

GZA GeoEnvironmental, Inc.

**FINAL
IPEC QUARTERLY LONG-TERM
GROUNDWATER MONITORING REPORT
QUARTER FOUR 2010
(REPORT NO. 12)
INDIAN POINT ENERGY CENTER
BUCHANAN, NEW YORK**

PREPARED FOR:

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AUGUST 19, 2012

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Quarter Four 2010 (Report No. 12)
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Dear Mr. Doroski:

GZA GeoEnvironmental of New York (GZA) is pleased to provide this Quarterly Groundwater Monitoring Report for Indian Point Energy Center located at 450 Broadway, Buchanan, NY.

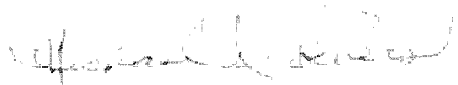
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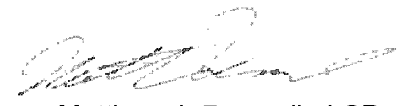
Very truly yours,

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1.0 EXECUTIVE SUMMARY

On behalf of Entergy Nuclear Northeast, Inc., GZA GeoEnvironmental of New York (GZA) has completed the Q4 2010 quarterly groundwater monitoring for the Indian Point Energy Center (IPEC), culminating in this report. Interpretations of the monitoring data have been made in the context of the current Conceptual Site Model¹ (CSM). Development of this model began at the outset of the site investigations and has been iteratively enhanced as subsequent data has become available, in part through quarterly monitoring. The report has been written with a focus on the subject quarter's data. Relationships to prior data, more in-depth technical explanations and exceptions to generalized statements and conclusions have typically been explained in the footnotes. This report format was chosen to allow efficient assimilation of the most current data and analyses by those already familiar with the project. The footnotes contain important information and should be carefully read by all, but particularly by those less familiar with the technologies involved and the project history. It is further noted that the analyses and conclusions presented in this report are based on the data and information available up to and including the subject quarter. Data that becomes available after the subject quarter, but before the finalization date of the report is sequentially reflected in the associated subsequent reports.

Consistent with our interpretation of earlier data, and based on the quarterly groundwater sampling data for Q4 2010, GZA concludes that groundwater contaminants continue to migrate toward the Hudson River to the West, and have not migrated off the Site to the North, East or South.

Radionuclide concentrations measured during Q4 2010 were combined with previous quarterly and post-quarterly data to compute rolling average concentrations reflective of groundwater contaminant levels over the past twelve months. These data were multiplied by the associated individual zone-specific groundwater flux values, derived from the Precipitation Mass Balance Model², to compute yearly average radionuclide release rates to the Discharge Canal and Hudson River. The CSM, upon which this radionuclide dose computation is based, continues to be validated through: (1) groundwater elevation data downloaded quarterly from a focused set of transducer-monitored well installations; and (2) the behavior of both the Unit 1 Strontium plume and the Unit 2 Tritium plume as evaluated each quarter. These data, in our opinion, continue to support the use of the current CSM as a basis for Long Term Monitoring Program design.

The most recent quarterly data further support the conclusion that the overall Tritium activity in the Unit 2 plume is generally showing a historically decreasing trend, from both qualitative and quantitative perspectives. These overall reductions are seen on **Figure G-17**, where the total Tritium activity has decreased by approximately 45% since Q2 2007, and 89% when compared to the bounding level Tritium activities. This overall trend is also evident on **Figures 6 and 6A**, where the shaded plume³ no longer extends downgradient to the river, as first observed in the

¹ The formulation and basis for the overall CSM and the Precipitation Mass Balance model are presented in the Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc., on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

² Refer to Appendix H of the Quarter 2 2009 Quarterly Long-Term Groundwater Monitoring Report for discussion of the recalibration of the Precipitation Mass Balance Model. Precipitation and groundwater elevation data were collected onsite between 2007 and 2009 and used to compute groundwater fluxes across the site. Based on analyses of these data, it was concluded that this data set sufficiently encompassed the historical variability in groundwater elevation and flux response to seasonal and yearly precipitation variability. Therefore, maximum onsite groundwater fluxes were calculated from the elevation data, and used to conservatively recalibrate the Precipitation Mass Balance Model, as discussed and employed in the Q2 2009 Quarterly LTM Report.

³ The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although, this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly

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Q2 2009 data. It is further visually evident from **Figure 6A** that the core of the plume has also shown a marked decrease in concentration and extent over time in the vicinity of MW-111. These findings are consistent with our CSM, which anticipates overall decreasing trends in Tritium activity.

Consistent with one of the purposes of this Report, we also point out and explain data which, when first considered, may initially appear inconsistent with the assumptions used to develop the CSM. Such examples, where Tritium has increased in recent quarters, include:

- A transient Tritium peak in Manhole A2 and, to a lesser extent, MH-A4 was observed during the previous (Q3 2010) quarterly monitoring round. Additionally, a similar peak was initially observed during Q2 2009, which initiated a series of investigations into the underlying correlation, and likely causation of the Tritium peaks observed in downgradient monitoring wells⁴. Beginning in mid-September 2010, another Tritium peak was observed in MH-A2 and MH-A4 (approximately 50-100 times the typical historical activity within MH-A2). Prior and more recent investigations indicate that these Tritium peaks appear to be associated with higher levels of washout⁵ entering the Fuel Storage Building (FSB) roof drain leading directly into MH-A2 when the vent fan is not operating⁶. The Q3 and Q4 2010 sample data from a standpipe, constructed in A2 during Q3 2010 to isolate FSB roof drain water, demonstrate that the recent Tritium activity within MH-A2 is directly proportional to the discharge from the FSB roof. Based on the investigations and associated data collected, it has been concluded that the elevated Tritium levels detected in MH-A2 and A4, as well as the proximate and downgradient monitoring wells (MW-41-40, MW-45-42 and MW-46) and manhole B-1, are due to the FSB roof condensate and, as such, do not indicate a new leak from a SSC (see **Section 3.4.4, MW-41-40** below for further discussion).
- The Q4 2010 result for MH-5 VCFD showed that the Tritium activity remained at previous baseline levels, following the rapid reduction⁷ from the clear increase in Q3 2010 by approximately a factor of ten when compared to the previous base line sampling results (see **Figure 6B** and **Section 3.4.4, MH-5 VCFD** below for further discussion).
- The flow rate into the Leak Collection Device (LCD) remained at baseline (<0.2 liters/day) during the current, Q4 2010, monitoring period. This return to baseline conditions, in October 2010, followed a clear increase in the volume of water collected, with an average flow rate of approximately 1.5 L/day measured in the previous (Q3 2010) quarter⁸. Investigations by GZA indicated that the increased flow observed in Q3

rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to conservatively represent three-dimensional contaminant data sets on two-dimensional maps.

⁴ Elevated Tritium activity has been observed at both MW-46 and MW-41-40 during the past two quarterly monitoring rounds (Q3 and Q4 2010); a similar peak was observed in MW-45-42 after the 2009 increase in MH-A2. MW-45-42 is located proximate to MH-A2; MW-41-40 is located directly adjacent to this storm drain system, between MH-A2 and A4; and MW-46 is located hydraulically downgradient of MH-A2. Therefore, the increase in Tritium activity at these two monitoring installations is likely related to the Tritium peaks observed in MH-A2 and A4.

⁵ The term "washout," as used herein, is the process by which Tritiated water vapor is transformed into Tritiated water as a liquid. In general, this transformation is driven by condensation (as is the primary underlying driver associated with MH-A2, above) and/or Tritium diffusion from the Tritiated water vapor into precipitation (rain and/or snow), either while it is still falling or after deposition.

⁶ It is noted that the Tritiated water vapor evaporating from the SFP is a permitted release through the Plant Vent located atop the VC building. Analyses were conducted to account for this release to the FSB roof in the dose computations. This same Tritium has therefore been "double counted" because it is again included in the storm drain and groundwater portions of the dose computations.

⁷ After the Q3 10 increase, the Post-Q3 2010 sampling data from only 10 days later show the Tritium activity in MH-5 VCFD had already returned to the previous baseline levels.

⁸ All of the water collected by the LCD is fully contained and does not enter the groundwater regime.

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2010 could potentially be correlated⁹ with the timing of atypically elevated water levels in the fuel pool, as associated with dry cask work. Following the limiting of these increases in pool water elevation, a marked decrease was observed in the LCD flow rate. Based on these observations, **Figure 6B** was developed in Q3 2010 and has been included in this, Q4 2010, quarterly report. This figure visually presents both the historical LCD flow rate data and the Tritium data for the sampling intervals located within the Unit 2 Tritium plume boundaries. The recent LCD data are discussed in more detail in **Section 3.4** below.

- Peaks in Tritium activity have been observed in multiple sampling ports of MW-31 and MW-32 since Q1 2009 and to a lesser extent since monitoring began. This long-term variability appears to be consistent with episodic releases of Tritium historically stored in the subsurface via natural and anthropogenic Retention Mechanisms¹⁰. This conclusion is further supported by the tracer data and other analyses discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report.
- While Retention Mechanisms clearly appear to impact Tritium activity as summarized above, more noticeable increases in Tritium levels in a number of intervals within MW-31 and MW-32 were initially observed during the Q1 and post Q1 2010 sampling events, where Tritium activities peaked at levels higher than previously measured. Similarly elevated Tritium activities continued through the Q2 2010, Q3 2010 and Post-Q3 2010 sampling events at these Unit 2 locations. These elevated Tritium activities appear to be related to a Q4 2009 surface spill proximate to these wells from a temporary rental RWST/R.O. processing skid¹¹, which was first detected during routine 80-10¹² sampling of MH-9 in mid-January 2010.

During the current (Q4 2010) sampling event, the Tritium activity in the majority of these sampling intervals (e.g. MW-31-63, MW-32-59, MW-32-149 and MW-32-173) are showing reductions in Tritium activity, approaching the typical historic Tritium levels at these monitoring locations¹³. These reductions appear to be in response to the dissipation of the RWST/R.O. spill as it moves downgradient towards the river, as previously predicted based on the short duration of the elevated Tritium levels measured at the release point in MH-9. While this downgradient migration results in decreasing Tritium levels proximate to the release point, downgradient wells may potentially exhibit additional future Tritium peaks, even possibly exceeding the Unit 2 Tritium I.L.s.

- The Tritium peaks referenced above resulted in an increase of the Unit 2 plume total Tritium activity in Q2 2010. However, as shown on **Figure G-17 (Appendix G)**, this previous increase was immediately followed by a decrease (of similar magnitude) beginning in Q3 and continuing in Q4 2010.

⁹ While the data trends appear to correlate, it is noted that simple correlation does not demonstrate causation.

¹⁰ These Retentions Mechanisms are discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report.

¹¹ This transient and localized surface spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor. As such, this equipment is not an in-place Unit 2 SSCs and is no longer on site.

¹² NRC Inspection Enforcement Bulletin (IEB) 80-10, Contamination of Nonradioactive System and Resulting Potential for Unmonitored, Uncontrolled Release of Radioactivity to Environment, May 6, 1980.

¹³ The Q4 2010 sample result in MW-32-85 shows a continued increasing trend in Tritium activity since Q1 2010 within this sampling interval. It is noted that the 2010 Tritium Investigation Level has NOT been exceeded at MW-32-85 from Q1 2010 through Q4 2010.

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- Our review of data found no conclusive evidence that the observed increases in Tritium activity result from the development of new, unidentified leaks in the Unit 2 SFP or other monitored Systems, Structures, or Components¹⁴.

The overall Sr-90 activity within the Unit 1 plume had generally been stable to decreasing in response to the West Pool demineralization operations conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs, completed in Q4 of 2008, resulted in a noticeable increase in Strontium activity proximate to the SFPs, followed by downgradient increases (see **Figure 7** and **7A**). This was expected given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing leakage rate from the SFPs¹⁵. As expected, the Strontium activities proximate to the pool have since decreased to pre-defueling levels (U1-NCD, MW-42-49, U1-SFDS), and Strontium activities downgradient of the pool are currently exhibiting decreasing trends approaching pre-defueling levels (MW-37, U1-CSS) or have decreased to pre-defueling levels (MW-50, MW-55, MW-57) in recent quarters. It is expected that the further downgradient wells will also fully return to pre-defueling levels once this transient perturbation has passed through the groundwater flow system. It is anticipated that this flushing mechanism will be protracted given the impact of partitioning on Strontium levels in the groundwater.

Based on the data and analyses provided herein, our conclusion is that the Tritium and Strontium plumes have both been undergoing overall long-term reductions in activity after the respective source interdictions. Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP¹⁶ and has decommissioned the Unit 1 SFPs, these plumes satisfy the requirements for Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. However, it is also concluded that, while a portion of the leakage from the above cited localized, transient spills traveled directly to the saturated groundwater regime and resulted in the observed transient “peaks” in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events). These localized release events also interfere with the goal of resetting Site Investigation Levels (I.L.s); updating of Strontium I.L.s must therefore await return to the original Strontium baseline levels existing prior to Unit 1 defueling in the downgradient wells (i.e. MW-

¹⁴ However, it is noted that the LCD flow rate spiked up during the previous (Q3 2010) quarter. While: 1) the flow rate did return to baseline during this quarter, 2) all LCD water is fully contained and does not enter the groundwater regime, and 3) the Tritium peaks observed in the groundwater monitoring intervals can be explained by the transient RWST/R.O. processing skid surface spill and associated Retention Mechanisms, peaks in MW-31, MW-32 and MH-5 VCFD appear to be potentially correlated, on a temporal basis, with this increased LCD flow rate. In this regard however, it is noted that while the data trends appear to correlate on a temporal basis, simple correlation does not demonstrate causation.

¹⁵ As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

¹⁶ Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the behavior observed in the Unit 2 collection device data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report and Section 3.4 of the Q3 2010 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms. In this regard, it is noted that these analyses cannot definitively and completely rule out the possibility of a remaining small leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s) and surface spill from the process skid discussed above. While it is not possible to quantify the size of the minimum detectable leak with any degree of certainty, we believe that the maximum leak rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time. This opinion is based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of more than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program; this amount of Tritium release to the river is still small (<0.01%) compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

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37, MW-50, MW-57), and additional seasonal data is required to better assess Tritium response to precipitation-driven Retention Mechanism release variability. Therefore, the ultimate confirmation of the above conclusions will require monitoring over a number of years so as to allow ranges in seasonal variation to be adequately reflected in the monitoring data and thus demonstrate the rate of continued depletion of Tritium and Strontium from the Retention Mechanisms. In this regard, it is important to recognize that even with the somewhat increased Tritium levels currently observed due to the transient surface spill from the rented RWST/R.O. skid, the amount of radionuclides being released through the groundwater pathway is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

In summary, based on the data collected to date, the apparent strength of the CSM to evaluate that data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).



2.0 SCOPE OF WORK

During Q4 2010, GZA performed groundwater monitoring at IPEC in Buchanan, New York (Site) as part of IPEC's overall Long Term Groundwater Monitoring Program (LTMP) at the Site¹⁷. The overall foundation for the development and execution of this LTMP is based on the CSM, a description of which is contained within GZA's Hydrogeologic Site Investigation Report¹⁸. The scope of work completed for this quarter's monitoring is described in the Sections below. Refer to **Figures 1 and 2** for a Site Location Plan and Site Plan. **Figure 3** provides a Lower Hudson Valley Geologic Map and **Figure 4** summarizes Current and Potential Future SSC Source Locations.

2.1 Groundwater Elevation Measurement

GZA maintains a network of long-term monitoring transducers and dataloggers as part of the instrumentation located across the Site. These instruments record groundwater elevation and temperature measurements at regular time intervals¹⁹, which are then downloaded on a quarterly basis²⁰. Transducer installation logs are presented in **Appendix B**.

During the quarterly sampling, GZA downloaded groundwater elevation data from the long-term monitoring transducers, which collected data over the entire duration of the quarter. The low-tide groundwater elevation data during Q4 2010 (10/16/2010) from these 22 transducers are presented in **Table 2** and compared to historic minimum and maximum values on **Figure 5A**²¹. The Q4 2010 groundwater elevation data at three locations (four transducer intervals) are outside 30% of the Q2-2007 through Q2-2009 range. Two of these locations (three transducer intervals) are Unit 2 perimeter wells where the maximum deviation was less than one foot in elevation. Additionally, the final interval showed a deviation of less than two feet in elevation from the Q2-2007 through Q2-2009 criteria. These data show no alterations in overall groundwater flow direction and no substantial variations in the overall horizontal and vertical groundwater gradients. Therefore, these data demonstrate that substantial variations to the observed flow field have not occurred. These data thus further validate the applicability of the Precipitation Mass Balance Model (PMBM) for use in subsequent radiological dose computations – see **Section 3.1**.

¹⁷ Refer to the "Quarterly Long-Term Groundwater Monitoring Report Q2-Q4 2007 (Report No. 1)," dated May 2008 for Site background information and a description of the environmental setting.

¹⁸ Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc, on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

¹⁹ Currently, transducers record groundwater elevation and temperature readings on a 20 minute time interval so as to allow capture of tidal variability. An original, more extensive network of pressure transducers provided critical data inputs for the development of the CSM and the computation of yearly radiological dose to the Hudson River. Over the first nine quarters of the LTM program (Q2 2007 through Q2 2009) sufficient data was collected from this more extensive network of transducers to capture groundwater elevation response to seasonal and yearly precipitation variability. Therefore, starting with the Q3 2009 quarterly report, the transducer monitoring program was refocused on a select subset of locations to routinely monitor the on-Site groundwater conditions going forward. These locations were selected to provide the data required to document that groundwater flow conditions remain consistent with the CSM, thus demonstrating the veracity of the subsequent dose computations. The rationale for the specific locations and depths included in the LTMP transducer redeployment are provided in Appendix K of the Q1 2009 Quarterly Monitoring Report (Report No.5), dated July 2, 2010 and Appendix J of the Q2 2009 Quarterly Monitoring Report (Report No.6).

²⁰ With regard to these ongoing long term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data are collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

²¹ Figure 5, which previously presented shallow and deep groundwater contours, can be found in quarterly reports prior to, and including Q2 2009. This figure is no longer required given that sufficient quarterly contour data has already been obtained (See Q2 2009 for further analysis).

Section 2.0 Scope of Work

2.2 Monitoring Installation Sampling

During Q4 2010, GZA collected groundwater samples for radionuclide analysis from scheduled sampling intervals within select monitoring installations (“wells”) as shown in **Table 3**. Chains of Custody for these samples are presented in **Appendix C**. Collection of additional groundwater sample volume to provide aliquots to regulatory agencies (e.g., Nuclear Regulatory Commission (NRC), NYDEC, etc.) was not required this quarter.

GZA used a number of different types of pumping equipment depending upon the sampling method and the characteristics of the individual monitoring installation²². **Table 1** lists the monitoring installations sampled, the sampling depths and elevations within sampling installations, and the sampling method and equipment used.

In general, GZA implemented two basic methods of sampling to collect representative groundwater samples: the Low Flow method and a modified well volume purge method. The Low Flow method allows collection of representative groundwater samples from discrete sampling zones within a monitoring installation, while limiting the accumulation of wastewater²³. As agreed by Entergy Nuclear Northeast, the NRC, NYSDEC, and GZA, the modified traditional purge method²⁴ allows for the collection of a representative groundwater sample from a monitoring installation after purging 1.5 volumes of water²⁵. We implemented this method in wells where low flow sampling was not practical. Sampling Data Sheets summarizing water quality data and sampling information are presented in **Appendix D**.

With all of the above sampling methods, GZA used dedicated sampling equipment, including polyethylene and/or nylon tubing and submersible electric pumps to the extent practical. The use of dedicated sampling equipment limits the possibility of cross-contamination between monitoring installations and/or individual multi-level samples within a single installation. Refer to **Table 1** for a summary of the sampling methods, equipment, frequency, and depths employed during this quarter’s groundwater monitoring round.

2.3 Vapor Containment Building Foundation Drain Sampling

GZA collected a water sample from on-Site manholes MH-5 VCFD²⁶, B-1 and B-6 to characterize discharge from foundation drains around and below the Unit 2 and 3 Vapor Containment Structures. These drains include both foundation drains around the building peripheries (“curtain drains”) as well as those around the sumps near the middle of the structures (“reactor sump footing drains”²⁷).²⁸

²² Refer to Section 4.3 of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1, dated May 2008, for sampling method and equipment selection rationale.

²³ As described in: Low-Flow Sample Collection, GZA, 7/18/2007

²⁴ As described in: Modified Traditional Groundwater Sample Collection, GZA, 7/18/2007

²⁵ When external factors (such as well-surface-flooding from storm water runoff or overland flow of plant component leaks) might have infiltrated the top of the well and impacted ambient groundwater conditions at a specific sampling location, GZA typically purged three to five volumes of water (using the modified traditional purge method) prior to collection of a sample to attempt to obtain a representative groundwater sample.

²⁶ GZA collects the water sample from the vapor containment foundation drain (VCFD) input into this manhole and not the manhole’s sump. Thus, the MH-5 VCFD sample name.

²⁷ We could not verify that a foundation drain exists around the reactor sump in Unit 2. The assumption that it does exist is based on the plans for Unit 3 and the similarities in construction of both units.

²⁸ These two Unit 2 drains which discharge into MH-5 VCFD, along with similar drains for Unit 3 which discharge into Manholes B-1 and B-6, form an integral part of the early leak detection monitoring network. However, sampling from these three manholes has generally been problematic for a number of reasons, but particularly due to conflicts with plant security measures which mandate that the manhole covers be permanently welded shut. Some limited access has been reestablished by modifying the manhole covers to allow for a small access opening. However, for Manholes B-1 and B-6, this modification still limits the ability to routinely collect samples clearly representative of only the foundation drain discharges rather than the total flow through the storm drains. The piping configuration in MH-5 does allow sampling specific to the foundations drains, hence the designation of this sample as

Section 2.0 Scope of Work

2.4 Proactive Mid-Quarter and Confirmatory Sample Collection

No proactive mid-quarter or confirmatory samples were collected Post-Q4 2010.

2.5 Preventative Maintenance

GZA performed general wellhead maintenance tasks, such as housekeeping of well vaults and roadboxes, and replacement of dedicated sampling equipment, tubing and transducers, as required.

MH-5 VCFD (i.e., Vapor Containment Foundation Drain). Further work is being undertaken on the manhole sampling systems in B-1 and B-6 to facilitate more representative sampling of these foundations drains.



3.0 DATA EVALUATION

The Long Term Monitoring Program was designed to provide data to address four main objectives:

- Monitor radionuclide activities and evaluate groundwater flow rate to both detect and characterize current and potential future off-Site groundwater contaminant migration to the Hudson River, both via direct groundwater discharge to the river and through infiltration into the Discharge Canal, from unplanned radionuclide releases of liquid effluents, so as to allow computation of potential radiation dose to the public from these releases;
- Monitor groundwater proximate to Systems, Structures and Components (SSCs) that exhibit a credible probability of resulting in a visually undetected release of radionuclides to the subsurface carrying an activity level of significance;
- Monitor groundwater along the property boundary to confirm that contaminated groundwater is not migrating off of the property to locations other than the river; and
- Monitor the groundwater plumes identified on-Site to demonstrate overall reductions in total activity over time as is consistent with the requirements of Monitored Natural Attenuation (MNA)²⁹, the selected remediation for the IPEC Site.

These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI). The following sections provide data analyses to address these four objectives.

3.1 Groundwater Mass Flux Computation

As presented in the Hydrogeologic Site Investigation Report, the groundwater flow in both the upper and lower flow zones is toward the power block area from the North, East and South, with subsequent discharge to the Hudson River to the West. We estimate that groundwater flow associated with infiltration from the watershed may be as deep as 350 feet, but still ultimately discharges to the river. A corollary to this conclusion is that there is no groundwater flow, and thus no off-Site radionuclide migration from the power block area to the North, East or South.

To estimate groundwater flow (i.e., groundwater mass flux) beneath the Site, a groundwater flow model was constructed based on a precipitation mass balance analysis. This analysis is based on the precept that, on a long term average, the groundwater flowing through and discharging from the aquifer is equal to the watershed infiltration recharge; this conclusion was reached because the only substantial source of recharge to the aquifer is areal recharge derived from precipitation. The previous fifteen year average for precipitation measured at the Site is approximately 36 inches per year. Based on a USGS infiltration study³⁰, as well as the Precipitation Mass Balance Model (PMBM) calibration³¹, approximately 25 percent of the

²⁹ The selection of MNA as the remedial strategy for the Site is discussed further in the Hydrogeologic Site Investigation Report.

³⁰ USGS. Water Use, Ground-Water Recharge and Availability, and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002.

³¹ The Precipitation Mass Balance Model (PMBM) was initially calibrated to groundwater fluxes based on a Darcy's Law Model with groundwater gradients derived from Q2 2007 (June 1, 2007) low-tide groundwater elevation contours (initial reference data set). The two models use different sets of input parameters which are not dependent or related to each other. This calibration not only verified the reasonableness of the overall groundwater flow rates predicted by the PMBM, but also allowed further discretization of the groundwater flow into upper and lower flow zones as well as flow volumes upgradient and downgradient of the Discharge Canal. After reviewing the groundwater elevation and precipitation data from the Indian Point meteorological station over the time period from Q2 2007 to Q2 2009, it was concluded that sufficient seasonal data had been collected to encompass the majority of the precipitation variability observed over the last fifteen years. Therefore, the PMBM was also recalibrated after collecting the final full

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precipitation falling on pervious surfaces over the Site watershed area recharges the groundwater system via infiltration.

Since precipitation represents the driving variable for groundwater flux in the PMBM³², the yearly precipitation just prior to Q4 2010 (approximately 37 inches) was calculated and input into the recalibrated model to compute the flows used in the estimation of Q4 2010 dose values. Based on the USGS study cited above, the aquifer recharge rate is therefore approximately 10 inches for the year prior to the Q4 2010 monitoring event. Applying this value to the pervious surfaces within the six individual groundwater flow zones shown on **Figure 4**, it is estimated that approximately 5 gpm of groundwater flowed into the Discharge Canal from the upper and lower zones during the previous year. In addition, approximately 9 gpm and 11 gpm of groundwater flowed into the Hudson River from the upper and lower zones, respectively. Storm water discharging into the Discharge Canal and directly into the Hudson River was estimated to be approximately 41 and 4 gpm, respectively. These flows are further subdivided into flow zones with the further detail shown in the table in **Appendix F**.

3.2 Groundwater Sampling

The following sections describe the groundwater sampling results and associated QA/QC protocols.

3.2.1 Groundwater Sampling Results

Groundwater samples collected on behalf of Entergy during Q4 2010 were analyzed at GEL Laboratories for Tritium, Sr-90, Cs-137, Co-60, and Ni-63³³. **Table 3** presents the Q4 2010 analytical results for these radionuclides. The rolling yearly averages, which are calculated using all the valid data from the previous year [Q1 10 through Q4 10], including Mid-Quarter and confirmatory samples, are also presented in **Table 3**. **Table 4** presents minimum detection concentrations (MDC), standard deviation, and I.L.s assigned to each well for the Q4-2010 analytical results. **Table 5** presents historic Site groundwater analytical data. Isopleth maps of rolling averages for Tritium and Sr-90 are presented in **Figures 6 and 7**, respectively. **Figure 8** presents a data map of rolling averages for Cs-137, Co-60, and Ni-63³⁴.

An overall evaluation of the sample handling, shipment and analytical procedures, indicates that the quality assurance quality control protocols have been met in Q4 2010 for all of the samples,

set of transducer data in Q2 2009. Data analyses demonstrated that recalibration to the Q4 2008 data set yielded the most conservative (highest dose to the river) calibration of the nine quarterly data sets obtained during the LTMP, thus this quarter's (Q4 2008) data set was adopted for further dose computations. The recalibration of the model to the Q4 2008 data yielded Unit 1 / 2 Zone and total groundwater fluxes approximately 40% and 25% greater, respectively, than the original reference (Q2 2007) data set. Further information and the data analyses are provided in the Q2 2009 LTM report.

³² To continue to validate the appropriateness and applicability of the PMBM, a subset of the existing transducers are being maintained and monitored quarterly as part of the Long Term Monitoring Program, starting with the Q3 2009 Quarterly Report. The primary objective of maintaining these transducers is to provide ongoing confirmatory data that demonstrate substantial changes to the on-Site groundwater flow field have not taken place and thus verify that the basic assumptions inherent in the PMBM continue to remain valid. The transducer locations are provided on **Figure 5A** of this quarterly report, and the rationale for the selection of these specific individual transducer locations is discussed in the Q1 and Q2 2009 quarterly reports. With regard to these ongoing long-term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data is collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

³³ It should be noted that samples were also analyzed for gamma emitters via gamma spectroscopy. Although only Co-60 and Cs-137 are reported, gamma spectroscopy should detect and identify other gamma emitters if they became present in groundwater.

³⁴ Isopleths were not drawn for Cs-137, Co-60, and Ni-63 because the few positive detections observed did not indicate the existence of a groundwater plume containing these radionuclides. This is likely a result of the high surface affinity (highly adsorptive nature) of these radionuclides for solid geological materials. They therefore tend to rapidly partition out of the groundwater.

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and the analytical results should be useable as presented in **Table 5**. This conclusion is further supported by a review of the Q4 2010 analytical data, as compared to previous historical trends. Refer to **Section 5.2.2** of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1 for further details pursuant to quality assurance quality control protocols.

3.3 Radionuclide Release Rates

The recalibrated PMBM-derived groundwater flows within each of the six flow zones are multiplied by yearly rolling average radionuclide levels within each zone to compute groundwater radionuclide release rates to the Discharge Canal and Hudson River. These groundwater radionuclide release rates are computed separately for upper and lower flow zones as well as upgradient and downgradient of the Discharge Canal. The selection of specific monitoring locations for each of the six zones is described in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases.

Storm drain flows³⁵ computed based on yearly precipitation rates are multiplied by radionuclide concentrations measured in the storm drains to compute the associated storm drain radionuclide release rates³⁶ to the Discharge Canal and Hudson River.

The radionuclide release rates from the groundwater and storm drains to the Discharge Canal and Hudson River for Q4 2010 are shown in the table below.

	GROUNDWATER AND SURFACE WATER TO RIVER (Ci/YR)	GROUNDWATER AND SURFACE WATER TO CANAL (Ci/YR)
Northern Clean Zone*	3.64E-04	0.00E+00**
Unit 2 North Zone	5.65E-04	5.90E-02
Unit ½ Zone	5.84E-03	6.53E-03
Unit 3 North Zone	2.77E-03	9.29E-04
Unit 3 South Zone	1.76E-03	2.43E-02
Southern Clean Zone*	4.19E-03	1.17E-02

* Activity in the Northern Clean Zone is attributable to an assumed Tritium background concentration of 150 pCi/L in the groundwater. The remaining radionuclides were assumed to not be present in this streamtube. Radionuclide release rate in the Southern Clean Zone is calculated from activity measured in monitoring wells MWV-40 and MWV-51.

** The radionuclide release rate to the Discharge Canal from the Northern Clean Zone is zero because the Discharge canal does not extend far enough to the north to be downgradient of the Northern Clean Zone.

These release rates are then used by Entergy to calculate the radiological dose to a hypothetical maximally exposed individual and the environment via the Discharge Canal and the Hudson River using the procedure outlined in the Off Site Dose Calculation Manual (ODCM) Reversion 3.

3.4 SSCs and Property Boundary Monitoring

In addition to providing the data for the dose computation discussed above, the Long Term Monitoring Program has been designed to also provide rapid detection of potential leaks from SSCs. This monitoring is specifically focused on those SSCs which exhibit a credible probability

³⁵ The storm drain flows also include groundwater discharges from the foundation drains for Unit 2 and Unit 3 VC Buildings, but not from the Unit 1 NCD and SFDS, which are otherwise accounted for.

³⁶ It is noted that storm drain samples are not typically taken at times coincident with peak, or even average storm drain flow rates. By its very nature, the vast majority of the flow through the storm drain system tends to be episodic and of short duration due to storm events; sampling rounds are generally scheduled to avoid such events. Radionuclide concentrations are primarily due to groundwater infiltration into the drains and thus tend to be highest during periods of little rain when this infiltration is not diluted by the storm water flow. This incongruence therefore yields a high bias to the dose computation because the elevated concentrations associated with low flow rates are multiplied by the much higher flow rates based on total yearly rainfall.

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of resulting in a visually undetected release of radionuclides to the subsurface³⁷. The monitored SSCs are shown on **Figure 4** and a description of the specific monitoring installations associated with each SSC are provided in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases. In addition to monitoring the SSCs, on-Site and off-Site wells are used to monitor the property boundaries for unanticipated radionuclide migration across these boundaries. Again, the rationale underpinning the selection of wells designated for this purpose is provided in the above cited Memorandum. These monitoring protocols are consistent with the NEI Groundwater Protection Initiative (GPI).

Entergy is also in the planning process to add an additional multi-level monitoring installation located near the south west corner of the Unit 3 Transformer Yard, downgradient of MW-46³⁸. While MW-46 was previously evaluated relative to Unit 3 monitoring effectiveness, and was found to be very useful for detecting potential future releases, we also concluded that without an additional monitoring well installation, there is a moderate risk that some releases could go undetected. In particular, it appears that a release in the vicinity of the Waste Holdup Tank pit could potentially proceed toward the river to the south of MW-46, given the likely hydrology associated with the pre-construction bedrock valley in this area. As such, we recommended, and Entergy agreed to, the construction of an additional monitoring installation at Unit 3 to increase the robustness of the Unit 3 well network and thus reduce this potential risk. Installation of this well is currently scheduled for 2011. The sampling of U1-NCD and U1-SFDS will also be continued as part of the Long Term Monitoring Program.

I.L.s were established for the associated monitoring wells to set quantitative radionuclide concentrations above which further action would be undertaken. As part of the ongoing groundwater monitoring program, the reported analytical concentrations are compared against I.L.s established based on the criteria shown in the table below. I.L.s are currently computed each year based on yearly averages of all the valid groundwater sampling analytical results of the previous year including Aliquot, Confirmatory, and Mid-Quarter sample results³⁹. The monitoring well-specific I.L.s are presented in **Table 4** and are established for comparison with 2010 analytical results based on the quarterly samples collected and analyzed in 2009.

³⁷ As discussed further in the following sections, reporting of visually identified spills/leaks within structures is included within Condition Reports under Entergy's Corrective Action Program. Additional emphasis has been placed on routine review of these reports as they potentially relate to GPI objectives.

³⁸ A cross section has also previously been developed through the Unit 3 area to supplement **Figure 4** and further demonstrate the relationship of site groundwater flow patterns and monitoring well placement relative to the individual Unit 3 SSCs (similar cross sections were previously developed for Units 1 and 2, as presented in the Hydrogeologic Site Investigation Report). This Unit 3 cross section C-C' is included in the Q1 2009 Quarterly Report as Figure 4A.

³⁹ The calculation of ILs and yearly rolling averages prior to the Q1 2009 Report were based on the analytical results from the quarterly sampling rounds only, and therefore excluded aliquot, confirmatory and mid-quarter sample results. For the Q1 2009 Report and thereafter, if an aliquot analytical result confirms that the original quarterly analytical result was false, then only the aliquot result is utilized in the yearly IL calculation. If the aliquot result confirms the original quarterly result is valid, then both the original and the aliquot results are averaged together and then averaged into the yearly IL calculation as a single value. Confirmatory analytical results have the potential to impact the use of the original quarterly sample in the same manner as aliquots; however, unlike aliquots, these "independent samples" are averaged directly into the yearly rolling average without "pre-averaging" with the associated quarterly sample. Similar to confirmatory samples, mid-quarter samples are also averaged directly into the yearly rolling average calculation. However, mid-quarter sample results do not have any impact on the use of the initial quarterly samples as can either aliquot or confirmatory samples, as described above. In the case of both confirmatory and mid-quarter sample results, direct averaging into the yearly average of these additional results can somewhat bias the yearly average toward a particular quarter/season. However, given that confirmatory and mid-quarter samples are typically taken to confirm and/or prepare for uncharacteristically high radionuclide concentrations, this direct averaging provides a high bias to the subsequent yearly dose computations, and is thus conservative. In cases such as this where some bias inevitably will be created, establishing a conservative bias in the dose computations is considered more important than maintaining a seasonal non-bias.

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WELL ID	INVESTIGATION LEVELS (I.L.s)		
	TRITIUM pCi/L	Sr-90 pCi/L	OTHER PLANT-RELATED RADIONUCLIDES
On-Site Boundary Wells (MW-40, MW-51, MW-52, and MW-107)	1,000**	2**	any detection*
Riverfront Boundary Wells (MW-60, MW-62, MW-63)	2,000**	2**	any detection*
All Other Wells	>2x average***	>2x average***	>2x average***

* A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

** The values of 1000 and 2000 pCi/L for H-3 and 2 pCi/L for Sr-90 have been chosen to be low enough to result in timely detection of a new release or change to an existing release and still be outside the normal expected range of sample results at these locations, to the extent possible with the currently available data over time.

*** Any positively detected radionuclide that has a result greater than 2 times the average from the previous year. However, the IL is not reached until an H-3 result is also greater than 1000 pCi/L or a Sr-90 result is also greater than 2 pCi/L.

In the event that the analytical results of a groundwater sample exceed the designated I.L., the following series of actions will be considered:

- Contact the laboratory to verify that all quality control checks were satisfactory, sufficient sample volume was used; required MDC's were met, etc.;
- Re-analyze Aliquots of the original sample;
- Re-sample the location (Confirmatory sample) to verify the result;
- Increase the frequency of sampling (Mid-Quarter samples) for this location⁴⁰;
- Initiate an investigation utilizing Entergy's corrective action program and related resources as appropriate (e.g. site engineering / radiation protection); and
- Initiation of source/ground water remediation techniques commensurate with the potential dose impact analyses and good environmental stewardship.

3.4.1 Proactive Mid Quarter Samples

During the Q4 2010 monitoring period, there were no planned operations that required increased sampling. As such, no proactive mid-quarter samples were collected Post-Q4 2010.

3.4.2 Previous Q3-2010 Investigation Level Exceedances

As indicated in the previous Q3 2010 Quarterly LTM Report, a comparison of the Q3 2010 analytical results to their respective I.L. values shows that the I.L.s were initially exceeded at ten sampling intervals, with five of these intervals exceeding the I.L. during both the Q3 2010 and Post-Q3 2010 sampling events. Three of these I.L. exceedances are still ongoing, and are discussed individually in **Section 3.4.4** below. The remaining seven I.L. exceedances (MW-31-49, MW-31-63, MW-32-59, MW-32-173, MW-39-102, MW-50-42 and MW-67-105) were resolved during the Q4 2010 sampling, as summarized below.

MW-31-49. The Q3 2010 Tritium activity at MW-31-49 increased by a factor of three, which was the highest Tritium activity measured at this interval since the initiation of the LTMP. Following this I.L. exceedance, a second Q3 2010 sample was collected at MW-31-49 which showed a noticeable decrease (thirteen-fold) in activity to a level well below the Tritium I.L. However, the Post-Q3 2010 result was once again elevated above the I.L., and to an activity twice that ever measured in this interval (including the previous Q3 2010 peak). The Post-Q3 2010 peak was

⁴⁰ It is noted that Mid-Quarter samples are also proactively obtained when plant operations could potentially result in an increased probability of a release to the subsurface.

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immediately followed by a decrease (factor of three) in Tritium activity during the current Q4 2010 quarter, to a level below the Tritium I.L.

These recent peaks in Tritium activity appear related to a somewhat delayed response to the transient RWST/R.O. skid surface spill⁴¹ in Q4 2009⁴², as potentially mediated by Retention Mechanisms. Given that the R.O. skid spill, the likely source of these peaks, has been terminated and the Tritium activity quickly returned to pre-release levels in MH-9, an overall, continued decrease to a pre-release Tritium activity is anticipated in MW-31-49. However, the residual impact of the transient RWST/R.O. spill, as mediated through the Retention Mechanisms, may be prolonged as additional future Tritium inputs move through the system (see further discussion below and in **Section 3.4.5**). It is noted that additional sampling intervals in both MW-31 and MW-32 also recorded decreases in Tritium activity to levels below their respective I.L.s during the current (Q4 2010) monitoring period. The decreasing trend observed in these intervals indicates that the source area Tritium activity should continue to approach a pre-R.O. spill Tritium activity in the upcoming quarterly sampling events⁴³.

