:	Desole Valve Pump
	39	7		

#### WATER QUALITY:

fine	Purged Volume (gai)	Yensp (**)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH :803	ORP	Turbidity (NTU)	Drive/Vent Cycle (spcmds)	Orive Pressur
		PUM	ON.					8 1 3	22
1324	0.5	1610	2.440	0.73		-55.9	***************************************		<b>,</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
330	Q.7	16.21	2.464	0.51		782	4.74	<b>_</b>	<b> </b>
1335	0.9	16.34	2.470	0.45	7.76	= 117.2	4.49	ļ	
1340		16.28	2.479	041	7.78	-1215	4.12	ļ	<b>-</b>
345	3	16.15	2 480	0.41	7. 19	-140.4	2.82		<b>}</b>
1350	1.6	16.25	7.480		7.80	-137.5	3.80	<b></b>	
1355	1.9	16.25	2.485	0.40	7.81	-140.2	3.00	<b></b>	X
356		PUMP	OFE	*	5 6° 22 6°0 23	iai	••••	***************************************	
1397		SINKI	SAMI	PLE TE	reimin	L ave	es.		
1409		SOME	OFF		<u> </u>		<u> </u>	<b></b>	
11509		PUMP	Car e		***************************************	<del> </del>		<b>†</b>	
								<b>}</b>	
						<b></b>	*****	<b>}</b>	
	<b></b>				************	***************************************		<b>*</b>	<b>*****</b> *******************************
						<b></b>		<b>*</b>	<b>************</b>
		<b></b>				<b></b>		<b>*</b>	<b>\$11.11.11.11.11.11.11.11.11.11.11.11.11.</b>
		ALLES AND			***************************************	*************		***************************************	<b>*</b>
	<b>_</b>			<u> </u>	***************************************	<b>************</b>	******************************	***************************************	******************
						<b>†</b>			
	<b></b>			<u></u>	<b></b>	<b>†</b>	<b>\$</b>	<b></b>	
	<del></del>			<b></b>		•		•	***************************************
	<del> </del>		;	-	<del></del>	*******************************		<b>\$</b>	•
	<u> </u>	<u> </u>	<b></b>			<b>}</b>		<del>*</del>	<del>}</del> -

Equipment Used	Equipment (dent <b>ification #</b>
YSL556 MPS Reader and 5563 Sonde	S. plan
suchslity meter	200704293

WELL ID: MW 67.105

SAMPLE ID: OIO

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

SITE: WEATHER:	Entergy - IPEC Buchanan NY Cloudy, Windy 50's		PROJECT NO: DATE: SAMPLER(S):	01.0017869.92 01.0017869.92 08, MB
*******************				
SAMPLING E	VTERVAL (depth in it below top of casing)		TOTAL VOLUME PURGED	1.65 za
	90.3 " 110.8		PURG <b>E RATE:</b> variable	(gal / min)
SAMPLING P	ORT	6	PURGE METHOD:	Double Valve Pump

#### WATER QUALITY:

3	Drive Pressur (psi)
1324   0,2   15.59   1620   0.35   6.84   192 6   5.67   1335   0.4   15.83   1.624   0.29   6.93   1964   5.49   1340   0.6   15.86   1627   0.30   6.95   1937   6.40   1345   0.8   15.74   1631   0.29   6.97   189   3.26   1350   1.0   15.78   1633   0.29   6.97   189   3.26   1400   1.2   15.71   1640   0.30   7.03   200 6   3.29   1407   1.5   15.76   1645   0.30   7.05   2012   3.20   1408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.40	22
1330 0.3 15.67 1.624 0.23 6.93 1.964 5.49 1.335 0.4 1.586 1.627 0.30 6.95 1.937 6.40 1.345 0.8 1.574 1.631 0.29 6.97 1.89 3 2.47 1.350 1.0 1.578 1.633 0.28 7.00 1.89 3 2.47 1.400 1.2 1.577 1.640 0.30 7.03 200 3.29 1.407 1.5 1.576 1.645 0.30 7.05 200 3.29 1.407 1.5 1.576 1.645 0.30 7.05 200 3.29 1.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.408 0.40	
1335 0.4 1583 1.624 0.27 6.93 1.964 5.49 1340 0.6 15.86 1.627 0.30 6.95 1.937 6.40 1345 0.8 1574 1.631 0.29 6.97 1.89 3 2.47 1350 1.0 1578 1.633 0.28 7.00 1889 3.26 1400 1.2 1577 1.640 0.30 7.03 200.6 3.29 1407 1.5 15.76 1.645 0.30 7.05 201.2 3.20 1408 0.40 0.50 7.05 201.2 3.20 1408 0.40 0.50 7.05 201.2 3.20 1409 5TAP DEF	
1340 0.6 15.86 1.627 0.30 6.95 1.937 6.40 1345 0.8 15.74 1.631 0.29 6.97 -1893 2.47 1350 1.2 15.78 1.633 0.28 7.00 -1889 3.26 1400 1.2 15.71 1.640 0.30 7.03 -200.6 3.29 1407 1.5 15.76 1.645 0.30 7.05 -201.2 3.20 1408 PUMP DEF 1409 START SAMPLE COLLECTION 1409 START SAMPLE COLLECTION	
1345 0.8 15.74 163 0.29 6.97 -189 3 24 1 1 2 5 1 1 2 5 1 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2 5 1 2	
1350   10   15.78   1633   0.28   7.00   1889   3.26   1400   2   15.77   1.640   0.30   7.03   200.6   3.29   1407   1.5   15.76   1645   0.30   7.05   2012   3.20   1408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408   0.408	<b></b>
1407 1.5 15.76 1.645 0.30 7.05 -2012 3.20 4 1408 PUMP DEE 1409 START SAMPLE GOLLECTION 1431 SAMPLE GOLLECTION	
1408 PUMP OF F 1409 START SAMPLE COLLECTION 1431 SAMPLE COMPLETED : 2 LIPEC	
1409 STAR SAMPLE GOLLECTION SAMPLE COMPLETED: 2 L IPEC	
SAMPLE COMPLETED : 2 L IPEC	
	<b></b>
	<b>,</b>
	<b>,</b>
	······································
	<b></b>
	<b></b>

	Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde		3
turbidity meter		200704293

WELL ID: MW 67 . 173

SAMPLE ID: 011

#### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER: Entergy - IPEC

Buchanan, NY

50'3

PROJECT NO:

DATE:

SAMPLER(S):

SAMPLING INTERVAL (depth in ft below top of casing)

164.8

188.3

TOTAL VOLUME PURGED:

1.35 gal

PURGERATE: variable (gal/min)

PURCE METHOD:

Double Valve Pump

SAMPLING PORT

173

5

#### WATER QUALITY:

Time	Purged Volume (gai)	Temp (C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/3)	p#1 (SU)	ORP	Turbidity (NTU)	Cycle (seconds)	Orive Pressure (psi)
1311	0 1	PUM	PON					18 18	22
1374	0.1	15.61	0.998	0.76	6.63	220.7	<del></del>		
1330	0.2	15.77	1025	0.41	6.55	1930	623		
1335	0.3	16.00	1.045	0.22	6.53	155.1	6.36		
1340	0.4	15.93	1.071	0.12	6.52	116.4	3.92	<b></b>	
1345	0.5	15.87	1.082	0.09	<u> </u>	63.1	4.06	<b></b>	
350	0.6	15.96	1.086	0.06	6.52	=17.2	3.86	ļ	
402	Q.8	15.99	1.080	***********	6.56	-39.7	400	ļ	<b></b>
1916		16.01	1074	0.05	6.59	= 49.9	3.92	·	
1321	1. 1	16.06	TOOL	0.06	6.60	= 476	388	<b></b>	
1426	1.2	16.03	1.0 <u>68</u>	0.05	6.60	< <u>+</u> _&_5_	3.95	<b></b>	<u> </u>
1427		PUMP	QEE	731 = -3			\$00,00,0000000000000000000000000000000	<b></b>	
1 2 2 2		STACI	SAM	PLE CC				<b></b>	
1450		<u>sam</u> y		PLE TET	· · · · · · · · · · · · · · · · · · ·	L TPE	<u> </u>		
1450		PUMP.	OF E			***********			<u></u>
a did a dia manda managana and a did a			y , , , , , , , , , , , , , , , , , , ,		************************		****************		
			************		*******		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
***************************************			*******	<b></b>		************************		ļ	
***************								<b>}</b>	
							**************************************	<b></b>	
							********	<b></b>	
****************					***************************************		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<b></b>	
	***************************************		***************************************				*********	<b>*</b>	<b></b>
	1						Nacional de la compansión de la compansi		