MW-31-63. The three Q3 2010 and Post-Q3 2010 data points defined a new Tritium peak at this location, where the Q3 result was increasing toward the peak from lower activities measured in Q2 and Post-Q2 2010, the first Post-Q3 result was at the peak, and the second Post-Q3 sample showed a decrease below both the first Post-Q3 and Q3 2010 activities. This nascent decreasing trend was further strengthened by a nearly two-fold decrease in the current, Q4 2010, Tritium activity to below the I.L. The decrease after the Q3 2010 peak is hypothesized to be in response to the continued dissipation of the transient RWST/R.O. surface spill as it further flushes through the groundwater system. Given that the apparent source of this peak has been terminated and Tritium is a non-sorbing radionuclide, Tritium levels in MW-31-63 appear to be relatively quickly returning to pre-release levels, similar to MW-31-49 above.

In this regard, it is noted that peaks in Tritium activity, likely related to mobilization of historically stored Tritium⁴⁴, have also been noted in MW-31-63 since the Q1 2009 sampling event, with somewhat less, but still noticeable variability evident all the way back to the beginning of monitoring. This behavior has also been noted in other sampling depths at this location as well as at proximate locations MW-32 and MW-30, particularly at shallower depth intervals⁴⁵.

⁴¹ The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor. As such, this equipment is not an in-place Unit 2 SSC and is no longer on site. This release was first detected during routine 80-10 sampling of MH-9. The Tritium levels were measured at ~85,000 pCi/L in this MH on January 14th and 15th, 2010, and then decreased to 4,650 pCi/L on January 19th, 2010. Typical Tritium levels prior and post-spill were ~1,500-4,000 pCi/L in MH-9. It is therefore likely that Tritiated water entered the subsurface through this storm drain pathway, as well as potentially through the upper portions of the MW-32 installation (see Q1 2010 Quarterly Report, 1/11/11).

⁴² Based on forensic research conducted by Entergy, it appears that the date of the spill was November 21, 2009.

⁴³ It has also been observed that these two recent Tritium peaks, as well as the previous peak in Q4 2009, appear to closely follow noticeable increases in flow into the LCD, and also coincide with a ten-fold increase in the Tritium level in MH-5 VCFD (see **Figure 6B**). These correlations lead to consideration of a potential link between LCD flow and peaks in groundwater Tritium activity.

Recent and ongoing investigations indicate that the increased LCD flow was likely related to particularly high SFP levels associated with dry cask work. Procedures have therefore been put in place to better control pool levels. Because the flow rate into the LCD has decreased back to baseline levels (typically less than 20 ml/day after 10/4/2010), the Tritium activity in MW-31-49 is also expected to decrease, if there is a link as contemplated above (and/or given the transient nature of the RWST/R.O. skid surface spill). Finally, it is also noted that flow into the LCD and MH-5 VCFD is captured, measured and discharged as a monitored releases.

⁴⁴ As discussed in the January 7, 2008 Hydrogeologic Site Investigation Report, it has been concluded that portions of the Tritium released prior to Energy's last remediation interdiction (rectifying the Transfer Canal liner weld imperfection in December 2007 - the final identified leak) have been stored in the subsurface (Retention Mechanism(s)).

⁴⁵ As discussed in previous quarterly reports, the historic variability in Tritium activity measured in MW-30, 31 and 32 has typically been attributed to the mobilization of Tritium stored in the shallow bedrock and/or within anthropogenic structural features. This storage/Retention Mechanism(s) was confirmed during tracer testing as described in the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008, and as further supported by more recent tracer data discussed in the Q1 2009 LTM Report. Therefore, while the storage/Retention Mechanism(s) clearly contribute to the observed Tritium variability, it is equally clear that some of this variability is likely attributable to localized transient release events.

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Therefore, while the initial Post-Q1 2010 peak at MW-31-63 has been associated with the transient RWST/R.O. skid spill, which had been terminated prior to the second Tritium peak observed in the Q3 2010 and Post-Q3 2010 samples, this subsequent peak is still likely due to the R.O. skid spill through replenishment of the Retention Mechanisms, thus resulting in further releases from these Retention Mechanisms into the groundwater flow regime (i.e. second peak)⁴⁶. Therefore, future Tritium increases at these sampling locations due to the transient RWST/R.O. processing skid spill are still likely, although an eventual, overall decrease in Tritium activity at this location is anticipated.

MW-32-59. The Q1 2010 through initial Q3 2010 samples⁴⁷ at this sampling location all exceeded the Tritium I.L. However, a noticeable decrease in Tritium activity was initially observed during the initial Q3 2010 sampling event, followed by a second decrease in Q3 2010 to well below the I.L. for MW-32-59. In spite of this decreasing trend, a subsequent Tritium peak was observed in Post-Q3 2010, with the Tritium activity back above the I.L. and slightly above the initial Q3 2010 result. This subsequent Post-Q3 2010 peak was immediately followed by another decrease in Tritium activity during the current, Q4 2010, quarter to an activity well below the I.L. for this interval (see **Figure 6B**).

Similar to the Tritium I.L. exceedances in multiple MW-31 sampling intervals, this recent Tritium peak is likely attributable to a delayed release from Retention Mechanisms which have been replenished by the transient RWST/R.O. skid surface spill which occurred in Q4 2009. In addition to entering the subsurface through the storm drain system, this spill also entered the MW-32 well vault⁴⁸, and may have penetrated the well casings, thus potentially explaining the particularly high Tritium activity observed in this shallowest interval of MW-32. Because the surface spill was transient in nature, as concluded, in part, from the MH-9 data, it is expected that the Tritium activity will continue an overall decrease at this location⁴⁹. However, this expected decrease could be masked by additional future contributions of Tritium from the storage/Retention Mechanism(s), as discussed more fully above for MW-31-63 and possibly seen in the Post-Q3 2010 result.

MW-32-173. The Q2 2010 through Post-Q3 2010 Tritium activities all exceeded the I.L. at this sampling interval, although a decreasing trend in Tritium activity was observed during the

⁴⁶ It is also possible that the Post-Q3 2010 peak at MW-31-63 could be related to the increased flow observed in the LCD. The Tritium activity at this location increased in Q3 2010 prior to the increased flow observed in the LCD; but the response timing between the two locations (MW-31-63 and the LCD) is unknown depending on the potential source location. The flow rate in the LCD has decreased to baseline conditions, so the Tritium activity in MW-31-63 is also expected to continue decreasing, if these data trends are related.

⁴⁷ The Post-Q2 2010 result was the highest Tritium activity measured at this location (in all MW-32 depth intervals) since the initiation of the LTMP, and exceeded the I.L. by a factor of nearly five.

⁴⁸ An initial sample was taken of the water remaining in the MW-32 vault on 2/1/2010. This water exhibited a Tritium activity of 390,000 pCi/L. Subsequent sampling of this water in May 2010 measured residual Tritium levels of ~65,000 pCi/L prior to the water being fully removed from the vault. It is further noted that the water in the vault contained other radionuclides in addition to Tritium. These included Co-60, Sb-125, Cs-134, Cs-137, etc. Therefore, the Q1 2010 groundwater data from wells proximate to, and downgradient of, the MH-9 and MW-32 vault release points were evaluated for detections of these radionuclides; none were found. However, Cs-137 was detected at MW-111 in Q2 2010. While this well is located downgradient of MW-32, no other wells showed detections of Cs-137, or the other radionuclides discussed above, in Q2 2010. Cs-137 at MW-111 and downgradient of MW-111 will be closely monitored in the upcoming quarterly reports.

⁴⁹ Inspection of **Figure 6B** indicates that the recent Post-Q3 2010 Tritium peak could also potentially be associated with the increased flow rate (1.5 liters/day average) recently observed in the LCD. Prior to the Post-Q3 2010 peak, the previous two sampling results showed a noticeable decreasing trend in Tritium at this location, which was expected due to the transient nature of the RWST/R.O. spill source, the chemical nature/transport behavior of Tritium, and the rapid decrease in Tritium activity observed in MH-9. The noticeable decrease at this sampling interval (MW-32-59) occurred prior to the increased flow rate measured in the LCD. However, the Post-Q3 2010 sample was collected after the increased flow rate in the LCD was observed, and therefore, could potentially be associated with the Q3 2010 conditions observed at the LCD. The current Q4 2010 sample result is also in agreement with the recent flow rates in the LCD, which have subsided to typical historical rates (<0.1 liters/day) since October 2010. In this regard however, it is noted that while the data trends appear to correlate on a temporal basis, simple correlation does not demonstrate causation.

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Q3 2010 and Post-Q3 2010 sampling events. This was followed by another decrease this quarter (Q4 2010) to an activity that is slightly below the I.L. Similar to the other MW-31 and MW-32 exceedances discussed above, the overall increase in Tritium activity at this interval over the previous three quarters was attributed to the transient RWST/R.O. skid surface spill which occurred in Q4 2009. As expected, a slightly delayed Tritium increase and a shallower slope to the increasing trend were observed in MW-32-173 when compared to MW-32-59 and MW-32-149, which provides evidence that this depth interval may be responding to vertically downward migration from above. This conclusion is supported by both the four-fold higher activities measured in intervals immediately above this point, as well as the strong vertically downward gradients exhibited by the bedrock formation at this location. As discussed above, the Tritium activity at this depth interval should continue to decrease as the Tritium activity above decreases (given the transient nature of the spill), but will likely decrease at a slower rate⁵⁰. It is also noted that the expected decrease could be masked by future contributions of Tritium from the storage/Retention Mechanism(s), as discussed more fully above for MW-31-63.

MW-39-102. During the previous (Q3 2010) quarter, the Strontium activity at this sampling interval slightly exceeded the I.L., which represented the highest Strontium activity measured at MW-39-102 since the initiation of the LTMP. Similarly, the sampling interval directly below MW-39-102 (MW-39-124) and the uppermost sampling interval (MW-39-67) at this monitoring location also showed increases in Strontium during Q3 2010. As discussed in the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008, MW-39 is located near the Legacy IP1 Storm Drain piping, which historically carried water collected in the Unit 1 SFDS. Previous testing along these pipes revealed that numerous sections were compromised and leaking; therefore, the SFDS discharge was rerouted in 1994 after detecting Strontium contamination in the effluent of the SFDS. As such, no active source of contamination was present in the Legacy piping after 1994, but several Strontium peaks were observed in multiple MW-39 sampling intervals since the initiation of the LTMP.

Therefore, releases from storage/Retention Mechanism(s) and/or the sorptive properties of Strontium (desorbs back into groundwater) possibly contributed to these previous peaks and the recent Q3 2010 I.L. exceedance in MW-39-102. It is also noted that in addition to terminating the Strontium contamination in the Legacy piping, the ultimate Strontium source (Unit 1 SFPs) has also been terminated during the defueling operations in 2008. As such, it was anticipated that the Q3 2010 Strontium peak in MW-39-102 (as well as the increases in MW-39-67 and MW-39-124) would likely be transient and return to a typical, lower activity at this interval. As expected, the Strontium activity in MW-39-102 decreased and was below the detection limit during the current (Q4 2010) quarter. Similarly, the Strontium activity decreased below the detection limit in MW-39-124 during this monitoring period; however, a slight increase was noted in the uppermost sampling interval, MW-39-67 over the same time frame. Because the ultimate source for this contamination is terminated, overall long-term decreases are expected in all three sampling intervals; however, future transient peaks may be noted as Strontium is temporarily released from the Retention Mechanism(s) or desorbs into groundwater.

MW-50-42. A slightly elevated Strontium activity was noted at MW-50-42 starting in Q3 2009; with a peak occurring in Q4 2009 and decreasing activities observed in Q1 2010 and Q2 2010. However, the Strontium activity again increased during the previous, Q3 2010, quarter and slightly exceeded the I.L. for this sampling interval⁵¹. This I.L. exceedance was immediately followed by a decrease in Strontium activity below the I.L. during the current, Q4 2010, quarter.

⁵⁰ The previous (Q3 2010 and Post-Q3 2010) sampling period results support this premise, as the Tritium activity decreased by ~1,700 pCi/L in MW-32-149 and only ~500 pCi/L in MW-32-173. Overall, the Tritium activity in MW-32-149 has decreased by ~8,200 pCi/L from Post-Q2 2010 to Q4 2010, while MW-32-173 has only seen a ~950 pCi/L decrease over that time period.

⁵¹ It is noted that these elevated levels in MW-50-42 are still noticeably lower than the Strontium activity in the interval below (MW-50-66).

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Furthermore, the Q4 2010 result also represents the lowest Strontium activity observed at this location since Q2 2009.

The Q3 2010 I.L. exceedance (and previously elevated activity) was likely related to a delayed response to the increase in water levels during defueling operation in the Unit 1 SFPs (see MW-50 graph on **Figure 7A**). As discussed above, the Strontium activity exhibited a decreasing trend from Q4 2009 to Q2 2010 prior to the Q3 2010 I.L. exceedance; thus the Q3 2010 result could indicate a contribution of Strontium from the storage/Retention Mechanism(s). Because the probable source is terminated, it is expected that the Strontium activity in MW-50-42 will continue an overall decreasing trend towards pre-defueling levels over the next few quarters. The eventual decrease to pre-defueling levels might extend over multiple quarterly monitoring events due to the sorptive behavior of this radionuclide and the Retention Mechanism(s) discussed previously.

MW-67-105. The Strontium result for Q3 2010 at MW-67-105 exceeded the I.L. and represented the historical maximum Strontium activity measured at this sampling interval (2.6 pCi/L) since the initiation of the LTMP. Furthermore, this Q3 2010 exceedance was preceded by a noticeable increase in Strontium activity during the Q2 2010 sampling event. Prior to Q2 2010, relatively low and stable Strontium levels (typically <1 pCi/L) were observed at MW-67-105, extending back to the first sample collected in August 2007. Following the Q3 2010 peak, the Q4 2010 data showed a reversal of the previously increasing trend, with Strontium activity now decreasing to below the I.L., and also now below the detection limit⁵².

Because this riverfront monitoring location is downgradient of Unit 1, the recent peak was likely a response to the Unit 1 SFP defueling operation, as the water containing higher Strontium activity migrated farther downgradient. Because the probable source has been terminated, the Strontium activity is expected to return to the historical, low levels seen from August 2007 through Q1 2010 at this sampling interval. However, future transient peaks may be noted as the perturbation is released from the Retention Mechanism(s) and passes through the system.

3.4.3 Q4 2010 Boundary Investigation Levels

A comparison of the Q4 2010 analytical results for the On-Site Boundary Wells to their respective I.L. values shows that the I.L.s were not met for any of the monitoring locations. Therefore, there was no requirement to further investigate radionuclide activity in these wells. However, monitoring installation MW-40 and MW-51 are being further evaluated on a routine basis, as discussed below.

MW-40 and MW-51. While there have been no historic I.L. exceedances at these two southern boundary locations, and the majority of the data from this quarter (Q4 2010) fall within previous ranges (Tritium activity in MW-40-81 was at the historic maximum, but still below 250 pCi/L), these monitoring locations continue to be evaluated on a routine basis given the sensitivity associated with the southern power block boundary. Even though it is recognized that the peak Tritium levels detected are low (less than 350 pCi/L) and near the lower limit of detection, there appears to be a general correlation in Tritium peaks (seasonal cyclical pattern) at multiple depth intervals in both of these monitoring installations (see **Figure H1** in **Appendix H**). This general correlation is evident in MW-51 during both the previous quarter (Q3 2010) and the current quarter (Q4 2010) as the depth intervals recorded an increase (similar magnitude) in Tritium activity during Q3 2010 and generally exhibited a decrease in Tritium activity during Q4 2010. MW-40 also remained consistent with the overall pattern, but it peaked earlier than MW-51, with the majority of its intervals increasing towards another peak this quarter.

⁵² Note that, beginning this quarter (Q4 2010), the laboratory MDC has been increased to approximately 2pCi/l.

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An appropriate metric to evaluate whether or not these cyclical trends are due to Tritiated groundwater migration from the power block area is the relative groundwater elevations between these locations and the power block areas where Tritium contamination exists. As discussed at length in the CSM sections of the Site Investigation Report, the southern boundary groundwater elevations are well above those in the power block area. As such, groundwater, and thus Tritium in the groundwater, cannot migrate from the power block to the south; in fact, groundwater is migrating in the opposite direction. This conclusion was previously validated for nine quarters (between Q2 2007 and Q2 2009) through analyses of groundwater elevation contours (see **Figure 5** in the quarterly reports prior to Q3 2009). In addition, starting with the Q1 2009 Quarterly Report, **Figure 5A** is being generated to specifically compare high importance transducer readings to historic maximum and minimum readings. The objective of this analysis is to demonstrate that substantial changes to the on-site groundwater flow field have not taken place and that the CSM remains valid. Multiple sampling zones from both the MW-40 and MW-51 monitoring installations are included in this analysis.

Based on these analyses, as well as the substantial body of data developed over the last 5 years of investigation which underpin our CSM, we conclude, with a high degree of confidence that the low level peaks in the Tritium activities observed in these two monitoring installations are not due to groundwater migration from the power block area. This conclusion has continued to be validated each quarter. However, we do not have a definitive explanation for the observed peaks. Further investigation into other potential mechanisms, such as seasonal atmospheric Tritium washout and seasonal laboratory biases are ongoing.

3.4.4 Q4 2010 SSC Investigation Levels

For the SSC monitoring wells, a comparison of the Q4 2010 analytical results to their respective I.L. values shows that the I.L.s were met at four sampling locations this quarter. The following table summarizes the cases where the I.L.s were met, with these exceedances individually discussed below.

WELL ID	RADIONUCLIDE	RESULT (pCi/L) ^{***}	REANALYZED RESULT (pCi/L)	INVESTIGATION LEVEL (pCi/L)
MW-32-149 (Q4 2010)	H3	1,550	NA*	1,000
MW-36-24	H3	2,620	NA*	2,563
MW-41-40	H3	2,430	NA*	1,002
MW-46	H3	3,130	NA*	1,844

* NA indicates that the sample was not reanalyzed.

** ND indicates that the radionuclide was not detected greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

*** A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

MW-32-149. The Q1 2010 through Post-Q2 2010 results at this interval showed a noticeable increase in Tritium activity to nearly ten times the I.L. in the Post-Q2 2010 sample⁵³. The Q3 2010 and Post-Q3 2010 samples also exceeded the Tritium I.L. at this interval, but a noticeable decrease in activity was noted during these sampling events. The I.L. was again exceeded at this interval during the current (Q4 2010) quarter, although the recent decreasing trend of Tritium activity continued through Q4 2010. Consequently, the Tritium activity at MW-32-149 has decreased by nearly 85% since the Post-Q2 2010 sampling event.

Similar to the other MW-31 and MW-32 exceedances discussed in **Section 3.4.2** above, this Tritium peak has also been attributed to the transient RWST/R.O. skid surface spill which occurred in Q4 2009. The quick response of this deep sampling interval to the Tritium surface

⁵³ Only the first sample collected at this location (1/19/2007) showed a higher Tritium activity (10,500 pCi/L) than the Post-Q2 2010 sample results (9,760 pCi/L).

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release provides further evidence that the spill may have penetrated the well casings and entered the subsurface immediately proximate to the sampling installation. This conclusion is based on the previously observed behavior of this sampling interval, which had historically exhibited a relatively uniformly decreasing trend for the last three years, absent the peaks observed in shallower intervals⁵⁴. Because the probable source has been terminated, we anticipate that the Tritium activity at MW-32-149 should continue to decrease to an activity below the I.L., similar to the other MW-31 and MW-32 intervals discussed in **Section 3.4.2** above. However, as discussed above for MW-32-59, the future behavior of this sampling interval is in question due to possible contributions from the storage/Retention Mechanism(s) and will therefore be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

MW-36-24. The Q4 2010 Tritium activity at this sampling interval slightly exceeded the I.L. Additionally, the Tritium I.L. was exceeded during the Q2 2010 sampling event⁵⁵. However, the Tritium activity decreased to a level approximately one order of magnitude below the I.L. between these two exceedances (Q3 2010). Based on the downgradient well location, the likely source of these Tritium peaks was the transient surface spill related to the temporary rental RWST/R.O. processing skid. Similar to the Q3 2010 result, the Tritium activity is expected to relatively quickly decrease below the I.L. at MW-36-24 because the probable source for the recent Q4 2010 peak is terminated and Tritium is a non-sorbing radionuclide. However, as discussed previously, future contributions from Retention Mechanism(s) may potentially create additional transient peaks at this sampling interval; as such, it will be further evaluated based on the additional data obtained during the upcoming quarterly monitoring round.

MW-41-40. The Tritium I.L. in this well was exceeded by nearly a factor of three during both the previous (Q3 2010) and current (Q4 2010) quarters⁵⁶. A noticeable increase in Tritium activity to approximately 60,000 pCi/L and 300,000 pCi/L was also concurrently observed in Manhole A2 during routine 80-10 Effluents Program sampling in Q3 2010 and Q4 2010, respectively. MW-41 is located directly adjacent to this storm drain system, between manholes A2 and A4. The transient Q3 2010 peak in MH-A2 occurred in early July 2010 (7/7/2010); however, the Tritium activity rapidly decreased (<1 week) to a baseline activity seen within this storm drain system. Conversely, the Q4 2010 peak was prolonged, with elevated Tritium activity observed for an extended time period (10/5/2010 – 11/10/2010) during this quarter. Additionally, an increase in Tritium activity was also observed downstream in this storm drain system at manhole A4 during both monitoring periods. Prior to these peaks, the Tritium activity in these manholes was consistently below 1,500 pCi/L for an entire year.

However, an additional prior Tritium peak was observed in MH-A2 in Q2 2009, with a concurrent Tritium I.L. exceedance in MW-45-42. This well is located immediately adjacent to MH-A2. Both locations exhibited rapid decreases of Tritium activity (in MW-45-42 to levels below the I.L.) during the following, Q3 2009, quarter. This initial peak in both MW-45-42 and MH-A2 initiated a series of investigations into the correlation and underlying cause of both the IL exceedance in the monitoring well as well as the increased Tritium in the manhole. The investigations quickly identified a likely cause of both the monitoring well and manhole peaks as associated with higher levels of washout entering the FSB building roof drain leading directly

⁵⁴ It is also noted that the sampling interval immediately above this interval, MW-32-85, did not exhibit a Tritium peak in Q1 2010; however, the Tritium activity increased during Q2 2010 through Q4 2010 to levels slightly below the Tritium I.L.

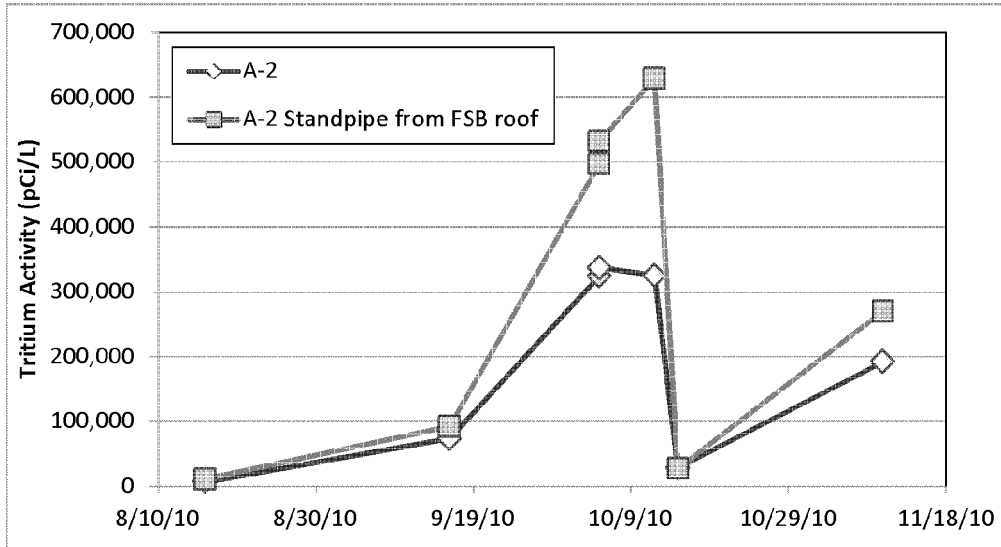
⁵⁵ It is also noted that the Tritium activity also increased in both of the deeper sampling intervals at this location (MW-36-41 and MW-36-52) during the Q2 2010 sampling event. An overall, slightly decreasing trend was noted from Q2 2010 to Q4 2010, following the Tritium peaks at both intervals.

⁵⁶ The Tritium activity slightly decreased from Q3 2010 to Q4 2010. A subtle increase in Tritium activity was also noted in the deeper sampling interval (MW-41-63) at this monitoring location during Q3 2010. Similar to MW-41-40, a slight decrease in Tritium activity was also noted at this depth from Q3 2010 to Q4 2010.

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into MH-A2 when the vent fan is not operating. Under specific climatic conditions, FSB evaporation can condense on the roof and be transported into the storm drain system via rain water.

The more recent Tritium peaks in Q3 and Q4 2010 provided additional information which helped inform further investigations. As one step in the investigative process to rule out a leak in a SSC, a standpipe was constructed which solely receives inflow from the FSB downspouts and isolates this water from other water sources to MH-A2. The Q3 and Q4 2010 sample data from this standpipe demonstrate, as shown below, that the recent Tritium activity within MH-A2 is directly proportional to the discharge from the FSB roof.



Based on the investigations and associated data collected, it has been concluded that the elevated Tritium levels detected in MH-A2 and A4 are due to the FSB roof condensate. Consequently, some of this highly Tritium-laden water was in all probability released into the groundwater from the storm drain system⁵⁷ and thus likely resulted in the Q3 2010 and Q4 2010 Tritium peaks observed in MW-41-40. Moreover, it would also then follow that the Tritium peaks seen in MW-46 and MH-B1, discussed below, as well as the earlier peak in MW-45-42, are all associated with the above described mechanism. As such, these monitoring well peaks in Tritium activity do not indicate a new leak from a SSC. Notwithstanding the above analyses, the behavior of this interval will be specifically evaluated further based on the additional data obtained during the upcoming quarterly monitoring rounds given that the Unit 3 FSB fan is in the process of being repaired.

MW-46. The Tritium activity at this monitoring location slightly exceeded the Tritium I.L. in the previous (Q3 2010) monitoring period. An additional increase was also noted during the current, Q4 2010, quarter to an activity that is nearly two times the Tritium I.L. and the second-highest activity historically measured at this location. MW-46 is located downgradient of MH-A2; therefore, this ongoing Tritium peak is likely related to washout entering the FSB building roof drain, as discussed above under MW-41-40. Similar to MW-41-40 and MH-A2, no other radionuclides were detected at MW-46 during both the Q3 2010 and Q4 2010 monitoring

⁵⁷ It is noted that the Tritiated water vapor evaporating from the SFP is a permitted release through the Plant Vent located atop the vapor containment building. Analyses were conducted to account for this release to the FSB roof in the dose computations. This same Tritium is therefore "double counted" because it has again been included in the storm drain and groundwater portions of the dose computations.

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events. This monitoring location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring rounds.

MH-5 VCFD, B-1 and B-6. The Unit 2 foundation drains which discharge into MH-5 VCFD, along with similar drains for Unit 3 which discharge into Manholes B-1 and B-6, form an integral part of the early leak detection monitoring network.

While the Q4 10 data showed that the MH-5 VCFD Tritium activity remained at baseline levels, the previous quarter (Q3-2010) showed a clear increase in Tritium activity (approximately by an order of magnitude) over base line levels⁵⁸ (see **Figure 6B**)⁵⁹. The other radionuclides analyzed (e.g. Strontium, Cesium, Cobalt) have previously been non-detect, and have remained non-detect through the Q3 2010 Tritium peak, and into Q4 2010, at MH-5 VCFD.

During quarter Q4 2010, the Unit 3 Tritium activity in manhole B-1 decreased by nearly one order of magnitude⁶⁰ as compared to the previous, Q3 2010 results, which exhibited historical maximum activities at this monitoring location. The Q3 2010 peak was consistent with the transient increase in Tritium activity also observed in MH-A2 during that period (See discussion above under MW-41-40). However, unlike the Q4 decrease observed in B-1, there was a second peak observed in MH-A2 and the Tritium activity seen at monitoring locations MW-41-40 and MW-46 remained elevated during Q4 2010. Given the continued activity in MH-A2, the reason for the decrease in Tritium activity in B-1 is not clear. Similar to the historical sampling events at B-1⁶¹, Cesium was also detected in this manhole at an activity comparable to the Q2 2010 and Q3 2010 results⁶². These Cesium levels are well below the 80-10 Effluents Program reporting limits, and are believed to be associated with Unit 1 contaminated construction backfill remaining in the vicinity of the Unit 3 VC Building. The remaining radionuclides were all non-detect during the current, Q4 2010, sampling event at B-1.

All radionuclides (including Tritium) were non-detect at B-6 during the Q4 2010 sampling event.

Leak Collection Device (LCD). The flow rate into the Unit 2 Leak Collection Device (LCD) remained at baseline during the current, Q4 2010, monitoring period. This return to baseline conditions, in October 2010, followed a clear increase in the volume of water collected by the LCD during the previous (Q3 2010) quarter, beginning on July 5, 2010⁶³. The flow rate averaged approximately 1.5 L/day over the quarter⁶⁴. Investigations indicated that the increased flow appeared attributable to atypically elevated water levels in the fuel pool as associated with dry cask work. Limiting such increases in pool water elevation in Q3 appeared to result in a marked decrease in the LCD flow rate back to levels generally consistent with the baseline of less than approximately 0.02 L/day at the very beginning of Q4 2010. Based on these observations, a figure (**Figure 6B**) has been included in this quarterly report (first included in the Q3 2010 quarterly report) which visually presents both the U2 Leak Collection Device

⁵⁸ After the Q3 10 increase, the Post-Q3 2010 sampling data from only 10 days later show the Tritium activity in MH-5 VCFD had already returned to the previous baseline levels.

⁵⁹ Potential correlations between the Q3 increased MH-5 VCFD Tritium activity and the increased LCD flow rate and increased activity in proximate monitoring wells MW-31 and MW-32 are discussed in **Section 3.4** of the Q3 2010 Quarterly Monitoring Report.

⁶⁰ It is noted that the current Tritium activity is still elevated (approximately two-fold) when compared with the baseline activity in this manhole.

⁶¹ A total of 10 samples have been collected from Manhole B-1 and low levels of Cesium has been positively detected in 6 of these samples.

⁶² At manhole B-1, the Cs-137 activity slightly decreased from the previous quarter (Q3 2010) to the current, Q4 2010, quarter.

⁶³ Potential correlations between the Q3 increased LCD flow rate and the increased Tritium activity in proximate monitoring wells MW-31 and MW-32, as well as MH-5 VCFD are discussed in **Section 3.4** of the Q3 2010 Quarterly Monitoring Report.

⁶⁴ The LCD collected approximately 50 liters of water during the July to October 2010 time frame, which is greater than the total volume of water collected during the previous 3 year period (April 2007 through June 2010). In this regard, however, it is noted that all of the water collected by the LCD is fully contained and does not enter the groundwater regime.

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data and the historical Tritium data for the sampling intervals located within the Unit 2 Tritium plume boundaries.

U1 NCD AND U1-SFDS. Sampling of the Unit 1 North Curtain Drain (U1-NCD) and the Unit 1 Sphere Foundation Drain Sump (U1-SFDS) are currently included as part of the Long Term Monitoring Program. These drains have been documented to capture a large proportion of the Strontium leakage from the Unit 1 SFPs, and continue to collect groundwater containing Strontium and Cesium and direct it to treatment⁶⁵. These drains have also historically been assumed to collect some groundwater contaminated with Tritium from the Unit 2 SFP. This conclusion was validated by the tracer test conducted as part of the hydrogeologic site investigation (see the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008).

Visual inspection of the U1-SFDS Tritium data demonstrates that the Q4 2010 activity continues the relatively stable trend (within an overall decreasing trend) in this drain over the last five quarters. The Q4 2010 Tritium activity in U1-NCD decreased by a factor of four from the peak established in Q1 and Q3 2010⁶⁶, and has reestablished the overall decreasing trend evident back to the middle of 2008, when LTMP data collection began.

Strontium data from these drains continues to show overall decreasing trends since the completion of U1 SFP defueling; as such, both drains have generally reached the pre-defueling Strontium levels, as summarized on **Figure 7A**.

3.4.5 Conclusions - Boundary and SSC Leak Detection Monitoring

Recognizing that measured activities in the Off-Site and On-Site Boundary Wells have remained below I.L. levels, this overall data set continues to demonstrate that radionuclides are migrating toward the Hudson River to the West, and are not migrating off of the property to the North, East or South, as expected given the measured groundwater flow directions from the property periphery toward the power block area.

Given the analyses discussed above, there is also no compelling reason to believe that any new unidentified leaks have developed in the SSCs monitored relative to Unit 2 or 3. As discussed in **Section 3.4.4** above, and based on a series of investigations beginning in 2009, we have concluded that the increases in Tritium activity in manholes A2 and A4 are related to SFP condensation which collects on the FSB roof when the exhaust fan is not operating⁶⁷. It has been further concluded that this condensation is also the underlying cause of the Tritium I.L. exceedances and peaks observed in both nearby and downgradient sampling locations, MW-41-40, MW-46 and B-1, respectively, as well as the 2009 peak in MW-45-42, located immediately adjacent to MH-A2. As such, these peaks in Tritium activity do not indicate a new leak from a SSC.

Additionally, as discussed in the Q1 2010 Quarterly Monitoring Report, a peak in Tritium activity was measured in MH-9 during routine 80-10 Effluents Program sampling. The Q1 2010 sample from the upper-most interval of MW-32 (MW-32-59) also exceeded its I.L. with the highest

⁶⁵ Prior to the Unit 1 SFP defueling, the U1-NCD and U1-SFDS drains were collecting approximately 20-40 times more Strontium than was discharging through groundwater into the Hudson River. Additionally, these drains were particularly effective during defueling and captured approximately 300-350 times more Strontium during this time frame. Currently, these drains are removing approximately 10 times more Strontium than is discharging into the Hudson River from groundwater.

⁶⁶ The Q3 2010 Tritium result in U1-NCD increased by nearly a factor of three relative to Q2 2010, and was the highest activity measured in this drain to date. The underlying cause for this peak in the U1-NCD is currently unclear.

⁶⁷ It is noted that the Tritiated water vapor evaporating from the SFP is a permitted release through the Plant Vent located atop the vapor containment building. Analyses were conducted to account for this release to the FSB roof in the dose computations. This same Tritium is therefore "double counted" because it has again been included in the storm drain and groundwater portions of the dose computations.

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Tritium activity measured since the initiation of the LTMP. After further investigation by IPEC, it appears that these Tritium increases originated from a Q4 2009 localized, transient surface spill just outside the Unit 2 SFB. The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor⁶⁸; the temporary leakage likely emanated from connection hoses during or just after the filtration process. It appears that this transient release entered both MH-9 and the well vault for MW-32 (which employs a drain emptying into MH-9), and may have also penetrated the MW-32 well casings. Both the storm drains and the well vault likely provided pathways for radionuclides to enter the subsurface. The Q2 2010 and Post-Q2 2010 data showed further I.L. exceedances both at deeper intervals (MW-32-173) and farther down gradient (MW-36-24 and MW-50-42), as would be expected as the spill worked its way through the groundwater flow regime. These additional Tritium exceedances were also attributed to this transient R.O. skid surface spill. The Q3 2010 and Post-Q3 2010 data demonstrated that the downgradient Tritium activities in MW-36-24 and MW-50-42 quickly returned below the I.L.; however, the Tritium levels in multiple "near source" sampling intervals (MW-31-49, MW-31-63, MW-32-59, MW-32-149, and MW-32-173) still exceeded the Tritium I.L. The Tritium activity in the majority of these MW-31 and MW-32 intervals (MW-31-49, MW-31-63, MW-32-59 and MW-32-173) decreased below the I.L. during the current, Q4 2010, monitoring round. However, a second Tritium I.L. exceedance was noted in MW-36-24, which is likely related to delayed input from Retention Mechanism(s).

Based on the above analyses, it is clear that the LTMP has provided valuable data aiding in the identification of releases to the groundwater.

Finally, increased leakage measured in the Unit 2 LCD from July 2010 to October 2010 appears attributable to raised pool levels within the U2 SFP during various dry cask fuel transfer procedures. While all the flow into the LCD is captured and released through monitored pathways, recent (Q3 2010 and Post-Q3 2010) peaks seen in MW-31-49, MW-32-59 and MH-5 VCFD could possibly be correlated with this increased flow rate. Based on the most-recent Q4 2010 data (October 2010 through December 2010), the flow into the LCD has decreased back to baseline levels of less than 0.02 L/day. This decrease appears to be in response to the post-investigation limiting of pool water elevation during dry cask work. Based on the Q3 2010 observations, Entergy has initiated investigations into potential leak pathways.

The overall U2 plume⁶⁹ has continued to generally exhibit overall, long-term reductions in Tritium activity since termination of the identified Unit 2 SFP leaks. While Q2 2010 increases in Tritium activity were observed in multiple monitoring locations within the delineated U2 plume⁷⁰, these data were consistent with both the Q4 2009 transient RWST/R.O. processing skid surface spill and the overall historic variability observed in Tritium levels attributed to episodic releases of Tritium stored in the subsurface via natural and anthropogenic Retention Mechanisms⁷¹. Reductions in Tritium activity have now been seen in numerous Unit 2 monitoring locations during Q3 2010 and Q4 2010.

Relative to the Unit 1 Strontium data, increased leakage was anticipated during final fuel removal from Unit 1 SFPs. This leakage was readily detected as increased Strontium in the

⁶⁸ As such, this unit is not an in-place, plant SSC, and is no longer on site.

⁶⁹ It is noted that there is no Tritium plume associated with Unit 3.

⁷⁰ It is noted that a one-quarter increase was observed in the total Tritium activity of the Unit 2 plume during Q2 2010, as elucidated in **Figure G-17**. This Tritium mass increase was attributed to the transient RO. skid surface spill. The Q3 and Q4 2010 data show reductions from the Q2 2010 level, with resumption of the previous decreasing trend in the total plume activity (see **Figure G-17**).

⁷¹ This conclusion is supported by the tracer data and other analyses discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report. These Retention Mechanisms are further discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report. However, given the more recent behavior observed in the Unit 2 Leak Collection Device (LCD) data, as well as previous data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms.

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groundwater by the Long Term Monitoring Program. The initial near-pool and subsequent downgradient Strontium increases have been routinely monitored as summarized on **Figure 7A**. Currently, the near-pool and more downgradient monitoring locations have generally returned to pre-defueling Strontium levels, with outliers (such as MW-37-40⁷²) expected to continue to show further decreases towards pre-defueling levels in the upcoming quarters. Additionally, the near-river sampling intervals (MW-67-39, MW-67-105, and MW-62-138) have recently exhibited an increase in Strontium activity, as the perturbation migrated downgradient.

Overall, GZA believes that further monitoring will continue to demonstrate the decreasing long term trends historically observed in groundwater activities over time for both the Unit 1 and Unit 2 plumes given the source interdictions completed by Entergy. However, ultimate confirmation of the rate of decrease will require monitoring over a number of years to demonstrate continued depletion of Tritium and Strontium from the Retention Mechanisms originally sourced by the historic Unit 2 SFP Tritium Unit 1 SFPs Strontium leakages, as well as the more recent Strontium leakage due to Unit 1 defueling and impacts associated with a number of recent, localized, transient spill events. It is further noted that quantification of these overall radionuclide reductions will require that ranges in seasonal variation be adequately reflected in the monitoring data and any further additions of radionuclides to the Retention Mechanisms, such as through the transient spills discussed above, be dissipated from the geohydrologic flow regime.

Given the above cited constraints, it is premature to begin recalibrating the I.L.s, which were originally established at the beginning of the LTMP in 2007. Since inception of this program, it has been observed that I.L.s have been routinely exceeded in a number of cases where subsequent data have demonstrated that no new leaks or spills have occurred. The majority of these cases occur where the radionuclide levels are generally low and/or near their detection limits. It appears that data variability, likely due to seasonal precipitation influences and local variations in flow paths and/or other in-situ processes, is the primary cause of these false positives⁷³, particularly pursuant to Tritium. Therefore, the basis upon which the I.L.s are computed needs to be re-evaluated in light of the long-term natural transient variability of the groundwater system in response to precipitation events, etc. Furthermore, while re-evaluation/re-setting of I.L.s is a clear goal, it is still premature given the lack of sufficient data. This is particularly true given the recent behavior in Strontium levels due to the Unit 1 defueling (see **Figure 7A**) and the transient Tritium spills discussed above and in the Q1 2009 LTM Report. As such, the current I.L.s will remain in effect while a sufficient data base is acquired to allow better quantification of the natural (non-leak related) variability in the data.

We draw five major conclusions from the above summarized data and analyses:

1. The current CSM for the IPEC site provides a good basis for the design of the Long Term Monitoring Program;
2. The procedures and rationale used for selecting monitoring locations for leak detection have been further validated given the clear detection of the confirmed Unit 1 SFPs increased leakage during fuel removal, the transient Q1 2009 U1 FSB distillation tank valve leak (see Q4 2009 Quarterly LTM Report for further discussion), the Tritium

⁷² It is noted that the 40 foot interval in the MW-37 monitoring installation is showing a delayed decrease in Strontium levels as compared to the depth intervals above and below. This response time lag is likely a result of the lower hydraulic conductivity (by two to three orders of magnitude) of the bedrock accessed by this depth interval.

⁷³ In this context, "false positive" does not refer to an error in the actual data value. Rather, it means that the I.L. exceedance in question did not result from a new release. While I.L.s are meant to be set at conservatively low values, and thus "false positives" should be expected, a corollary objective is to set I.L. values which keep the number of false positives low enough to eliminate development of complacency.

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increases in Manhole A2 in Q2 2009, Q3 2010 and Q4 2010, and the Q4 2009 RWST/R.O. processing skid surficial release to MH-9⁷⁴;

3. Higher than normal water levels in the Unit 1 SFPs during defueling resulted in increased activities in the groundwater proximate to, and downgradient of those structures, and in Strontium levels following this documented increased release rate take longer to materialize in the groundwater than might otherwise be expected⁷⁵;
4. Localized, transient Tritium spills have a pronounced short term impact on Unit 2 Tritium plume activity, with potential longer term impacts via Retention Mechanism(s); and
5. Even with the somewhat increased Tritium levels still being observed in downgradient wells due to the transient RWST/R.O. skid surface spill, the amount of all radionuclides being released through the groundwater pathway is still small (<0.01%) compared to permitted levels of radionuclides discharged to the river through the Discharge Canal.

3.5 Plume Natural Attenuation Monitoring

The fourth and final objective of the Long Term Monitoring Program is to evaluate if the groundwater plumes identified on-Site demonstrate overall reductions in total activity over time, as is consistent with the requirements of Monitored Natural Attenuation (MNA), the selected remediation for the IPEC Site⁷⁶.

Given the likely ages of the SFP leaks identified and characterized during the hydrogeologic investigation, it is probable that the Unit 2 (Tritium) and Unit 1 (Strontium) plumes had reached steady state conditions prior to the beginning of the LTMP. Given that: (1) the identified leaks in the Unit 2 SFP have all been previously repaired (the last leak repaired in 2007) and; (2) the water in the Unit 1 West Pool underwent intensified demineralization (beginning in April 2006 with a reduction in Strontium levels of over 95 percent) and the pools were fully defueled and drained in, one might expect that the plumes should have started to markedly attenuate toward zero with time. Both plumes have in fact generally shown significant levels of attenuation, when they are viewed in their entirety and past release events and expected seasonal variability in the sampling data are accounted for. However, the attenuation has not been as rapid as we originally anticipated during time frames subsequent to the source interdictions implemented by Entergy.

In the case of the Unit 2 Tritium plume, levels have dropped markedly from the highest levels measured during the two-year hydrogeologic investigation. However, the rate of Tritium decrease with time has decreased. While the decreasing trend since source interdiction is clear, the rate of reduction has been difficult to predict due to the impact of natural geologic and anthropogenic Retention Mechanisms. These subsurface features have trapped and stored Tritium that was released during historic Unit 2 SFP leaks, and are still likely releasing this Tritium to the groundwater flow regime in an episodic manner after the physical leaks have been terminated. This conclusion is consistent with the original CSM presented in the Hydrogeologic Site Investigation Report, as further supported by the tracer test data in that report as well as subsequent tracer data, as described in Section 3.6 of the Q1 2009 Quarterly Monitoring Report, dated July 2, 2010. In addition, trend identification is further complicated by impacts associated with localized transient releases (most recently, the RWST/R.O. processing skid surface spill). As described above, these transient spills appear to have resulted in a number of

⁷⁴ Additionally, the recent peaks in MW-31-49 and MW-32-59 could possibly be related to the recent (July 2010 through October 2010) increased leakage rates at the Unit 2 Leak Collection Device.

⁷⁵ Given the proximity of monitoring installations to documented release events, the delay in release arrival is likely due primarily to Strontium partitioning and the time required for leakage to traverse anthropogenic features.

⁷⁶ The selection of MNA as the remediation for the Site is more fully discussed in the Hydrogeologic Site Investigation Report.

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Tritium peaks (increase and then decrease in Tritium activity) proximate to the spill, with still increasing trends in Tritium activity in a number of downgradient wells. As such, these increases do not appear to be indicative of a new leak in the Unit 2 SFP. Further discussion of this quarter's data pursuant to evaluation of the Unit 2 Tritium plume MNA is provided in **Section 3.5.1** below.

Relative to the Unit 1 Strontium plume, Strontium levels should drop more slowly than Tritium levels. This is because, in addition to the Retention Mechanisms discussed above for Tritium (which also apply to Strontium), Strontium also undergoes partitioning whereby this radionuclide is adsorbed from the groundwater onto solid surfaces (both geologic and anthropogenic). When the input of Strontium to the groundwater is reduced (such as via the initial fuel pool demineralization and subsequent decommissioning) the solid surfaces desorb the "stored" Strontium back into the groundwater, thus maintaining Strontium levels. Strontium partitioning is therefore expected to substantially slow plume attenuation. Despite partitioning effects, some plume attenuation was observed in response to pool demineralization prior to defueling, particularly proximate to the pool. However, defueling of Unit 1 resulted in a temporarily increase in the leakage rate of West Pool water into the formation. This was expected based on previous work on the Unit 1 SFPs, but was unavoidable given the requirement to raise the pool level for fuel rod removal⁷⁷. The increased leakage rate had resulted in a noticeable increase in Strontium levels in the immediate vicinity, and downgradient of, the fuel pool. However, as more currently observed, the near-pool and more downgradient monitoring locations have generally returned to pre-defueling Strontium levels, with outliers expected to continue to show further decreases towards pre-defueling levels in the upcoming quarters, as discussed further in **Section 3.5.2** below.

3.5.1 Unit 2 Tritium Plume Attenuation

Qualitative Evaluation

From a qualitative perspective, a reduction in overall Tritium activity in the Unit 2 plume can be seen through a comparison of the Q4 2010 delineated plume boundary (**Figure 6A**) to those in early LTMP quarterly reports (2007 and 2008). Not only have Tritium levels within the plume generally shown an overall, long-term decreasing trend, but the reductions over the more recent quarters, downgradient of the discharge canal, have become particularly evident in the delineated, shaded bounds of the plume. This quarter continues the trend where the shaded plume⁷⁸ no longer extends to the river as it did in previous quarters through 2008. Additionally, the rolling average Tritium activity in MW-111, indicative of the core of the plume, has shown an overall decrease by a factor of nearly two over the last two years (from 70,150 pCi/L in Q1 2009 to 38,240 pCi/L this quarter, (Q4 2010), and by nearly an order of magnitude since tracking of the plume began. This trend over time has been summarized on **Figure 6A**, which is a compilation of the quarterly Tritium plume maps as well as that from the Investigation Report.

⁷⁷ As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

⁷⁸ The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

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Mann-Kendall Quantitative Analysis

To more quantitatively evaluate MNA progress, a Mann-Kendall analysis, as referenced in USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis,⁷⁹ was performed on the Tritium levels measured through Q4 2010 at monitoring locations associated with the IP2-SFP and downgradient Unit 2 Tritium plume⁸⁰. Each of the vertical monitoring intervals at each monitoring installation was analyzed separately. In general, only data collected after final completion of the multi-level installation⁸¹ was used. However, there were a number of exceptions to this generalization where open borehole and/or borehole packer testing data were also used. These data were incorporated where possible given the importance of early time data (proximate to when documented leaks were still active). Additional, more detailed discussion relative to the basis for including these data is provided in Section 3.6 of the Q1 2009 Quarterly LTM Report.

Graphs showing the variation in Tritium concentration over time in the immediate vicinity of the Unit 2 SFP are presented as **Figures G-1, G-2 and G-3** in **Appendix G**, for MW-30, 31 and 32, respectively. Additional graphs are also presented in the appendix for the other monitoring locations downgradient of the Unit 2 SFP (see **Figures G-4 through G-14** for MW-33 through 37, 42⁸², 49, 50, 53⁸², 55 and 111) and downgradient, river boundary wells (see **Figures G-15 and G-16** for MW-66 and 67, respectively). The Mann-Kendall analyses for the individual monitoring points are summarized on **Table G-1** in **Appendix G**. The table includes the results of the analysis for each depth interval (“well”) at each of the multi-level monitoring locations enumerated above. The table is color coded, with green shading designating wells showing a decreasing trend, yellow for no trend, and red for an increasing trend.

Comparison of **Table G-1** for Q4 2010 to that from Q3 2010 indicates that there have been no changes, with the exception of MW-42-49 which has changed to a decreasing trend from a no-trend designation. Of the 32 non-river-boundary intervals included on the table for Q4 2010, approximately one-half (18) show a decreasing trend, one more than last quarter⁸³. It is important to note that this group of “decreasing wells” includes all those located within the core

⁷⁹ USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis, EPA QA/G9, QA00 UDATE; EPA/600/R-96/084, July, 2000.

⁸⁰ The Mann-Kendall statistical technique was initially chosen because it is particularly well suited for data sets with a limited number of points. The method was subsequently retained because it is also a non-parametric analysis and therefore does not introduce bias by presupposing any particular shape for the trend curve. In addition, the method is robust with respect to outliers, which allows it to handle the variability inherent in the data set. Finally, the method tolerates non-uniform sampling frequencies. This is important because while the sampling frequency is typically quarterly, more frequent samples are proactively taken when a scheduled operation carries an increased risk of potential release, and also when something unexpected is observed that could indicate a new leak or spill.

⁸¹ The majority of the boreholes were completed as a multi-level installation. These multi-level completions were designed to segregate the borehole length into individual sampling zones with depth. The sampling zones were generally established to coincide with the more productive zones of the fractured bedrock and overburden (both natural soils and backfill). These sampling zones were then isolated from each other with various types of seals placed in the open borehole. The objective of the seals is to prevent vertical flow through the borehole and thus establish the same conditions in the formation which existed prior to the drilling of the borehole. As such, the Tritium data is considered depth-discrete. It is noted that the multi-level installations at some monitoring locations were removed and replaced with upgraded systems, such as for the monitoring installation at MW-32.

⁸² MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP could be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above.

⁸³ The Q3 and Q4 2010 Mann-Kendall analysis designated four increasing trends to non-river boundary monitoring intervals. Only two of these monitoring intervals exhibited increasing trends during the previous quarter. The shift to additional wells with increasing trends is consistent with the anticipated impact of the RWST/R.O. skid spill given that these newly designated “increasing trend” intervals are located in the vicinity of the spill, have noticeable increases in Tritium activity since Q4 2009 (date of transient release), and exhibited a “no trend” status prior to this transient surface spill.

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of the plume with the highest Tritium activities (MW-30-69, MW-33 and MW-111). These high-activity wells better represent overall plume behavior because they encompass a great percentage of the Tritium activity in the plume. For the river boundary monitoring intervals, slightly less than one-half (4 of 9) show a decreasing trend, the same as last quarter⁸⁴.

Notwithstanding the above, it is noted that the Mann Kendal analysis is becoming increasingly less useful for evaluating the behavior of the plume in response to the termination of the identified leaks in the Unit 2 SFP, the reason these analyses were implemented. This is primarily due to the impact of two localized, transient Tritium surface spills⁸⁵, the most critical of which is the RWST/R.O. skid spill. These spills have been shown to result in increases in activity, which, while valid measures of plume behavior, impair the ability of the trend analysis to serve as a measure of the effectiveness of Unit 2 SFP leak identification and termination, the intended purpose of this analysis. Due to these spills, a number of wells have transitioned from decreasing trend, to no trend to increasing trend. As such, the practice to date of providing a discussion of each monitoring interval exhibiting a no trend or increasing trend is being suspended, starting with this quarter (Q4 10⁸⁶), until the spills have flushed through the groundwater system. The summary table and the individual interval Tritium plots are still provided in **Appendix G**.

Tritium Plume Total Activity Analysis

Another method to analyze plume behavior is to compute the total Tritium activity in the plume at multiple snapshots over time. This procedure⁸⁷ was implemented for each quarterly LTMP sampling round from Q2 2007 to Q4 2010. In addition, the bounding Tritium concentrations from Figure 8.1 of the Hydrogeologic Site Investigation Report⁸⁸ have also been included as a starting point for the graph. These data are summarized as a histogram on **Figure G-17** in **Appendix G**.

As can be seen from the figure, the total Tritium activity in the plume downgradient of the Unit 2 SFP has shown a distinctly decreasing trend over time. After a noticeable increase in total Tritium mass in Q2 2010⁸⁹, the total Tritium activity noticeably decreased during Q3 2010, and resumed the historical trend during the current (Q4 2010) quarterly monitoring period. The temporary, total Tritium activity increase observed during Q2 2010 appears to have been caused by the transient surface spill related to RWST/R.O. skid operations. As such, the total Tritium activity is expected to continue its overall decreasing trend, similar to the current (Q4

⁸⁴ Closer inspection of the current "no trend" river boundary wells (MW-66-21, MW-67-219, MW-67-276 and MW-67-323) reveals that the normalized test statistic decreased from Q3 2010 to Q4 2010 at all four intervals. As such, these intervals are all statistically shifting towards the "decreasing trend", which is currently defined at a 95% confidence interval, with the addition of the current, Q4 2010, monitoring data.

⁸⁵ In addition, effectiveness is further impacted by a limitation of the Mann Kendal analysis method, itself. This method only evaluates the number of increases relative to decreases, and does not weight the analysis relative to the magnitude of each change. Therefore, once a clearly decreasing trend, even of substantial magnitude, has reached a nearly horizontal asymptotic behavior, numerous insignificantly small positive and negative changes over time (such as due to sampling and hydrogeologic variability) can overwhelm the relatively short, early-time string of decreasing changes, thus resulting in a switch from a decreasing trend to a no-trend status. This is particularly true when a 95% confidence interval is applied.

⁸⁶ It is noted that the individual interval discussions provided in Q3 2010 generally also describe the Q4 2010 behavior

⁸⁷ The individual sampling point Tritium concentrations were multiplied by the groundwater volumes in representative zones (discretized over area and depth), as computed using soil and bedrock effective porosities developed from the pumping and tracer tests (see the Hydrogeologic Site Investigation Report for further information).

⁸⁸ Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc, on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

⁸⁹ Approximately 70% of the sampling intervals used in the total Unit 2 Tritium activity calculations recorded an increase in Tritium activity from Q1 2010 to Q2 2010. As such, the total Tritium activity increased from 0.017 Ci to 0.021 Ci during this quarter. Similarly, an increase in Unit 2 Tritium I.L. exceedances was observed in Q2 2010. It should be noted that an increase in Tritium activity for sampling locations completed in soil (backfill) have greater impacts on the total Tritium mass calculations due to difference in overburden porosity vs. bedrock porosity.

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2010) quarterly monitoring round, given the transient nature of the spill. Based on the Q4 2010 data, the total Tritium activity in the plume has decreased approximately 45 percent since Q2 2007, and has decreased by approximately 90 percent when compared to the bounding Tritium concentrations. It is noted that the time/activity data appear to be approaching a non-zero horizontal asymptote⁹⁰. While the general “first order” plume decay is what would be expected for a plume undergoing Monitored Natural Attenuation after source termination, a non-zero asymptote suggests a continued input of Tritium into the groundwater flow regime. The data currently available lead us to believe this continuing Tritium input is likely associated with the Retention Mechanism(s), the localized transient releases detected to data and/or potentially a small unidentified Unit 2 SFP leak, as described in this and earlier reports.

Conclusion- Unit 2 Tritium Plume MNA

Based on the data and analyses provided above, our conclusion is that the Tritium plume associated with the historic Unit 2 SFP leaks is undergoing overall, long-term reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP, this Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation⁹¹. Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report.

Finally, it is important to recognize that even with the somewhat increased Tritium activities recently observed due to the RWST/R.O. skid transient surface spill, the amount of Tritium being released through the groundwater pathway is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

3.5.2 Unit 1 Strontium Plume Attenuation

Despite the effects of partitioning, as discussed in **Section 3.5** above, the overall Strontium activity within the Unit 1 plume had generally shown some attenuation in response to the West Pool demineralization conducted by Entergy in preparation for defueling. This work began in 2006 and resulted in an approximately 98% reduction in Strontium in the West Pool (see **Figure 7A**: U1-NCD, U1-SFDS, MW-42, U1-CSS). However, the final defueling of the Unit 1 SFPs resulted in a noticeable increase in Strontium levels proximate to the SFPs (U1-NCD, U1-SFDS, MW-42, and U1-CSS); all of which have shown large sustained decreases since mid 2009 to pre-defueling levels or even lower than pre-defueling levels. Farther downgradient (MW-53, MW-55, MW-54, MW-57, MW-50, and MW-37), increases in the Strontium plume activities were also measured, but generally after a time lag as compared to wells more proximate to the SFPs. The majority of these more downgradient monitoring locations have most recently shown decreases to pre-defueling levels. The farthest downgradient, river boundary wells (MW-67 and MW-62) have possibly shown Strontium activity increases in the past few quarterly sampling events; however, the Strontium activity in MW-67-39 has noticeably decreased over the past four quarterly monitoring rounds and is currently lower than the pre-

⁹⁰ One physical cause for a horizontal asymptote would include a persistent, unidentified leak still remaining in the Unit 2 SFP. With Tritium at approximately 30,000,000 pCi/L in the SFP, a leak directly from the pool of only approximately 10 L/day would be sufficient to provide the required Tritium input to the groundwater. To date, the available data do not appear to support the existence of such a leak. The rationale underlying this continued conclusion is based, in part, on the impact of a number of transient spills, as well as the Retention Mechanisms discussed more fully in Section 3.6 of the Q1 2009 Quarterly Monitoring Report. However, this conclusion is continually reassessed on a quarterly basis as new data becomes available. In particular, the Q3 2010 quarter's LCD data as well as that for MH-5 VCFD resulted in the initiation of additional investigations.

⁹¹ It is noted that the previously clear attenuation of the Unit 2 Tritium plume has been confounded by a number of localized, transient surface spills. Entergy is currently in the process of reviewing and addressing work practices which may have contributed to the occurrence of these spills.

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defueling levels observed at this interval. This overall increase in Strontium activity, followed by a longer term decrease, was expected given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing the leakage rate from the SFPs prior to fully draining the pool⁹².

The data for Q4 2010 indicate that the overall Strontium levels continued to exhibit a general decrease and have now generally reached, or are even lower than, pre-defueling levels in the immediate vicinity of the pool (U1-NCD, MW-42, MW-56, U1-SFDS, U1-CSS and MW-53). These monitoring locations would be expected to be the first to reflect the complete decommissioning of the SFPs given their location/function. Somewhat farther downgradient, the Q4 2010 data are consistent with the "tail" portion of the perturbation as the previous increase in U1-SFPs leakage works its way towards the river. This behavior is most evident at monitoring locations MW-37, MW-50⁹³, and MW-57⁹⁴ where, for the most part, the maximum Strontium levels were recorded in 2009 and have shown an overall decrease over the past few quarters, approaching pre-defueling activities. MW-54, however, appeared to have already exhibited a Strontium peak in Q4 2008, and then decreased back to previous levels, even though this monitoring installation is relatively far downgradient. Similarly, the maximum post-defueling Strontium activity within all three sampling intervals at MW-55 was recorded in Q2 2009 and Q3 2009; the Strontium activity noticeably decreased following these peaks to levels that are currently lower than pre-defueling activities at this monitoring location. This behavior serves to again emphasize that the IPEC Site is located in a bedrock fracture controlled hydrologic regime⁹⁵. As such, this type of localized "distance-based inconsistency" is to be expected and likely indicates that these wells are closer to (or within) the more pervious preferential flow pathway that is hypothesized to be responsible for the convergence and narrowing of the Tritium and Strontium plumes as they move toward the river from sources centered at widely spaced locations upgradient⁹⁶.

Farther downgradient, in the vicinity of the river, increases in Strontium activity in MW-62 may be reflective of the Unit 1 SFPs defueling operations. The MW-62-138 depth interval (along with, but to a lesser extent the shallower intervals in overburden) appears to show two distinct Strontium peaks in Q1 2009 and Q4 2009⁹⁷. Furthermore, a third, smaller magnitude, increase in Strontium activity was observed during the previous (Q3 2010) quarterly monitoring round; however, the activity decreased to below the detection limit during the current, Q4 2010, monitoring round. Additionally, it is noted that the Strontium levels in this monitoring installation

⁹² As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

⁹³ As noted in **Section 3.4.2** above, the Q3 2010 Strontium result in MW-50-42 exceeded the I.L. at this sampling interval. Conversely, a decrease in Strontium activity was observed in MW-50-66 during Q3 2010. Furthermore, decreases in the Strontium activity in both MW-50-42 and MW-50-66 were observed during the current, Q4 2010, monitoring round, consistent with the "tail" portion of the perturbation.

⁹⁴ Based on Q2 2010 data; both sampling intervals in this monitoring location have approximately reached pre-defueling Strontium levels. This monitoring location is sampled annually, thus no samples were collected during Q3 2010 and Q4 2010.

⁹⁵ While groundwater flow through the fractured bedrock at the IPEC Site is highly preferential at small areal scales, it is characterized by sufficiently interconnected small bedrock fractures to allow the hydrogeologic system to function and be modeled as a non-homogeneous, anisotropic, porous media at Site-wide scales.

⁹⁶ By way of contrast, in a homogeneous porous media uniform flowfield, the centerlines of plumes that start at widely spaced locations (spaced perpendicular to the groundwater flow path) will typically remain widely spaced (although the edges of the plumes will likely move closer as the plumes get wider through dispersion). In the case of fracture flow at IPEC however, not only do the Strontium and Tritium plume centerlines converge, but the plumes also get narrower as they move downgradient. In addition, MW-50 displays high relative Strontium concentrations and fault gouge was encountered during the drilling of this well. These behaviors/data are typical of a more fractured zone preferentially controlling groundwater flow and thus the migration of the contaminants therein (see the Site Hydrologic Investigation Report for further CSM-focused discussion of this issue).

⁹⁷ The increase in Q1 2009 in MW-62-138 was followed by a steady decrease over the next two quarterly monitoring events, and the peak in Q4 2009 was followed by a greater magnitude decrease in Q1 2010; the Q2 2010 Strontium activity slightly increased compared to Q1 2010.

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are all relatively low (below 3 pCi/l), and this location does not appear to be proximate to (or within) the preferential flow path cited above for the Strontium plume. Therefore, the peaks in Strontium observed may not be associated with the Unit 1 defueling, and may be due to nothing more than hydrogeological variability. Another riverfront monitoring installation downgradient of the Unit 1 Strontium plume, MW-67, has also possibly exhibited impacts from the Unit 1 SFPs defueling. The Strontium data in the shallowest depth interval, MW-67-39, demonstrated a moderate increase in Strontium activity in Q4 2009, dissimilar to the previous overall decreasing trend that was seen at this sampling interval from Q4 2007 (pre-defueling) through Q3 2009. The Q4 2009 perturbation has been followed by slight, but distinct, Strontium decreases from Q1 2010 through Q4 2010 (trends consistent with "tailing off" portion of an adsorbing radionuclide), and the current, Q4 2010, activity is approximately four times lower than the pre-defueling activity within this interval. The monitoring interval directly below MW-67-39 (MW-67-105) had also shown increases in Strontium activity during the Q2 2010 and Q3 2010 quarterly monitoring events, after previously exhibiting generally stable Strontium levels since the initiation of the LTMP. Additionally, the Q3 2010 result exceeded the Strontium I.L. at MW-67-105, as discussed in **Section 3.4.2** above. Because the Strontium source was terminated, the Strontium activity at this interval was expected to decrease once the perturbation passed through the system. Accordingly, the Strontium activity rapidly decreased below the detection limit at MW-67-105 during the current, Q4 2010, quarterly monitoring round.

From an overall, long-term perspective, Strontium levels downgradient of the Unit 1 SFPs are generally behaving as expected. The monitoring installations closest to the SFPs (e.g., U1-NCD, MW-42, U1-CSS and U1-SFDS) exhibited strong peaks in Strontium activity in response to defueling, and then have decreased to, and even below, pre-defueling activities. Monitoring installations farther downgradient are generally showing decreases in Strontium activity over the past four quarterly sampling rounds and are generally approaching pre-defueling levels (e.g., MW-37, MW-55, and MW-57). As expected, the Strontium activities in a portion of these sampling intervals have already decreased to pre-defueling levels. Monitoring installations closer to the river may still show Strontium increases (similar to the recent increases at MW-67-39 and MW-67-105) as the additional leakage experienced during defueling flushes through the groundwater flow system. It is expected that completion of this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also continue their overall downward trend once this perturbation has fully passed through the system; decreasing trends are expected and predicted given that Entergy has terminated all leaks in the Unit 1 SFPs through decommissioning and the Unit 1 Strontium plume continues to decrease in accord with Monitored Natural Attenuation.

Based on the Strontium data and plume analysis provided above, our conclusion is that the Strontium plume associated with the historic Unit 1 SFPs leak is undergoing overall, long-term reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation.



4.0 CONCLUSIONS AND PLANNED FUTURE WORK

Given the data collected to date, the apparent strength of the CSM to evaluate those data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).

Based on the specific results and evaluation of the Q4 2010 groundwater monitoring within the context of the Long Term Monitoring Program, IPEC plans to continue routine groundwater monitoring, related monitoring network maintenance, and reporting of the data and engineering analyses. In this context, it is noted that the analyses and conclusions presented in this report are based on the data and information available up to and including the subject quarter. Data that becomes available after the subject quarter, but before the finalization date of the report is sequentially reflected in the associated subsequent reports.

This work will be conducted in accordance with the IPEC Radiological Groundwater Monitoring Program IP-SMM-CY-110, and will incorporate the enhancements described herein.

More specifically, evaluation of data collected during Q4 2010 has shown the following:

- While I.L.s have again been met at a number of Unit 2 locations this quarter, there is no compelling evidence that any new unidentified leaks have developed in the Unit 2 SFP or other monitored Systems, Structures, or Components. In fact, after previously exceeding the Tritium I.L.s for multiple quarters in a number of upgradient Unit 2 locations, the Tritium activity in many of these locations decreased below the Tritium I.L. during the current, Q4 2010, monitoring round. Additional rationale underlying this continued conclusion is discussed more fully in Section 3.6 of the Q1 2009 Quarterly Monitoring Report. The validity of this conclusion is also not diminished by the previous Q1 2010 through Post-Q3 2010 I.L. exceedances in multiple sampling intervals proximate to the Unit 2 SFP, as well as those farther downgradient, because these Tritium increases have been generally shown to be due to a localized, transient surface spill from a rental RWST/R.O. processing skid during Q4 2009 (see **Section 3.4.5**). Given that this Tritium release was eliminated, it is expected that the Tritium activities will continue to decrease to pre-spill levels at these sampling intervals; although future releases from the storage/Retention Mechanism(s), replenished by these spills and historic SFP leaks, could create additional perturbations in Tritium levels.

The above conclusion is continually reassessed on a quarterly basis as new data becomes available. In particular, while the LCD flow rate and the MH-5 VCFD Tritium activity have both returned to baseline levels, the previous increases exhibited in the Q3 2010 data have resulted in the initiation of additional investigations⁹⁸.

- Previously identified, more historic transient leaks included: the additional leakage from the Unit 1 SFPs during the 2008 defueling operations, the transient leakage from the distillation tank valves in Q1 2009, and the three transient surficial Tritium releases to Unit 3 Manhole A2 during the Q2 2009, Q3 2010 and Q4 2010 quarters:
 - Based on past work, additional leakage was expected during the raising of water levels in the Unit 1 SFPs for final fuel removal to ISFSI storage. Unit 1 SFPs leakage was terminated with the drainage and sealing of the pools. This previous, transient leakage was initially verified as pronounced increases in Strontium and Cesium in

⁹⁸ While all LCD and MH-5 VCFD water is contained and is release through monitored pathways, the increases observed in MW-31, MW-32 and MH-5 VCFD appear to be potentially correlated, on a temporal basis, with the increased LCD flow rate⁹⁸. While the data trends appear to correlate on a temporal basis, it is noted that simple correlation does not demonstrate causation.

Section 4.0 Conclusions and Planned Future Work

the monitoring locations closest to Unit 1. These near-pool locations have since decreased to pre-defueling levels, but additional Strontium increases have subsequently been observed farther downgradient as this transient input migrates through the system. The transient Strontium behavior at individual U1 monitoring locations is provided in Figure 7A, as we continue to monitor the Unit 1 Strontium Plume.

- The Q1 2009 leakage from the distillation tank valves was independently⁹⁹ identified based on an increase in Tritium levels in monitoring installation MW-42 proximate to the tanks, and subsequent increases in downgradient wells (MW-53-82, U1-CSS, and MW-50-42). These valves were immediately repaired and the leakage was terminated. Based on the observed data trends, it appears that the Tritium input into the groundwater flow regime from the waste distillation tank valving leak has generally dissipated through the system¹⁰⁰. However, additional potential impacts of this release via the Retention Mechanism(s) will be specifically evaluated during subsequent monitoring rounds.
- An elevated Tritium activity was detected in Unit 3 Manhole A2 during routine 80-10 Effluents Program sampling during Q2 2009. This manhole is located proximate to the Unit 3 FSB. Subsequent re-sampling of this manhole showed rapidly decreasing Tritium activity, indicating that this was a transient event. This elevated Tritium was also detected in a proximate groundwater monitoring installation (MW-45), likely due to exfiltration of Tritium from the manhole. This initial peak in both MW-45-42 and MH-A2 initiated a series of investigations into the correlation and underlying cause of both the IL exceedance in the monitoring well as well as the increased Tritium in the manhole. A second elevated Tritium activity was also detected in MH-A2 (as well as MH-A4) during routine 80-10 Effluents Program sampling during the previous, Q3 2010, monitoring period. Similar to the peak observed in Q2 2009, the subsequent re-sampling indicated a rapid decrease in Tritium activity within the storm drain system. However, a prolonged increase in Tritium activity was detected in MH-A2 and A4 during the current, Q4 2010, quarter. The more recent Tritium peaks in Q3 and Q4 2010 provided additional information which helped inform further investigations. Based on these investigations, focused on sampling of the FSB roof drains, and associated data collected, it has been concluded that the elevated Tritium levels detected in MH-A2 and A4 are due to condensation of SFP evaporation on the FSB roof when the vent fan is not operating. This condensate then enters the building roof drain and discharges directly into MH-A2 during rainfall events. A number of groundwater monitoring intervals, including MW-41-40, MW-46 and B-1 have also been shown to correlate with the Tritium input into MH-A2. As such, these monitoring well peaks in Tritium activity do not indicate a new leak from a SSC.

As such, these data support the validity of the current CSM for use as a basis for Long Term Monitoring Program design. It is further noted that, while a portion of the above five documented localized release events traveled directly to the saturated groundwater

⁹⁹ The valve leakage was initially identified during routine visual inspection rounds and immediately terminated. Given that the leak was within the Unit 1 FSB structure, it was documented in a Condition Report under Entergy's Corrective Action Program. This valve leak and repair subsequently came to light within the GPI program during investigations into the cause of the abrupt increase in Tritium levels in MW-42. Additional emphasis has therefore been placed on routine review of these reports as they potentially relate to GPI objectives.

¹⁰⁰ Additional portions of these releases likely remain above the water table in the release area as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

Section 4.0 Conclusions and Planned Future Work

regime and resulted in the observed transient “peaks” in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

- While the current Tritium I.L. levels proved helpful over the previous four quarters (Q1 through Q4 2010) in identifying a localized, transient surface spill from a rental RWST/R.O. skid, data collected during previous quarters have generally demonstrated that the I.L.s originally established are somewhat too sensitive relative to natural seasonal/precipitation-driven transient variations in radionuclide activities, as well as the variability inherent in the laboratory analyses. Relative to Strontium from the Unit 1 SFPs, the previous increases in activity in a number of monitoring points, due to the previous Unit 1 defueling operations, limit our ability to establish Strontium baseline levels for assessment of new I.L.s pursuant to the Monitored Natural Attenuation (MNA) of this plume. It is anticipated that this additional Strontium activity will take a number of quarters to completely flush through the onsite groundwater flow system and attenuate to reasonably stable levels. As such, the originally established I.L.s for both Tritium and Strontium will continue to be used until sufficient data is collected to allow re-evaluation of I.L. levels for the radionuclides of interest.
- From both qualitative and quantitative perspectives, the overall quarterly monitoring data set supports the conclusion that the overall Tritium activity in the Unit 2 plume has decreased substantially since termination of the identified Unit 2 SFP leaks. These overall reductions have become particularly evident on the more recent quarterly report **Figures 6 and 6A** where the shaded plume¹⁰¹ no longer extends to the river, as it did prior to Q2 2009. It is further visually evident from **Figure 6A** that the core of the plume (with quarterly rolling average activities greater than 100,000 pCi/L and 2007 bounding core activities greater than 250,000 pCi/L) has also shown a marked decrease in activity and extent. Based on the data and analyses provided above, our conclusion is that the Tritium plume associated with the historic leaks in the Unit 2 SFP has undergone long-term, overall reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site¹⁰². Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP¹⁰³, this Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation.

¹⁰¹ The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

¹⁰² It is noted that the previously clear attenuation of the Unit 2 Tritium plume has been confounded by a number of localized, transient surface spills. Entergy is currently in the process of reviewing and addressing work practices which may have contributed to the occurrence of these spills.

¹⁰³ Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the more recent behavior observed in the Unit 2 LCD and MH-5 VCFD data, additional investigations/data evaluations are underway. In this regard, it is noted that these analyses cannot definitively and completely rule out the possibility of a remaining small Unit 2 SFP leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s) and surface spill from the process skid discussed above. While it is not possible to quantify the size of the minimum detectable leak with any degree of certainty, we believe that the maximum leak

Section 4.0 Conclusions and Planned Future Work

- The overall Strontium activity within the Unit 1 plume had generally been stable or decreasing in response to West Pool demineralization conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs resulted in an initial, noticeable increase, followed by a subsequent and commensurate decrease, in Strontium levels proximate to the SFPs, with later increases in the downgradient Strontium levels (see **Figure 7** and **7A**). This is as was predicted given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing leakage rate from the SFPs¹⁰⁴. As anticipated, the levels proximate to the pool have decreased to pre-defueling Strontium levels (and in a number of cases to below pre-defueling levels), and levels downgradient of the pool are generally showing continued decreases as this additional Strontium-contaminated water flushes through the groundwater flow system. It is expected that this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also achieve an overall downward trend below pre-defueling levels once this perturbation is finished passing through the system. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation. However, as indicated above, the establishment of updated I.L.s for the Unit 1 Strontium plume must await return to the original Strontium baseline levels in the downgradient monitoring locations, which existed prior to Unit 1 defueling.
- The amount of radionuclides being released through the groundwater pathway, even with the somewhat increased Tritium levels currently observed due to the RWST/R.O. skid transient surface spill, is still small compared to permitted levels of radionuclides discharged to the river through the Discharge Canal.

rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time, as based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of greater than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program, this amount of Tritium release to the river is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

¹⁰⁴ As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.