Equipment Used	Equipment Identification #
YSLSS6 MPS Report that 9863 Sende	2
(turbidity meter	200704293

WELL ID:	MW	<u>SIL</u>	`	211
SAMPLE II	D:	Oic	:	

CLIENT: SITE: WEATHER:	Entergy IPEC Buchanan, NY		PROJECT NO: 01.0017869.92  DATE: 3.1 / 11   55    SAMPLER(S): (3.0 / 13 / 3 / 3 / 3 / 3 / 3 / 3 / 3 / 3 /	
************************				
Sampling 8	NTERVAL (depth in it below top of casing)		TOTAL VOLUME PURGED:	
	<u> 229 S</u>		PURGERATE: variable (gal/min)	
SAMPLING	PORT		PURGE METHOD: Souble Valve Pump	
		4	,	
estimate an example and exampl		***********************		,000000
SVATER QU	ALITY:			

(in <b>x</b>	Purged Volume (gal)	Temp (°C)	Specific Conductivity (\$50m)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vers Cycle (seconds)	Drive Pressure (psi)
0.535.7	£2	<u>Carri</u>			* * * *		****************	<u></u>	***************************************
300	0.2	16.17	1 33	<u> </u>		<u> </u>		J. Sii	
	<u> </u>	14.24		0.53		<u>- 70.4.</u>			
111.4.6	1 1	11.13	4 + 5.34.6.8	Cac	1		157		
000		15 17	11111	1 21	1.2.25.2		formation consideration and the con-		
		16 39	1362	LO AY	7.20		<u></u>	<b></b>	****
1053	3. 7	122.22						ļ	
1165	2 9	222.92		LLLLL	7	1152 7	1.25	¥	· ·
1.04						<b>*</b>			
17785		SALTA	I SAN	III had	ale CD		<b>_</b>		************
1116		المست		CALINI	<u> </u>		Li	***************************************	
1116				<b></b>		***************************************		***************************************	
	T	<b>.</b>							
		<b></b>		<b>,</b>	•			<b></b>	····
				**************	•				
				•		****************	*****************		
			<b></b>	***********************			<b></b>		
			<b></b>			<b>}</b>			
			<b></b>	***		<b></b>			
							<b></b>		
						} ••••••••	<b></b>		
						<u></u>			***********************
			<b></b>						
	1								

Equipment Used	Equipment Identification #
Y SI 556 MPS Reader and 3563 Sonde	á.
turbishry meter	20070733

SAMPLE ID: CHO

## GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: SITE: WEATHER:	Entergy - IPEC Buchanan, NY  Lucid / Lucid / 525		PROJECT NO: 01.0017869.92  DATE: 11 12 13 13 13 13 13 13 13 13 13 13 13 13 13
270000000000000000000000000000000000000			
SAMPLING INTERVAL (depth in ft below top of casing)			TOTAL VOLUME PURGED: 2 75 gal
	250.5 to 233.3		PURGE RATE: <u>variable</u> (gal/min)
SAMPLING I	PORT		PURGE METHOD: Double Valve Pump
	276_	.3	
		**********	

#### WATER QUALITY:

Time	Paged Valume	Comp (°C)	Specific Conductions (\$/cm)	Dissolved Oxygen (g/l)	p# 1585	ORP	Tarbidig (NTC)	Drave/Vera Cycle (seconds)	Drive Pressure (psi)
0957					***		<b></b>	<b>.</b>	
1021	0.2				<u> \$2</u>		<u> </u>	646	4.1
1011	6.6	<u> cz.el</u>			700		<del> ,,,</del>		<b></b>
3 C 2 k:		15.17	0462	<u> </u>					<b></b>
TO WELL		15.4.2		10223		<u>- 1 11 , 7, </u>	144.4		<b></b>
	<u> </u>	542		- Sq			3 ( )	<b></b>	<b></b>
16.22	<u> </u>			<u> </u>	725				<b></b>
1101	12		0 334				13.11	ļ	<u> </u>
1006				<b></b>				***************************************	<b></b>
1001		5424		المنتفضض المتعاربة				·	
1123	<u></u>		<b></b>	1726 123	* >		1	<del></del>	
11.13				ļ					
			<u> </u>	<u> </u>			-	·	<u> </u>
·					*****************		•		
						~~~ <del>}</del>	***************************************		
		ļ					<b></b>	•	
				<del> </del>					
		<b></b>		<b></b>					<u> </u>
		<b></b>		<b>\$</b>				1	<del></del>
		<b></b>		***************************************					1
				<u>†</u>			<u> </u>	-	
	-	<u> </u>		<b>†</b>			<del>\[ \]</del>		
				***************************************					
					***************************************		<del>                                     </del>	·	<u> </u>

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	*
turbidity meter	200109293

WELL ID: MW 67-323

SAMPLE ID: CIC

## GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

SITE: WEATHER:	Entergy IPEC Buchanan, NY	PROJECT N <b>O</b> : D <b>ATE:</b> SAM <b>PLER(S)</b> :	91.0017869.92 3.1 / 12 / C / I
***************************************	······································		
SAMPLING !	NTERVAL (depth in ft below top of casing)	TOTAL VOLUME PURG	ED: gal
	21/2	PURGE RATE: Satisfie	(gal/min)
SAMPLING I	TROP	PURGE METHOD:	Double Valve Pump
	333		

#### WATER QUALITY:

Time	Parged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved (haygen (g/l)	βH :SU)	ORP	Furbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
2437			000 <b>i</b>				*********************		47
1202		15.41	asse	100	Ø.40	. 50.3			
1017	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	15.31	CXX	C. 636			******************	<b>.</b>	
3 67 2 62	0.3	15.42	4		4	LLXLL			
104.1	1.62	12.14	<u> </u>	S		lazkasi			
1051	3	19.03		Simulari Si		220		<u></u>	
19.33	: 3	14 10		C222	4			<b></b>	
	7	14 14			2 / 2			<b></b>	<b></b>
	3	14 71	C33	. C	L <u>a</u>		andri Sandan	<u></u>	<u> </u>
		MOMO.		***************************************					
1 1 1 2					112.4.17	Kara		<b></b>	
			الإشييكسيك			112			***************
1134			4		<b></b>	·····			ļ
					**************************				} ************************************
					•	<b></b>			·····
				 	<b></b>	<b></b>		<u> </u>	
				į		<b></b>		<b></b>	
					ļ	<b></b>	***************************************		<b></b>
		<b>,</b>			<b></b>	<b>Ļ</b>			
					<b></b>	•		<b>_</b>	
				*******************************	<b></b>			ļ	<u></u>
				ļ	ļ	<u></u>		ļ	<b></b> .
					<b></b>				
				<b>Andreis</b>					-
Automorphism (Commons)						•			

	Equipment Used	Equipment Iden	tification#
Y St 556 MPS Reader and 5563 Sc		.15	
turbidity meter		2.070	<u> 4272                                  </u>

WELL ID: MW <u>67-340</u>

SAMPLE ID: Cho

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT Energy IPEC SITE: Suchanan, NY WEATHER:	>>>	PROJECT NO: 01 0017869.92  DATE: 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3336450000000000000000000000000000000000		
SAMPLING INTERVAL (depth in ft below top of casing)		TOTAL VOLUME PURGED:  gal  PURGE RATE: voriable (gal/min)
		PURGE RATE: (gal/min)
SAMPLING PORT	5	PURGE METHOD: Double Valve Pump
<u>340_</u>	4	
	*****************	

#### WATER QUALITY:

Tisse	Parged Volume (gail)	Yemp (*C)	Specific Conductivity (Stem)	Dissolved Oxygen+g/l)	pH (SU)	ORP	Turbidity (NTU)	Orive/Vent Cycle (seconds)	Drive Pressuri (psi)
0/4/2/2			(						44.7
istaa kantikaalaan oo oo Liistaa kanaalaan oo oo	1.7. Z.	15 33		1.6.1	4 34			<b></b>	<u> </u>
	1 () (4	15.51		0.52		12.2		<u></u>	
15 44		15.44	6 435	000	11111	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	Li 74		
1041	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	151	0.184	<u> </u>	2 2 3				
1051			0.39.2.		2.4.2	225 4	221		
		15.62	LC_LXX		7 2 2		3.33	1	<b>_</b>
1100	7, 0			4.23	7.2.2	1.2512		<u> </u>	<b></b>
11526		10000	<u> </u>			<del></del>	<b></b>	<del> </del>	
1111.	<u></u>	LIALI	Lialmii	<u> </u>					
1:22			is Suda	LLL IX.i)			J.S	-	***************************************
11.2x				<b></b>	<b></b>	<b></b>	<u> </u>		
				}·			<u> </u>		***********
ver en				<b></b>	***********************	<b></b>	<u></u>		
		<b></b>		<b>}</b>			-	-	***************************************
		<b></b>			*************			- <del> </del>	***************************************
		<u> </u>		<b></b>					~~~
		<b></b>		<b></b>	<u> </u>		<b></b>		***************************************
						<b>}</b>	<b></b>		ANNO CONTRACTOR CONTRACTOR AND A BANK AND A STREET AND A S
					<b></b>	<b></b>	<u>.</u>		
		<b></b>	<u> </u>	}		<b></b>	<u></u>		
				***		<b></b>			
		ļ	<b></b>				<b></b>	·	***************
			<del> </del>		<b></b>	ļ			
	1			1	Į	1	1	1	