TABLES

Table 1 Groundwater Sampling Methods, Equipment, Frequency, and Depths

Table 2 Historic Quarterly Low Tide Groundwater Elevations

Table 3 2010 4th Groundwater Analytical Results and Averages

Table 4 2010 4th Quarter Groundwater Analytical Results and I.L.s

Table 5 Historic Groundwater Analytical Results

TABLE 1
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

WellID ¹	Sampling Method	Sampling Equipment Used	Projected 2011 Sampling Frequency ²	SAMPLING INTERVAL ³				SAMPLING DEPTH ⁴	
				Elevation in Feet msl		Feet Below TOC	Elevation in Feet msl	Elevation in Feet msl	
				Top	Bottom			Top	Bottom
MW-30-69	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	67.3	71.3	8.4	4.4	69.3	6.4
MW-30-84	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	77.3	85.4	-1.6	-9.5	83.8	-8.1
MW-31-49	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	44.8	49.3	40.8	26.3	48.8	26.8
MW-31-63	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	55.3	63.8	20.3	11.8	63.3	12.3
MW-31-85	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	69.8	85.4	5.8	-9.6	84.8	-9.2
MW-32-59	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	26.3	61.3	48.8	15.8	58.8	18.3
MW-32-85	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	79.3	92.8	-2.2	-15.7	85.3	85.3
MW-32-131	Waterloo Low Flow	Waterloo Multilevel System	Inactive	125.8	138.3	-48.7	-61.2	130.8	-53.7
MW-32-149	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	125.8	156.8	-70.2	-79.7	149.3	-72.2
MW-32-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	165.8	174.3	-88.7	-97.2	172.8	-95.7
MW-32-190	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	180.3	193.8	-103.2	-116.8	190.3	-113.7
MW-33	Low Flow	Peristaltic Pump	Annually	8.0	30.0	10.6	-11.7	16	2.8
MW-34	Low Flow	Peristaltic Pump	Inactive	5.0	30.0	13.5	-11.4	16.5	2.0
MW-35	Low Flow	Peristaltic Pump	Annually	6.5	30.0	12.1	-11.4	15.0	3.6
MW-36-24 ²	Low Flow	Peristaltic Pump	Quarterly	11.0	24.0	0.8	-12.2	17.0	-5.2
MW-36-41	Low Flow	Peristaltic Pump	Inactive	36.0	41.0	-24.2	-29.2	37.0	-25.2
MW-36-52	Low Flow	Peristaltic Pump	Quarterly	48.0	53.0	-36.2	-41.2	50.0	-38.2
MW-37-52	Low Flow	Peristaltic Pump	Quarterly	12.0	22.0	3.0	-7.0	17.0	-2.0
MW-37-52	Low Flow	Peristaltic Pump	Quarterly	28.0	32.5	-13.0	-17.5	29.0	-14.0
MW-37-40	Low Flow	Peristaltic Pump	Quarterly	38.5	40.5	-23.5	-24.5	39.0	-24.0
MW-37-57	Low Flow	Peristaltic Pump	Quarterly	52.0	57.0	-37.0	-42.0	55.0	-40.0
MW-38	Low Flow	Peristaltic Pump	Inactive	5.0	40.0	9.3	-25.7	25.4	-11.1
MW-39-67	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	65.0	70.5	15.0	9.5	67.0	13.0
MW-39-84	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	76.5	85.0	3.5	-5.0	83.5	-3.5
MW-39-102	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	93.0	103.0	-13.0	-23.0	101.5	-21.5
MW-39-124	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	115.0	126.0	-35.0	-46.0	124.0	-44.0
MW-39-183	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	169.5	186.0	-89.5	-106.5	182.5	-102.5
MW-39-195	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	193.0	198.6	-113.0	-118.4	195.0	-115.0
MW-40-27	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	18.2	35.2	55.0	38.0	26.7	46.5
MW-40-46	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	44.2	53.7	29.0	19.5	46.2	27.0
MW-40-81	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	64.7	84.2	8.5	-11.0	80.7	-7.5
MW-40-100	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	93.2	106.7	-20.0	-33.5	100.2	-27.0
MW-40-127	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	125.2	136.7	-52.0	-63.5	127.2	-54.0
MW-40-162	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	158.7	190.3	-85.5	-116.9	161.7	-88.5
MW-41-40	Low Flow	Peristaltic Pump	Quarterly	22.0	42.0	32.9	12.9	36.0	18.9
MW-41-63	Modified Well Vol. Purge	Water Pump	Quarterly	59.0	64.0	-4.1	-9.1	61.0	-6.1
MW-42-49	Modified Well Vol. Purge	Submersible Pump	Quarterly	31.0	51.0	38.7	18.7	41.0	28.7
MW-42-78	Modified Well Vol. Purge	Water Pump	Quarterly	69.0	79.0	0.7	-9.3	74.0	-4.3
MW-43-28	Low Flow	Submersible Pump	Quarterly	8.0	62.0	40.8	20.7	23.0	25.8
MW-43-62	Low Flow	Submersible Pump	Quarterly	42.0	62.0	6.8	-13.2	54.0	-5.2
MW-44-66	Modified Well Vol. Purge	Submersible Pump	Quarterly	52.0	67.0	41.5	26.5	63.0	30.5
MW-44-102	Modified Well Vol. Purge	Water Pump	Quarterly	79.0	104.0	14.5	-10.5	86.0	13.5
MW-45-42	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	27.5	42.5	26.2	11.2	37.0	16.6
MW-45-61	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	51.5	61.5	2.2	-7.8	58.0	-4.4
MW-46	Modified Well Vol. Purge	Submersible Pump	Quarterly	6.0	30.0	12.1	-11.9	10.5	7.6
MW-45-56	Low Flow	Submersible Pump	Inactive	36.0	56.0	34.3	14.3	52.0	18.3
MW-47-80	Modified Well Vol. Purge	Water Pump	Inactive	76.0	80.0	0.3	-9.7	72.0	-1.7

J:\17-000-18-000\17869\17869-02\MG-QI-2010\FINAL\Tables\ Table 1 - Groundwater: Sampling Methods, Equipment, Frequency and Depths.xlsx; Methods, Frequency, Depths

TABLE 1
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

WellID ¹	Sampling Method	Sampling Equipment Used	Projected 2011 Sampling Frequency ²	SAMPLING INTERVAL ³				SAMPLING DEPTH ⁴	
				Elevation in Feet msl		Feet Below TOC	Elevation in Feet msl	Feet Below TOC	Elevation in Feet msl
				Top	Bottom				
MW-48-23	Low Flow	Peristaltic Pump	Inactive	8.0	23.0	7.4	-7.6	15.8	-4.4
MW-48-37	Low Flow	Peristaltic Pump	Inactive	33.0	38.0	-17.6	22.6	35.8	-20.4
MW-49-36	Low Flow	Peristaltic Pump	Quarterly	15.0	25.0	-0.3	-10.4	20.0	-5.3
MW-49-42	Low Flow	Peristaltic Pump	Quarterly	32.0	42.0	-17.4	37.0	37.0	-22.3
MW-49-65	Low Flow	Peristaltic Pump	Quarterly	60.0	65.0	-45.4	60.4	61.0	-46.4
MW-50-42	Low Flow	Peristaltic Pump	Quarterly	22.0	42.0	-7.1	-27.1	27.0	-12.1
MW-50-66	Low Flow	Peristaltic Pump	Quarterly	62.0	67.0	-47.1	-32.1	66.0	-45.1
MW-51-40	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	29.7	44.2	38.0	23.5	36.7	28.0
MW-51-79	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	63.2	81.2	4.5	-13.5	78.7	-11.0
MW-51-104	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	101.2	111.2	-33.5	-43.5	103.7	-36.0
MW-51-135	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	130.2	143.7	-62.5	-76.0	135.2	-67.5
MW-51-163	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	154.7	166.2	-87.0	-98.5	162.7	-95.0
MW-51-189	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	184.2	197.8	-116.5	-129.9	189.2	-121.5
MW-52-11	Modified Well Vol. Purge	Peristaltic Pump	Annually	2.0	12.0	14.8	4.8	16.0	6.8
MW-52-18	Waterloo Low Flow	Waterloo Multilevel System	Annually	16.0	30.0	4.9	-15.1	17.5	-2.6
MW-52-48	Waterloo Low Flow	Waterloo Multilevel System	Annually	48.0	56.0	-33.1	-41.1	48.0	-33.1
MW-52-64	Waterloo Low Flow	Waterloo Multilevel System	Annually	59.0	71.5	-44.1	-56.6	64.0	-49.1
MW-52-122	Waterloo Low Flow	Waterloo Multilevel System	Annually	110.5	123.5	-95.6	-108.6	122.0	-107.1
MW-52-162	Waterloo Low Flow	Waterloo Multilevel System	Annually	154.5	164.0	-139.6	-149.1	161.5	-146.6
MW-52-181	Waterloo Low Flow	Waterloo Multilevel System	Annually	171.0	198.1	-156.1	-183.0	181.0	-166.1
MW-53-82	Low Flow	Submersible Pump	Quarterly	62.0	82.0	8.3	-11.7	75.0	-4.7
MW-53-120	Modified Well Vol. Purge	Water Pump	Quarterly	100.0	120.0	-29.7	-49.7	105.0	-34.7
MW-54-37	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	29.0	42.0	-15.9	-28.9	36.5	-23.4
MW-54-58	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	51.5	64.0	-38.4	-50.9	57.5	-44.4
MW-54-123	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	116.0	126.0	-102.9	-112.9	125.0	-109.9
MW-54-144	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	135.0	155.5	-121.9	-142.4	144.0	-130.9
MW-54-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	170.5	182.0	-157.4	-168.9	175.5	-159.4
MW-54-190	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	185.0	203.6	-171.9	-190.3	190.0	-176.9
MW-55-24	Low Flow	Peristaltic Pump	Quarterly	14.0	24.0	4.3	-5.8	16.0	2.3
MW-55-35	Low Flow	Peristaltic Pump	Quarterly	30.0	35.0	-11.8	-16.8	32.0	-13.8
MW-55-54	Low Flow	Peristaltic Pump	Quarterly	41.0	54.0	-25.8	-35.8	47.0	-28.8
MW-56-53	Modified Well Vol. Purge	Submersible Pump	Semi-Annually	49.2	54.2	21.0	16.0	52.0	18.3
MW-56-83	Modified Well Vol. Purge	Water Pump	Semi-Annually	69.9	84.9	6.4	-14.6	74.0	-3.7
MW-57-11	Modified Well Vol. Purge	Peristaltic Pump	Annually	6.0	11.0	9.0	4.0	16.0	5.0
MW-57-20	Modified Well Vol. Purge	Peristaltic Pump	Annually	15.5	20.5	-0.5	-5.5	19.0	-4.0
MW-57-45	Modified Well Vol. Purge	Peristaltic Pump	Annually	30.5	45.5	-15.5	-30.5	46.0	-25.0
MW-58-26	Modified Well Vol. Purge	Peristaltic Pump	Semi-Annually	16.0	26.0	-1.4	-11.4	26.0	-5.4
MW-58-65	Low Flow	Peristaltic Pump	Semi-Annually	50.0	65.0	-35.4	-50.4	51.0	-39.4
MW-59-32	Low Flow	Peristaltic Pump	Inactive	21.0	31.0	-6.5	-16.5	27.0	-12.5
MW-59-45	Low Flow	Peristaltic Pump	Inactive	35.0	45.0	-20.5	-30.5	42.0	-27.5
MW-59-68	Low Flow	Peristaltic Pump	Inactive	53.0	68.0	-38.5	-53.5	58.0	-43.5
MW-60-35	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	24.9	39.4	-12.4	-26.9	34.9	-22.4
MW-60-53	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	45.4	59.4	-32.9	-46.9	53.4	-40.9
MW-60-72	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	66.4	78.9	-53.9	-66.4	72.4	-59.9
MW-60-135	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	124.9	141.4	-112.4	-128.9	134.9	-122.4
MW-60-154	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	147.4	164.9	-134.9	-152.4	151.4	-141.9
MW-60-176	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	170.9	200.4	-158.4	-187.8	175.9	-163.4

J:\17-000-18-000\17869\17869-02\MG-Q1-2010\FINAL\Tables\ Table 1 - Groundwater: Sampling Methods, Equipment, Frequency and Depths.xlsx; Methods, Frequency, Depths

TABLE 1
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

WellID ¹	Sampling Method	Sampling Equipment Used	Projected 2011 Sampling Frequency ²	SAMPLING INTERVAL ³				SAMPLING DEPTH ⁴	
				Elevation in Feet msl		Feet Below TOC	Elevation in Feet msl	Elevation in Feet msl	
				Top	Bottom			Top	Bottom
MW-62-18	Low Flow	Peristaltic Pump	Quarterly	14.7	10.0	0.0	13.5	1.2	
MW-62-37	Low Flow	Peristaltic Pump	Quarterly	33.3	18.6	-23.6	34.5	-19.8	
MW-62-53	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	49.6	54.1	-41.3	53.1	-40.3	
MW-62-71	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	61.1	82.6	-69.8	71.1	-58.3	
MW-62-92	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	88.6	99.1	-83.3	91.6	-78.8	
MW-62-138	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	126.1	143.6	-113.8	138.1	-125.3	
MW-62-182	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	177.6	198.7	-164.8	182.1	-169.3	
MW-63-18	Low Flow	Peristaltic Pump	Quarterly	8.0	35.0	-3.8	14.9	6.7	
MW-63-34	Low Flow	Peristaltic Pump	Quarterly	30.0	15.8	-20.8	31.5	-17.3	
MW-63-50	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	41.5	58.0	-45.7	49.5	-37.2	
MW-63-93	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	81.5	100.5	-69.2	95.0	-80.7	
MW-63-112	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	105.5	112.0	-94.2	111.5	-99.2	
MW-63-121	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	118.0	127.5	-105.7	121.0	-108.7	
MW-63-163	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	150.5	165.0	-138.2	162.5	-150.2	
MW-63-174	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	168.0	191.1	-155.7	174.0	-161.7	
MW-66-21	Modified Well Vcl. Purge	Peristaltic Pump	Quarterly	7.0	27.0	6.0	14.1	0	
MW-66-36	Modified Well Vcl. Purge	Peristaltic Pump	Quarterly	31.0	36.0	-17.0	33.6	-19.5	
MW-67-39	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	28.8	54.3	-15.8	38.3	-25.8	
MW-67-105	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	90.3	110.8	-77.3	104.8	-92.3	
MW-67-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	164.8	188.3	-151.8	172.3	-159.8	
MW-67-219	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	205.8	229.8	-196.3	218.8	-206.3	
MW-67-276	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	293.8	281.3	-237.8	275.3	-262.8	
MW-67-323	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	317.8	328.3	-304.8	322.3	-309.8	
MW-67-340	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	335.3	347.9	-322.3	336.8	-327.3	
MW-107	Low Flow	Submersible Pump	Annually	105.1	126.1	34.9	32.7	110.1	
MW-111	Low Flow	Peristaltic Pump	Semi-Annually	11.6	17.4	7.0	16.5	2.4	
U3-4D	Modified Well Vcl. Purge	Peristaltic Pump	Quarterly	25.0	27.6	-10.2	25.6	-10.8	
U3-71	Low Flow	Peristaltic Pump	Quarterly	0.2	1.2	3.1	5.7	2.8	
U3-12	Low Flow	Peristaltic Pump	Quarterly	0.6	1.6	2.7	5.7	2.6	
U1-CSS	Low Flow	Peristaltic Pump	Semi-Annually	NA	10.2	NA	14.0	6.1	
LAF-002	Low Flow	NA	Quarterly	NA	NA	NA	NA	NA	
U1-NCID	Grab	NA	Quarterly	NA	NA	NA	NA	NA	
U1-SFDS	Grab	NA	Quarterly	NA	NA	NA	NA	NA	
MH-5 VCP1 ⁵	Grab	NA	Quarterly	NA	NA	NA	NA	NA	
B-1 ⁶	Grab	NA	Quarterly	NA	NA	NA	NA	NA	
B-6 ⁶	Grab	NA	Quarterly	NA	NA	NA	NA	NA	

Notes:

- For nested multi-level monitoring wells, suffix of well ID indicates depth (rounded to nearest foot) from reference point on casing to bottom of well screen. For Waterloo multi-level systems, suffix indicates depth (rounded to nearest foot) from reference point on casing to top of sampling port. Well IDs without a suffix are open bedrock wellbores.
- Projected sampling frequencies presented for 2011 are subject to change.
- For nested multi-level monitoring wells, interval includes well screen and sand pack. For Waterloo multi-level systems, interval includes open wellbore between bottom of 1st packer above and top of 1st packer below sampling port. For open bedrock wellbores, interval extends from bottom of casing to bottom of hole.
- Sampling depths within sampling intervals (i.e. location of pump intake) have been located adjacent to a transmissive zone where possible.
- DM pattern denotes sampling interval is positioned within overburden. Open box indicates sampling interval is in bedrock.
- These locations are storm drains.

TABLE 2
 HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS
 INDIAN POINT ENERGY CENTER
 BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (feet msl)															
	Quarter 2 nd , 2007	Quarter 3 rd , 2007	Quarter 4 th , 2007	Quarter 1 st , 2008	Quarter 2 nd , 2008	Quarter 3 rd , 2008	Quarter 4 th , 2008	Quarter 1 st , 2009	Quarter 2 nd , 2009	Quarter 3 rd , 2009	Quarter 4 th , 2009	Quarter 1 st , 2010	Quarter 2 nd , 2010	Quarter 3 rd , 2010	Quarter 4 th , 2010	
IR-1	NA	-0.86	-1.57	-2.15	-1.13	-1.05	-1.69	-3.28	-1.52	-0.27	-3.59	-0.36	-0.56	-0.71	NA	
E-2	50.23	48.62	51.87	53.73	52.11	52.90	50.75	NA	NA	NA	51.69	52.46	53.33	50.49	NA	
MW-30-69	11.83	11.55	12.00	NA	12.28	11.77	11.71	12.33	11.81	13.76	NA	NA	NA	NA	11.56	
MW-30-84	NA	12.83	12.83	NA	13.06	12.83	13.13	12.68	12.82	12.48	NA	13.26	12.76	11.31	12.32	
MW-31-19	44.69	NA	45.40	47.50	46.14	45.39	44.13	46.44	45.40	-	-	-	-	-	-	
MW-31-63	NA	41.56	NA	42.71	43.96	42.17	44.12	44.12	43.20	-	-	-	-	-	-	
MW-31-85	39.59	NA	40.81	43.19	41.89	40.58	39.64	42.10	40.64	-	-	-	-	-	-	
MW-32-48	NA	42.12	46.73	48.81	47.77	46.98	45.79	48.08	47.31	-	-	-	-	-	-	
MW-32-59	NA	41.44	45.99	47.99	46.75	46.72	44.48	46.83	45.62	-	-	-	-	-	-	
MW-32-85 (MW-32-92) ¹⁷	10.27	12.35	12.78	13.30	13.17	12.30	12.16	12.60	11.61	-	-	-	-	-	-	
MW-32-131 (MW-32-140) ¹⁷	13.11	11.96	13.21	25.01	15.67	11.34	11.53	11.86	11.06	-	-	-	-	-	-	
MW-32-149 (MW-32-165) ¹⁷	8.18	9.87	10.06	10.20	10.04	9.71	9.77	10.00	9.18	-	-	-	-	-	-	
MW-32-173	NA	9.73	9.86	9.92	9.70	9.45	9.45	9.68	8.81	-	-	-	-	-	-	
MW-32-190 (MW-32-196) ¹⁷	6.74	8.05	7.88	7.88	7.52	7.16	7.05	7.24	6.26	-	-	-	-	-	-	
MW-33	10.68	9.80	10.38	11.49	11.66	10.55	10.60	11.23	10.52	-	-	-	-	-	-	
MW-34	9.87	9.82	10.44	11.63	12.03	10.54	10.54	11.25	6.71	-	-	-	-	-	-	
MW-35	10.03	9.67	10.37	11.65	12.06	10.68	11.36	NA	NA	-	-	-	-	-	-	
MW-36-24	8.89	7.31	7.67	6.85	6.86	7.58	9.05	NA	7.25	-	-	-	-	-	-	
MW-36-41	8.22	NA	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-	-	
MW-36-52	7.43	6.43	6.45	6.29	6.29	6.99	7.45	8.12	6.62	-	-	-	-	-	-	
MW-37-22	5.51	5.15	4.83	4.66	4.18	5.36	5.55	5.24	5.52	-	-	-	-	-	-	
MW-37-52	5.51	5.07	4.82	4.63	4.05	5.64	5.64	5.52	5.32	-	-	-	-	-	-	
MW-37-40	5.40	6.83	6.19	6.19	5.95	6.18	6.04	5.46	6.19	-	-	-	-	-	-	
MW-37-57	7.07	6.23	6.39	6.28	6.07	6.64	7.20	6.50	6.56	-	-	-	-	-	-	
MW-38	3.01	2.19	1.46	2.22	1.53	2.12	2.22	2.24	2.24	-	-	-	-	-	-	
MW-39-67	NA	NA	26.84	32.30	31.69	25.96	25.21	28.74	NA	-	-	-	-	-	-	
MW-39-81	NA	NA	26.64	31.94	31.48	25.78	25.12	28.62	NA	-	-	-	-	-	-	
MW-39-100	NA	NA	26.38	30.99	31.34	25.52	24.79	28.32	NA	-	-	-	-	-	-	
MW-39-102	NA	NA	26.31	31.56	NA	NA	NA	NA	NA	-	-	-	-	-	-	
MW-39-124	NA	NA	26.05	28.37	30.67	25.07	24.43	27.74	NA	-	-	-	-	-	-	
MW-39-183	NA	NA	25.28	29.74	29.83	22.33	23.79	26.78	NA	-	-	-	-	-	-	
MW-39-195	NA	NA	24.36	28.80	28.89	23.35	22.70	25.63	NA	-	-	-	-	-	-	
MW-40-27	NA	NA	55.46	60.39	59.09	54.70	54.22	59.53	57.25	-	-	-	-	-	-	
MW-40-46	NA	47.27	33.19	59.35	59.09	52.35	52.35	59.13	56.56	-	-	-	-	-	-	
MW-40-81	NA	41.65	47.45	56.06	55.78	47.28	46.83	55.67	53.13	-	-	-	-	-	-	
MW-40-100	NA	39.47	45.18	54.10	53.75	44.83	44.32	53.29	51.24	-	-	-	-	-	-	
MW-40-127	NA	38.89	44.60	53.61	53.39	44.33	43.87	53.29	50.59	-	-	-	-	-	-	
MW-40-162	NA	36.67	41.69	50.69	50.26	41.32	40.66	46.76	46.80	-	-	-	-	-	-	
MW-41-40	29.87	NA	32.48	36.57	33.81	31.28	30.71	33.62	48.80	-	-	-	-	-	44.88	
MW-41-63	25.94	NA	27.77	33.31	32.76	27.53	26.96	30.38	32.05	-	-	-	-	-	-	
MW-42-49	NA	NA	34.55	34.96	34.81	34.52	34.43	34.78	34.47	-	-	-	-	-	-	
MW-42-78	NA	NA	35.71	36.63	36.28	35.58	35.07	36.03	35.75	-	-	-	-	-	-	
MW-43-28	32.75	31.08	31.98	33.47	33.95	32.51	32.15	33.43	32.66	-	-	-	-	-	-	
MW-43-62	30.83	NA	NA	NA	32.16	30.48	31.76	34.13	30.88	NA	30.28	32.00	34.23	37.14	31.95	
MW-44-67	33.36	NA	NA	NA	35.47	34.00	34.00	34.96	34.50	-	-	-	-	-	-	
MW-44-102	23.10	NA	24.84	NA	30.88	25.86	25.16	28.09	27.41	-	-	-	-	-	-	
MW-45-42	NA	24.82	28.47	34.19	37.16	28.63	25.45	29.03	29.03	-	-	-	-	-	-	
MW-45-61	NA	24.33	27.57	32.91	32.46	27.16	26.68	29.99	23.25	-	-	-	-	-	-	
MW-46	12.80	11.95	12.57	15.05	14.97	12.62	12.81	14.29	12.47	12.83	NA	16.49	12.45	13.22	-	
MW-47-56	NA	21.83	20.77	23.05	31.53	22.84	22.37	26.51	23.43	-	-	-	-	-	-	
MW-47-80	22.29	21.41	21.82	26.53	28.35	21.52	21.08	26.37	24.18	-	-	-	-	-	-	
MW-48-23	-0.08	-0.27	-0.39	-1.14	-1.23	-0.18	-0.18	-0.91	-0.19	-	-	-	-	-	-	
MW-48-37	0.64	0.76	-0.06	-0.18	0.32	0.06	-0.15	0.04	0.04	-	-	-	-	-	-	
MW-49-26	1.04	0.90	0.40	-0.37	0.51	0.37	0.49	-0.25	0.54	-	-	-	-	-	-	
MW-49-42	0.31	0.90	1.02	0.41	0.92	1.02	0.68	1.02	0.51	-	-	-	-	-	-	
MW-49-65	0.82	1.01	0.34	0.07	0.70	0.68	0.47	-0.08	0.57	-	-	-	-	-	-	
MW-50-42	7.24	NA	NA	NA	5.24	6.40	7.06	5.66	6.09	-	-	-	-	-	-	

TABLE 2
HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (feet msd)															
	Quarter 2 nd , 2007	Quarter 3 rd , 2007	Quarter 4 th , 2007	Quarter 1 st , 2008	Quarter 2 nd , 2008	Quarter 3 rd , 2008	Quarter 4 th , 2008	Quarter 1 st , 2009	Quarter 2 nd , 2009	Quarter 3 rd , 2009	Quarter 4 th , 2009	Quarter 1 st , 2010	Quarter 2 nd , 2010	Quarter 3 rd , 2010	Quarter 4 th , 2010	
NW-50-66	3.71	NA	NA	1.97	2.24	2.83	2.34	1.95	2.82	46.45	42.45	43.37	41.72	-	-	
NW-51-40	NA	48.69	50.07	51.95	52.35	49.44	49.24	49.32	49.44	49.44	49.44	49.44	49.44	41.89	41.24	
NW-51-79	NA	39.92	41.07	42.91	44.17	40.71	40.36	42.75	42.75	42.75	42.75	42.75	42.75	-	-	
NW-51-102	NA	35.98	38.07	38.46	39.04	36.56	36.03	37.78	37.78	37.78	37.78	37.78	37.78	-	-	
NW-51-104	NA	NA	37.93	38.41	39.02	36.49	36.03	37.99	37.99	37.99	37.99	37.99	37.99	-	-	
NW-51-135	NA	37.42	39.47	39.99	40.71	38.10	37.68	39.75	39.75	39.75	39.75	39.75	39.75	-	-	
NW-51-163	NA	33.79	34.83	36.15	36.77	34.30	33.90	35.74	35.74	35.74	35.74	35.74	35.74	-	-	
NW-51-189	NA	29.33	30.16	31.54	31.79	29.65	29.36	30.81	30.81	30.81	30.81	30.81	30.81	29.07	29.60	
NW-52-11	6.04	5.61	8.12	8.47	8.85	8.65	8.44	8.19	8.20	8.20	8.20	8.20	8.20	-	-	
NW-52-18	6.64	NA	8.63	6.04	6.07	5.89	6.02	5.78	5.87	5.87	5.87	5.87	5.87	-	-	
NW-52-48	7.08	NA	6.55	7.08	5.95	6.20	6.14	6.05	6.05	6.05	6.05	6.05	6.05	-	-	
NW-52-64	5.95	NA	5.90	5.25	5.20	5.21	5.16	5.20	4.89	4.89	4.89	4.89	4.89	-	-	
NW-52-118	5.34	NA	4.41	4.44	4.32	4.36	4.44	4.23	4.23	4.23	4.23	4.23	4.23	-	-	
NW-52-122	5.25	NA	4.36	4.32	4.18	4.21	4.55	4.11	4.20	4.20	4.20	4.20	4.20	-	-	
NW-52-163	0.67	NA	-0.80	-1.31	-0.80	-0.98	-1.30	-2.07	-1.18	-1.18	-1.18	-1.18	-1.18	-	-	
NW-52-181	0.41	NA	1.08	1.56	1.00	1.30	1.64	2.38	1.51	1.51	1.51	1.51	1.51	-	-	
NW-53-82	NA	9.59	10.03	11.89	12.60	10.35	NA	11.11	NA	11.11	9.87	11.15	11.67	9.98	11.27	
NW-53-120	9.91	9.18	9.39	10.87	11.49	9.16	NA	10.55	9.78	10.43	9.43	10.55	11.02	9.60	10.53	
NW-53-35	NA	NA	6.40	6.27	6.36	6.16	6.41	5.75	5.87	5.87	5.87	5.87	5.87	-	-	
NW-53-37	7.52	NA	6.58	6.45	6.53	6.30	6.58	5.90	6.04	6.04	6.04	6.04	6.04	-	-	
NW-54-58	6.85	NA	5.82	5.60	5.55	5.53	5.76	5.49	5.17	5.17	5.17	5.17	5.17	-	-	
NW-54-123	5.69	NA	4.16	3.65	3.52	4.01	4.06	2.99	3.56	3.56	3.56	3.56	3.56	-	-	
NW-54-144	8.83	NA	7.13	6.60	6.48	6.92	6.97	6.53	6.53	6.53	6.53	6.53	6.53	-	-	
NW-54-173	5.17	NA	3.52	2.99	2.85	3.27	3.29	2.72	2.72	2.72	2.72	2.72	2.72	-	-	
NW-54-190	5.08	NA	3.46	2.91	2.76	3.16	3.13	2.00	2.49	2.49	2.49	2.49	2.49	-	-	
NW-55-24	8.56	7.82	7.97	8.17	8.16	8.18	9.02	8.35	8.06	8.39	7.80	8.58	8.56	8.02	8.27	
NW-55-35	8.10	7.29	7.52	7.60	7.59	7.69	8.30	7.63	7.63	7.63	7.63	7.63	7.63	-	-	
NW-55-54	8.47	7.65	8.08	8.32	8.32	8.22	8.82	7.89	7.89	8.14	7.66	8.39	8.34	7.97	8.19	
NW-56-53	21.04	20.10	NA	29.93	NA	NA	21.90	27.33	NA	22.06	-	-	-	-	-	
NW-56-83	21.10	20.16	22.18	26.41	29.16	NA	21.51	25.13	22.60	22.60	-	-	-	-	-	
NW-57-11	9.57	8.83	9.36	10.99	12.07	10.03	10.27	11.11	10.09	10.09	-	-	-	-	-	
NW-57-20	9.38	NA	NA	NA	NA	10.63	9.92	10.63	9.84	9.84	-	-	-	-	-	
NW-57-45	8.03	NA	NA	NA	10.59	NA	NA	10.71	NA	NA	-	-	-	-	-	
NW-58-26	9.08	6.49	6.58	8.32	NA	7.29	7.19	7.56	7.40	7.40	-	-	-	-	-	
NW-58-65	6.03	6.83	6.32	NA	7.36	7.13	6.46	6.68	6.70	6.70	-	-	-	-	-	
NW-59-32	1.05	NA	0.67	0.42	0.77	0.81	0.47	0.31	1.37	1.37	-	-	-	-	-	
NW-59-45	1.06	1.27	1.97	NA	9.25	NA	2.52	0.44	NA	NA	-	-	-	-	-	
NW-59-68	2.91	2.51	1.32	1.58	-0.11	NA	-1.79	-5.66	7.95	7.95	-	-	-	-	-	
NW-60-55	1.28	1.28	1.32	1.58	1.63	0.82	2.04	1.99	3.07	3.07	-	-	-	-	-	
NW-60-53	-0.63	-1.24	-1.67	-2.04	-1.37	-1.76	-2.03	-2.70	NA	NA	-	-	-	-	-	
NW-60-55	NA	-0.28	-0.73	-1.10	-0.47	-0.90	-1.21	-1.91	NA	NA	-	-	-	-	-	
NW-60-72	0.74	-0.09	-0.45	-0.68	-0.14	-0.64	NA	-1.43	0.28	0.28	-	-	-	-	-	
NW-60-135	0.94	0.11	-0.44	-0.90	-0.27	-0.71	-1.02	-1.72	0.11	0.11	-	-	-	-	-	
NW-60-151	0.03	-0.96	-1.61	-2.07	-1.49	-1.91	-2.25	-2.99	NA	NA	-	-	-	-	-	
NW-60-176	-0.48	-1.38	-2.03	-2.47	-1.82	-2.16	-2.59	-3.41	NA	NA	-	-	-	-	-	
NW-62-18	0.25	0.25	-0.37	-0.79	0.13	0.06	-0.12	-0.82	NA	NA	-	-	-	-	-	
NW-62-37	0.59	0.61	-0.03	-0.46	0.49	0.59	-0.15	-1.13	0.11	0.11	-	-	-	-	-	
NW-62-52	NA	0.48	-0.30	-1.13	-0.19	-0.64	-0.93	-1.64	-0.42	-0.42	-	-	-	-	-	
NW-62-53	0.95	0.54	-0.25	-1.01	-0.10	-0.16	-0.84	-2.03	-0.44	-0.44	-	-	-	-	-	
NW-62-71	0.89	0.72	-0.56	-1.26	-0.55	-0.56	-1.24	-2.15	-0.70	-0.70	-	-	-	-	-	
NW-62-92	1.07	0.58	-0.09	-0.76	-0.11	-0.10	-0.85	-1.68	-1.03	-1.03	-	-	-	-	-	
NW-62-138	1.40	0.77	0.09	-0.49	0.13	0.26	-0.37	-1.33	-0.40	-0.40	-	-	-	-	-	
NW-62-181	1.33	0.38	0.33	0.69	-0.32	-0.36	-0.92	NA	-0.88	-0.88	-	-	-	-	-	
NW-62-182	NA	-0.33	-1.83	-0.78	-1.29	-1.25	-1.85	-2.66	-1.82	-1.82	-	-	-	-	-	
NW-63-18	0.11	0.09	-0.10	-0.37	0.09	0.32	-0.68	-0.61	0.02	0.02	-	-	-	-	-	
NW-63-34	0.51	0.19	-0.09	-0.40	0.15	0.35	-0.13	-0.74	0.18	0.18	-	-	-	-	-	
NW-63-50	0.85	0.29	-0.38	-1.03	-0.55	-0.55	-1.24	-2.08	-0.45	-0.45	-	-	-	-	-	
NW-63-51	1.15	0.48	-0.19	-0.87	-0.25	-0.16	-0.89	NA	-0.01	-0.01	-	-	-	-	-	

NW-000-15-0001-78691-7869-02-MG-04-2010-03-NAL-Table-2
Table 2 - Historic Quarterly Low Tide Groundwater Elevations (ft. msd)

TABLE 2
HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (feet ms)														
	Quarter 2 nd , 2007	Quarter 3 rd , 2007	Quarter 4 th , 2007	Quarter 1 st , 2008	Quarter 2 nd , 2008	Quarter 3 rd , 2008	Quarter 4 th , 2008	Quarter 1 st , 2009	Quarter 2 nd , 2009	Quarter 3 rd , 2009	Quarter 4 th , 2009	Quarter 1 st , 2010	Quarter 2 nd , 2010	Quarter 3 rd , 2010	Quarter 4 th , 2010
MW-65-93	NA	0.55	-0.20	-0.87	-0.30	-0.24	-0.98	-1.68	-0.13	-	-	-	-	-	-
MW-65-112	0.03	-0.82	-1.36	-2.05	-1.69	-1.60	-2.26	-3.14	-1.45	-	-	-	-	-	-
MW-65-121	1.41	0.60	-0.18	-0.78	-0.24	-0.05	-0.86	-1.49	0.11	-	-	-	-	-	-
MW-65-163	0.70	-0.09	-0.83	-1.48	-0.86	-0.96	-1.54	-2.46	-0.98	-	-	-	-	-	-
MW-65-174	0.88	0.05	-0.65	-1.29	-0.62	-0.61	-1.19	-1.9*	-0.59	-	-	-	-	-	-
MW-65-18	NA	NA	NA	NA	38.60	43.22	NA	48.19	36.98	40.08	38.06	39.94	42.26	49.37	NA
MW-65-80	NA	NA	NA	NA	34.97	32.72	33.71	33.30	33.30	33.79	32.81	33.69	33.98	49.35	NA
MW-66-21	0.26	0.17	-0.22	-0.74	0.05	0.17	0.29	-0.33	0.50	0.52	0.10	-0.01	1.82	1.05	1.02
MW-66-36	0.81	0.48	-0.04	-0.51	0.35	0.15	0.10	-0.86	0.51	-	-0.25	-0.43	1.75	1.49	0.36
MW-67-39	NA	1.02	0.34	-0.33	0.36	0.41	-0.02	-0.07	0.81	-	-1.25	-0.76	-0.13	-0.09	-1.70
MW-67-105	NA	1.39	0.61	-0.64	0.57	0.65	0.16	-0.67	-0.43	-	-	-	-	-	-
MW-67-173	NA	0.75	-0.14	-0.83	-0.28	-0.26	-0.82	-1.62	-1.55	-	-	-	-	-	-
MW-67-219	NA	0.74	-0.19	-0.91	-0.32	-0.32	-0.86	-1.87	-1.59	-	-	-	-	-	-
MW-67-276	NA	1.61	0.60	-0.13	0.44	0.41	-0.14	-1.03	-0.91	-	-	-	-	-	-
MW-67-333	NA	0.18	-0.96	-1.55	-1.13	-1.35	-1.93	-2.86	-2.73	-	-	-	-	-	-
MW-67-346	NA	0.63	0.52	1.31	-0.87	-0.96	-1.56	-2.42	-2.40	-0.76	-	-	-	-	-
MW-107	116.85	113.87	117.48	121.79	118.94	115.09	115.76	120.28	117.52	-	-	-	-	-	-
MW-108	9.28	8.61	8.77	9.98	10.07	NA	9.02	9.65	9.26	-	-	-	-	-	-
MW-109	9.52	6.80	7.22	9.50	10.12	7.82	7.88	7.82	4.95	-	-	-	-	-	-
MW-111	9.56	9.66	9.74	10.54	11.24	9.74	10.48	10.87	9.4*	-	-	-	-	-	-
MW-11	NA	1.31	1.16	0.76	0.81	NA	NA	NA	1.08	-	-0.77	1.02	5.06	NA	NA
MW-1	NA	NA	30.15	NA	30.04	29.52	NA	29.10	NA	-	-	-	-	-	-
U1-C58S	NA	8.98	NA	NA	19.11	15.39	NA	15.39	13.89	-	-	-	-	-	-
U3-1	4.20	NA	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-	-
U3-2	5.34	NA	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-	-
U3-3	7.53	6.52	6.63	8.67	9.25	8.25	8.94	9.13	7.29	-	-	-	-	-	-
U3-4D	NA	3.91	3.80	3.22	2.71	3.49	2.69	3.41	3.75	-	-	-	-	-	-
U3-4S	3.91	4.13	3.80	3.74	3.97	4.31	3.81	4.01	4.23	-	-	-	-	-	-
U3-C1	NA	1.64	3.58	3.36	0.99	2.36	0.81	0.64	1.92	2.43	0.12	0.20	2.58	NA	0.26
U3-T1	4.51	4.12	3.67	3.99	3.86	4.33	3.69	3.83	4.12	-	-	-	-	-	-
U3-T2	4.33	4.02	3.79	4.20	3.94	4.28	3.76	4.05	4.20	-	-	-	-	-	-

Notes:

NA = Data Not Available

- Quarter 2, 2007 groundwater elevations were measured on 6/1/07 at 6:20 am.
- Quarter 3, 2007 groundwater elevations were measured on 9/25/07 at 4:52 am.
- Quarter 4, 2007 groundwater elevations were measured on 12/9/07 at 4:15 am.
- Quarter 1, 2008 groundwater elevations were measured on 1/3/08 at 1:14 a.m.
- Quarter 2, 2008 groundwater elevations were measured on 4/4/08 at 5:14 pm.
- Quarter 3, 2008 groundwater elevations were measured on 7/10/08 at 11:35 am.
- Quarter 4, 2008 groundwater elevations were measured on 11/11/08 at 5:54 am.
- Quarter 1, 2009 groundwater elevations were measured on 1/9/09 at 2:42 am.
- Quarter 2, 2009 groundwater elevations were measured on 5/22/09 at 2:41 pm.
- The rationale for this reduced transducer redeployment is included in the June 14, 2010 memorandum which was included as Appendix J in the Quarter 1, 2009 Report, a reduced number of transducers will be maintained in long term operation.
- Quarter 3, 2009 groundwater elevations were measured on 8/9/09 at 8:18 am.
- Quarter 4, 2009 groundwater elevations were measured on 11/28/09 at 3:45 pm.
- Quarter 1, 2010 groundwater elevations were measured on 1/30/10 at 6:00 am.
- Quarter 2, 2010 groundwater elevations were measured on 4/09/10 at 12:06 pm.
- Quarter 3, 2010 groundwater elevations were measured on 7/31/10 at 12:30 am.
- Quarter 4, 2010 groundwater elevations were measured on 10/16/10 at 1:36 am.
- MW-32 groundwater elevations from 2nd quarter, 2007 were based on an initial Waterloo Multi-Level configuration, which was subsequently reconfigured, initial depth intervals approximately corresponding to current configuration are listed in parentheses. The current configuration intervals MW-32-48 and MW-32-173 have no representative equivalent within the old configuration.

TABLE 5
 HISTORIC GROUNDWATER ANALYTICAL RESULTS
 INDIAN POINT ENERGY CENTER
 BUCHANAN, KY

Well ID ¹	ANALYSIS RESULTS										Well ID ¹							
	TRITIUM (PCU/L)					C-137 (PCU/L)						C-60 (PCU/L)						
	SAMPLE ZONE CENTER, elevation in msl ²	SAMPLE ZONE depth in below top of casing ³	Date	Time	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC		Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	
MW-30-88	601	69.3	1/15/2008	15:00	3.13E+05	2.78E+04	6.18E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	
	602	69.3	6/23/2008	10:50	3.02E+05	3.12E+04	3.42E+02	3.42E+02	3.42E+02	1.05E+01	1.05E+01	4.32E+02	3.02E+04	1.12E+01	1.12E+01	3.42E+02	NA	NA
	603	69.3	6/23/2008	14:45	2.03E+05	2.03E+05	1.03E+02	3.42E+02	3.42E+02	1.05E+01	1.05E+01	4.32E+02	3.02E+04	1.12E+01	1.12E+01	3.42E+02	NA	NA
	604	69.3	1/29/2009	10:45	1.00E+05	1.00E+05	5.18E+02	3.42E+02	3.42E+02	1.05E+01	1.05E+01	4.32E+02	3.02E+04	1.12E+01	1.12E+01	3.42E+02	NA	NA
	605	69.3	1/29/2009	14:05	1.07E+05	9.73E+03	6.84E+02	3.42E+02	3.42E+02	1.05E+01	1.05E+01	4.32E+02	3.02E+04	1.12E+01	1.12E+01	3.42E+02	NA	NA
	606	69.3	6/12/2007	10:30	2.27E+05	2.73E+03	6.84E+02	3.42E+02	3.42E+02	1.05E+01	1.05E+01	4.32E+02	3.02E+04	1.12E+01	1.12E+01	3.42E+02	NA	NA
	607	69.3	7/15/2007	9:55	9.21E+04	7.40E+03	7.93E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	608	69.3	8/1/2007	11:41	1.03E+05	1.09E+03	6.13E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	609	69.3	8/1/2007	10:00	9.90E+04	2.90E+03	6.13E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	610	69.3	8/1/2007	11:00	2.33E+05	6.99E+03	6.13E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
611	69.3	8/21/2007	9:45	1.07E+05	2.11E+03	7.23E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	
612	69.3	8/21/2007	11:42	9.80E+04	2.94E+03	7.23E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	
613	69.3	9/12/2007	11:00	9.20E+04	2.76E+03	7.23E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	
614	69.3	10/23/2007	11:40	1.32E+05	3.90E+03	4.94E+02	2.52E+02	2.52E+02	6.15E+01	6.15E+01	2.22E+02	1.62E+04	5.76E+02	6.15E+01	6.15E+01	2.22E+02	NA	NA
615	69.3	2/4/2008	13:00	1.53E+05	5.51E+03	3.94E+02	3.34E+02	3.34E+02	3.92E+01	3.92E+01	1.62E+02	1.62E+04	5.76E+02	3.92E+01	3.92E+01	1.62E+02	NA	NA
616	69.3	5/6/2008	11:01	7.60E+04	2.07E+03	4.95E+02	2.07E+02	2.07E+02	3.70E+01	3.70E+01	1.92E+02	1.92E+04	3.70E+01	3.70E+01	1.92E+02	NA	NA	
617	69.3	8/9/2008	11:27	1.09E+05	3.97E+03	4.95E+02	2.09E+02	2.09E+02	3.70E+01	3.70E+01	1.92E+02	1.92E+04	3.70E+01	3.70E+01	1.92E+02	NA	NA	
618	69.3	8/9/2008	11:29	8.53E+04	2.03E+03	5.03E+02	3.12E+02	3.12E+02	5.12E+01	5.12E+01	2.32E+02	2.32E+04	5.12E+01	5.12E+01	2.32E+02	NA	NA	
619	69.3	11/2/2008	10:27	9.55E+04	2.03E+03	3.92E+02	4.09E+02	4.09E+02	5.53E+01	5.53E+01	2.32E+02	2.32E+04	5.53E+01	5.53E+01	2.32E+02	NA	NA	
620	69.3	1/16/2009	11:00	1.07E+05	2.51E+03	1.93E+02	8.74E+02	8.74E+02	7.33E+01	7.33E+01	3.62E+02	3.62E+04	7.33E+01	7.33E+01	3.62E+02	NA	NA	
621	69.3	4/21/2009	10:27	1.00E+05	4.60E+03	4.23E+02	1.34E+02	1.34E+02	4.48E+01	4.48E+01	1.92E+02	1.92E+04	4.48E+01	4.48E+01	1.92E+02	NA	NA	
622	69.3	6/1/2009	12:02	2.02E+05	3.21E+03	3.77E+02	3.12E+02	3.12E+02	5.53E+01	5.53E+01	2.32E+02	2.32E+04	5.53E+01	5.53E+01	2.32E+02	NA	NA	
623	69.3	8/6/2009	12:16	1.64E+05	4.77E+03	2.26E+02	6.79E+02	6.79E+02	6.10E+01	6.10E+01	2.92E+02	2.92E+04	6.10E+01	6.10E+01	2.92E+02	NA	NA	
624	69.3	9/12/2009	10:45	9.91E+04	2.91E+03	2.77E+02	4.43E+02	4.43E+02	8.30E+01	8.30E+01	3.72E+02	3.72E+04	8.30E+01	8.30E+01	3.72E+02	NA	NA	
625	69.3	11/2/2009	11:21	9.01E+04	2.63E+03	1.93E+02	4.26E+02	4.26E+02	8.14E+01	8.14E+01	3.72E+02	3.72E+04	8.14E+01	8.14E+01	3.72E+02	NA	NA	
626	69.3	1/27/2010	11:30	1.25E+05	3.99E+03	6.13E+02	3.42E+02	3.42E+02	7.18E+01	7.18E+01	3.22E+02	3.22E+04	7.18E+01	7.18E+01	3.22E+02	NA	NA	
627	69.3	4/29/2010	17:55	1.60E+05	2.01E+03	7.93E+02	7.47E+02	7.47E+02	3.45E+01	3.45E+01	1.82E+02	1.82E+04	3.45E+01	3.45E+01	1.82E+02	NA	NA	
628	69.3	6/4	1.61E+05	4.67E+03	2.73E+02	1.31E+02	1.31E+02	1.31E+02	9.40E+01	9.40E+01	4.52E+02	4.52E+04	9.40E+01	9.40E+01	4.52E+02	NA	NA	
629	69.3	6/4	1.52E+05	4.40E+03	4.30E+02	2.56E+02	2.56E+02	2.56E+02	4.79E+01	4.79E+01	2.32E+02	2.32E+04	4.79E+01	4.79E+01	2.32E+02	NA	NA	
630	69.3	6/4	7.28E+04	3.72E+03	1.93E+02	9.14E+02	9.14E+02	9.14E+02	6.53E+01	6.53E+01	3.02E+02	3.02E+04	6.53E+01	6.53E+01	3.02E+02	NA	NA	
631	69.3	6/4	8.20E+04	1.11E+05	2.23E+02	3.53E+02	3.53E+02	3.53E+02	7.30E+01	7.30E+01	3.42E+02	3.42E+04	7.30E+01	7.30E+01	3.42E+02	NA	NA	
632	69.3	6/4	9.20E+04	1.23E+05	3.65E+03	4.73E+02	1.93E+02	1.93E+02	4.41E+01	4.41E+01	1.92E+02	1.92E+04	4.41E+01	4.41E+01	1.92E+02	NA	NA	
633	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
634	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
635	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
636	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
637	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
638	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
639	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
640	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
641	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
642	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
643	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
644	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
645	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
646	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
647	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
648	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
649	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
650	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
651	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
652	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
653	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+01	8.79E+01	4.22E+02	4.22E+04	8.79E+01	8.79E+01	4.22E+02	NA	NA	
654	69.3	6/4	1.23E+05	1.08E+03	1.44E+02	6.99E+02	6.99E+02	6.99E+02	8.79E+0									

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, TN

Well ID ¹	ANALYSIS RESULTS											Well ID ¹										
	SAMPLE COLLECTION			TRITIUM (PCU/L)			Sr-90 (PCU/L)			Cs-137 (PCU/L)			MDS (PCU/L)									
	SAMPLE ID	SAMPLE ZONE CENTER, elevation in msl ²	SAMPLE ZONE CENTER, depth in below top of casing ³	Date	Time	Result	Std. Dev.	MDC	Result	Std. Dev.	MDC		Result	Std. Dev.	MDC	Result	Std. Dev.	MDC				
MW31-46	004	483	26.8	8/22/07	1023	1.09E+04	1.27E+03	5.17E-01	8.03E+01	3.03E+01	3.03E+01	1.03E-01	3.68E+00	4.15E+00	NA	NA	NA	MW31-46				
	005	483	26.8	9/11/2007	1310	6.62E+03	3.72E+02	-2.26E-01	-1.20E+00	6.21E-01	6.21E-01	0.02E+00	3.03E+00	4.72E+00	NA	NA	NA					
	006	483	26.8	10/25/2007	1520	8.77E+03	9.99E+02	4.20E+00	-6.78E-01	4.20E+00	4.20E+00	3.94E+00	3.94E+00	3.21E+00	3.21E+00	NA	NA		NA			
	007	483	26.8	1/6/2008	1031	3.97E+02	1.79E+02	2.18E-02	8.97E-01	8.97E-01	8.97E-01	5.02E-00	4.48E+00	4.48E+00	3.02E+00	3.02E+00	NA		NA	NA		
	009	483	26.8	9/20/08	1202	2.08E+04	1.30E+03	4.52E+00	3.92E-01	3.92E-01	3.92E-01	1.10E+00	1.10E+00	7.02E-01	3.02E+00	3.02E+00	NA		NA	NA		
	010	483	26.8	8/9/2008	1145	1.56E+04	8.41E+02	4.45E-01	8.24E-01	8.24E-01	8.24E-01	1.72E+00	1.72E+00	3.03E+00	3.03E+00	NA	NA		NA	NA		
	011	483	26.8	10/26/2008	1120	4.01E+03	2.28E+02	1.11E-02	7.44E-01	7.44E-01	7.44E-01	1.20E+00	1.20E+00	4.37E-01	4.37E-01	NA	NA		NA	NA		
	012	483	26.8	1/16/2009	1115	7.77E+02	1.79E+02	1.13E-02	4.11E-01	4.11E-01	4.11E-01	1.13E+00	1.13E+00	4.93E+00	4.93E+00	NA	NA		NA	NA		
	013	483	26.8	6/6/09	1109	1.11E+04	1.69E+03	1.69E+02	1.08E-01	1.08E-01	1.08E-01	5.74E-01	5.74E-01	4.61E-01	1.08E+00	1.08E+00	NA		NA	NA	NA	
	014	483	26.8	4/14/2009	1036	4.04E+04	1.43E+03	1.65E+02	4.85E-01	4.85E-01	4.85E-01	5.71E-01	5.71E-01	1.44E+00	3.98E+00	3.98E+00	NA		NA	NA	NA	
	015	483	26.8	9/22/2009	1142	9.34E+03	1.13E+03	3.73E+02	5.72E-01	5.72E-01	5.72E-01	9.45E-01	9.45E-01	1.48E+00	3.92E+00	3.92E+00	NA		NA	NA	NA	
	016	483	26.8	7/9/2009	1153	7.46E+03	2.61E+02	2.73E+02	1.91E-01	1.91E-01	1.91E-01	1.98E+00	1.98E+00	1.04E+00	3.92E+00	3.92E+00	NA		NA	NA	NA	
	017	483	26.8	8/14/2009	1113	3.18E+04	9.35E+02	1.03E+02	3.21E-02	7.92E-01	7.92E-01	1.97E+00	1.97E+00	5.31E-00	3.23E-00	4.71E+00	4.71E+00		NA	NA	NA	NA
	018	483	26.8	10/22/2009	1218	4.88E+04	8.63E+02	1.93E+02	5.63E-01	8.72E-01	8.72E-01	2.92E+01	2.92E+01	6.17E+00	6.17E+00	6.17E+00	6.17E+00		NA	NA	NA	NA
	019	483	26.8	1/9/2010	1707	4.46E+02	1.19E+02	1.19E+02	1.89E-01	7.92E-01	7.92E-01	4.10E-01	4.10E-01	1.48E+00	1.48E+00	1.48E+00	1.48E+00		NA	NA	NA	NA
	020	483	26.8	3/5/2010	1130	4.89E+02	1.71E+02	1.92E+02	1.47E-01	5.12E-01	5.12E-01	4.10E-01	4.10E-01	4.53E+00	4.53E+00	4.53E+00	4.53E+00		NA	NA	NA	NA
	021	483	26.8	4/14/2010	1042	1.16E+04	3.90E+02	1.20E+02	1.11E-01	4.62E-01	4.62E-01	5.28E-01	5.28E-01	9.05E+00	9.05E+00	9.05E+00	9.05E+00		NA	NA	NA	NA
	022	483	26.8	7/21/2010	1130	1.73E+04	1.29E+02	2.23E+02	5.11E-01	7.92E-01	7.92E-01	9.18E-01	9.18E-01	7.42E+00	7.42E+00	7.42E+00	7.42E+00		NA	NA	NA	NA
	023	483	26.8	8/24/2010	1443	5.40E+04	1.59E+03	1.21E+02	3.03E-01	4.71E-01	4.71E-01	2.74E+00	2.74E+00	1.07E+01	1.07E+01	1.07E+01	1.07E+01		NA	NA	NA	NA
	024	483	26.8	8/24/2010	1211	4.11E+03	5.26E+02	1.24E+02	1.62E-01	7.92E-01	7.92E-01	1.21E+00	1.21E+00	5.26E-02	5.26E-02	5.26E-02	5.26E-02		NA	NA	NA	NA
025	483	26.8	9/7/2010	1349	1.04E+05	3.02E+03	1.92E+02	1.15E-01	4.31E-01	4.31E-01	3.53E+00	3.53E+00	6.68E-00	6.68E-00	6.68E-00	6.68E-00	NA	NA	NA	NA		
026	483	26.8	11/6/2010	1155	3.35E+04	9.81E+02	1.92E+02	-3.04E-02	5.11E-01	5.11E-01	-2.32E+00	9.51E+00	9.51E+00	8.72E+00	8.72E+00	NA	NA	NA	NA			
027	483	26.8	1/7/2010	1210	6.89E+03	1.44E+03	5.30E-01	3.03E-01	1.06E+00	1.06E+00	1.99E+00	1.99E+00	9.40E+00	9.40E+00	9.40E+00	9.40E+00	NA	NA	NA	NA		
028	483	26.8	1/8/2010	925	1.41E+04	9.09E+02	6.50E-01	4.50E-01	1.02E+00	1.02E+00	4.30E-01	3.03E+00	3.03E+00	1.97E+00	1.97E+00	NA	NA	NA	NA			
029	483	26.8	6/12/2007	1420	5.00E+03	7.63E+02	4.32E+02	4.72E-01	6.42E-01	6.42E-01	5.21E-01	1.52E+00	1.52E+00	2.02E+00	2.02E+00	NA	NA	NA	NA			
030	483	26.8	8/7/2007	1115	4.00E+04	7.77E+02	5.13E+02	1.41E-01	7.42E-01	7.42E-01	9.43E+00	9.43E+00	4.19E+00	4.19E+00	4.19E+00	4.19E+00	NA	NA	NA	NA		
031	483	26.8	9/11/2007	1325	3.77E+04	1.13E+03	2.30E+02	1.37E-01	4.52E-01	4.52E-01	4.39E-01	3.51E+00	3.51E+00	3.03E+00	3.03E+00	NA	NA	NA	NA			
032	483	26.8	10/5/2007	1455	3.50E+04	1.94E+03	4.30E+02	-1.63E-01	4.50E-01	4.50E-01	1.07E+00	1.07E+00	4.01E-00	4.12E+00	4.12E+00	NA	NA	NA	NA			
033	483	26.8	1/8/2008	1132	1.24E+04	7.32E+02	1.92E+02	-8.88E-02	3.46E-01	3.46E-01	-2.49E-01	4.48E+00	4.48E+00	4.48E+00	4.48E+00	NA	NA	NA	NA			
034	483	26.8	6/6/08	1616	1.02E+04	7.32E+02	1.92E+02	1.44E-01	3.46E-01	3.46E-01	6.17E+01	6.17E+01	3.46E+00	3.46E+00	3.46E+00	3.46E+00	NA	NA	NA	NA		
035	483	26.8	8/7/2008	1122	1.70E+04	4.17E+02	1.94E+02	-8.22E-01	2.51E-01	2.51E-01	1.36E-01	1.28E+00	1.28E+00	1.48E+00	1.48E+00	NA	NA	NA	NA			
036	483	26.8	8/30/2008	1234	2.21E+04	1.07E+03	5.92E+02	-6.34E-01	4.33E-01	4.33E-01	9.39E-01	9.39E-01	3.73E-01	3.73E-01	3.73E-01	3.73E-01	NA	NA	NA	NA		
037	483	26.8	10/9/2008	1214	2.30E+04	1.08E+03	1.73E+02	2.20E-01	2.33E-01	2.33E-01	2.21E+00	2.21E+00	7.72E-00	7.72E-00	7.72E-00	7.72E-00	NA	NA	NA	NA		
038	483	26.8	1/18/2009	1130	2.55E+04	8.07E+02	1.94E+02	3.95E-01	7.40E-01	7.40E-01	1.02E-02	6.01E-00	6.01E-00	5.48E+00	5.48E+00	NA	NA	NA	NA			
039	483	26.8	2/6/2009	1133	3.28E+04	3.89E+02	1.71E+02	6.43E-01	6.81E-01	6.81E-01	-1.32E+00	-1.32E+00	7.48E-01	7.48E-01	7.48E-01	7.48E-01	NA	NA	NA	NA		
040	483	26.8	4/14/2009	1207	3.24E+04	1.10E+03	1.83E+02	2.95E-01	6.81E-01	6.81E-01	1.76E+00	1.76E+00	4.65E-00	4.65E-00	4.65E-00	4.65E-00	NA	NA	NA	NA		
041	483	26.8	5/29/2009	1284	3.16E+04	5.51E+02	1.95E+02	5.59E-01	5.59E-01	5.59E-01	1.98E+00	1.98E+00	7.12E-00	7.12E-00	7.12E-00	7.12E-00	NA	NA	NA	NA		
042	483	26.8	7/21/2009	1230	1.45E+04	6.23E+02	2.12E+02	1.95E-01	7.92E-01	7.92E-01	3.40E+01	3.40E+01	1.44E+00	1.44E+00	1.44E+00	1.44E+00	NA	NA	NA	NA		
043	483	26.8	9/14/2009	1245	1.41E+04	5.09E+02	2.13E+02	1.51E-01	3.52E-01	3.52E-01	-1.33E+00	-1.33E+00	6.72E-00	6.72E-00	6.72E-00	6.72E-00	NA	NA	NA	NA		
044	483	26.8	10/22/2009	1245	4.41E+04	5.48E+02	1.93E+02	8.11E-01	8.72E-01	8.72E-01	-1.92E+00	-1.92E+00	6.05E-00	6.05E-00	6.05E-00	6.05E-00	NA	NA	NA	NA		
045	483	26.8	1/9/2010	1320	2.00E+04	3.93E+02	1.57E+02	1.08E+00	7.42E-01	7.42E-01	1.92E-01	1.63E+00	1.63E+00	6.73E+00	6.73E+00	NA	NA	NA	NA			
046	483	26.8	1/26/2010	1300	3.56E+04	2.21E+03	6.56E+02	5.44E-01	9.39E-01	9.39E-01	1.63E+00	1.63E+00	1.56E+00	1.56E+00	1.56E+00	1.56E+00	NA	NA	NA	NA		
047	483	26.8	3/9/2010	1217	7.35E+04	1.11E+03	1.72E+02	1.20E-01	4.22E-01	4.22E-01	2.77E+00	2.77E+00	4.62E+00	4.62E+00	4.62E+00	4.62E+00	NA	NA	NA	NA		
048	483	26.8	4/14/2010	1305	1.94E+04	3.48E+02	1.20E+02	1.50E-01	4.43E-01	4.43E-01	-4.33E+00	-4.33E+00	9.18E+00	9.18E+00	9.18E+00	9.18E+00	NA	NA	NA	NA		
049	483	26.8	7/27/2010	1219	5.11E+04	1.93E+03	2.93E+02	3.68E-01	9.18E-01	9.18E-01	2.95E+00	2.95E+00	7.03E-00	7.03E-00	7.03E-00	7.03E-00	NA	NA	NA	NA		
050	483	26.8	8/27/2010	1524	6.17E+04	1.80E+03	1.72E+02	5.31E-01	6.43E-01	6.43E-01	-1.31E+00	-1.31E+00	8.27E+00	8.27E+00	8.27E+00	8.27E+00	NA	NA	NA	NA		
051	483	26.8	8/9/2010	1311	6.69E+04	1.99E+03	1.93E+02	4.60E-01	7.92E-01	7.92E-01	3.89E-01	3.89E-01	1.77E+00	1.77E+00	1.77E+00	1.77E+00	NA	NA	NA	NA		
052	483	26.8	8/23/2010	1528	6.63E+04	1.81E+03	1.64E+02	3.99E-01	7.92E-01	7.92E-01	8.18E-01	8.18E-01	4.58E-01	4.58E-01	4.58E-01	4.58E-01	NA	NA	NA	NA		
053	483	26.8	10/23/2010	1232	2.25E+04	2.02E+02	1.14E+02	1.14E+00</														

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, KY

Table with columns for Well ID, Sample Zone Center, Date, Tritium (PCU/L), Sr-90 (pCi/L), Cs-137 (pCi/L), MDC, Result, and various chemical analytes (Ct-60, Ct-90, etc.). Rows include MW-37-57, MW-33, MW-35, MW-39-51, MW-38-51, MW-38-52, MW-38-53, MW-38-54, MW-38-55, MW-38-56, MW-38-57, MW-38-58, MW-38-59, MW-38-60, MW-38-61, MW-38-62, MW-38-63, MW-38-64, MW-38-65, MW-38-66, MW-38-67, MW-38-68, MW-38-69, MW-38-70, MW-38-71, MW-38-72, MW-38-73, MW-38-74, MW-38-75, MW-38-76, MW-38-77, MW-38-78, MW-38-79, MW-38-80, MW-38-81, MW-38-82, MW-38-83, MW-38-84, MW-38-85, MW-38-86, MW-38-87, MW-38-88, MW-38-89, MW-38-90, MW-38-91, MW-38-92, MW-38-93, MW-38-94, MW-38-95, MW-38-96, MW-38-97, MW-38-98, MW-38-99, MW-39-01, MW-39-02, MW-39-03, MW-39-04, MW-39-05, MW-39-06, MW-39-07, MW-39-08, MW-39-09, MW-39-10, MW-39-11, MW-39-12, MW-39-13, MW-39-14, MW-39-15, MW-39-16, MW-39-17, MW-39-18, MW-39-19, MW-39-20, MW-39-21, MW-39-22, MW-39-23, MW-39-24, MW-39-25, MW-39-26, MW-39-27, MW-39-28, MW-39-29, MW-39-30, MW-39-31, MW-39-32, MW-39-33, MW-39-34, MW-39-35, MW-39-36, MW-39-37, MW-39-38, MW-39-39, MW-39-40, MW-39-41, MW-39-42, MW-39-43, MW-39-44, MW-39-45, MW-39-46, MW-39-47, MW-39-48, MW-39-49, MW-39-50, MW-39-51, MW-39-52, MW-39-53, MW-39-54, MW-39-55, MW-39-56, MW-39-57, MW-39-58, MW-39-59, MW-39-60, MW-39-61, MW-39-62, MW-39-63, MW-39-64, MW-39-65, MW-39-66, MW-39-67, MW-39-68, MW-39-69, MW-39-70, MW-39-71, MW-39-72, MW-39-73, MW-39-74, MW-39-75, MW-39-76, MW-39-77, MW-39-78, MW-39-79, MW-39-80, MW-39-81, MW-39-82, MW-39-83, MW-39-84, MW-39-85, MW-39-86, MW-39-87, MW-39-88, MW-39-89, MW-39-90, MW-39-91, MW-39-92, MW-39-93, MW-39-94, MW-39-95, MW-39-96, MW-39-97, MW-39-98, MW-39-99, MW-40-01, MW-40-02, MW-40-03, MW-40-04, MW-40-05, MW-40-06.

Table 5 - Historic Groundwater Analytical Results
Table 5

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

Well ID ¹	SAMPLE ID	SAMPLE ZONE CENTER, elevation in msl ²	SAMPLE ZONE CENTER, depth in below top of casing ³	SAMPLE COLLECTION			ANALYSIS RESULTS										Well ID ¹		
				Date	Time	MDC	TRITIUM (PCU/L)		Sr-90 (PCU/L)		C-137 (PCU/L)		Cs-60 (PCU/L)		NKS (PCU/L)				
							Std. Dev. ⁴	Result	Std. Dev. ⁴	Result	Std. Dev. ⁴	Result	Std. Dev. ⁴	Result	Std. Dev. ⁴	Result		Std. Dev. ⁴	Result
MW-52-118 MW-52-112	604	NA	HA	4/8/2009	12:03	1.15E+02	1.08E+02	3.84E-01	3.84E-01	2.02E+00	2.02E+00	5.72E-05	1.72E-05	3.62E+00	3.62E+00	NA	NA	MW-52-118	
	601	-107.1	14.55	5/28/2007	14:55	6.78E+01	1.47E+02	4.28E-01	5.52E-01	2.72E+00	2.72E+00	3.92E-05	1.76E-05	3.38E+00	3.29E+00	1.94E+00	1.18E+01	MW-52-112	
	602	-107.1	14.55	8/29/2007	12:05	6.42E+01	1.17E+02	4.19E-01	7.10E-01	1.99E+00	1.99E+00	4.02E-05	4.92E-05	4.02E+00	4.02E+00	NA	NA		
	603	-107.1	14.55	4/28/2008	12:53	6.29E+01	8.06E+01	1.95E-01	2.32E-01	3.29E+00	3.29E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	604	-107.1	14.55	4/29/2008	14:27	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	605	-107.1	14.55	6/6/2007	12:57	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	606	-107.1	14.55	6/6/2007	14:30	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	607	-107.1	14.55	4/29/2008	10:32	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	608	-107.1	14.55	4/29/2008	12:56	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
	609	-107.1	14.55	4/29/2008	17:59	6.29E+01	1.95E+02	1.95E-01	4.62E-01	1.95E+00	1.95E+00	3.52E-05	3.29E-05	3.29E+00	3.29E+00	NA	NA		
MW-52-101	601	-166.1	12.06	4/29/2007	12:06	2.04E+02	1.09E+02	3.19E-01	5.77E-01	3.08E+00	3.08E+00	3.02E-05	2.01E-05	4.10E+00	4.10E+00	1.07E+01	1.17E+01	MW-52-101	
	602	-166.1	12.06	8/6/2007	11:40	1.19E+02	1.77E+02	1.48E-02	5.65E-01	6.77E-01	1.21E+00	1.21E+00	3.02E-05	3.02E-05	3.02E+00	3.02E+00	NA	NA	
	603	-166.1	10.24	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	604	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	605	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	606	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	607	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	608	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	609	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
	610	-166.1	12.07	4/30/2008	12:07	1.47E+02	9.95E+01	1.31E+02	4.92E-01	4.92E-01	2.48E+00	2.48E+00	6.72E-05	2.38E+00	4.47E+00	4.47E+00	NA	NA	
MW-54-37	601	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01	MW-54-37	
	602	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	603	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	604	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	605	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	606	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	607	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	608	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	609	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		
	610	-109.2	10.92	4/29/2008	10:15	5.00E+03	3.40E+02	3.11E-01	1.52E+00	1.52E+00	1.52E+00	3.02E-05	1.52E-05	3.02E+00	3.02E+00	2.22E+01	2.11E+01		

Table 5 - Historic Groundwater Analytical Results

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, NY

Well ID ¹	Sample ID	Sample Zone Center, depth in below top of casing ²	Sample Zone Center, depth in below top of casing ²	SAMPLE COLLECTION			TRITIUM (PCU/L)			C-13 (PCU/L)			C-6 (PCU/L)			NKS (PCU/L)	MDC	Weid ID ³
				Date	Time	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	Result			
MW-54-37	013	-24	183E+3	2.2E+2	1.3E+2	4.7E+2	1.2E+2	6.7E-2	3.0E+2	3.4E+2	1.1E+2	1.6E+2	3.0E+2	3.3E+2	2.0E+1	3.3E+2	3.9E+2	3.9E+2
	014	-24	121E+3	2.1E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	015	-24	172E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	016	-24	165E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	017	-24	169E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	018	-24	171E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	019	-24	174E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	020	-24	175E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	021	-24	176E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	022	-24	177E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	023	-24	178E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	024	-24	179E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
025	-24	180E+3	2.2E+2	1.3E+2	4.3E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2	
MW-54-14	001	-109	183E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	002	-109	184E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	003	-109	185E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	004	-109	186E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	005	-109	187E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	006	-109	188E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	007	-109	189E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	008	-109	190E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	009	-109	191E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	010	-109	192E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	011	-109	193E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	012	-109	194E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
MW-54-123	001	-123	183E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	002	-123	184E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	003	-123	185E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	004	-123	186E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	005	-123	187E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	006	-123	188E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	007	-123	189E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	008	-123	190E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	009	-123	191E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	010	-123	192E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	011	-123	193E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2
	012	-123	194E+3	2.2E+2	1.3E+2	4.7E+2	1.3E+2	3.2E-2	4.9E+2	7.9E+2	1.2E+2	1.3E+2	3.1E+2	7.3E+2	3.3E+2	3.9E+2	3.9E+2	3.9E+2

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, TN

Well ID ¹	SAMPLE COLLECTION			ANALYSIS RESULTS				Well ID ¹								
	SAMPLE ID	SAMPLE ZONE CENTER, elevation in msl ²	SAMPLE ZONE CENTER, depth ft below top of casing ³	TRITIUM (PCT/D)		Sr-90 (PCT/D)		C-137 (PCT/D)		N-163 (PCT/D)						
				Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC				
MW 56-55	604	193	52	2.63E+2	1.27E+2	1.11E+3	5.70E-3	9.71E-01	3.33E-01	5.27E-01	3.92E+00	1.9E+00	1.9E+01	3.8E+01	1.3E+01	MW 56-55
				3.92E+4	1.64E+2	1.53E+3	3.40E-3	7.72E-01	7.72E-01	5.42E+00	6.9E+00	2.1E+00	1.4E+00	3.9E+00	2.3E+00	RA
				2.08E+2	1.98E+2	1.93E+3	4.84E-3	9.21E-01	6.33E-01	2.8E+00	4.9E+00	2.1E+00	2.1E+00	4.3E+00	3.9E+00	RA
				6.88E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.29E+2	1.93E+2	2.07E+3	1.49E-3	7.28E-01	7.28E-01	1.2E+00	9.4E+00	1.2E+00	1.2E+00	2.6E+00	3.9E+00	RA
				6.06E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 56-58	601	193	74	5.9E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				6.06E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 57-20	602	193	19	4.9E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 57-45	601	193	40	8.2E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 57-11	602	193	10	8.2E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 58-26	601	193	20	5.9E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 59-20	601	193	37	5.9E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
MW 59-45	601	193	42	5.9E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				3.2E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				4.84E+2	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA
				1.65E+3	1.92E+2	1.93E+3	2.94E-3	6.21E-01	3.47E-01	2.7E+00	6.9E+00	3.9E+00	2.1E+00	6.9E+00	3.9E+00	RA

F:\17000-1E0991780317809-92.MG\QI-2010\EN-AL\Tables;
Table 5 - Historic Groundwater Analytical Results.xlsx;
Table 6

TABLE 5
HISTORIC GROUNDWATER ANALYTICAL RESULTS
INDIAN POINT ENERGY CENTER
BUCHANAN, KY

Well ID ¹	SAMPLE COLLECTION		TRITIUM (PCU/L)			Sr-90 (PCU/L)			Ct-137 (PCU/L)			Cs-137 (PCU/L)			NKS (PCU/L)			Wed ID ¹				
			SAMPLE ZONE CENTER, elevation in msl ²	SAMPLE ZONE CENTER, depth in below top of casing ³	Date	Time	MDC	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	Result	Std. Dev. ⁴	MDC	Result		Std. Dev. ⁴			
																				ANALYSIS RESULTS		
																				8.65E+02	1.07E+03	4.65E-02
U3-43	023	25.6	21/2/2000	14:15	0.65E+02	1.07E+03	4.65E-02	7.35E-01	3.15E+03	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	4.35E+00	NA	NA	U3-43				
	024	25.6	4/12/2000	12:49	1.07E+03	2.06E+02	1.71E+02	4.65E-02	7.35E-01	5.03E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	025	25.6	7/23/2000	13:21	0.98E+02	1.68E+02	1.71E+02	4.65E-02	7.35E-01	2.21E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	026	25.6	10/22/2000	14:04	1.73E+02	1.13E+02	1.71E+02	4.65E-02	7.35E-01	2.73E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	001	NA	2/18/2000	14:12	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	002	NA	2/18/2000	14:10	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	003	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	004	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	005	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	006	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	007	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	008	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	009	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	010	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	011	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	012	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	013	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	014	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	015	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	016	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	017	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	018	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	019	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	020	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	021	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	022	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	023	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	024	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	025	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	026	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					
	027	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA	U3-43				
	028	NA	2/18/2000	14:05	1.42E+02	1.72E+02	1.71E+02	4.65E-02	7.35E-01	2.05E+00	3.05E+05	1.71E+00	1.91E+00	3.65E+00	3.65E+00	NA	NA					

TABLE 5
 HISTORIC GROUNDWATER ANALYTICAL RESULTS
 INDIAN POINT ENERGY CENTER
 BUCHANAN, KY

Well ID ¹	ANALYSIS RESULTS												Well ID ¹						
	SAMPLE COLLECTION			TRITIUM (pCi/L)			Sr-90 (pCi/L)			C-137 (pCi/L)				Cs-60 (pCi/L)					
	Sample ID	Sample Zone Center, depth 0 below top of casing ²	Sample Zone Center, elevation in msl ³	Date	Time	Result	MDC	Std. Dev. ⁸	MDC	Result	Std. Dev. ⁸	MDC		Result	Std. Dev. ⁸	MDC	Result	Std. Dev. ⁸	MDC
LAC-002	601	NA	-2.3	6/25/2016	12:47	5.20E+01	1.71E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	601	NA	-2.3	6/25/2016	12:47	3.02E+01	1.33E+02	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00	1.33E+00
	603	NA	-2.3	9/12/2008	13:14	4.71E+01	1.50E+02	3.85E+01	6.45E+02	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01
	604	NA	-2.3	1/24/2008	13:38	2.03E+01	1.02E+02	3.20E+01	1.02E+02	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01	8.30E+01
	602	NA	-2.3	7/25/07	14:45	4.30E+01	1.20E+02	3.20E+01	1.02E+02	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00
	605	NA	-2.3	1/29/2007	9:14	7.64E+01	1.37E+02	1.44E+01	4.14E+02	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01
	606	NA	-2.3	1/24/2007	10:50	2.00E+01	1.44E+02	4.97E+01	1.37E+02	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01	3.32E+01
	608	NA	-2.3	4/12/2008	0:30	4.03E+01	1.44E+02	4.03E+01	1.44E+02	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01
	610	NA	-2.3	1/17/2009	10:42	8.19E+01	1.63E+02	1.63E+02	1.63E+02	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01	7.03E+01
	612	NA	-2.3	1/19/2009	12:35	4.21E+01	1.53E+02	1.53E+02	1.53E+02	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01	5.43E+01
	613	NA	-2.3	5/11/2010	13:44	4.21E+01	1.53E+02	6.55E+01	1.53E+02	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01	7.73E+01
	614	NA	-2.3	1/22/2010	14:41	1.02E+02	1.13E+02	1.94E+01	1.13E+02	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01	4.92E+01
B-1	601	NA	NA	6/29/2007	12:35	7.93E+02	2.07E+02	1.92E+02	1.92E+02	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01
	602	NA	NA	8/14/2007	11:30	1.02E+02	2.79E+02	1.92E+02	1.92E+02	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01
	603	NA	NA	10/27/2007	14:49	1.02E+02	4.63E+02	4.71E+02	4.71E+02	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01
	604	NA	NA	1/22/2008	13:08	2.27E+02	1.61E+02	1.29E+01	1.29E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01	5.02E+01
	606	NA	NA	4/15/2008	18:25	1.17E+02	1.57E+02	2.71E+02	2.71E+02	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01
	607	NA	NA	6/24/2008	13:30	8.01E+02	1.83E+02	1.29E+02	1.29E+02	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01
	609	NA	NA	2/22/2010	14:10	1.49E+02	2.13E+02	1.29E+02	1.29E+02	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01	3.90E+01
	608	NA	NA	4/23/2010	16:44	8.15E+02	1.91E+02	1.29E+02	1.29E+02	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01	6.73E+01
	609	NA	NA	8/17/2010	15:40	1.40E+02	6.48E+02	1.29E+02	1.29E+02	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01	6.43E+01
	610	NA	NA	1/17/2010	11:10	2.37E+02	2.72E+02	3.95E+02	3.95E+02	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01	7.58E+01
B-6	601	NA	NA	7/27/07	9:20	4.03E+02	1.67E+02	1.92E+02	1.92E+02	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01	4.97E+01
	602	NA	NA	8/14/2007	8:30	5.46E+02	1.62E+02	3.06E+02	3.06E+02	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01	6.20E+01
	604	NA	NA	1/16/2008	11:30	1.07E+02	1.70E+02	1.92E+02	1.92E+02	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01	4.44E+01
	605	NA	NA	4/25/2008	14:15	5.23E+01	8.43E+01	1.43E+02	1.43E+02	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01
	606	NA	NA	6/22/09	9:40	1.08E+02	1.48E+02	1.48E+02	1.48E+02	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01	7.93E+01
	607	NA	NA	2/12/2010	9:26	4.88E+02	1.63E+02	1.48E+02	1.48E+02	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01	3.72E+01
	608	NA	NA	5/18/2010	9:40	4.48E+02	1.62E+02	1.48E+02	1.48E+02	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01	5.71E+01
	609	NA	NA	8/27/2010	13:43	1.49E+02	1.62E+02	1.92E+02	1.92E+02	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01	9.78E+01
	610	NA	NA	11/8/2010	11:45	1.05E+02	1.33E+02	1.43E+02	1.43E+02	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01	6.50E+01

Notes
 1. For each multi-level monitoring well, wells of well ID indicates depth, unless noted back from reference point on casing to bottom of well screen. For Water-to-mud level systems, mud level indicates depth (rounded to nearest foot) from reference point on casing to top of sampling port. Well IDs without a suffix are open bedrock wells or
 2. Sampling depths to film sampling intervals (0 to 9 in. of pump intake); location of mud transmission rate to the casing possible
 3. NA indicates that the correlative data was not analyzed
 4. Current well identifications are shown for each location. Minor name changes have been made based on altered franchise installation
 5. Dot pattern denotes sampling interval is positioned within overburden soils. Open box indicates sampling interval is in bedrock
 6. All monitoring well EBT1, sample EBT-01B, 01D, and 31C were collected for laboratory and field QA/QC (B-B-Ind, D-Duplicate, S-S-Log). Only the applicable sample results were included in the calculations for rolling averages
 7. These locations are storm drains, not monitoring wells
 8. Column designated as "Std. Dev." provides the three sigma uncertainty values



FIGURES

- Figure 1 Site Location Plan**
- Figure 2 Site Plan**
- Figure 3 Lower Hudson Valley Geologic Map**
- Figure 4 Current and Potential Future SSC Source Locations**
- Figure 5A Long-Term Transducer Monitoring Evaluation Map**
- Figure 6 4th Quarter 2010 Average Tritium Activity Map**
- Figure 6A Temporal Trends in Unit 2 Rolling Average Tritium Activity Maps**
- Figure 6B Unit 2 Leak Collection Device Evaluation – Quarter 4 2010**
- Figure 7 4th Quarter 2010 Average Strontium-90 Activity Map**
- Figure 7A Sr-90 Baseline Analysis – Unit 1 Defueling Evaluation**
- Figure 8 4th Quarter 2010 Average Cesium, Cobalt, and Nickel Activity Map**