Equipment Used	Equipment Identification #
YSLSS6 NPS Reader and 5563 Soride	45-
turbidity meter	

# GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: SITE: WEATHER	Entergy - IPEC Buchanan, NY Share - Court S SS S	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 11.1.2.1.6.9 
-----------------------------	--	--	-----------------------------------

WATER Q	CALITY:	btw =	9.09		icer Actual	Depth 7	<u> 535</u>	Transfer Transfer	Q 2 (8.2) (2	45
Time	DTW or Actual Depth	Temp > °C)	Specific Conductivity (\$/\$m)	Dissolved Oxygen 1g/0	pH (SU)	URP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure	Notes
340	7 5 74				,					~~~
1365			MY OFF	Ω.,	ls. c	llerild	<u>C </u>			
13.64		And the second second second second second	24.C. State		************				************************	·
1361	T7.324.			4.23	7.17	107			************	
1358	1216	and the second second second second	0 683	1. 63.1	7.46				************	******************************
1404	ln 123		0.643	1.18	7 26	615	50%		tita alatata alatata ata a ala gang gang gang g	
14 0				1.18			1118		****	***************************************
130.0.		<u>)</u>		1.21	118		<u>liži.</u>		tanki da	
		im 114.			111		254		***********************	~~~~
1445	11415		<u> </u>		1.20	<u> </u>				
440		15.54		19	1.14	ું જ	3.91		***************************************	***************************************
1445						324			***************************************	***************************************
1350		100 35	<u> </u>	1.57	722	<u> </u>	سللتين		·····	
1459	<u> </u>			1.186			11.01		**********	
1454	1 1 102		<u>,0.000</u>		<u> </u>	5-1.3.	19.14			
17400		Shan		<u> </u>						
1945						<b>.</b>			*******************	********
	7400	DEE.		<u> </u>	<b></b>					******
				<b> </b>					***************************************	·····
				<b></b>	<b></b>	<u> </u>			*******************************	***************
	and the second s				<b></b>	<b>.</b>				*****************
				<b>ļ</b>	<b></b>	**********			***********************	•
				ļ	<b></b>	<u> </u>				***************************************
					<u> </u>					***************************************
					ļ	<del> </del>				
						L		L	*************************	

	999-0-19
Equipment Used	Equi <b>pment</b>
Equipment Com	Identification #
YSI 556 SIPS Reader and 5563 Somde	.4-
urbidity meter	2,627901259

Total volume purged DV gal

			 CHARLES.
WATER ST	3 5 5 5	1331112	 VHONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing

Groundwater Elevation measurements are given in feet mis-

WELL	(D: <u></u>	155
SAMPI	E ID:	<u>u.3</u>

# GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: SITE: WEATHER	Entergy - IPEC Biachanan, NY	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 
-----------------------------	------------------------------	--	-------------------

ATER Q	UALITY:	DIW =			icer Actua	l Depth	: ##4		
Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (s/l)	e <b>H</b> (SU)	СВР	Furbidity (NTU)	Flow Rate (g35/br)	Notes
La Santa br>La Santa									******
								(a)	~~~~~~~~~~
Santanianan Santanianan		70 CV	4.34	( A)	754	16.14			
	72. FS[	a de la Maria	9:7.3	\$2.5×	111				
<u> </u>	9 3 / 4	2q. 113	î nêş		7,14.9		2 5 5		******
	12,484	20.00	: 백년소	8, 46	7.57		€2 (A.A.		***************
	12 187	35.33	46.3	41.4.9			(* 1777		
		71. 77	11/42		2.55				
dindradino Lindradino		7		4 1 2	1.72		( (1)		A. B.
					2.407	764 5	A . 11		***************
	7 1 2 2 2		llandii ii aa Sadda dhada			160			****************
dadayaa dhaa			er edd car						
									***************************************
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							in in a new construction.
									*****************
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					****************				V
*****************		***************************************		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	************************				***************************************
		***************************************	***************************************	***************************************				***************************************	***************
							***************************************		*********
***************						*********	***************************************		************
*****			***************************************		• • • • • • • • • • • • • • • • • • • •	***************************************			************
***************************************						P-/- 0.000	***************************************		***************
					***************************************				*****************
	<u> </u>					•••••••••••••••••••••••••••••••••••••••	•••••••	MANAGERICA	
***********								·····	************

Equipment Used	Equipment Identification #
YSI 536 MPS Reader and 5563 Sonde	
those meter	
inchelity meter	150 10 10 5C/

NOTES	CON	OBSER	V.	TIONS:
783163	-3.3D	()13.75-14	V . 2	

Total volume (	parged	\	$\geq \leq$	_ia1
----------------	--------	---	-------------	------

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation itleasurements are given in feet insl

# GZA GeoEnvironmental of New York WELL ID: U3-41D Modified Traditional Purge Sampling Data Sheet

SAMPLE ID: 022

200101254

CLIENT: SITE: WEATHER:	Entergy - IP Buchasan, I	NY T				PROJECT & DATE: SAMPLER(			92 ;   O'Y B	<del>~</del>
WATER COL	UMN HEIG 21. 2.5 DTB	HT (N)	) ↑ 2 ← DIW		17.0 Water Col	55 nam He <b>ight</b>	Well Diam ft	eter: Diameter	4 Multipliers	10
		ER WELL VO	LUME:	0.453 Multiplier	<b>.</b>	Well V	<del></del>	2 3 gal	0.163 0.653	- Constant of the Constant of
11.13	. *	1.5	æ	Designed Pur	) ge Volume	_gai TOTAL VO	LUME PUR	RGED:	₹.5	gal
WATER QU	ALITY: Voiene: Praged (g.d)	DTW =: DTW or Actual Depth	Lemp (°C)	Transdace Specific Conductivity (S/cm)	Actual Dep Dissolved Oxygen (g/0		ORF	Turbidity (NTU)	Notes	*************
1113 1120 1132 1143 1159 1203 1203 1316 1306 1315	2	3 4 960 7 34 5 80 2 6 6 4 4 27 3 4 9 1 6 5		2 6 1 6 2 6 2 7 2 6 2 7 2 6 3 6 2 6 3 6 2 6 2 1 5 72 2 1 5 72 2 1 6 7 7 6 7 7	1 0 6 2 5 7 2 5 2 2 6 3 3 6 3 3 13 2 6 2 2 5 3	\$ 15 \$ 55 \$ 63 \$ 73 \$ 73 \$ 73 \$ 73 \$ 75 \$ 75 \$ 75 \$ 75 \$ 75 \$ 75 \$ 75 \$ 75	45 3 24 4 34 5 14 8 14 7 23 9 23 2 23 22 23 22	55.4.5 53.10 55.7 5.97 5.93 5.33 5.51 1.224 4		
Equipment Used  YSI 556 MPS Resider and 3363 Smade							•	uipment lification f	d .	

# NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing. Graundwater Elevation measurements are given in feet mst.

turbidity meter

WELL	): <u>`</u>	1			:
SAMPLE	E ID	: <u>O</u>	2	(	

# GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLENT: SITE: WEATHER	Entergy - IPEC Buchanin, NY Chooley - 122 22 4 505	PROJECT NO: DATE: SAMPLER(S): PUMP DEPTH:	01.0017869.92 3V 1 3 6 9 C.3 616
	1	rump depin:	17

WATER Q	CALITY:	otw=	4.29			l Depth Z	115	Mangdu. <u>Mandin</u>	G - 4.2
Time	DTW or Actual Depth		Specific Combuctivity (5/cm)	Dissolved Oxygen (g/l)	p <b>H</b> (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
15cc.	2.77.02					<b></b>			
1311		20.34		328	6.87	11192		***************	
1515	I 2 172		Programme and a section of the secti	1253	1200	licát.	461		Cos
1521	12.163	20.60	1.1.2.1	230	11.15	131.	6.33		
524	2 163		1.120	1.70	1.19	Barris Street Constitution Street	4.35		10.50
ra 3i	12.159	20.62	ke en sagar an en	1.34	4.2.4.	•	4 4 3		<u></u>
636	12.158	20.56	**********		Liling.	Litiz.	433		0.60
154	2.252	20.79	***************************************		1.25	<u> </u>	5.10.		0.76
545		20.16			12.2.		<u> </u>		
351	June 1	20.74	***************************************			55.9			0.40
		20.74	NAMES OF THE PROPERTY OF THE P			545			
LCQ	7 7 4 5		*******************************	120	***************************************	532	9-12		
<u>) (</u>		بسمتد				سنمعت		····	
				aful			TPEC		******************
<u> </u>		10.00	r cer			······		**************	
والمراجع والم والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراج					***************************************	~~			
المدارات والاروم والمام والمواجع			************	**********************	**************				*************************
			verine, and a second	*****************		~~~~	***************************************	**************	Management of the State of the
***				***************************************		********			
*****			*****					100000000 - FRANKO (1900)	
				***************************************				*****************	
			<u> </u>			******			~~~
									]

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6-
flow meter	12. 1 # 1
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Total volume purged 1 245 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing

Grandwater Elevation measurements are given in feet aisl

# APPENDIX E: POST-Q4 2009 MID-QUARTER SAMPLING DATA SHEETS

APPENDIX E: POST-Q4 2009 MID-QUARTER SAMPLING DATA SHEETS

NO POST QUARTER 4-2009 SAMPLES COLLECTED

**APPENDIX F: DOSE CALCULATIONS** 



Site Indian Point
Job No. 17869.91

Prepared By: JAS
Reviewed By: mib

## Parameter Values:

				Totals		
		Total Catchment	Total Improved Zone		T	
		Zone (ft^2)	(ft^2)	Recharge (ft/yr)	Precipitation (ft/yr)	
		3.969.765	1,432,972	0.69	2.64	
уеаг		0,000,100	1,100,010	Surface Area		
2009				Unit 3 North	Unit 3 South	
2005	Northern Clean Zone	Unit 2 North Improved	Unit 1/2 Improved	Improved Zone	Improved Zone	Southern Clean
	Improved (ft^2)	Zone (ft^2)	Zone (ft^2)	(ft^2)	(ft^2)	Improved Zone (ft^2)
	0	148,214	433,904	316.210	321,290	213,354
	Northern Clean		100,	Unit 3 North	Unit 3 South	=,
	Unimproved Zone	Unit 2 North Unimproved	Unit 1/2 Unimproved	Unimproved Zone	Unimproved Zone	Southern Clean Zone
	(ft^2)	Zone (ft^2)	Zone (ft^2)	(ft^2)	(ft^2)	Unimproved (ft^2)
	106,429	204,317	438,221	323,116	268,862	585,600
	Discounted Area	Discounted Area Within	Discounted Area	Discounted Area	Discounted Area	Discounted Area Within
	Within Zone	Zone	Within Zone	Within Zone	Within Zone	Zone
	50,265	0	291,186	106,718	17,730	144,347
				Unit 3 North		
	Northern Clean Zone	Unit 2 North Catchment	Unit 1/2 Catchment	Catchment Zone	Unit 3 South Zone	Southern Clean Zone
	Catchment (ft^2)	Zone (ft^2)	Zone (ft^2)	(ft^2)	(ft^2)	(ft^2)
	156,694	352,531	1,163,311	746,044	607,882	943,302
				Activity (pCi/L)		
				Groundwater		
	Northern Clean Zone					
	Catchment	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South Zone	Southern Clean Zone
2						
Upper Zone Before Canal						
	150	297	3,568	350	742	184
E						
Lower Zone Before Canal						
7 4 9 0	150	251	2,420	1,253	452	186
	Northern Clean Zone	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South Zone	Southern Clean Zone
al er						
Upper Zone After Canal	450		0.000		7.40	404
	150	230	3,036	338	742	184
er er						
Lower Zone After Canal	150	512	958	528	452	186
	100	012		Discharging to Cana		100
					<u> </u>	
	Storm Water for	Storm Water for Unit 2	Storm Water for Unit	Storm Water for	Storm Water for	Storm Water for
	Northern Clean Zone	North	1/2	Unit 3 North	Unit 3 South	Southern Clean Zone
		1.337		0	0	0
	NA NA	Avg MH-4a	NA NA	Avg CB-14 and CB-34	Avg U3-CB-B8	Avg D1. C3, E6, & E10
			Stormwator	Discharging to River	(nCi/L)	
			Storriwater	Discharging to River	(pci/L)	
	Storm Water for	Storm Water for Unit 2	Storm Water for Unit	Storm Water for	Storm Water for	Storm Water for
	Northern Clean Zone	North	1/2	Unit 3 North	Unit 3 South	Southern Clean Zone
		0	0	0	Onic o Goden	0
	NA NA			-	NA NA	
	NA NA	Avg. MH-1 and MH-12	Avg MH-14	Avg CB-15	NA NA	Avg E13,CB-C2

## Potential Water Received by Storm Drain System

#### =(Improved Area) x Precipitation

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
0	391,161	1,145,145	834,532	847,937	563,078	ft^3/yr
0	1,072	3,137	2,286	2,323	1,543	ft^3/day
0.00	5.57	16.30	11.88	12.07	8.01	GPM
0	11,076,450	32,426,905	23,631,305	24,010,893	15,944,594	L/Yr

The total amount of water available to be received by the storm system is computed as the combined area of buildings and paved areas in the catchment multiplied by the annual precipitation rate. Note this conservatively assumes that the amount of water lost to the atmosphere or other sinks after precipitation has fallen on paved or built up surfaces is zero.

## Water Directly Recharged to Aquifer from Precipitation

## =Unimproved Area x Recharge

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
73,030	140,199	300,700	221,716	184,489	401,829	ft^3/yr
200	384	824	607	505	1,101	ft^3/day
1.04	2.00	4.28	3.16	2.63	5.72	GPM
2.067,977	3,969,997	8,514,878	6,278,311	5,224,145	11.378,533	L/Yr

Note that this calculation reflects recharge to the aquifer in non-paved areas. The Recharge value listed above and used in this calculation reflects only that portion of precipitation that actually recharges the aquifer.



Site Indian Point
Job No. 17869.91

Prepared By: J

#### Water Recharged to Aquifer (Direct Recharge Plus Storm Water Leakage Minus Building Drain Removal)

=(Direct Recharge + X% Water Received by Storm System) - (Y% x Water Removed by Building Drains)

Total Water Discharged to Aquifer

d Lower Zone	[Northern Clean Area Catchment + (0% Storm Drain Water)] <sup>1</sup>	[Unit 2 North + (50% Storm Drain Water)]-[5gpm]	[Unit 1/2 Area Catchment + (30% Storm Drain Water)]- [7.5 gpm]	[Unit 3 North Area Catchment + (60% Storm Drain Water)]- [7.5gpm]	[Unit 3 South Area + (10% Storm Drain Water)]	[Southern Clean Zone Area + (40% Storm Drain Water)]	Units
ᄪ	73,030	-15,533	117,275	195,467	269,283	627,060	ft^3/yr
bber	200 1.04	-43 -0.22	321 1.67	536 2.78	738 3.83		ft^3/day GPM
_ >	2.067,977	-439,840	3,320,857	5,535,002	7,625,234	17,756,371	L/Yr

Th**ere** are no improved surfaces in Northern Clean Zone.

While actual footing drain flow rates will vary with the magnitude and/or intensity of precipitation, the Unit 2 North Zone calculation includes a constant removal of 5 gpm from the groundwater system by the Unit 2 footing drain. This flow rate is fixed in the model because continuous flow data for the drain is not routinely measured. The value of 5 gpm is based on measurements made during the pumping test conducted on RW-1 in 2006. Since yearly precipitation prior to C4 2009 was ~4 inches less than the fourteen year average, the actual footing drain withdrawal rate was likely less than the fixed 5 gpm value used by the model. As such, the model indicates that all the groundwater flow in this zone is accounted for by the drain (i.e., the model shows no groundwater flow to the river through this zone, the model approximation is conservative (i.e., results in a high bias to the dose computation). This is because the water removed from the Unit 2 footing drain, which would otherwise contribute to groundwater flow is applied to the Unit 2 shorth Zone.