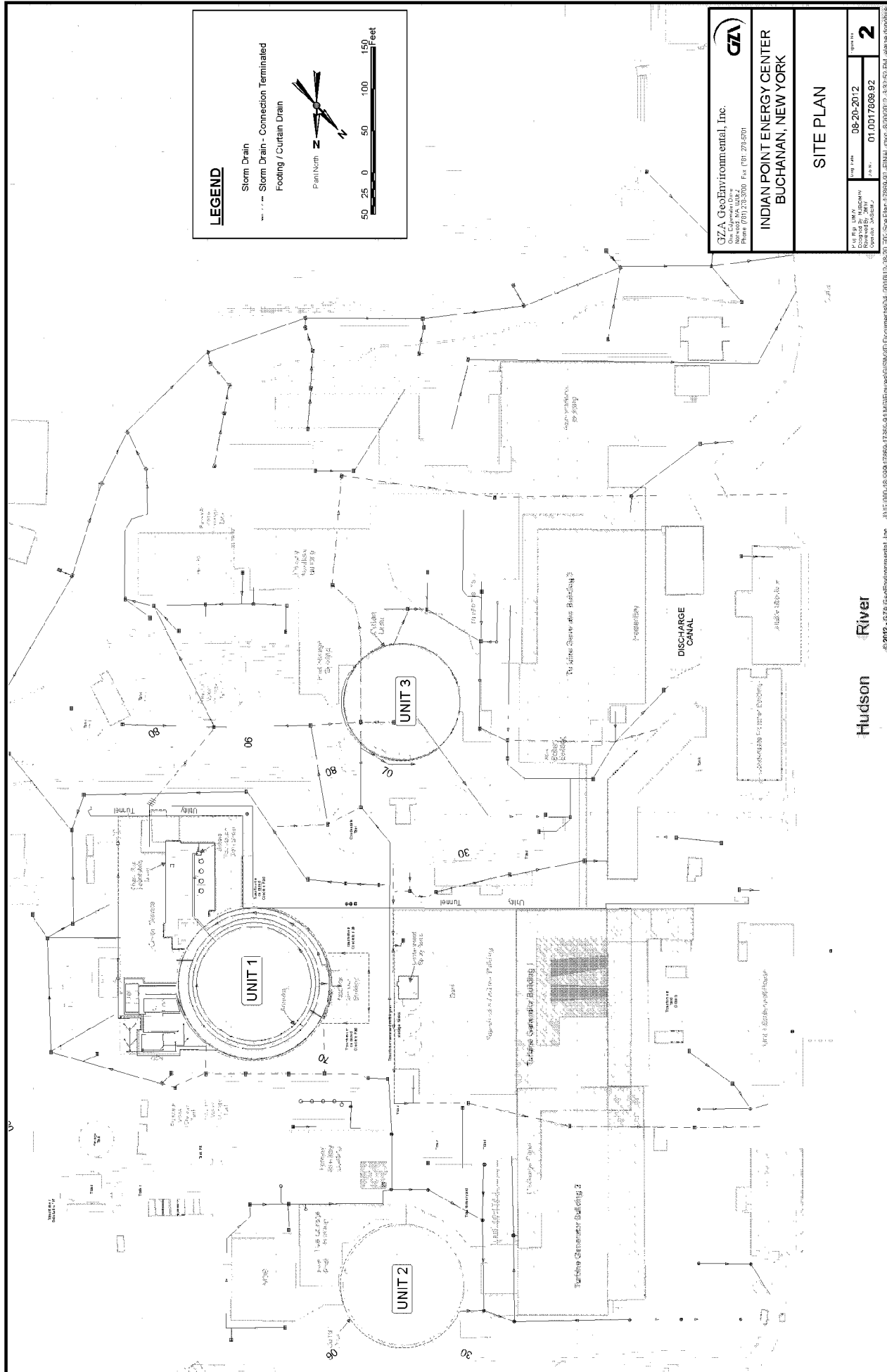
GZA GeoEnvironmental, Inc.
 1000 Massachusetts Ave.
 New York, NY 10022
 Phone: 781.278.3700 Fax: (781) 278-3701

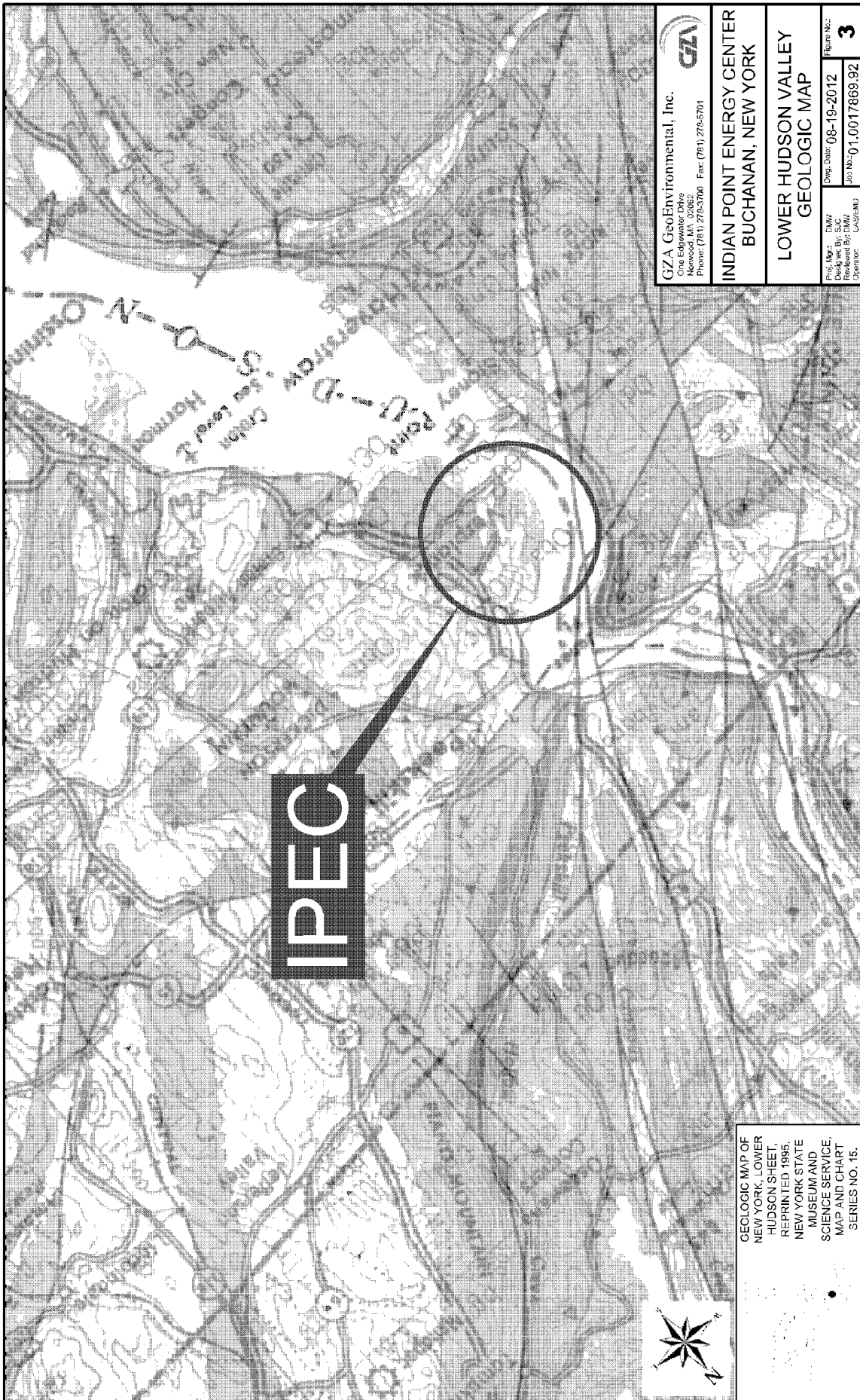
INDIAN POINT ENERGY CENTER
 BUCHANAN, NEW YORK

SITE LOCATION PLAN

Proj. No.	08-20-2012	Sheet No.	1
Prep. By	MB	Reviewed By	MB
Checked By	MB	Drawn By	MB
Scale	AS SHOWN	Date	01/00/17/869.92

Site Location





IPEC

GZA GeoEnvironmental, Inc.
 One Edgewater Drive
 Honesdale, NY 17033
 Project: (761) 275-3700 Fax: (761) 275-5701

**INDIAN POINT ENERGY CENTER
 BUCHANAN, NEW YORK**

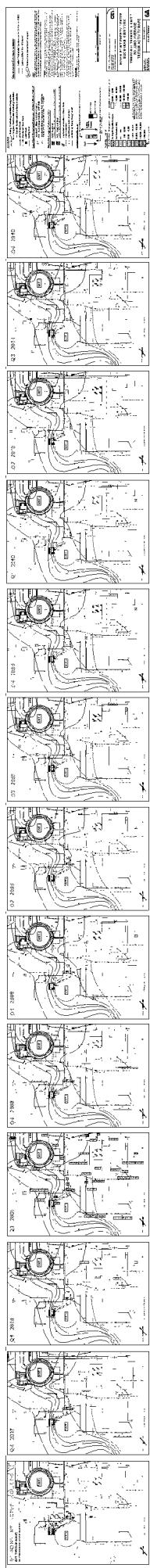
**LOWER HUDSON VALLEY
 GEOLOGIC MAP**

Proj. No.: DMW
 Drawn by: S.C.
 Operator: CAS/MD
 Date: 08-19-2012
 Job No.: 01.0017869.92
 Figure No.: **3**

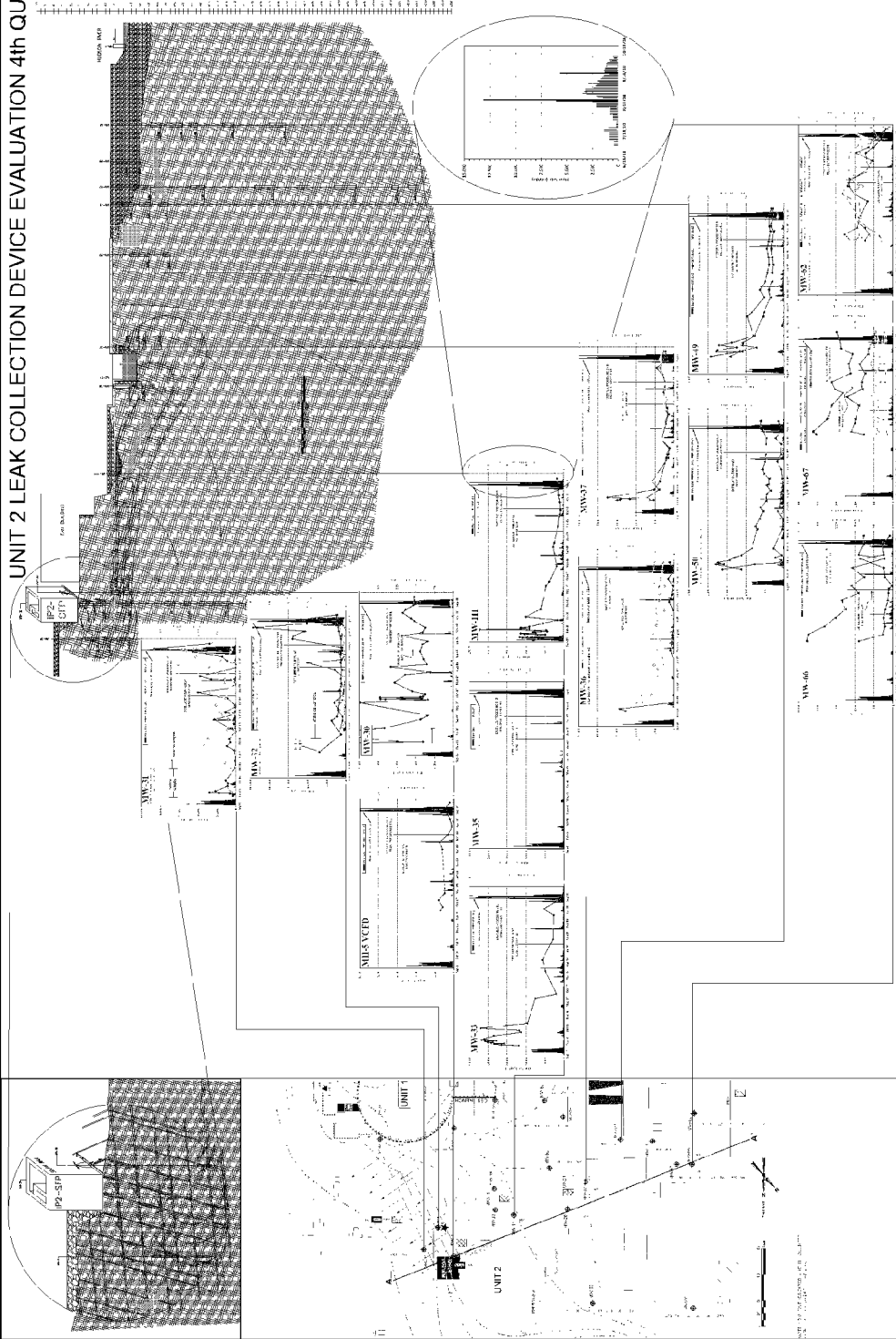


GEOLOGIC MAP OF
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 NEW YORK STATE
 MUSEUM AND
 SCIENCE SERVICE,
 MAP AND CHART
 SERIES NO. 45.

GZA--\\17.000-18.999\17869-92\17869-92\Figures\402010\12-08-20_F03_Lower Hudson Valley Geologic Map 17869-92_FINAL.dwg [F0-3] August 20, 2012 - 4:17pm etoinc.dcn@che



UNIT 2 LEAK COLLECTION DEVICE EVALUATION 4th QUARTER 2010



CROSS SECTION 'A-A'

1. Construction of Unit 2 is in accordance with the approved plans and specifications, and the same shall be maintained throughout the life of the unit.

2. The construction of the Unit 2 shall be in accordance with the approved plans and specifications, and the same shall be maintained throughout the life of the unit.

3. The construction of the Unit 2 shall be in accordance with the approved plans and specifications, and the same shall be maintained throughout the life of the unit.

LEGEND

INDICATED

- 1. Existing Structure
- 2. Proposed Structure
- 3. Proposed Structure to be Demolished
- 4. Proposed Structure to be Relocated
- 5. Proposed Structure to be Expanded
- 6. Proposed Structure to be Contracted
- 7. Proposed Structure to be Repaired
- 8. Proposed Structure to be Replaced
- 9. Proposed Structure to be Relocated
- 10. Proposed Structure to be Expanded
- 11. Proposed Structure to be Contracted
- 12. Proposed Structure to be Repaired
- 13. Proposed Structure to be Replaced

PROBABLE LEAK RELEASE

- 1. Probable Leak Release
- 2. Probable Leak Release
- 3. Probable Leak Release
- 4. Probable Leak Release
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- 6. Probable Leak Release
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- 14. Probable Leak Release
- 15. Probable Leak Release

DATE SPECIFIC DATA

- 1. Date Specific Data
- 2. Date Specific Data
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CONDUIT INTERVAL

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- 15. Conduit Interval

CONDUIT ELECTRICAL DISTANCE

- 1. Conduit Electrical Distance
- 2. Conduit Electrical Distance
- 3. Conduit Electrical Distance
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CONDUIT ELECTRICAL DISTANCE

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CONDUIT ELECTRICAL DISTANCE

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CONDUIT ELECTRICAL DISTANCE

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- 12. Conduit Electrical Distance
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- 14. Conduit Electrical Distance
- 15. Conduit Electrical Distance

UNIT 2 LEAK COLLECTION DEVICE EVALUATION 4th QUARTER 2010

1. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

2. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

3. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

4. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

5. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

6. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

7. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

8. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

9. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

10. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

11. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

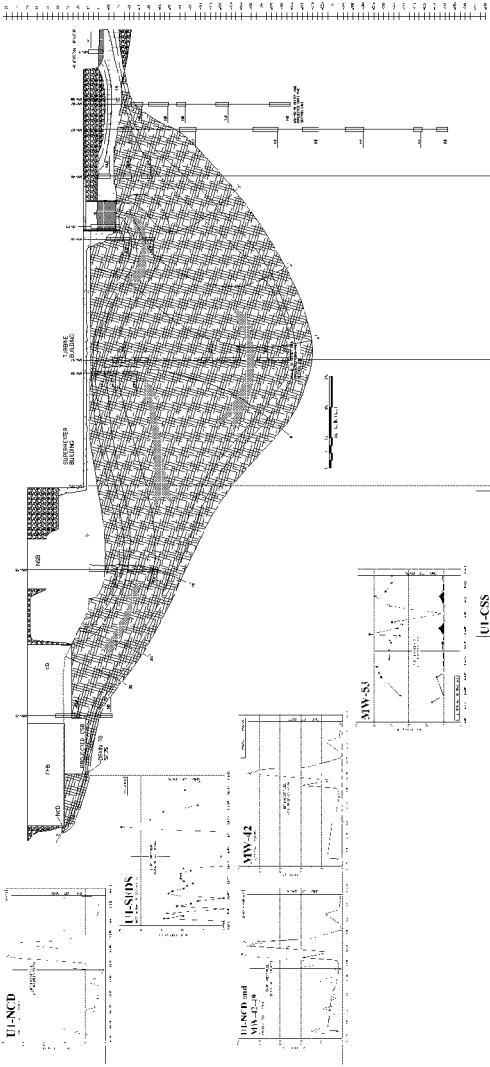
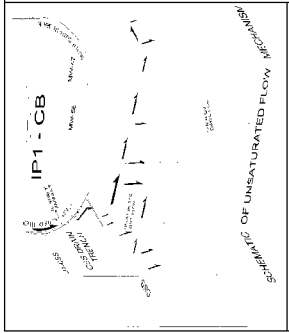
12. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

13. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

14. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

15. Unit 2 Leak Collection Device Evaluation 4th Quarter 2010

Sr-90 BASELINE ANALYSIS - UNIT 1 DEFUELING EVALUATION 4th QUARTER 2010



LEGEND

8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING

ESOPHET PLAN

ESOPHET PLAN

LEGEND

8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING

ESOPHET PLAN

ESOPHET PLAN

LEGEND

8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING

CONTIGUOUS

CONTIGUOUS

ESOPHET PLAN

ESOPHET PLAN

LEGEND

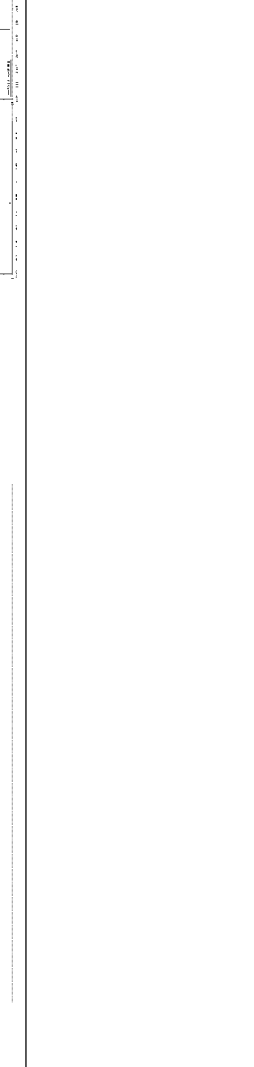
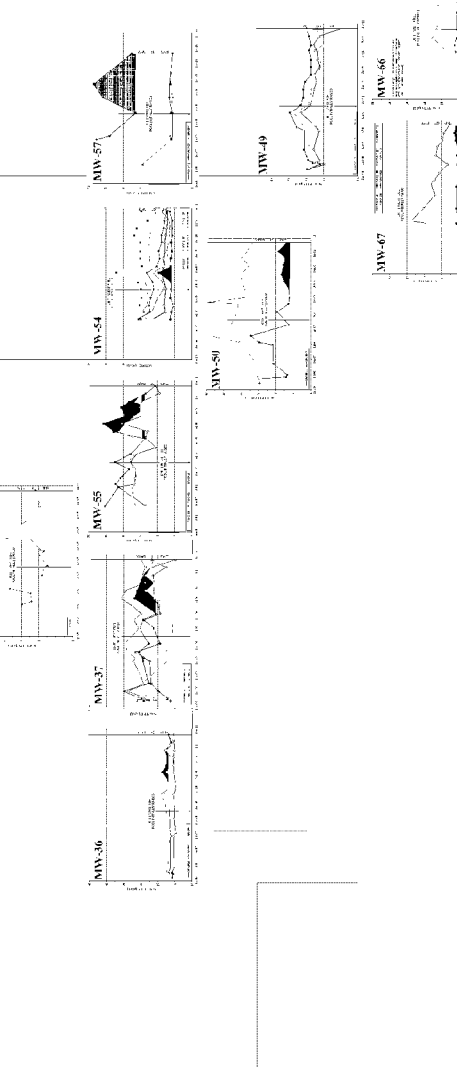
8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING

ESOPHET PLAN

ESOPHET PLAN

LEGEND

8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING
 8.5M DUCT CRASHING



4th QUARTER 2010 ROLLING AVERAGE CESIUM, COBALT, AND NICKEL ACTIVITY MAP

Well ID	Depth (ft)	Cesium (ppm)	Cobalt (ppm)	Nickel (ppm)
...
...
...
...
...
...
...

Well ID	Depth (ft)	Cesium (ppm)	Cobalt (ppm)	Nickel (ppm)
...
...
...
...
...
...
...

Well ID	Depth (ft)	Cesium (ppm)	Cobalt (ppm)	Nickel (ppm)
...
...
...
...
...
...
...

LEGEND

- Long Term Insulation Leaking
- Sunday Feasible for Maintenance Installation
- Active Storm Drain
- Catch Basin
- Flooding Drain

Localized Transient Releases: Surface Spills and Washout

- Unit 1 Fuel Storage Enclosure - 3/07/2008
- Unit 3 Fuel Storage Enclosure - 11/05/2010
- Unit 3 Fuel Storage Enclosure - 11/05/2010
- Unit 3 Fuel Storage Enclosure - 11/05/2010

Probable Latency Release Sites

- All Identified leaks repaired as of December 2010
- Unit 1 Waste Fuel Pool
- Unit 1 Waste Fuel Pool
- Unit 1 Waste Fuel Pool

Depth-Specific Data

- Multiple Transient Releases at Depth
- Latency Release at Depth
- Latency Release at Depth

Cesium Data 1

- Average Co. pp/L
- Series-Specific
- Not Detected (ND)
- ND - 10
- 10 - 50
- 50 - 100
- 100 - 200
- 200 - 300
- 300 - 500
- 500 - 1,000
- 1,000 - 5,000
- 5,000
- > 50C

Cobalt Data 1

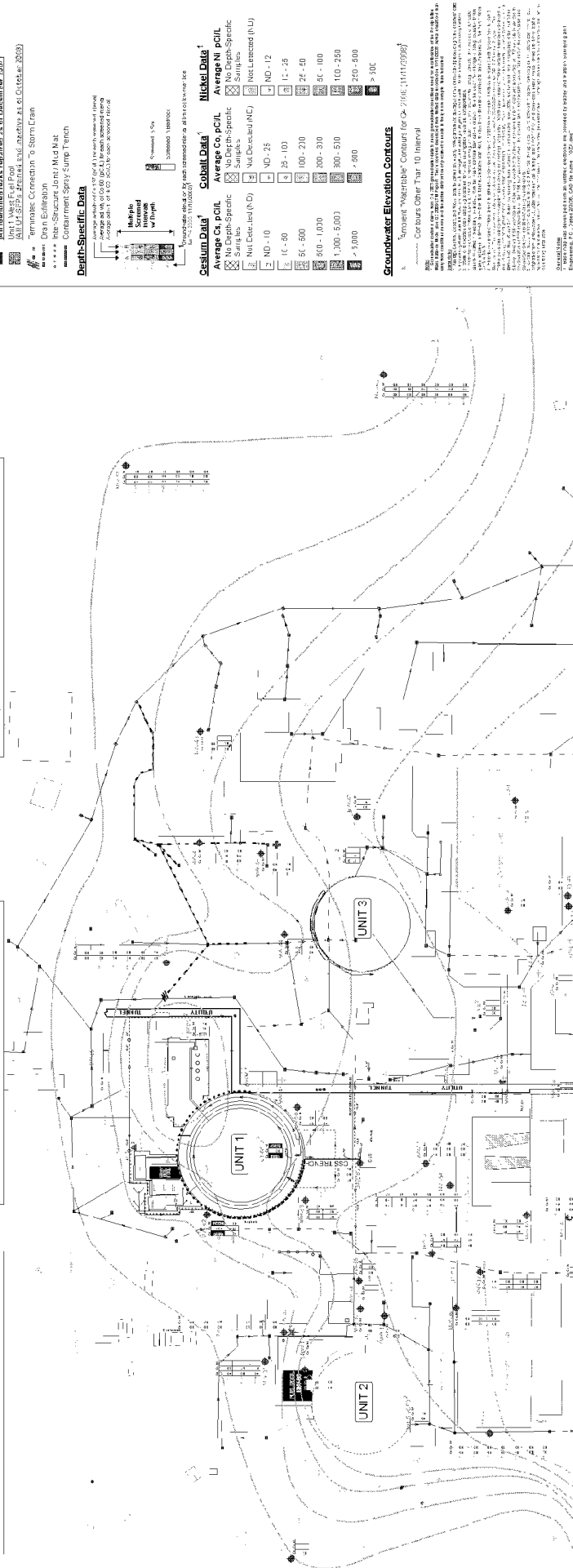
- Average Ni. pp/L
- Series-Specific
- Not Detected (ND)
- ND - 25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 300
- 300 - 500
- 500 - 1,000
- 1,000 - 5,000
- 5,000
- > 50C

Nickel Data 1

- Average Ni. pp/L
- Series-Specific
- Not Detected (ND)
- ND - 12
- 12 - 25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 300
- 300 - 500
- 500 - 1,000
- 1,000 - 5,000
- 5,000
- > 50C

Groundwater Elevation Contours

- Annual "Worstcase" Contour for 04/21/06 (11/11/09) 2
- Contours Other Than 10 Interval



HUDSON RIVER

GZA GeoEnvironmental, Inc.
 1000 Park Avenue
 Suite 400
 New York, NY 10022-1400
 Phone: (212) 261-5000
 Fax: (212) 261-5001

INDIAN POINT ENERGY CENTER
 BUCHANAN, NEW YORK

4th QUARTER 2010 ROLLING AVERAGE
 CESIUM, COBALT, AND NICKEL
 ACTIVITY MAP

Rev. 08-11-2012
 Date of Issue: 08-11-2012
 Drawing No.: D10017898-92
 Scale: 1" = 100'



APPENDIX A: LIMITATIONS

HYDROGEOLOGICAL LIMITATIONS

1. The conclusions and recommendations submitted in this report are based in part upon the radiological, chemical and physical data from water analyses. These data were obtained from specific sampling locations at specific times. The full nature and extent of variations in the data between these specific locations and times are not known. The conditions existing between these specific locations and times have only been inferred using interpolation and extrapolation based on judgment.
2. The subsurface profiles described in the text and presented in the report figures are intended to convey anticipated trends in subsurface conditions. The conditions shown are approximate and generalized and were developed, in part, based on judgment. For specific information at specific locations, refer to the individual subsurface investigation logs.
3. Water level readings (piezometric pressures) have been made in the specific borings, monitoring wells, and Waterloo installations at times and under conditions stated. These data have been reviewed and interpretations have been made in the text and on the figures of this report. However, it must be noted that temporal and spatial fluctuations in the level of the groundwater may occur due to variations in rainfall and other factors different from those prevailing at the time and location measurements were made.
4. Where quantitative laboratory testing has been conducted by an outside laboratory, GZA has relied upon the validity of the data provided, and has not conducted an independent laboratory evaluation of the reliability of these data.
5. Radiological and chemical analyses have been performed for specific parameters during the course of this study, as summarized in the text. Additional constituents not searched for may be present in soil and groundwater at the site.
6. Variations in the types and concentrations of contaminants and variations in their flow paths may occur due to seasonal water table fluctuations, past and current plant operational practices, the passage of time, and other factors. Should additional data (water analyses, water elevations, subsurface deposits, plant construction and operation, etc.) become available in the future, these data should be reviewed by GZA, and the conclusions and recommendations presented herein modified accordingly.
7. This monitoring report was developed by GZA GeoEnvironmental Inc for the exclusive of Entergy Nuclear Northeast (Entergy) at the Indian Point Energy Center. Any use of data or information provided in the report, by parties other than Entergy, is prohibited without the prior written permission of Entergy and GZA.



APPENDIX B: TRANSDUCER INSTALLATION LOGS

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	HR-1#2
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

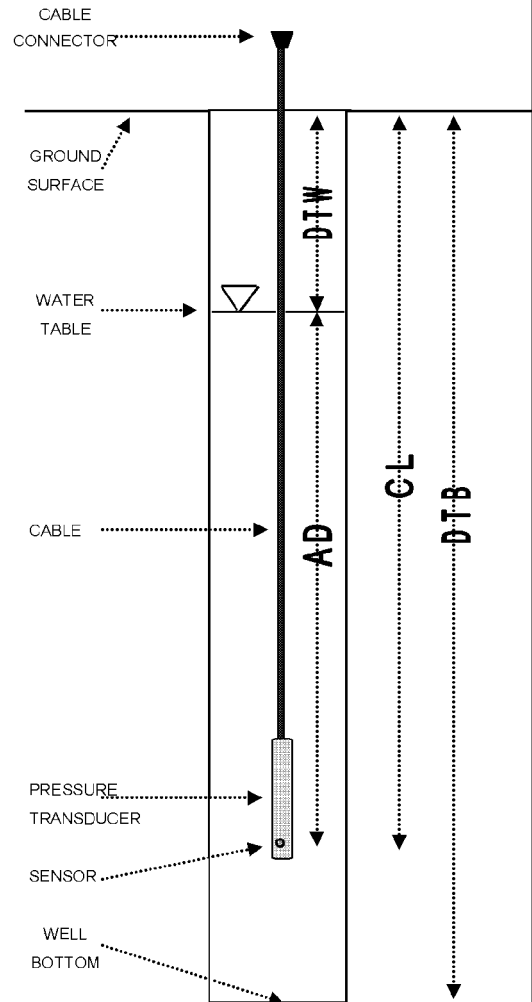
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>--</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.99</u>	DATE	<u>12/8/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.50</u>		
SERIAL NUMBER	<u>9401</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>1.40</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>--</u>	FT
GROUND ELEVATION:	<u>14.99</u>	FT M.S.L.
CASING ELEVATION:	<u>18.50</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.50</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1154</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>17.10</u>	FT
ACTUAL DEPTH:	<u>+</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 17.100</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.50</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 17.10</u>	FT
REFERENCE ELEVATION:	<u>= 1.40</u>	FT M.S.L.
TEST NAME:	<u>HR-1#2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1154</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference -0.071. Ok. No test to download. Reset and start new test. Error in communication. Could not start test.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	HR-1#2
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

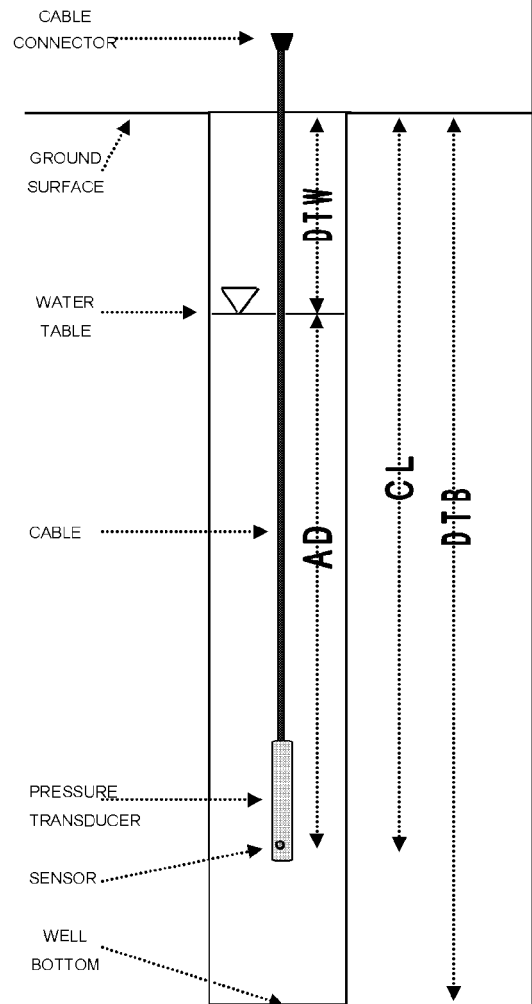
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>--</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.99</u>	DATE	<u>12/3/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.50</u>		
SERIAL NUMBER	<u>9401</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>1.71</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>--</u>	FT
GROUND ELEVATION:	<u>14.99</u>	FT M.S.L.
CASING ELEVATION:	<u>18.50</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.50</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1154</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>16.79</u>	FT
ACTUAL DEPTH:	<u>+ 5.342</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 22.132</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.50</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 16.79</u>	FT
REFERENCE ELEVATION:	<u>= 1.71</u>	FT M.S.L.
TEST NAME:	<u>HR-1#2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1154</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 No connection. Troubleshoot and reconnect.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	Entergy Indian Point Energy Center	WELL ID	I-2n
			SHEET	1 of 1
			FILE NO.	01.0017869.92
			PROJECT LOCATION	Indian Point

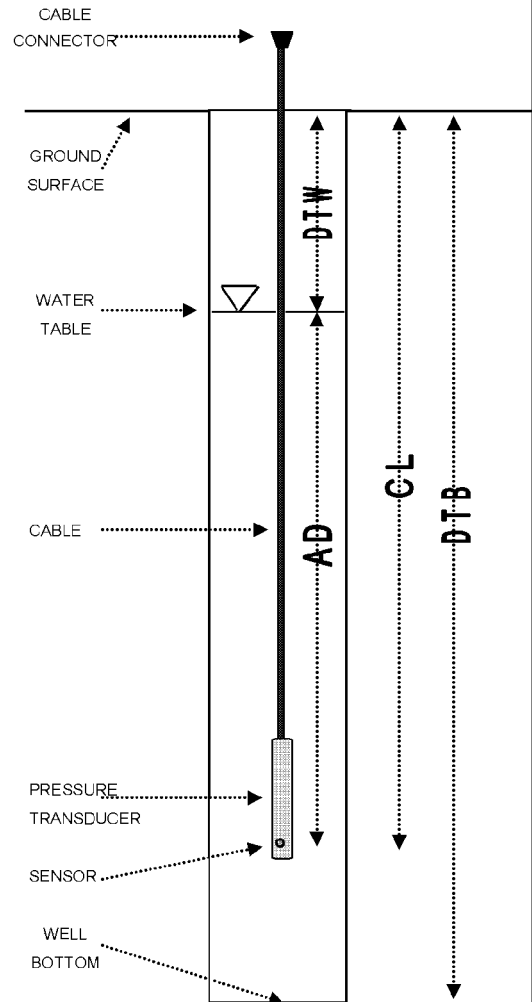
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>41.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>80.92</u>	DATE	<u>11/17/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>82.23</u>		
SERIAL NUMBER	<u>16587</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>50.75</u>
	<u>M Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>41.00</u>	FT
GROUND ELEVATION:	<u>80.92</u>	FT M.S.L.
CASING ELEVATION:	<u>82.23</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>1.31</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1138</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>31.48</u>	FT
ACTUAL DEPTH:	<u>+ 40.729</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 72.209</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>82.23</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 31.48</u>	FT
REFERENCE ELEVATION:	<u>= 50.75</u>	FT M.S.L.
TEST NAME:	<u>I-2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1138</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference -0.721. Reset.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	Entergy Indian Point Energy Center	WELL ID	I-2n
			SHEET	1 of 1
			FILE NO.	01.0017869.92
			PROJECT LOCATION	Indian Point

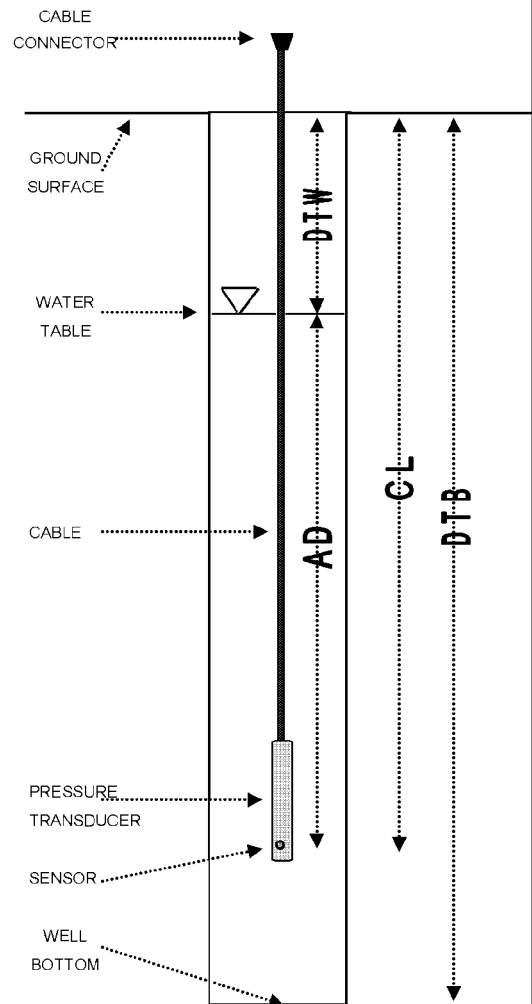
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>41.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>80.92</u>	DATE	<u>12/3/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>82.23</u>		
SERIAL NUMBER	<u>16587</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>52.24</u>
	<u>M Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>41.00</u>	FT
GROUND ELEVATION:	<u>80.92</u>	FT M.S.L.
CASING ELEVATION:	<u>82.23</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>1.31</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1138</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>29.99</u>	FT
ACTUAL DEPTH:	<u>+ 42.713</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 72.703</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>82.23</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 29.99</u>	FT
REFERENCE ELEVATION:	<u>= 52.24</u>	FT M.S.L.
TEST NAME:	<u>I-2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1138</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference -0.499. Reset.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-36-24
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

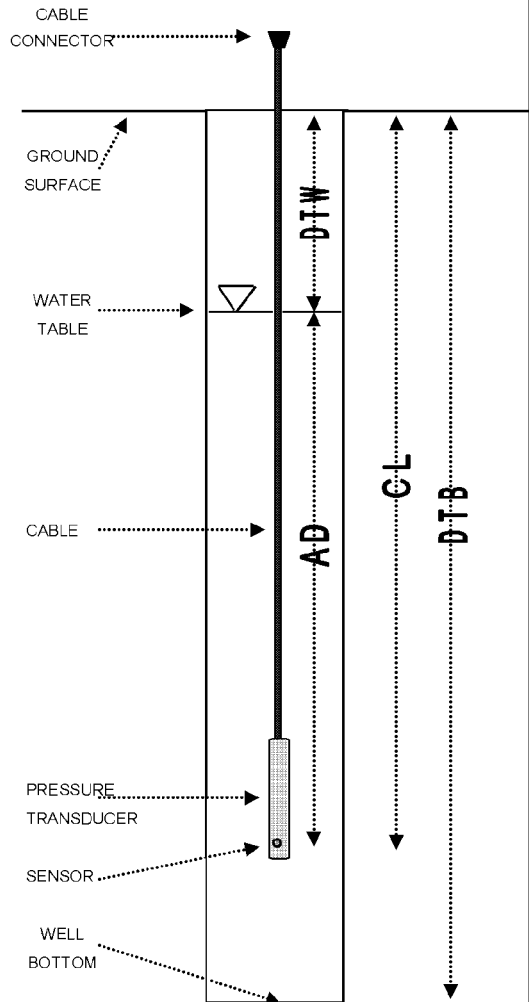
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>54.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>11.799</u>	DATE	<u>11/4/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>11.598</u>		
SERIAL NUMBER	<u>5376</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>6.87</u>
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ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>24.00</u>	FT
GROUND ELEVATION:	<u>11.799</u>	FT M.S.L.
CASING ELEVATION:	<u>11.598</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.201</u>	FT
	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1411</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>4.73</u>	FT
ACTUAL DEPTH:	<u>+ 59.241</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 63.971</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>11.598</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 4.73</u>	FT
REFERENCE ELEVATION:	<u>= 6.868</u>	FT M.S.L.
TEST NAME:	<u>MW-36-24</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1411</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference found -3.103. Reset.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-37-40
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

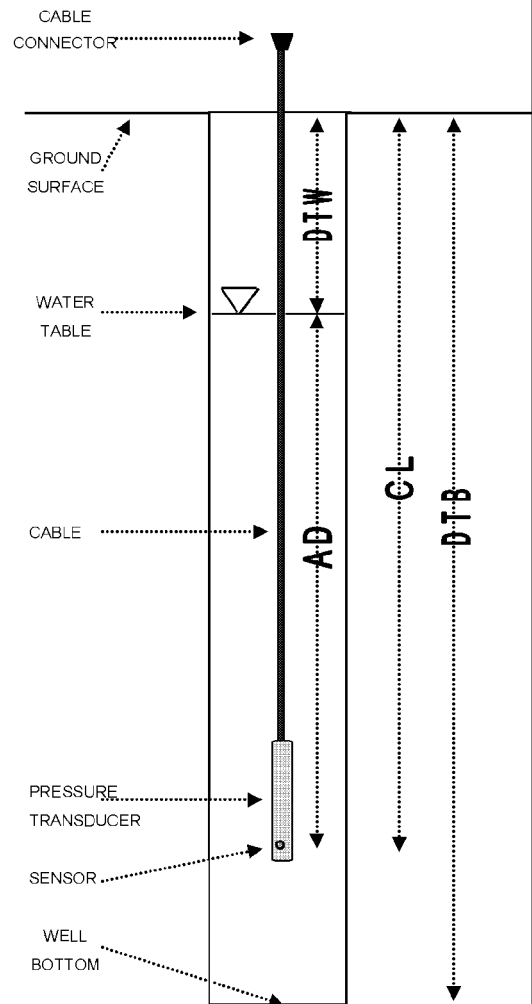
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>57.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>15.021</u>	DATE	<u>11/4/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>14.852</u>		
SERIAL NUMBER	<u>2280</u>	CASING DIAMETER (INCH)	<u>1</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT) *	<u>6.21</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>40.00</u>	FT
GROUND ELEVATION:	<u>15.021</u>	FT M.S.L.
CASING ELEVATION:	<u>14.852</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.169</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1018</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>8.64</u>	*FT
ACTUAL DEPTH:	<u>+</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 8.640</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>14.852</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 8.64</u>	*FT
REFERENCE ELEVATION:	<u>= 6.212</u>	*FT M.S.L.
TEST NAME:	<u>MW-37-40</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1018</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	Entergy Indian Point Energy Center	WELL ID	MW-41-40
			SHEET	1 of 1
			FILE NO.	01.0017869.92
			PROJECT LOCATION	Indian Point