North Zone.

#### Groundwater Discharged to Canal

#### =Water Recharged to Aquifer x X% flowing to Canal

1 Lower e	Northern Clean Area Catchment x 0%	Unit 2 North x 15.2%	Unit 1/2 Area Catchment 24.2%	Unit 3 North Area Catchment x 22.9%	Unit 3 South Area x68.4%	Southern Clean Zone Area x 0%	Units
anc Zon	0	-2,361	28,381	44,762	184,189	0	ft^3/yr
l s	0	-6	78	123	505	0	ft^3/day
<u>a</u>	0.00	-0.03	0.40	0.64	2.62	0.00	GPM
ם כ	0	-66,856	803,647	1,267,515	5,215,660	0	L/Yr

#### Groundwater Discharged to River

#### =Water Recharged to Aquifer x X% flowing to River x Y% Flowing in Appropriate Vertical Zone

Φ	Northern Clean Area Catchment x 100% x	Unit 2 North × 84.8% x	Unit 1/2 Area Catchment x 75.8% x	Unit 3 North Area Catchment x 77.1%	Unit 3 South Area	Southern Clean Zone	
lo Z	59.3%	15.1%	11.7%	x 47.9%	x 31.6% x 31.3%	Area x 100% x 55.2%	Units
e Z	43,307	-1,989	10,401	72,188	26,634	346,137	ft^3/yr
<u>a</u>	119	-5	28	198	73	948	ft^3/day
) >	0.62	-0.03	0.15	1.03	0.38	4.93	GPM
	1.226,310	-56,321	294,514	2,044,126	754,197	9,801,517	L/Yr
	Northern Clean Area		Unit 1/2 Area	Link O Ningth Annual			
1	Northern Clean Area		Unit 1/2 Area	Unit 3 North Area			
<u>o</u>	Catchment x 100% x	Unit 2 North x 84.8% x	Catchment 75.8% x	Catchment x 77.1%	Unit 3 South Area	Southern Clean Zone	
Zone		Unit 2 North x 84.8% x 84.9%			Unit 3 South Area x 31.6% x 68.7%	Southern Clean Zone Area x 100% x 44.8%	Units
er Zone	Catchment x 100% x		Catchment 75.8% x 88.3%	Catchment x 77.1%			
ower Zone	Catchment x 100% x 40.7%	84.9%	Catchment 75.8% x 88.3%	Catchment x 77.1% x 52.1%	x 31.6% x 68.7%	Area x 100% x 44.8% 280,923	
LowerZone	Catchment x 100% x 40.7% 29,723	<b>84.9</b> % -11,183	Catchment 75.8% x 88.3% 78,494 215	Catchment x 77.1% x 52.1% 78,517	x 31.6% x 68.7% 58,459	Area x 100% x 44.8% 280,923 770	ft^3/yr

#### Water Remaining in Storm Drains and Discharged to Canal

#### =Storm Drain Water x X% Not Leaking to Groundwater and Not Discharging to River

					Southern Clean Zone	
Northern Clean Area	Unit 2 North (45% Unit 2 North and 30% of Unit 1/2 Storm Drain Water), Plus 5	Unit 1/2 Area	Unit 3 North Area Catchment (3% Unit	Unit 3 South Area (3% Unit 3 North and 42% Unit 3		
Catchment (0% Storm	· '	Catchment (0%	3 North Storm Drain	South Storm	Clean Zone Storm Drain	
,	0, \ , ,					
Drain Water)	footing drain.	Storm Drain Water)	Water)	Drain Water)	Water)	Units
0	870,566	0	25,036	381,169	1,243,173	ft^3/yr
0	2,385	0	69	1,044	3,406	ft^3/day
	12.39	0.00	0.36	5.42	17.69	GPM
ı	12.00	0.00				

## Water Remaining in Storm Drains and Discharged to River

Northern Clean Area Catchment (0% Storm Drain Water)	Unit 2 North (5% Storm Drain Water)	Unit 1/2 Area Catchment (10% Storm Drain Water)	Unit 3 North Area Catchment (7% Storm Drain Water)	Unit 3 South Area (5% Storm Drain Water)	Southern Clean Zone Area (5% Storm Drain Water)	Units
0	19,558	114,515	58,417	42,397	28,154	ft^3/yr
0	54	314	160	116	77	ft^3/day
	0.28	1 63	0.83	0.60	0.40	GPM
0	U.28	1.03	0.03	0.00	0 40	01 101

#### Facility Groundwater Flux Calculation

Site Indian Point
Job No. 17869.91

Prepared By: JAS
Reviewed By: mib

## Flux Calculations

#### Conceptual Model: Migration Pathway Summary

	Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone
GW	100% Upper and Lower Zone To River	84.8% Upper Zone and Lower Zone Flow To River. 15.2% Upper Zone and Lower Zone Flow to Canal	75.8% Upper Zone and Lower Zone To River. 24.2% Upper Zone and Lower Zone to Canal	77.1% Upper Zone and Lower Zone To River. 22.9% Upper Zone and Lower Zone to Canal	31.6% Upper Zone and Lower Zone To River. 68.4% Upper Zone and Lower Zone to Canal	100% Upper and Lower Zone To River
sw	NA	To Canal (Storm Water Considered Clean; Estimated at 5.5 GPM) and To River (5% Storm Water)	To Canal (60% Storm Water) and To River (10% Storm Water)	To Canal (33% Storm Water) and To River (7% Storm Water)	To Canal (85% Storm Water) and To River (5% Storm Water)	To Canal (55% Storm Water) and To River (5% Storm Water)

Flux (pCi/Yr)

	North Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	South Clean Zone	Total
GW to River-Upper Zone	1.84E+08	0.00E+00	8.94E+08	6.90E+08	5.60E+08	1.81E+09	4.14E+09
GW to River- Lower Zone	1.26E+08	0.00E+00	2.13E+09	1.17E+09	7.48E+08	1.48E+09	5.66E+09
GW to Canal	0.00E+00	0 00E+00	2.87E+09	4.44E+08	3.87E+09	0.00E+00	7.18E+09
SW to Canal	NA	3.30E+10	0.00E+00	0.00E+00	0.00E+00	0.00E+00	3.30E+10
SW to River	NA	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
						Curies/Yr ==>	0.05

#### Notes:

The recharge rate used herein, 26% of precipitation (~10 in/yr), is within the range of values discussed in the USGS modeling report! The reported recharge ranged from 3.6 inches/year to 7.5 inches/year for a till to 20 inches per year for coarse grained glacially stratified deposits. A yearly rolling average precipitation value measured at the Facility meteorological station is also used in the computations. The catchment area was defined using an AutoCAD topo map for the Site and surrounding area. The catchment was defined by starting at the area marked "line of water grant" and tracking eact, away from the River, to define portions of the commitment of the statement of the s

1. USGS. Water Use. Ground-Water Recharge and Availability. and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002

# APPENDIX G: UNIT 2 TRITIUM PLUME TREND ANALYSES

## TABLE G1 MANN-KENDALL TREND EVALUATION SUMMARY TRITIUM IN GROUNDWATER NEAR UNIT 2 INDIAN POINT ENERGY CENTER BUCHANAN, NY