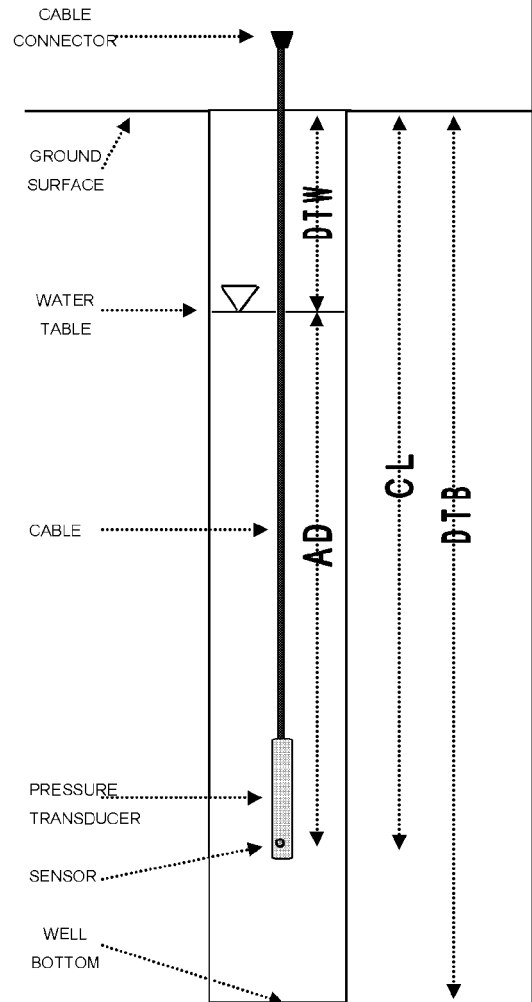
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>64.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>54.87</u>	DATE	<u>10/25/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>54.13</u>		
SERIAL NUMBER		CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>31.02</u>
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ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>40.00</u>		FT	
GROUND ELEVATION:	<u>54.87</u>		FT M.S.L.	
CASING ELEVATION:	<u>54.13</u>		FT M.S.L.	
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>			
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.74</u>		FT	
MEASURED CABLE LENGTH:	<u>--</u>		FT	
TIME OF MEASUREMENT:	<u>1322</u>		HRS	
MEASUREMENT TAKEN FROM:	<u>TOC</u>			
DEPTH TO WATER:	<u>23.11</u>		FT	
ACTUAL DEPTH:	<u>+</u>		FT	
THEORETICAL CABLE LENGTH:	<u>=</u>	<u>23.110</u>		FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>		check	
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>		check	
ELEVATION OF MEASURING POINT:	<u>54.13</u>		FT M.S.L.	
DEPTH TO WATER:	<u>-</u>	<u>23.11</u>		FT
REFERENCE ELEVATION:	<u>=</u>	<u>31.02</u>		FT M.S.L.
TEST NAME:	<u>MW-41-40</u>			
LOGGING INTERVAL:	<u>20</u>		MIN	
TEST START TIME:	<u>1322</u>		HRS	



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-43-28
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

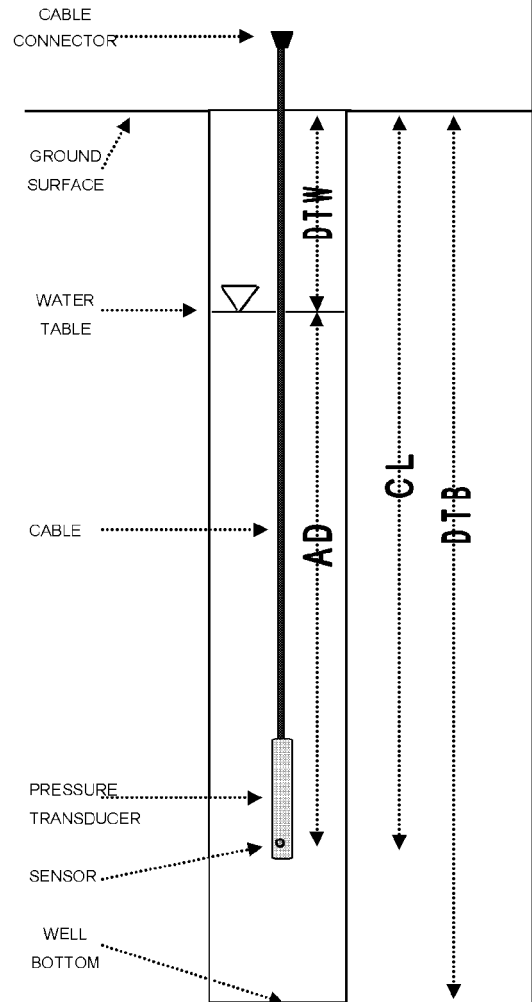
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>63.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>48.760</u>	DATE	<u>10/25/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>48.021</u>		
SERIAL NUMBER	<u>11331</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>32.58</u>
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ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>28.00</u>	FT
GROUND ELEVATION:	<u>48.760</u>	FT M.S.L.
CASING ELEVATION:	<u>48.021</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.739</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>09:11</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>15.44</u>	FT
ACTUAL DEPTH:	<u>+ 25.838</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 41.278</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>48.021</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 15.44</u>	FT
REFERENCE ELEVATION:	<u>= 32.581</u>	FT M.S.L.
TEST NAME:	<u>MW-43-28</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>09:11</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-43-28
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

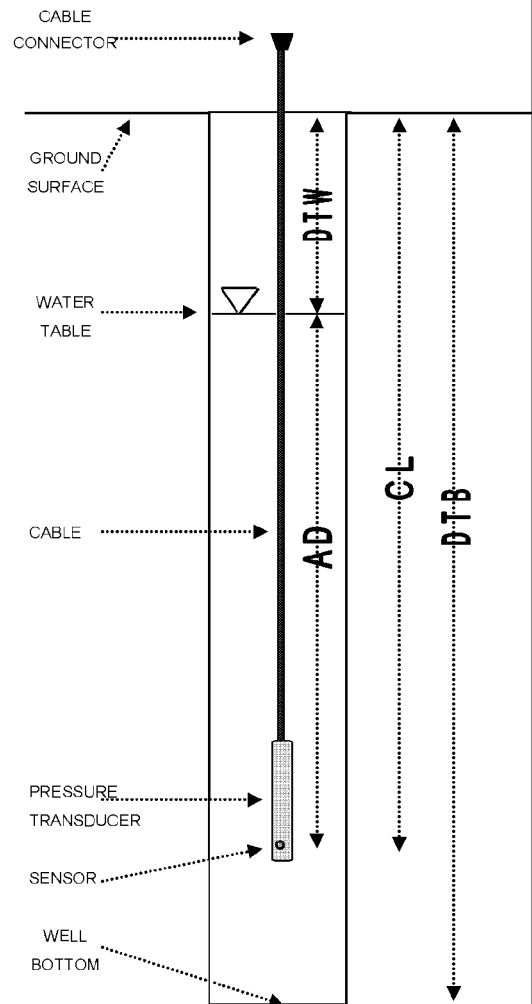
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>63.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>48.760</u>	DATE	<u>12/13/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>48.021</u>		
SERIAL NUMBER	<u>11331</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>33.25</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>28.00</u>	FT
GROUND ELEVATION:	<u>48.760</u>	FT M.S.L.
CASING ELEVATION:	<u>48.021</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.739</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1154</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>14.77</u>	FT
ACTUAL DEPTH:	<u>+ 25.840</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 40.610</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>48.021</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 14.77</u>	FT
REFERENCE ELEVATION:	<u>= 33.251</u>	FT M.S.L.
TEST NAME:	<u>MW-43-28</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1154</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference -0.772. Reset.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-50-66
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

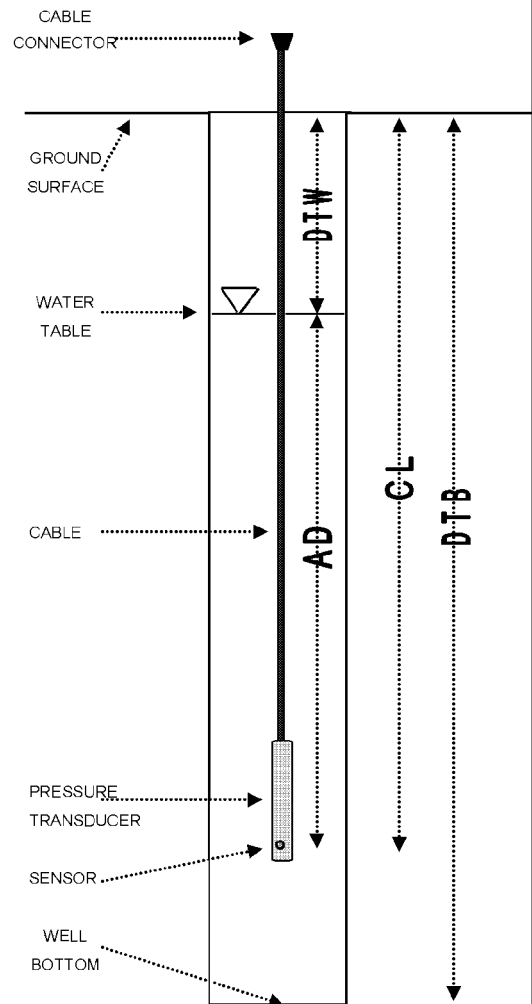
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>67.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.92</u>	DATE	<u>11/12/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>14.61</u>		
SERIAL NUMBER	<u>14459</u>	CASING DIAMETER (INCH)	<u>1</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>4.02</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>65.75</u>	FT
GROUND ELEVATION:	<u>14.92</u>	FT M.S.L.
CASING ELEVATION:	<u>14.61</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.31</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:		HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>10.59</u>	FT
ACTUAL DEPTH:	<u>+</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 10.590</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>14.614</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 10.59</u>	FT
REFERENCE ELEVATION:	<u>= 4.024</u>	FT M.S.L.
TEST NAME:	<u>MW-50-66</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:		HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-58-65
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

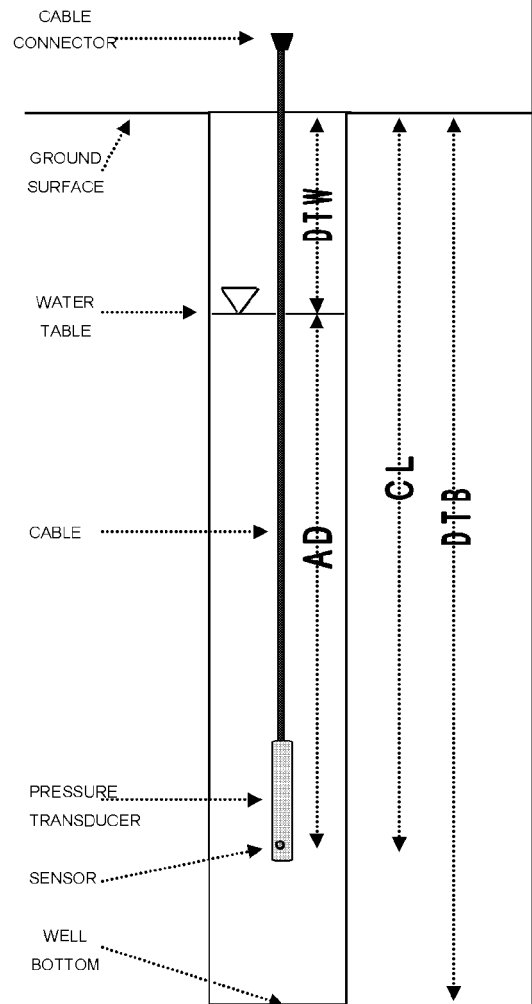
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>72.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.57</u>	DATE	<u>11/11/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>14.25</u>		
SERIAL NUMBER	<u>5619</u>	CASING DIAMETER (INCH)	<u>1</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>7.04</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>65.00</u>	FT
GROUND ELEVATION:	<u>14.57</u>	FT M.S.L.
CASING ELEVATION:	<u>14.25</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.32</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:		HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>7.21</u>	FT
ACTUAL DEPTH:	<u>+</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 7.210</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>14.25</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 7.21</u>	FT
REFERENCE ELEVATION:	<u>= 7.04</u>	FT M.S.L.
TEST NAME:	<u>MW-58-65</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:		HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Off by -0.574. Reset.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-66-21
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

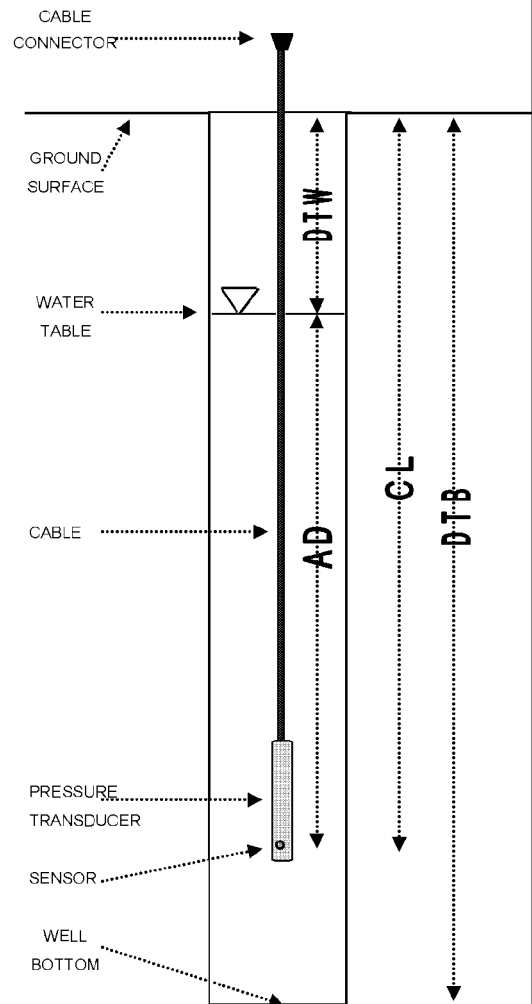
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>37.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.122</u>	DATE	<u>11/10/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>13.407</u>		
SERIAL NUMBER	<u>15849</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>0.74</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>21.00</u>	FT
GROUND ELEVATION:	<u>14.122</u>	FT M.S.L.
CASING ELEVATION:	<u>13.407</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.72</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1004</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>12.67</u>	FT
ACTUAL DEPTH:	<u>+ 9.83</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 22.50</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>13.407</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 12.67</u>	FT
REFERENCE ELEVATION:	<u>= 0.737</u>	FT M.S.L.
TEST NAME:	<u>MW-66-21</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1004</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	U3-C1-2
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
	PROJECT LOCATION		Indian Point

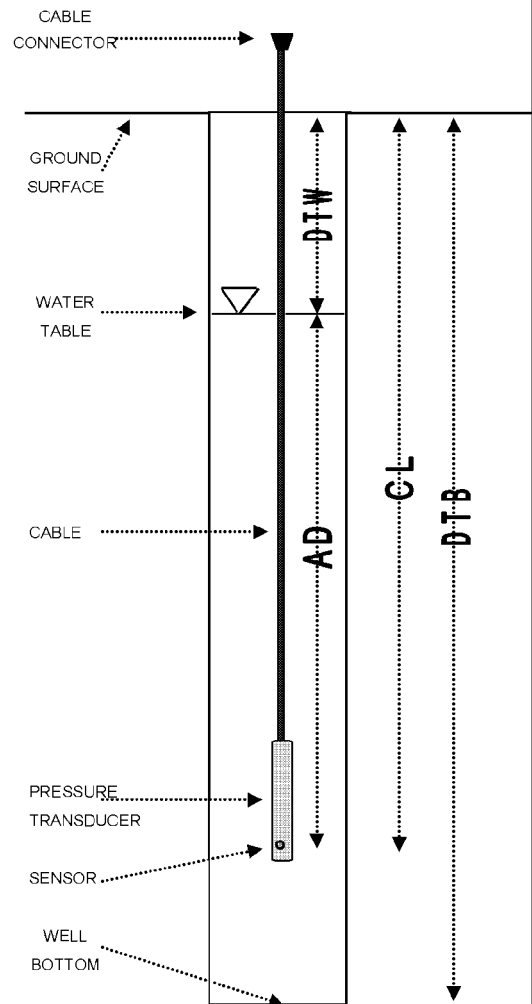
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>NA</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>15.003</u>	DATE	<u>12/6/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.060</u>		
SERIAL NUMBER	<u>11949</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>3.16</u>
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ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>NA</u>	FT
GROUND ELEVATION:	<u>15.003</u>	FT M.S.L.
CASING ELEVATION:	<u>18.060</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.057</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1425</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>14.90</u>	FT
ACTUAL DEPTH:	<u>+ -17.471</u>	FT
THEORETICAL CABLE LENGTH:	<u>= -2.571</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.060</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 14.90</u>	FT
REFERENCE ELEVATION:	<u>= 3.160</u>	FT M.S.L.
TEST NAME:	<u>U3-C1-2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1425</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Reset and clean. Difference > 17.

TRANSDUCER INSTALLATION LOG

GZA GEOENVIRONMENTAL OF NEW YORK 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	U3-C1
	Energy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

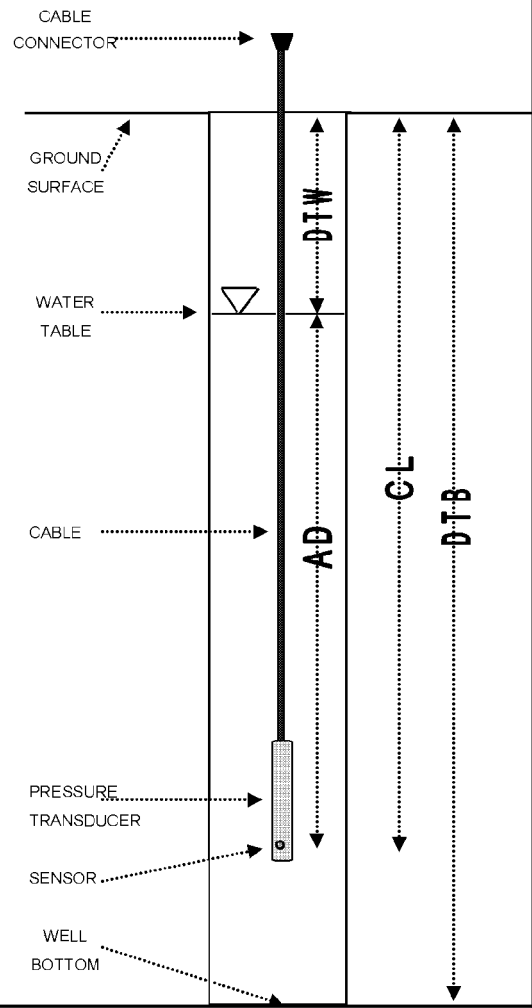
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>NA</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>15.003</u>	DATE	<u>12/6/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.060</u>		
SERIAL NUMBER	<u>5548</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>3.46</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>NA</u>	FT
GROUND ELEVATION:	<u>15.003</u>	FT M.S.L.
CASING ELEVATION:	<u>18.060</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.057</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>1405</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>14.60</u>	FT
ACTUAL DEPTH:	<u>+ 13.622</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 28.222</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.060</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 14.60</u>	FT
REFERENCE ELEVATION:	<u>= 3.460</u>	FT M.S.L.
TEST NAME:	<u>U3-C1</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>1405</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER
DTB - DEPTH TO BOTTOM OF WELL
AD - ACTUAL DEPTH OF TRANSDUCER UNDER WATER
CL - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:
 Difference -2.379. Reset.
 Transducer reading = 3.436
 Reference Elevation = 3.622
 Difference of 0.186 at time of programming due to water level change. Cleaned transducer.

GZA	WELL ID:	U3-C1
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APPENDIX C: CHAINS OF CUSTODY

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Project #: 50013510
 GEL Quote #: 50013510
 CUR Number: 50013510
 PO Number:

Client Name: Entergy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue

Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)

Sample ID	Matrix	Volume	TSCA Regulated	Should this sample be considered:	Sample Analysis Requested (5)						Preservative Type (6)	Comments
					Gamma Spec (GS)	Tritium (H3)	Strontium 90 (S90)	Other	Other	Other		
MW-45-42-(022)	GW	2 Liter Poly	Y	N	1	1	1	1	1	1	1	Note: extra sample is required for sample specific QC
MW-45-61-(022)	GW	2 Liter Poly	Y	N	1	1	1	1	1	1	1	

TAT Required: Normal Rush Specify: _____ Subject to surcharge: Yes No Fax Results: Yes No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<i>[Signature]</i>	10/22/10	1550	<i>[Signature]</i>	10/22/10	1550

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped:
 Airbill #:
 Airbill #:

1. Chain of Custody Number: _____
 2. QC Codes: N = Normal Sample, EB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSB = Matrix Spike Duplicate, Samp, G = Grab, C = Composite
 3. Field Filtered: For liquid matrices, indicate with "Y" for yes the sample was field filtered or "N" for no. For solids, indicate with "Y" for yes the sample was field filtered or "N" for no. For samples that were not field filtered.
 4. Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Miss Liquid, SQ=Soil, SD=Soil, SS=Soil, SL=Soil, SS=Soil, SW=Soil, SF=Soil, N=Soil
 5. Sample Analysis Requested: Analytical method requested (i.e. 6260B, 6040B/7290A) and number of containers provided for each (i.e. 6260B - 3, 6040B/7290A - 1).
 6. Preservative Type: BA = Hydrochloric Acid, N1 = Nitric Acid, SR = Sodium Hydroxide, SA = Acetic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added, leave field blank.
WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT

For Lab Receiving Use Only
 Custody Seal Intact?
 YES NO
 Cooler Temp: _____ C

Page: 1 of 1
 Project #: Energy GW Mon Prog
 GEL Quote #:
 CUC Number: 50013510
 PO Number: 50013510

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Client Name: Entergy
 Project/Site Name: Indian Point Energy Center
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Phone #: (914) 736-8405
 Fax #: (914) 734-6247

Collected by: CB, NB
 Send Results To: Patrick Donahue

Sample ID
 * For changes, indicate start and stop date/time

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military (UTC))	QC Code	Field Filtered	Sample Matrix
MW-43-28-(017)	10/25/10	1129	N	N	GW
MW-43-62-(017)	10/25/10	1106	N	N	GW

Total number of containers considered:	Should this sample be considered:	Sample Analysis Requested ¹⁵ (Fill in the number of containers for each test)		Preservative Type (6)	Comments Note: extra sample is required for sample specific QC
		TSCA Regulated	Radionuclide		
1	Y	1	1		2 Liter Poly
1	Y	1	1		2 Liter Poly

TAT Requested: Normal Rush: Specify: _____ Fax Results: Yes No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards
 Sample Collection Time Zone: Eastern Pacific Other _____
 Mountain

Chain of Custody Signatures
 Received by (signed) _____ Date _____ Time _____
 GEL PM: ERIN TRENT

Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____

Airbill #: _____

For Lab Receiving Use Only
 Chain of Custody Initiated? YES NO
 Cooler Temp: _____ C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a - F - for gas the sample was field filtered; for solids the sample was not field filtered.
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, M = Misc. Liquid, SL = Sediment, SI = Sludge, SS = Solid Waste, OS = Oil, F-File, F-Wipe, U=Line, F=Feed, N=Nod
 5) Sample Analysis Requested: Analytical method requested (e.g. 8200B, 601007/100A) and number of containers provided for each (e.g. 4200B - 2, 601007/100A - 1).
 6) Preservative Type: HA = Hydrochloric Acid, NA = Nitric Acid, SD = Sodium Phosphate, SA = Sulfuric Acid, AA = Ascorbic Acid, BX = Benzene, ST = Sodium Thiosulfate, if no preservative is added = leave field blank
 WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Project #: Energy GW Mon Prog
 G.L. Quote #: _____
 CUR Number: 50013510
 PO Number: _____

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue

Sample ID: _____
 * For estimates, indicate start and stop date/time

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered	Sample Matrix
MW-42-49-(023)	10/27/10	1223	N	N	GW
MW-42-78-(018)	10/27/10	1356	N	N	GW

Sample Analysis Requested ¹⁵⁾ (Fill in the number of containers for each test)	← Preservative Type (6)	Comments	Total number of containers						
			Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Should this sample be considered:	Radioactive	
		Note: extra sample is required for sample specific QC	1	1	1	1	1	Y	N
		2 Liter Poly	1	1	1	1	1	Y	N
		2 Liter Poly							

TAT Requested: Normal / Rush Specify: _____ Subject to recharge: _____ Fax Results: Yes / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures				Sample Shipping and Delivery Details	
Retinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<u>Curry</u>	<u>10/27/10</u>	<u>1450</u>	<u>ERIN TRENT</u>	<u>10/27/10</u>	<u>1650</u>

Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only
 Correctly Seal Inact? NO
 Cooler Temp: C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, EB = Trip Blank, FD = Field Duplicate, MS = Matrix Spike Sample, MSB = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid samples, indicate with a - F - for yes the sample was field filtered or - N - for sample was not field filtered.
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, ML = Misc Liquid, SO = Soil, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Filter, P = Wipe, U = Urine, F = Fecal, N = Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 6200B, 6010B/4700A) and number of containers provided for each (i.e. 5200B - 3, 6010B/4700A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SB = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added, leave field blank.
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Page: 1 of 1
Project #: Energy GW Mon Prog
GEL Quote #: _____
COC Number: 50013510
PO Number: _____

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Client Name: Energy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB

Send Results To: Patrick Donahue

Sample ID

* For composites - indicate start and stop date/time

U3-4D-(026)

Date Collected
(mm-dd-yy)

*Time Collected
(Military)
(hh:mm)

QC Code
(a)

Field Filtered
(b)

Sample Matrix
(c)

Radon

Should this sample be considered:

TSCA Regulated

Total number of containers

Gamma Spec (GS)

Tritium (H3)

Strontium 90 (Sr90)

Preservative Type (6)

Comments

Note: extra sample is required for sample specific QC

2 Liter Poly

Sample Analysis Requested⁽⁵⁾ (Fill in the number of containers for each test)

TAT Requested: Normal: Rush: _____ Specify: _____ Subject to Surcharge: _____ Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Sample Collection Time Zone

Eastern
 Pacific
 Central
 Mountain

Chain of Custody Signatures

Sample Shipping and Delivery Details

Received By (Signed) _____ Date _____ Time _____

Received by (signed) _____ Date _____ Time _____

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Date Shipped: _____

Airbill #: _____

Airbill #: _____

Airbill #: _____

Airbill #: _____

1. Chain of Custody Number a Client Determined

2. QC Codes: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite

3. Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered

4. Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc. Liquid, SO = Soil, SD = Solid Waste, O = Oil, F = Filter, F = Wipe, U = Urine, F = Fecal, N = Nasal

5. Sample Analysis Requested: Analytical method requested (i.e. 8260B, 8010B, 7700A) and number of containers provided for each (i.e. 8260B 3, 6010B 7, 7700A 1)

6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY

YELLOW = FILE

PINK = CLIENT

For Lab Receiving Use Only

Correctly Seal Hazard?

YES NO

Cooler Temp:

C

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Sample Analysis Requested ⁽⁵⁾, (Fill in the number of containers for each test)

Phone #: (914) 736-8405

Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue

Sample ID

* For composite - indicate start and stop date/time

MW-46-(022)

Date Collected (mm-dd-yy)

*Time Collected (Military) (hh:mm)

QC Code

Field Filtered ⁽⁴⁾

Sample Matrix ⁽⁶⁾

Should this sample be considered:

Radiactive

TSCA Regulated

Total number of containers

Tritium (H3)

Gamma Spec (GS)

Strontium 90 (Sr90)

← Preservative Type (6)

Comments
 Note: extra sample is required for sample specific QC

2 Liter Poly

TAT Requested: Normal Rush: _____ Specify: _____ (Subject to charges) Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Sample Collection Time Zone
 Eastern
 Pacific
 Other _____
 Mountain

Chain of Custody Signatures

Sample Shipping and Delivery Details

Relinquished By (Signed) _____ Date _____ Time _____

Received by (signed) _____ Date _____ Time _____

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Date Shipped: _____

Airbill #: _____

Airbill #: _____

1) Chain of Custody Number = Client Determined

2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite

3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered

4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SD=Soil, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Feet, N=Nasal

5) Sample Analysis Requested: Analytical method required (i.e. 8260B, 8010B, 7170A) and number of containers provided for each (i.e. 8260B 3, 8010B/7170A - 1)

6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, RX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY

PINK = CLIENT

For Lab Receiving Use Only

Custody Seal intact?

YES NO

Cooler Temp: _____

C

Page: 1 of 1
 Project # Enterdy GW Mon Prog
 GEL Quote # _____
 COC Number (1): _____
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Client Name: Enterdy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CLMB

Send Results To: Patrick Donahue

Sample Analysis Requested (6) (Fill in the number of containers for each test)

Sample ID	*Date Collected (mm-dd-yy)	Time Collected (Military)	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:		Total number of containers	Preservative Type (6)	Comments
						Radioactive	TSCA Regulated			
U3-T1-(030)	10/29/10	1604	N	N	GW	Y	N	1		2 Liter Poly
U3-T2-(035)	10/29/10	1122	N	N	GW	Y	N	1		2 Liter Poly

TAT Requested: Normal Rush _____ Specify: (Subject to Surcharges) Fax Results: Yes / No No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone
 Eastern Pacific Other _____
 Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

TAT Requested: Normal Rush _____ Specify: (Subject to Surcharges) Fax Results: Yes / No No

Chain of Custody Signatures		Sample Shipping and Delivery Details	
Relinquished By (Signed)	Date	Time	Date
<u>Erin Trent</u>	10/29/10	1630	10/29/10 1630

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only
 Custody Seal intact? YES / NO
 Cooler Temp: _____

1. Chain of Custody Number = Client Determined
 2. QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, ER = Equipment Blank, MS = Matrix Spike Duplicate Sample, C = Grab, C = Composite
 3. Field Filtered: For liquid matrices, indicate with a - F - for yes the sample was field filtered or - N - for no sample was not field filtered.
 4. Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Mixture Liquid, SO = Soil, SD = Solid Waste, G=Oil, F=Filter, P=W per, U=Urine, F=Feces, N=Nasal
 5. Sample Analysis Requested: Analytical methods requested (i.e. 8240B, 8610B, 8700A) and number of containers provided for each (i.e. 8240B - 3, 6010B/7470A - 1).
 6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank.
WHITE = LABORATORY
PINK = CLIENT
YELLOW = FILE

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Project #: Entergy GW Mon Prog
 GEL Quote #: _____
 COC Number (1): _____
 PO Number: 50013510
 GEL Work Order Number: _____
 See www.gel.com for GEL's Sample Acceptance SOP

Client Name: <u>Entergy</u>		Phone #: <u>(914) 736-8405</u>		Sample Analysis Requested (5) (Fill in the number of containers for each test)		← Preservative Type (6)	
Project/Site Name: <u>Indian Point Energy Center</u>		Fax #: <u>(914) 734-6247</u>					
Address: <u>450 Broadway, Suite 3, Buchanan, NY 10511</u>		Send Results To: <u>Patrick Donahue</u>		Total number of containers		Comments Note: extra sample is required for sample specific QC	
Collected by: <u>CB, MB</u>							
Sample ID MW-111-(035)		Date Collected <u>11/01/10 1455</u>		Time Collected (Military) (hh:mm) <u>1455</u>		Should this sample be considered:	
		QC Code (5) <u>N</u>		Field Filtered (6) <u>N</u>			
Sample Matrix (6) <u>GW</u>		Radioactive <u>Y</u>		Tritium (H3) <u>1</u>		Gamma Spec (GS) <u>1</u>	
Strontium 90 (Sr90) <u>1</u>		Iodine 131 (I131) <u>1</u>		Cesium 137 (Cs137) <u>1</u>		Plutonium 239 (Pu239) <u>1</u>	
Americium 241 (Am241) <u>1</u>		Uranium 235 (U235) <u>1</u>		Uranium 238 (U238) <u>1</u>		Thorium 232 (Th232) <u>1</u>	
Radium 226 (Ra226) <u>1</u>		Potassium 40 (K40) <u>1</u>		Sodium 22 (Na22) <u>1</u>		Chlorine 36 (Cl36) <u>1</u>	
Argon 41 (Ar41) <u>1</u>		Calcium 45 (Ca45) <u>1</u>		Scandium 46 (Sc46) <u>1</u>		Vanadium 51 (V51) <u>1</u>	
Chromium 51 (Cr51) <u>1</u>		Manganese 54 (Mn54) <u>1</u>		Cobalt 60 (Co60) <u>1</u>		Nickel 63 (Ni63) <u>1</u>	
Zinc 65 (Zn65) <u>1</u>		Gallium 67 (Ga67) <u>1</u>		Germanium 76 (Ge76) <u>1</u>		Selenium 75 (Se75) <u>1</u>	
Bromine 82 (Br82) <u>1</u>		Krypton 81 (Kr81) <u>1</u>		Rubidium 87 (Rb87) <u>1</u>		Strontium 90 (Sr90) <u>1</u>	
Yttrium 90 (Y90) <u>1</u>		Zirconium 95 (Zr95) <u>1</u>		Niobium 94 (Nb94) <u>1</u>		Molybdenum 99 (Mo99) <u>1</u>	
Technetium 99 (Tc99) <u>1</u>		Ruthenium 106 (Ru106) <u>1</u>		Rhodium 105 (Rh105) <u>1</u>		Palladium 103 (Pd103) <u>1</u>	
Silver 110 (Ag110) <u>1</u>		Cadmium 115 (Cd115) <u>1</u>		Indium 115 (In115) <u>1</u>		Tin 113 (Sn113) <u>1</u>	
Antimony 124 (Sb124) <u>1</u>		Tellurium 132 (Te132) <u>1</u>		Iodine 131 (I131) <u>1</u>		Xenon 135 (Xe135) <u>1</u>	
Barium 137 (Ba137) <u>1</u>		Lanthanum 139 (La139) <u>1</u>		Cerium 140 (Ce140) <u>1</u>		Praseodymium 141 (Pr141) <u>1</u>	
Neodymium 147 (Nd147) <u>1</u>		Promethium 147 (Pm147) <u>1</u>		Samarium 152 (Sm152) <u>1</u>		Europium 152 (Eu152) <u>1</u>	
Gadolinium 153 (Gd153) <u>1</u>		Terbium 159 (Tb159) <u>1</u>		Dysprosium 165 (Dy165) <u>1</u>		Holmium 165 (Ho165) <u>1</u>	
Erbium 167 (Er167) <u>1</u>		Thulium 170 (Tm170) <u>1</u>		Ytterbium 177 (Yb177) <u>1</u>		Lutetium 177 (Lu177) <u>1</u>	
Hafnium 182 (Hf182) <u>1</u>		Tantalum 182 (Ta182) <u>1</u>		Tungsten 187 (W187) <u>1</u>		Rhenium 187 (Re187) <u>1</u>	
Osmium 192 (Os192) <u>1</u>		Iridium 192 (Ir192) <u>1</u>		Platinum 198 (Pt198) <u>1</u>		Gold 197 (Au197) <u>1</u>	
Mercury 201 (Hg201) <u>1</u>		Thallium 205 (Tl205) <u>1</u>		Lead 206 (Pb206) <u>1</u>		Bismuth 209 (Bi209) <u>1</u>	
Polonium 210 (Po210) <u>1</u>		Astatine 210 (At210) <u>1</u>		Radon 222 (Rn222) <u>1</u>		Francium 223 (Fr223) <u>1</u>	
Radium 226 (Ra226) <u>1</u>		Actinium 227 (Ac227) <u>1</u>		Thorium 232 (Th232) <u>1</u>		Protactinium 231 (Pa231) <u>1</u>	
Uranium 235 (U235) <u>1</u>		Neptunium 237 (Np237) <u>1</u>		Plutonium 239 (Pu239) <u>1</u>		Americium 241 (Am241) <u>1</u>	
Curium 244 (Cm244) <u>1</u>		Berkelium 247 (Bk247) <u>1</u>		Californium 251 (Cf251) <u>1</u>		Einsteinium 252 (Es252) <u>1</u>	
Fermium 257 (Fm257) <u>1</u>		Mendelevium 258 (Md258) <u>1</u>		Nobelium 259 (No259) <u>1</u>		Lawrencium 260 (Lr260) <u>1</u>	
Rutherfordium 261 (Rf261) <u>1</u>		Dubnium 262 (Db262) <u>1</u>		Seaborgium 266 (Sg266) <u>1</u>		Bohrium 264 (Bh264) <u>1</u>	
Hassium 277 (Hs277) <u>1</u>		Meitnerium 276 (Mt276) <u>1</u>		Darmstadtium 281 (Ds281) <u>1</u>		Roentgenium 280 (Rg280) <u>1</u>	
Copernicium 285 (Cn285) <u>1</u>		Nihonium 286 (Nh286) <u>1</u>		Flerovium 289 (Fl289) <u>1</u>		Tennessine 288 (Ts288) <u>1</u>	
Oganesson 294 (Og294) <u>1</u>		Unlabeled <u>1</u>		Unlabeled <u>1</u>		Unlabeled <u>1</u>	

TAT Requested: Normal Rush: _____ Specify: _____
 Submit to: Subcontractor: _____ Fax Results: Yes / No /
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zones
 Eastern Pacific Other _____
 Mountain

Chain of Custody Signatures

Relinquished By (Signed) Date: <u>11/01/10</u> Time: <u>1530</u>	Received by (Signed) ERIN TRENT Date: <u>11/01/10</u> Time: <u>1530</u>
Method of Shipment: <u>FEDEX</u>	Date Shipped: _____
Airbill #: _____	Airbill #: _____

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

1.) Chain of Custody Number = Client Determined
 2.) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MD = Matrix Spike Sample, MSD = Matrix Spike Duplicate, Sample, G = Grab, C = Composite
 3.) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for sample was not field filtered
 4.) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, ML=Misc. Liquid, SO=Soil, SD=Sediment, SL=Sludge, SS=Solid Waste, O=Oil, F=Fuel, P=Wipe, Ua/Umc, P/F/FCal, N/Nasal
 5.) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/7170A) and number of containers requested for each (i.e. 8260B - 3, 6010B/7170A - 1)
 6.) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

For Lab Receiving Use Only
 Custody Seal Intact?
 YES / NO
 Cooler Temp:
 _____ C

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:
 Phone #: (914) 736-8405
 Fax #: (914) 734-6247

Project #: Energy GW Mon Prog
 GEL Quote #: _____
 COC Number (1): 50013510
 PO Number: _____

Client Name: Entergy
 Project/Site Name: Indian Point Energy Center
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Sample ID: MW-55-24-(016)
MW-55-35-(015)
MW-55-54-(016)

Sample Analysis Requested (5) (Fill in the number of containers for each test)

Sample ID	Tritium (H3)	Gamma Spec (SS)	Sr-90 (Sr90)	Nickel 63 (Ni63)	Preservative Type (6)
MW-55-24-(016)	1	1	1	1	
MW-55-35-(015)	1	1	1	1	
MW-55-54-(016)	1	1	1	1	