Well ID	Number of Data Points	Number of Times below MDC	Minimum Tritium Activity (pCi/L)	Maximum Tritium Activity (pCi/L)	Mann- Kendall Statistic (S)	Normalized Test Statistic (Z)	Probability	Trend at 95% Level of Significance
MW-30-69	32	0	7.36E+04	6.01E+05	-179	-2.89	0.998	decreasing
MW-30-84	19	0	3.78E±03	1.25E±04	-15	-0.49	0.688	no trend
MW-31-49	31	0	2.98E+02	4.84E+04	21	0.34	0.633	no trend
MW-31-63	19	0	5.00E±03	4.06E+04	12	0.38	0.650	no trend
MW-31-85	19	0	3.17E+02	1.88E+04	69	2.38	0.991	increasing
MW-32-59	18	0	4.13E+02	6.43E+04	-41	-1.52	0.935	110 trend
MW-32-85	17	0	5.42E+03	1.26E+04	-10	-0.37	0.645	no trend
MW-32-131	6	1	1.29E+02	1.13E+04	2	NA	0.575	no trend
MW-32-149	15	0	1.99E+02	1.05E+04	-67	-3.27	0.999	decreasing
MW-32-173	13	0	4.31E+02	5.89E+03	-60	-3.60	1.000	decreasing
MW-32-190	16	0	1.63E+03	1.13E+04	-74	-3.29	0.999	decreasing
MW-33	22	0	2.30E+04	2.64E+05	-85	-2.37	0.991	decreasing
MW-35	19	0	1.04E+03	1.19E+05	-75	-2.59	0.995	decreasing
MW-36-24	14	2	1.54E+02	3.42E+04	7	0.33	0.629	no trend
MW-36-52	14	0	6.06E±03	2.68E±04	-63	12.00	7.000	decreasing
MW-37-22	16	0	2,26E+03	3.49E+04	-52	-2,30	0.989	decreasing
MW-37-32	16	0	2.49E+03	3.01E±04	-62	-2.75	0.997	decreasing
MW-37-40	15	0	4.22E+03	1.70E+04	-87	-4.26	1.000	decreasing
MW-37-57	16	0	4.05E+03	4.48E+04	-82	-3.65	1.000	decreasing
MW-42-49	16	0	1.12E+03	7.22E+04	-14	-0.59	0.721	no trend
MW-42-78	11	0	3.46E+02	1.28E+03	-17	-1.25	0.894	no trend
MW-49-26	18	0	3.10E+03	1.54E+04	-123	-4.62	1.000	decreasing
MW-49-42	18	0	2.25E+03	1.13E+04	-125	-4.70	1.000	decreasing
MW-49-65	18	0	1,26E±03	5.76E±03	-105	-3,94	1.000	decreasing
MW-50-42	19	4	1.01E+02	9.75E+03	-48	-1.64	0.950	no trend
MW-50-66	23	0	2.08E+03	1.08E+04	-177	-4.65	1.000	decreasing
MW-53-82	13	0	4.54E+02	1.32E+04	-18	-1.04	0.850	no trend
MW-53-120	16	0	4.42E+03	9.61E+03	-62	-2.75	0.997	decreasing
MW-55-24	12	0	7.82E+02	3.08E+03	-25	-1.65	0.950	decreasing
MW-55-35	11	0	8.53E+02	9.04E+03	-21	-1.56	0.940	no trend
MW-55-54	12	0	5.47E+03	1.31E+04	-46	-3.09	0.999	decreasing
MW-111	31	0	6.81E+03	5.78E+05	-166	-2.80	0.997	decreasing

Notes: Calculations based on Mann-Kendall trend evaluations as presented in U.S. EPA Practical Methods for Data Analysis, U.S. EPA QA/G-9 QA00 UPDATE, July 2000, Section 4.3.4

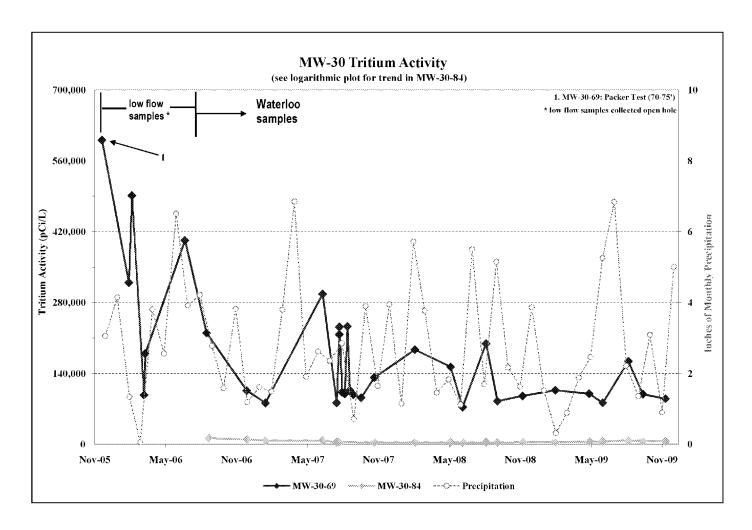


FIGURE G1

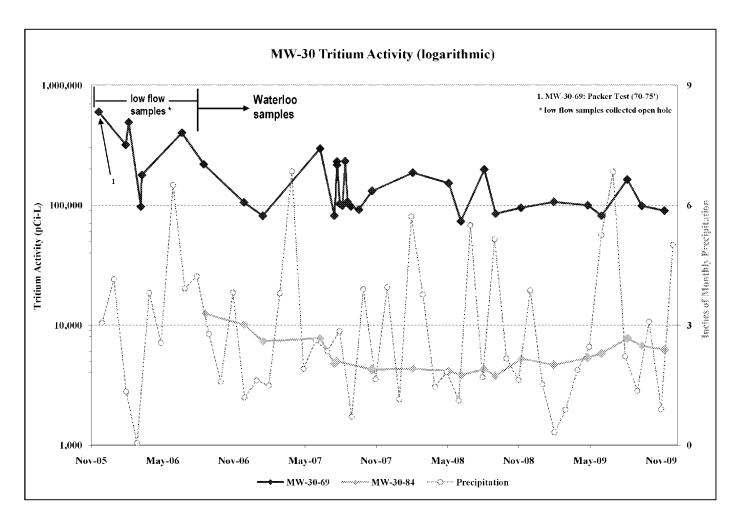


FIGURE G1a

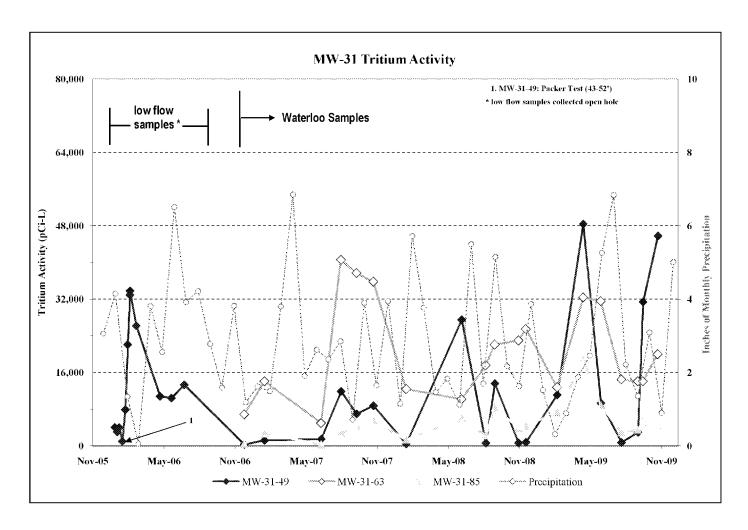


FIGURE G2

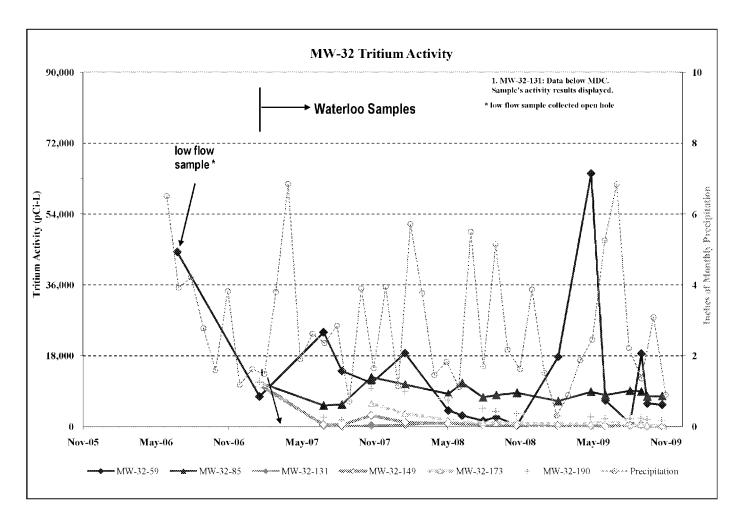


FIGURE G3

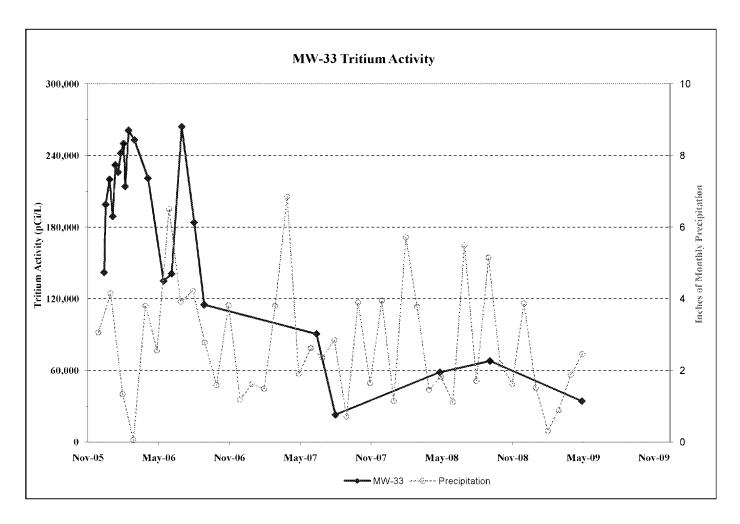


FIGURE G4

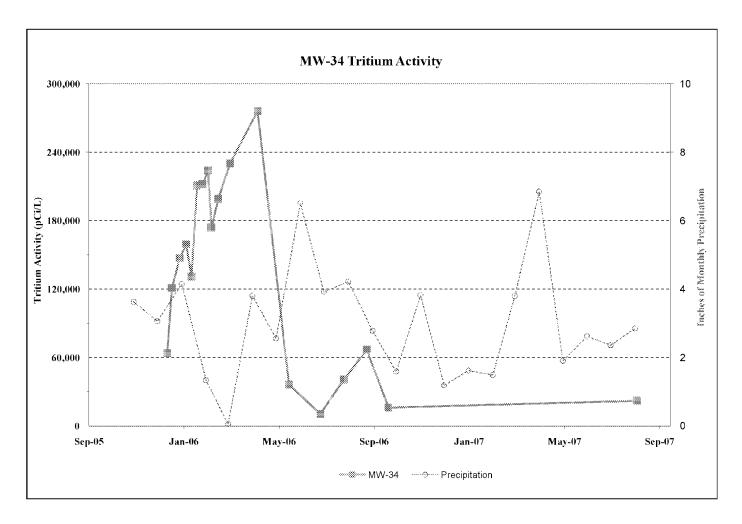


FIGURE G5

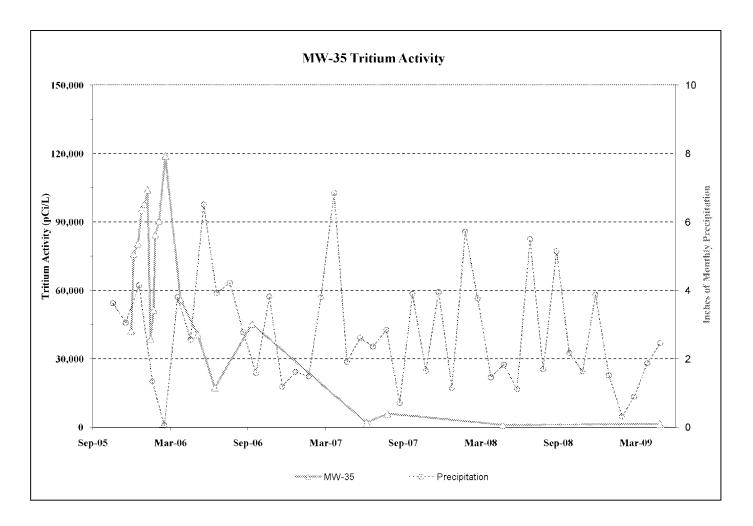


FIGURE G6

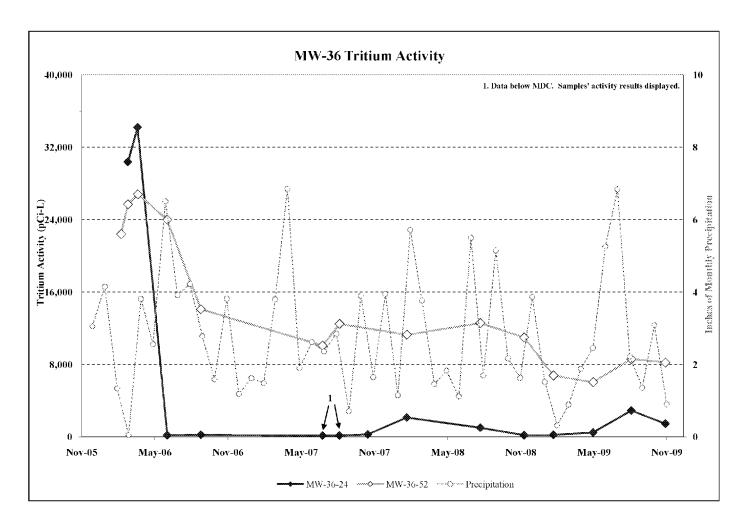


FIGURE G7

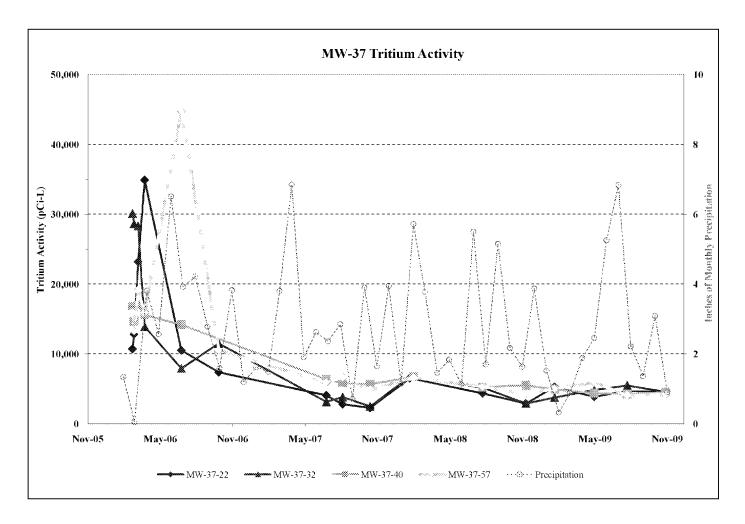


FIGURE G8

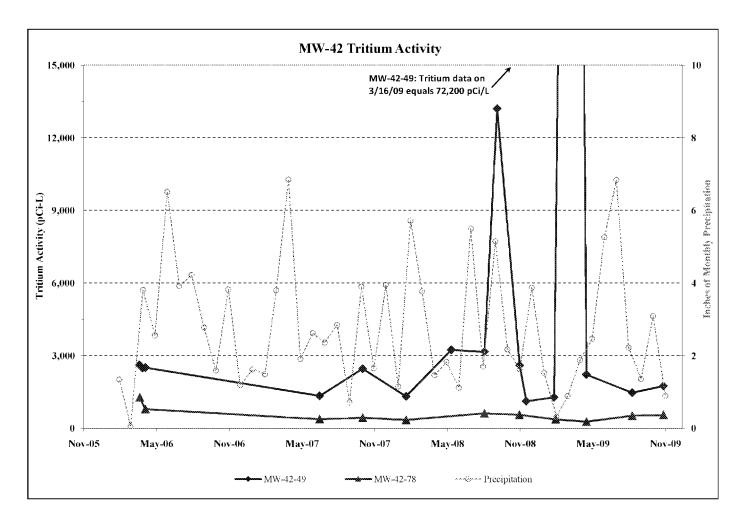


FIGURE G9

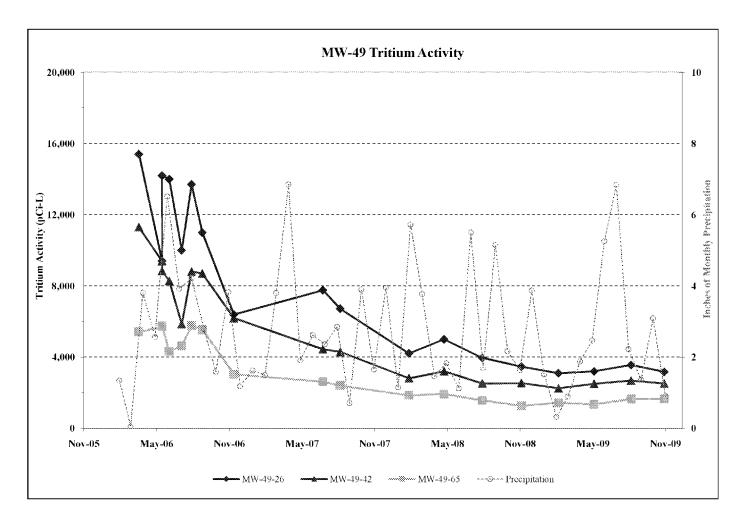


FIGURE G10

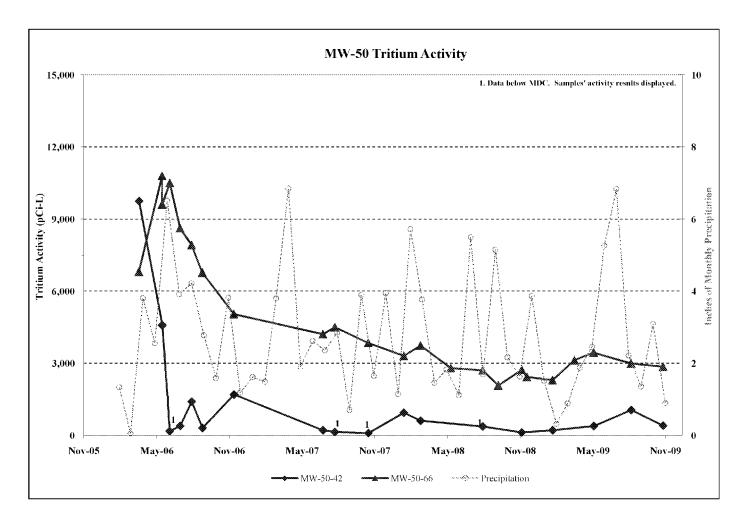


FIGURE G11

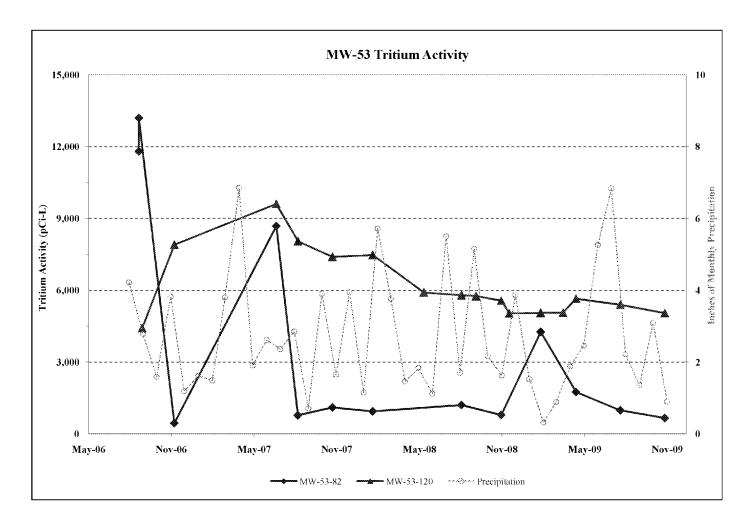


FIGURE G12

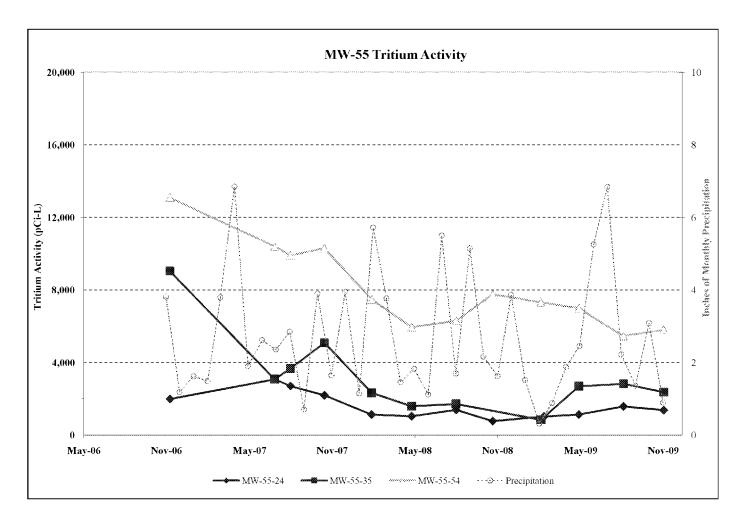


FIGURE G13

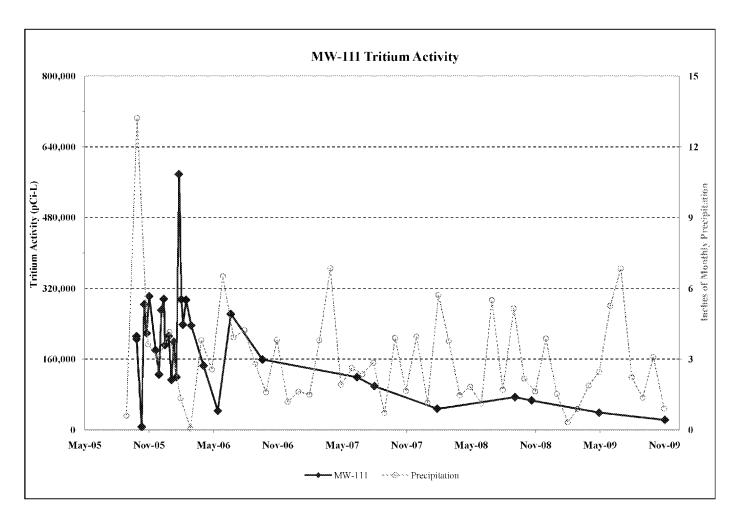
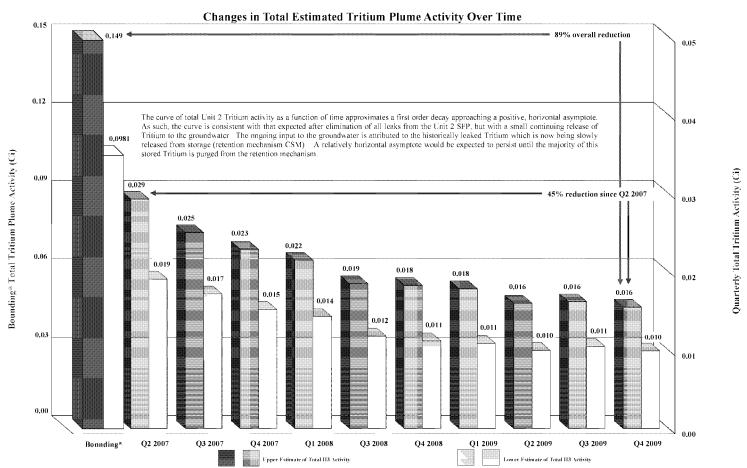


FIGURE G14

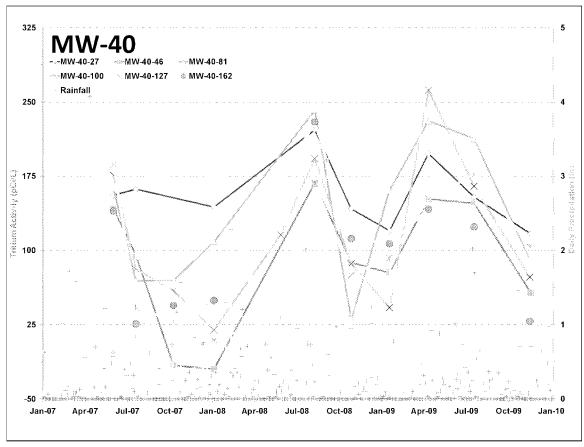


its: Lower extinute is based in a percent of 0 0002 which was deemed from a pumping test conducted in 2006. Type extinates based on 2006 to present which in the previous attended in 2007 to previous format pumping and the previous and approximate interval in the previous attended in 2007 to previous format pumping the conducted in 2007 to previous attended in 2007 to previous format previous attended in 2007 to previous format pumping the conducted in 2007 to previous attended in 2007 to previous format previous format pumping the conducted in 2007 to previous format pu

he boundary activity estimate, however, an amproved a longer period of time, and is focused on the Tribum levels vessing during the earliest postnow of the grounds also meeting about 10 magnitude period of time, believe termination of all the relatified SFP leads. Tribum concentrations were at their highest levels, but the notiver's of monitoring installations was still being stated. The about the present of 
FIGURE G15

# **APPENDIX H: SOUTHERN BOUNDARY WELLS**

# TEMPORAL TRITIUM TRENDS IN SOUTHERN BOUNDARY WELLS



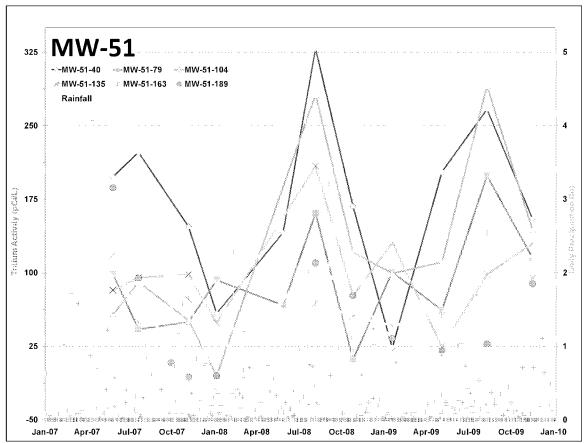


FIGURE H1