Comments:
 Note: extra sample is required for sample specific QC

Sample ID	Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code (2)	Field Filtered (3)	Sample Matrix (4)	Should this sample be considered:	Total number of containers
MW-55-24-(016)	11/01/10	1410	N	N	GW	Radioactive TSCA Regulated	1
MW-55-35-(015)	11/01/10	1426	N	N	GW		1
MW-55-54-(016)	11/01/10	1336	N	N	GW		1

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Mountain Other

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<i>[Signature]</i>	11/01/10	1530	ERIN TRENT	11/01/10	1530

Method of Shipment: FEDEX
 Date Shipped:
 Airbill #:
 Airbill #:

For Lab Receiving Use Only
 Custody Seal Intact?
 YES NO
 Cooler Temp:
 C

1 - Chain of Custody Number = Client Determined
 2 - QC Code: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MSB = Matrix Spike Sample, MSF = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3 - Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered
 4 - Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, WL = Waste Liquid, SO = Soil, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Wipe, U = Urine, F = Fecal, N = Nail
 5 - Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B, 7070A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7070A - 1)
 6 - Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AX = Acetic Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate, if no preservative is added = leave field blank
 WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Collected by: CB, MB Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh-mm)	QC Code	Field Filtered	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)	← Preservative Type (6)	Comments
						Radiactive	TSCA Regulated				
U3-4S-(002)	10/29/10	1140	N	N	GW	Y	N	1	1		Note: extra sample is required for sample specific QC
								1	1		2 Liter Poly

TAT Requested: Normal: Rush: _____ Specify: _____ Fax Results: Yes / No
 (Subject to Surcharges)

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Other _____

Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<u>ICarp...</u>	10/29/10	1630	ERIN TRENT	10/29/10	1630

Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT

For Lab Receiving Use Only

Custody Seal Intact?	YES / NO
Cooler Temp:	_____ C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, C = Grab, C' = Composite
 3) Field Filtered: For liquid matrices, indicate with a - F - for yes the sample was field filtered or - N - for sample was not field filtered.
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Milky Liquid, SO=Soil, SD=Solids, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Feed, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 6269B, 6010B/7470A) and number of containers provided for each (i.e. 6269B - 3, 6010B/7470A - 1).
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate, if no preservative is added = leave field blank

WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 796-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Project #:

Client Name:

Phone #:

Fax #:

Project/Site Name:

Address:

Collected by:

Send Results To:

Sample Analysis Requested (6)

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:		Total number of containers	Gamma Spec (GS)	Strontium 90 (Sr-90)	Preservative Type (6)	Comments
						TSCA Regulated	Radiactive					
MW-63-112-(015)	11/02/10	1505	N	N	GW	Y	N	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-63-121-(015)	11/02/10	1146	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-163-(015)	11/02/10	1149	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-174-(015)	11/02/10	1150	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-18-(015)	11/02/10	1222	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-34-(015)	11/02/10	1304	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-50-(015)	11/02/10	1507	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-63-93-(016)	11/02/10	1508	N	N	GW	Y	N	1	1	1	2 Liter Poly	

TAT Requested: Normal: Rush: Specify: (Subject to Surcharges) Fax Results: Yes / No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Sample Collection Time Zone: Eastern Central Mountain Pacific Other

Chain of Custody Signatures			Sample Shipping and Delivery Details		
Requisitioned By (Signed)	Date	Time	Received by (signed)	Date	Time
<i>Erin Trent</i>	11/02/10	1555	<i>Erin Trent</i>	11/02/10	1555

Method of Shipment: FEDEX Date Shipped: Airbill #: Airbill #:

For Lab Receiving Use Only
 Custody Seal Intact? YES NO
 Colder Temp: C

Chain of Custody Number = Client Determined
 1) QC Code: N = Normal Sample, TB = Trip Blank, FB = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, C = Grab, C = Composite
 2) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for no sample was not field filtered
 3) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Mobile Liquid, SO = Soil, SB = Seawater, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Pipe, U = Urine, F = Food, N = Nail
 4) Sample Analysis Requested: Analytical method requested (i.e. 3249B, 60105/7179A) and number of containers provided for each (i.e. 8269B - 3, 60105/7179A - 1)
 5) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, BX = Hexane, ST = Sodium Thiosulfate, B = no preservative is added = leave field blank
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, BX = Hexane, ST = Sodium Thiosulfate, B = no preservative is added = leave field blank
 WHITE = LABORATORY
 PINK = CLIENT
 YELLOW = FILE

Page: 1 of 1
 Project #: Entergy GW Mon Prog
 GEL Quote #:
 COC Number: 50013510
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405 Sample Analysis Requested (5) (Fill in the number of containers for each test)

Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: OB, MB Send Results To: Patrick Donahue

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Cook to	Field Filtered (4)	Sample Matrix (6)	Should the sample be considered:	Sample Analysis Requested (5)					Comments	
							Radionuclide	TSCA Regulated	Total number of containers	Gamma Spec (GS)	Strontium 90 (S-90)		Preservative Type (6)
MW-31-49-(028)	11/03/10	1155	N	N	GW	Y	N	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC	
MW-31-63-(028)	11/03/10	1232	N	N	GW	Y	N	1	1	1	2 Liter Poly		
MW-31-85-(028)	11/03/10	1200	N	N	GW	Y	N	1	1	1	2 Liter Poly		

TAT Requested: Normal: Rush: _____ Specify: _____ Fax Results: Yes / No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Sample Collection Time Zone: Eastern Pacific Other _____ Mountain

Chain of Custody Signatures

Retransmitted By (Signed) Date Time Received by (signed) Date Time

1 Erin Trent 11/23/10 1700 Erin Trent 11/23/10 1700

2

3

Method of Shipment: FEDEX Date Shipped:

Airbill #: _____

Airbill #: _____

For Lab Receiving Use Only

Custody Seal Intact? YES NO

Cooler Temp: _____ C

Chain of Custody Number: Client Determined

QC Codes: N = Normal Sample; TB = Trip Blank; FD = Field Duplicate; EB = Equipment Blank; MS = Matrix Spike Sample; MSD = Matrix Spike Duplicate Sample; G = Grab; C = Composite

Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered

Matrix Codes: DW = Drinking Water; GW = Groundwater; SW = Surface Water; WW = Waste Water; W = Water; ML = New Liquid; SD = Sediment; SL = Sludge; SS = Solid Waste; O = Oil; F = Filter; P = Pipe; U = Urine; F = Fecal; N = Nosal

Sample Analysis Requested: Analytical method requested (i.e. 8260B, 8010B/7470A) and number of containers provided for each (i.e. 8260B - 3, 8010B/7470A - 1)

Preservative Type: HA = Hydrochloric Acid; NI = Nitric Acid; SH = Sodium Hydroxide; SA = Sulfuric Acid; AA = Acetic Acid; BX = Hexane; ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT

Page: 1 of 1
 Project #: **Entergy GW Mon Prog**
 GEL Quote #: _____
 COC Number: _____
 PO Number: **50013510**
GEL Work Order Number:
 Client Name: **Entergy**
 Phone #: **(914) 736-8405**
 Fax #: **(914) 734-6247**
GEL Chain of Custody and Analytical Request
 See www.gel.com for GEL's Sample Acceptance SOP
 GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)
 Total number of containers: _____
 Tritium (H3): _____
 Gamma Spec (GS): _____
 Strontium 90 (Sr90): _____
 Preservative Type (6): _____
 Comments: Note: extra sample is required for sample specific QC

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code	Field Filtered (N)	Sample Matrix (M)	Should this sample be analyzed:	Sample Analysis Requested ⁽⁵⁾		Comments
							Radioactive	TSCA Regulated	
MW-32-149-(022)	11/03/10	1609	N	N	GW	Y	N	1	2 Liter Poly
MW-32-173-(020)	11/03/10	1553	N	N	GW	Y	N	1	2 Liter Poly
MW-32-190-(024)	11/03/10	1607	N	N	GW	Y	N	1	2 Liter Poly
MW-32-59-(022)	11/03/10	1208	N	N	GW	Y	N	1	2 Liter Poly
MW-32-85-(025)	11/03/10	1245	N	N	GW	Y	N	1	2 Liter Poly

TAT Requested: Normal Rush: _____ Specify: _____
 Subject to Surcharges: _____
 Fax Results: Yes / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Other _____
 Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards
 Chain of Custody Signatures
 Received by (signed) _____ Date _____ Time _____
 GEL PM: **ERIN TRENT**
 Method of Shipment: **FEDEX** Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, EB = Field Duplicate, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid samples, indicate with a - Y - for yes the sample was field filtered or - N - for no. For samples that were not field filtered.
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc Liquid, SD=Soil, SD-Substrate, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Fecal, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 82603, 60108/7470A) and number of containers provided for each (i.e. 82608 - 3, 60108/7470A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT
 For Lab Receiving Use Only
 Custody Seal Intact? YES / NO
 Cooler Temp: _____ C

GEL Chain of Custody and Analytical Request
 See www.gel.com for GEL's Sample Acceptance SOP
GEL Work Order Number: 50013510

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1778

Client Name: Entergy
 Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center
 Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Collected by: **CB, MB** Send Results To: Patrick Donahue

Sample ID	*Due Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered (y/n)	Sample Matrix (y/n)	Show this sample as considered:		Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	<-- Preservative Type (6)	Comments
						Radioactive	TSCA Regulated						
MW-36-24-(020)	11/04/10 1615		N	N	GW	Y	N	1	1	1	1		2 Liter Poly
MW-36-41-(014)	11/04/10 1655		N	N	GW	Y	N	1	1	1	1		2 Liter Poly
MW-36-52-(019)	11/04/10 1555		N	N	GW	Y	N	1	1	1	1		2 Liter Poly

LAB Requested: Normal: Rush: Specify: Fax Results: Yes / No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Sample Collection Time Zone: Eastern Pacific Central Other Mountain

Chain of Custody Signatures
 Received by (Signed) Date Time
 ERIN TRENT 11/04/10 1730
 Method of Shipment: FEDEX Date Shipped:
 Airbill #: Airbill #:

For Lab Receiving Use Only
 Custody Seal Intact? YES NO
 Cooler Temp: C

1) Chain of Custody Number = Chain Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid mat. hcs, indicate with a 'Y' for yes the sample was field filtered or 'N' for sample was not field filtered
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, ML=Misc. Liquid, SD=Soil, SL=Sludge, SB=Soil Waste, O=Oil, F=Filter, U=Urine, F=Fecal, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (ie. 8280B, 6010B, 7470A) and number of containers provided for each (ie. 8260B - 3, 6010B/7470A - 1)
 6) Preservative Type: EA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Page: 1 of 1
 Project #: Energy GW Mon Prog
 GEL Quote #:
 CDC Number: 50013510
 PO Number:

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405

Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)

Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	OC Code ^(2b)	Field Filtered ⁽³⁾	Sample Matrix ⁽⁴⁾	Should this sample be considered:		Total number of containers		Tritium (H3)	Gamma Spec (G5)	Strontium 90 (Sr90)	← Preservative Type (6)	Comments	
						Radioactive	TSCA Regulated								
MW-37-22-(020)	11/04/10	1428	N	N	GW	Y	N	1	1	1	1		2 Liter Poly	Note: extra sample is required for sample specific QC	
MW-37-32-(020)	11/04/10	1314	N	N	GW	Y	N	1	1	1	1		2 Liter Poly		
MW-37-40-(020)	11/04/10	1206	N	N	GW	Y	N	1	1	1	1		2 Liter Poly		
MW-37-57-(020)	11/04/10	1349	N	N	GW	Y	N	1	1	1	1		2 Liter Poly		

TAT Requested: Normal Rush Specify: _____ Fax Results: Yes No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Central Mountain Other _____

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures				Sample Shipping and Delivery Details			
Relinquished By (Signed)	Date	Time	Received by (Signed)	Date	Time	GEL PM:	ERIN TRENT
<u>Patrick Donahue</u>	11/04/10	1730	<u>Erin Trent</u>	11/04/10	1730	Method of Shipment:	FEDEX
						Airbill #:	
						Airbill #:	

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a - F - for yes the sample was field filtered or - N - for sample was not field filtered
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SL=Sediment, SO=Soil, LS=Liquid, SL=Soil, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Fecal, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 8010B/7470A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7470A - 1).
 6) Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

For Lab Receiving Use Only
 Custody Seal Intact? YES NO
 Cooler Temp: _____ C

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

50013510

Sample Analysis Requested ¹⁵ (Fill in the number of containers for each test)

← Preservative Type (6)

Comments
 Note: extra sample is required for sample specific QC

2 Liter Poly

2 Liter Poly

Client Name: Entergy
 Project/Site Name: Indian Point Energy Center
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Phone #: (914) 736-8405
 Fax #: (914) 734-6247

Send Results To: Patrick Donahue

Sample ID: MW-30-69-(036)
 MW-30-84-(027)

*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code #	Field Filtered	Sample Matrix #
11/05/10	1156	N	N	GW
11/05/10	1235	N	N	GW

Should this sample be considered:

Radioactive: Y N
 TSCA Regulated: Y N

Total number of containers: Tritium (H3) 1 1 1 1 1 1
 Gamma Spec (GS) 1 1 1 1 1 1
 Strontium 90 (Sr90) 1 1 1 1 1 1

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Other Mountain

TAI Requested: Normal Rush Specify: Fax Results: Yes / No

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Received by (Signed) Date Time

ERIN TRENT
 11/05/10 13:20

Method of Shipment: FEDEX

Date Shipped:

Airbill #:

Airbill #:

For Lab Receiving Use Only

Canopy Seal Intact? YES NO

Cooler Temp: C

- Chain of Custody Number = Client Determined
- QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
- Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for no. For solids the sample was not field filtered.
- Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc Liquid, SO = Soil, SD = Sediment, SF = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Pipe, U = Urine, F = Fecal, N = Nasal
- Sample Analysis Requested: Analytical method requested (e.g. 8260B - 3, 6010/7474 - 1)
- Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, SA = Sulfuric Acid, AA = Ascorbic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Project #: Entergy GW Mon Prog
GEL Quote #: _____
COC Number #1: _____
PO Number: 50013510

Client Name: Entergy Phone #: (914) 736-8405
Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
Address: 450 Broadway, Suite 3, Buchanan, NY 10511
Collected by: CB, MB Send Results To: Patrick Donahue

Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)				Should this sample be considered:	Total number of containers		Preservative Type (6)		
OC Code	Field Filtered ^(b)	QC Code ^(a)	Time Collected (Military) (hh:mm)	Radioactive	TSCA Regulated	Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Comments
UI-CSS-(015)	N	N	11/08/10 1450	Y	N	1	1	1	Note: extra sample is required for sample specific QC
									2 Liter Poly

TAT Requested: Normal Rush Specify: _____ (Subject to Surcharge)
 Fax Results: Yes / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Other _____
 Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Chain of Custody Signatures			Sample Shipping and Delivery Details		
Received by (signed)	Date	Time	GEL PM:		
<u>Erin Trent</u>	<u>11/08/10</u>	<u>15:30</u>	<u>ERIN TRENT</u>		

1) Chain of Custody Number = Client Determined
 2) OC Code: N = Normal Sample, TB = Trip Blank, FB = Field Duplicate, ER = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate, Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a Y - if yes the sample was field filtered or a N - if not, sample was not field filtered
 4) Matrix Codes: BW=Drinking Water, GW=Cgroundwater, SW=Surface Water, WW=Waste Water, W-Water, ML=Misc, LAPP=L, SO=Soil, SD=Soil Inert, SL=Sludge, SS=Solid Waste, O-Oil, F-Filter, P-Wipe, U-Urine, F-Fecal, N-Nasal
 5) Sample Analysis Requested: Analytical method requested (e.g. 8560B - A, 603/607/704 - 1)
 6) Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

Page: 1 of 1
 Project #: Entergy GW Mon Prog
 GEL Quote #:
 COC Number: 50013510
 PO Number:

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP
GEL Work Order Number:

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Client Name: Entergy
Phone #: (914) 736-8406
Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center
Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB
Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code		Field Filtered (6)	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (5) (Fill in the number of containers for each test)					Preservative Type (6)	Comments
			QC Code (2)	QC Code (2)			Radioactive	TSCA Regulated		Tritium (H3)	Gamma Spec (G5)	Strontium 90 (Sr90)				

* For composite - indicate start and stop date/time

B-6-(010)	11/08/10	1145	N	N	N	GW	Y	N	1	1	1	1		2 Liter Poly	
-----------	----------	------	---	---	---	----	---	---	---	---	---	---	--	--------------	--

IAT Requested: Normal: Rush: Specify: _____ Fax Results: Yes / No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern, Pacific, Central, Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Requested By (Signed)	Date	Time	Received by (Signed)	Date	Time
	11/08/10	1530	SECURED STORAGE	11/08/10	1530

GEL PM: ERIN TRENT
Method of Shipment: FEDEX
Date Shipped:
Airbill #:
Airbill #:

For Lab Receiving Use Only
Custody Seal Intact?
 YES / NO
Cooler Temp:
 C

1) Chain of Custody Number = Client Determined
 2) CC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a 'Y' for yes the sample was field filtered or a 'N' for no. For solid matrices, indicate with a 'Y' for yes the sample was field filtered or a 'N' for no.
 4) Matrix Codes: DW = Drinking Water, CW = Groundwater, SW = Surface Water, WW = Waste Water, MW = Mill Water, LW = Leachate, HW = Heavy Metal Waste, FFW = Fuel Filter Waste, FW = Fuel Waste, LW = Leachate, HW = Heavy Metal Waste, FFW = Fuel Filter Waste, FW = Fuel Waste
 5) Sample Analysis Requested: Analyt. cal. method requested (i.e. 8250B, 4010B, 7470A) and number of containers provided for each (i.e. 4260B - 3, 6010B/7470A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, SA = Sulfate Acid, AA = Ascorbic Acid, HX = Hexamine, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

**WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT**

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

50013510

Client Name: Entergy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: **CB, MB** Send Results To: Patrick Donahue

Sample Analysis Requested⁽⁵⁾ (Fill in the number of containers for each test)

Sample ID <i>* For composites - indicate start and stop date/time</i>	Date Collected (mm-dd-yy)	Time Collected (Military time)	QC Code <i>(2)</i>	Field Filtered <i>(3)</i>	Sample Matrix <i>(4)</i>	Should this sample be considered:		Total number of containers	Sample Analysis Requested ⁽⁵⁾						Preservative Type (6)	Comments
						Radioactive	TSCA Regulated		Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Level 1	Level 2	Level 3		
MW-62-138-(015)	11/09/10	1431	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-62-18-(015)	11/09/10	1157	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-62-182-(015)	11/09/10	1443	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-62-37-(015)	11/09/10	1156	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-62-53-(014)	11/09/10	1249	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-62-71-(015)	11/09/10	1102	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-62-92-(015)	11/09/10	1115	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	

TAT Requested: Normal Rush: Specify: Subject to Shipment: Fax Results: Yes No Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Sample Collection Time Zone:
Eastern
Central
Mountain
Other

Chain of Custody Signatures

Sample Shipping and Delivery Details

Requested By (Signed)	Date	Time	Received by (signed)	Date	Time
<i>Erin Trent</i>	11/09/10	1515	<i>Erin Trent</i>	11/09/10	1515

GEL PM: ERIN TRENT
Method of Shipment: FEDEX
Date Shipped:
Airbill #:
Airbill #:

1 Chain of Custody Number = Client Determined
2 QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
3 Field Filtered: For top of matrices, indicate with a - Y - for yes the sample was field filtered or - N - for no (for sample was not field filtered)
4 Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc Liquid, SO=Soil, SD=Soil Sample, SS=Solid Waste, O=Oil, F=Filter, Pa=Pipe, Ua=Urine, F=Feed, N=Nasal
5 Sample Analysis Requested: Analytical method requested (1 v. 8260B, 60102/7470A) and number of containers provided for each (i.e. 8260B - 3, 60102/7470A - 1).
6 Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, RX = Hexane, ST = Sealant, Thiosulfate. If no preservative is added = leave field blank.

WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT
For Lab Receiving Use Only
Custody Seal Intact? YES NO
Cooler Temp: C

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Phone #: (914) 736-8405
Fax #: (914) 734-6247

Client Name: Entergy
Project/Site Name: Indian Point Energy Center

Address:
450 Broadway, Suite 3, Buchanan, NY 10611

Collected by: *CP, MB*
Send Results To: Patrick Donahue

Sample Analysis Requested (6) (Fill in the number of containers for each test)

Sample ID <small>* For composites - indicate start and stop date/time</small>	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code (a)	Field Filtered (b)	Sample Matrix (c)	Should this sample be considered:		Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (S90)	Nickel 63 (Ni63)	Preservative Type (d)	Comments
						Radioactive	TSCA Regulated							
MW-66-21-(015)	11/10/10	1513	N	N	GW	Y	N	1	1	1	1	1		2 Liter Poly
MW-66-36-(014)	11/10/10	1233	N	N	GW	Y	N	1	1	1	1	1		2 Liter Poly

TAT Requested: Normal: Rush: Specify: _____ Fax Results: Yes / No No Yes

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone:
Eastern Pacific Other _____
Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<i>Erin Trent</i>	11/10/10	1545	<i>ERIN TRENT</i>	11/10/10	1545

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT
Method of Shipment: FEDEX
Date Shipped: _____
Airbill #: _____
Airbill #: _____

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Tap Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike, MSD = Matrix Spike Duplicate Sample, C = Grab, C = Composite
 3) Field Filtered: For liquid matrices indicate with a 'Y' - for 'yes' the sample was field filtered or 'N' - for sample was not field filtered
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc. Liquid, SQ = Soil, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, P = Filter, P = Wipe, U = Urine, F = Fecal, N = Nuisance
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 4100B, 4700) and number of containers provided for each (i.e. 8260B - 3, 4100B/4700 - 1)
 6) Preservative Type: BA = Hydrochloric Acid, ME = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate, If no preservative is added = Iance field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

For Lab Receiving Use Only

Customary Seal Intact?	YES/NO
Cooler Temp:	C

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Project # 1 of 1 Entergy GW Mon Prog
GEL Quote #:
COC Number ¹⁾:
PO Number: 50013510

GEL Work Order Number:
Client Name: Entergy Phone #: (914) 736-8405
Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
Address: 450 Broadway, Suite 3, Buchanan, NY 10511
Collected by: CB, MB Send Results To: Patrick Donahue

Sample Analysis Requested ⁵⁾ (Fill in the number of containers for each test)

Sample ID	Should this sample be considered:		Total number of containers		Preservative Type (6)	Comments
	TSCA Regulated	Radiactive	Gamma Spec (GS)	Strontium 90 (Sr90)		
MW-67-105-(014)	Y	N	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-67-173-(015)	Y	N	1	1	2 Liter Poly	
MW-67-219-(014)	Y	N	1	1	2 Liter Poly	
MW-67-276-(014)	Y	N	1	1	2 Liter Poly	
MW-67-323-(014)	Y	N	1	1	2 Liter Poly	
MW-67-340-(014)	Y	N	1	1	2 Liter Poly	
MW-67-39-(015)	Y	N	1	1	2 Liter Poly	

Sample Matrix: GW (Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Sludge, SS=Solid Waste, OS=Oil, F=Filter, P=Wipe, U-Urine, F-Fecal, N=Nasal)

Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Sludge, SS=Solid Waste, OS=Oil, F=Filter, P=Wipe, U-Urine, F-Fecal, N=Nasal

Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/8270A) and number of containers provided for each (i.e. 8260B - 3, 6010B/8270A - 1).

Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

TAJ Requested: Normal: Rush: Specify: (Subs to Subcharge) Fax Results: Yes / No /

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Timing Zone: Eastern Pacific Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<u>Valery B...</u>	<u>11/10/10</u>	<u>1545</u>	<u>ERIN TRENT</u>		

Method of Shipment: **FEDEX** Date Shipped:

Airbill #: 2

Airbill #: 3

For Lab Receiving Use Only

Custody Seal Intact? YES

Cooler Temp: C

Chain of Custody Number = Client Determined

QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate, Sample, G = Grab, C = Composite

Field Filtered: For liquid matrices, indicate with a 'Y' - for yes the sample was field filtered or 'N' - for sample was not field filtered.

Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Sludge, SS=Solid Waste, OS=Oil, F=Filter, P=Wipe, U-Urine, F-Fecal, N=Nasal

Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/8270A) and number of containers provided for each (i.e. 8260B - 3, 6010B/8270A - 1).

Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

WHITE = LABORATORY
PINK = CLIENT
YELLOW = FILE

Project #: Entergy GW Mon Prog
 GEL Quote #: _____
 GEL Number: 50013510
 PG Number: 50013510

Circuit Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue
 Sample ID: _____
 *For composites - indicate start and stop date/time

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code (2)	Field Filtered (3)	Sample Matrix (4)	Should this sample be considered?	TSCA Required	Total number of containers	Gamma Spec (G5)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
MW-58-26-(011)	11/11/10	1512	N	N	GW	Y	N	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-58-65-(011)	11/11/10	1353	N	N	GW	Y	N	1	1	1	2 Liter Poly	

TAT Requested: Normal Risk Specific Fax Results: Yes No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Central Mountain Other

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards
 Chain of Custody Signatures
 Relinquished By (Signed) _____ Date _____ Time _____
 Received by (signed) _____ Date _____ Time _____
Case begins 11/21/10 1000
Sealed 11/21/10 1000
 2
 3

Method of Shipment: **FEDEX**
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____
 GEL PM: **ERIN TRENT**

For Lab Receiving Use Only
 Custody Seal Intact? YES NO
 Cooler Temp: _____ C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a -F- for Yes the sample was field filtered or -N- for sample was not field filtered
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Mobile Liquid, SL = Solid, SD = Sediment, SH = Shale, SS = Solid Waste, O = Oil, F = Filter, P = Pipe, J = Juice, F = Fecal, N = Nasal
 5) Sample Analysis Requested: Analytical method requested (ie 8260F, 8010B, 8747A) and number of containers provided for each (ie 8260F - 3, 8010B/8747A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, M = Nitric Acid, SH = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = None field black
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

GEL Work Order Number:
Phone #: (914) 736-8405
Fax #: (914) 734-6247

Project #: Energy GW Mon Prog
GEL Quote #: _____
COC Number (1): _____
PO Number: 50013510
Client Name: Entergy

Sample Analysis Requested (6) (Fill in the number of containers for each test)

Sample ID <small>* For composites - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:		Total number of containers	Preservative Type (6)	Comments
						Radionuclide	TSCA Regulated			
MW-49-26-(022)	11/11/10	1423	N	N	GW	Y	N	1		Note: extra sample is required for sample specific QC
MW-49-42-(022)	11/11/10	1413	N	N	GW	Y	N	1		
MW-49-65-(022)	11/11/10	1418	N	N	GW	Y	N	1		

Send Results To: Patrick Donahue

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Limit Zone:
 Eastern
 Pacific
 Other

FAI Requested: Normal: Result: _____ Specify: _____ Fax Results: Yes No

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Retiquished By (Signed)	Date	Time	Received by (signed)	Date	Time
<u>[Signature]</u>	11/11/10	1600	<u>ERIN TRENT</u>	11/21/10	1600

Method of Shipment: **FEDEX** Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT

For Lab Receiving Use Only:
 Custody Seal Intact? YES NO
 Cooler Temp: C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FB = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a 'Y' for yes the sample was field filtered or 'N' for sample was not field filtered
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, ML=Misc Liquid, SD=Solid, SL=Sludge, SS=Solid Waste, Q=Oil, F=Filter, P=Wipe, U=Urine, F=Feces, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8250B, 6010E/7470A) and number of containers provided for each (i.e. 8250B - 3, 6010E/7470A - 1)
 6) Preservative Type: HA - Hydrochloric Acid, NI - Nitric Acid, SH - Sulfuric Acid, AA - Ascorbic Acid, HX - Hexane, ST - Sodium Thiosulfate, FMS preservative (sealed - leave field blank)
WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT

Page: 1 of 1
 Project #: Entergy_GW_Mon_Prog
 GEL Quote #: _____
 COC Number ⁽¹⁾: _____
 PO Number: 50013510
GEL Chain of Custody and Analytical Request
****See www.gel.com for GEL's Sample Acceptance SOP****
GEL Work Order Number:
 GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CP Send Results To: Patrick Donahue
 Sample ID
 * For comparatives indicate start and stop date/time

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered (b)	Sample Matrix (a)	Should this sample be considered:	Total number of containers	Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)	Preservative Type (6)	Comments
						Radioactive				
MW 50-42-(023)	11/12/10	1210	N	N	GW	Y	1	Gamma Spec (GS)		
MW 50-66-(028)	11/12/10	1230	N	N	GW	Y	1	Tritium (H3)		2 Liter Poly
							1	Sr-90 (Sr90)		2 Liter Poly
							1	Nickel 63 (Ni63)		Note: extra sample is required for sample specific QC

TAT Requested: Normal: Rush: _____ Specify: _____ (Subject to Surcharges) Fax Results: Yes / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Mountain Other _____

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**
 Chain of Custody Signatures
 Received by (signed) _____ Date _____ Time _____
 1 ERIN TRENT 11/12/10 1600
 2 _____
 3 _____
 GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only
 Contain Seal Intact? YES / NO
 Cooler Temp: _____ C
 Chain of Custody Number = Client Determined
 1) QC Codes: N = Normal Sample, TB = Trip Blank, FB = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 2) Field Filtered For liquid matrices, indicate with a 'Y' - for yes the sample was field filtered or 'N' - for no sample was not field filtered
 3) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc Liquid, SOL = Solid, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, F = Fuel, P = Waste, U = Urine, F = Fecal, N = Nail
 4) Sample Analysis Requested Analytical method requested (ie. 8260B, 601BE/7470A) and number of containers provided for each (ie. 8260B: 3, 601BE/7470A: 1)
 5) Preservative Type: HA = Hydrochloric Acid, M = Nitric Acid, SB = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BX = Boric Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
 WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

Page: 1 of 1
 Project #: Entergy GW Mon Prog
 GEL Quote #: _____
 COC Number ⁽¹⁾: _____
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue

Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hhmm)	QC Code ⁽⁴⁾	Field Filtered ⁽⁴⁾	Sample Matrix ⁽⁴⁾	Should this sample be considered:		Total number of containers			Preservative Type ⁽⁶⁾	Comments	
						Radonfree	TSCA Regulated	Tridium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)			
MW-56-53-(009)	11/15/10	1248	N	N	GW	Y	N	1	1	1		2 Liter Poly	Note: extra sample is required for sample specific QC
MW-56-83-(011)	11/15/10	1437	N	N	GW	Y	N	1	1	1		2 Liter Poly	

TAT Requested: Normal: Rush: _____ Specify: _____ (Subject to Surcharge) Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Other _____

Chain of Custody Signatures

Received By (Signed)	Date	Time	Date	Time
<i>[Signature]</i>	11/19/10	0800	11/19/10	0800
<i>[Signature]</i>	11/19/10	0800	11/19/10	0800

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Chain of Custody Number = Client Determined
 1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc. Liquid, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Wipe, U = Urine, F = Fecal, N = Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8240B, 6010B/7470A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7470A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, AA = Acetic Acid, HX = Hexanic Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

For Lab Receiving Use Only
 Custody Seal Intact? YES / NO
 Cooler Temp: _____ C

WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT

Page: 1 of 1
 Project #: Energy GW Mon Prog
 GEL Quote #:
 COC Number: 1
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CO, MB Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code (a)	Field Filters (b)	Sample Matrix (d)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (5) (Fill in the number of containers for each test)						Preservative Type (6)	Comments	
						Radioactive	TSCA Regulated		Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)						
MW-39-102-(010)	11/15/10	1612	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-124-(010)	11/15/10	1246	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-183-(010)	11/15/10	1253	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-195 (010)	11/15/10	1325	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-67-(010)	11/15/10	1628	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-84-(010)	11/15/10	1638	N	N	GW	Y	N	1	1	1	1	1	1	1	1	2 Liter Poly	

TAT Requested: Normal: Rush: _____ Specify: _____ (Subject to Surcharges) Fax Results: Yes / No / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Mountain Central Other _____

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures		Sample Shipping and Delivery Details	
Relinquished By (Signed)	Date	Time	Date
<u>Carly Bignardi</u>	11/15/10	1700	11/15/10
			1700

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped:
 Airbill #:
 Airbill #:

1. Chain of Custody Number -- Client Determined
 2. QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, C = Grab, G = Composite
 3. Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or - N - for sample was not field filtered
 4. Matrix Codes: DW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, ML - Misc. Liquid, SD - Sediment, SL - Sludge, SS - Solid Waste, O - Oil, F - Filter, P - Wipe, U - Urine, F - Fecal, N - Nasal
 5. Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6910B/7370A) and number of containers provided for each (i.e. 8260B - 3, 6910B/7370A - 1)
 6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added in leave field blank
 WHITE - LABORATORY
 YELLOW - FILE
 PINK - CLIENT
 For Lab Receiving Use Only
 Custody Seal Intact?
 YES NO
 Cooler Temp
 C

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOPs

GEL Work Order Number:

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Page: 1 of 1
 Project #: Entergy GW Mon Prog
 GEL Quote #: _____
 COC Number ⁽¹⁾: _____
 PO Number: 50013510

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Collected by: MB Send Results To: Patrick Donahue

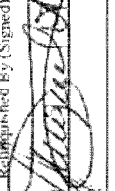
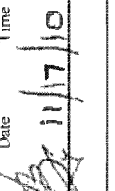
Sample ID: _____
 * For composites - indicate start and stop date/time

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	OC Code (3)	Field Filtered (5)	Sample Matrix (6)	Should this sample be considered:	TSCA Regulated	Total number of containers	Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
B-1-(010)	11/17/10	1110	N	N	GW	Radioactive	N	1	1	1	1		2 Liter Poly

TAT Requested: Normal: Rush: _____ Specify: _____ Fax Results: Yes / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Sample Collection Time Zone: Eastern
 Eastern Pacific Central Other _____
Chain of Custody Signatures

Received by (Signed)	Date	Time
	11/17/10	1539
	11/17/10	1539

Received by (Signed): _____ Date: _____ Time: _____
 Date Shipped: _____
 Method of Shipment: FEDEX
 Airbill #: _____
 Airbill #: _____

Sample Shipping and Delivery Details

GEL PM: ERIN TRENT

For Lab Receiving Use Only:

Custody Seal Intact? YES / NO
 Cooler Temp: _____ C

1) Chain of Custody Numbers = Client Determined
 2) QC Codes: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered - For liquid matrices, indicate with a 'Y' for yes; the sample was field filtered or 'N' for sample was not field filtered
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, WL=Water, ML=Misc. Liquid, SO=Soil, SD=Soil/Dredge, SL=Sludge, SS=Solid Waste, OS=Oil, F=Filter, P=Wipe, L=Leak, N=Normal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 8010B/870A) and number of containers provided for each (i.e. 8260B - 3, 6210B/470A - 1)
 6) Preservative Type: HA = Hydrochloric Acid, HCl = Nitric Acid, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Boric Acid, ST = Sodium Thiosulfate. If no preservative is added = Base field blank
WHITE = LABORATORY YELLOW = FIELD PINK = CLIENT

Page: 1 of 1
 Project # Entergy GW Mon Prog
 GEL Quote #:
 COC Number ⁽¹⁾: 50013510
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Collected by: CB, MB Send Results To: Patrick Donahue

Sample ID <small>* For composites - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military (hhmm))	QC Code (*)	Field Filtered ⁽ⁿ⁾	Sample Matrix ⁽ⁿ⁾	Should this sample be considered:		Total number of containers	Sample Analysis Requested ⁽⁶⁾ (Fill in the number of containers for each test)						Comments Note: extra sample is required for sample specific QC
						Radioactive	TSCA Regulated		Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Preservative Type (6)		
MW-60-35-(015)	11/18/10	1325	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-35-(015)-B	11/18/10	1325	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-35-(015)-D	11/18/10	1325	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-35-(015)-S	11/18/10	1325	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-53-(015)	11/18/10	1222	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-72-(015)	11/16/10	1317	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-135-(015)	11/16/10	1322	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-154-(015)	11/16/10	1340	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-60-176-(015)	11/16/10	1406	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	

TAT Requested: Normal: Rush: _____ Specify: _____ (Subject to Surcharge)
 Fax Results: Yes / No / _____
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Mountain Central Other _____

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures
 Received by (signed) _____ Date _____ Time _____
 SECURED STORAGE 11/19/10 0805
 Date _____ Time _____
 Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only
 Custody Seal Intact?
 YES NO
 Cooler Temp: _____ C

Chain of Custody Number - Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a -Y- for yes the sample was field filtered or -N- for sample was not field filtered
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc Liquid, SQ=Soil, SD=Sediment, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Feal, N=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 810B/7470A) and number of containers provided for each (i.e. 8260B - 3, 810B/7470A - 1).
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate, F no preservative is added = leave field blank

WHITE = LABORATORY
 YELLOW = FILE
 PINK = CLIENT

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:
 Project # Entropy GW Mon Prog
 GEL Quote #
 COC Number (U):
 PO Number: 50013510

Client Name: Entropy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511
 Collected by: Miguel Britos Send Results To: Patrick Donahue

Sample ID <i>* For composites - indicate start and stop date/time</i>	Dair Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code (N)	Field Filtered (N)	Sample Matrix (GW)	Should this sample be considered:	TSCA Regulated (N)	Radionuclide (Y)	Sample Analysis Requested ⁽³⁾ (Fill in the number of containers for each test)					Comments Note: extra sample is required for sample specific QC
									Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Total number of containers	
LAF-002-(014)	11/22/10	1441	N	N	GW		N	Y	1	1	1	1	1	2 Liter Poly

TAT Requested: Normal Rush: Specify: _____
 Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone:
 Eastern Pacific
 Central Other _____
 Mountain

Chain of Custody Signatures
 Received by (Signed) _____ Date _____
 Time _____
 Relinquished By (Signed) Miguel Britos Date 11/24/10 Time 0905
 GEL PM: ERIN TRENT
 Method of Shipment: FEDEX Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, ED = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or a - N - for no the sample was not field filtered.
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc, LQ=Liquid, SO=Soil, SLS=Sediment, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Pipe, Q=Junk, F=fecal, N=Nail
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/7470A) and number of containers provided for each (i.e. 3260B - 3, 6010B/7470A - 1).
 6) Preservative Type: UA = Hydrochloric Acid, M = Nitric Acid, SH = Sulfuric Acid, AA = Ascorbic Acid, HV = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY **YELLOW = FILE** **PINK = CLIENT**
 For Lab Receiving Use Only
 Custody Seal Intact? YES/NO
 Cooler Temp: C

Page: 1 of 1
 Project # Entergy GW Mon Prog
 GEL Quote #:
 COC Number (1):
 PO Number: 50013510

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 556-8171
 Fax: (843) 766-1178

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: Miguel Britos Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hhmm)	QC Code (2)	Field Filtered (3)	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (5) (Fill in the number of containers for each test)						Comments Note: extra sample is required for sample specific QC
						Rad/Nuclide	TSCA Regulated		Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Level 1	Level 2	
MW-54-123-(015)	11/23/10	1512	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly
MW-54-144-(015)	11/23/10	1230	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly
MW-54-173-(015)	11/23/10	1225	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly
MW-54-190-(015)	11/23/10	1222	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly
MW-54-37-(015)	11/23/10	1447	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly
MW-54-58-(015)	11/23/10	1455	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly

TAT Requested: Normal: Rush: _____ Specify: _____ (Subject to Sampling) Fax Results: Yes / No / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern Pacific Other: _____
 Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures
 Received By (Signature) Date Time
Miguel Britos 11/24/10 0900
 ERIN TRENT 11/24/10 0900
 Method of Shipment: **FEDEX** Date Shipped:
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only
 Custody Seal Intact?
 YES NO
 Cooler Temp: _____
 C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, ED = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for no. For solid samples, indicate with a - Y - for yes the sample was field filtered or - N - for no. For samples that were not field filtered.
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc Liquid, SO=Soil, SD=Sediment, SL=Sludge, SS=Solid Waste, Co=Oil, F=Filter, P=Wipe, Ur=Urine, Po=Fecal, Ni=Nasal
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/7070A) and number of containers provided for each (i.e. 3250B - 3, 6070B/7070A - 1).
 6) Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = zero field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Project #: Entergy GW Mon Prog
GEL Quote #: _____
COC Number ⁽¹⁾: 50013510
PO Number: _____

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405 Sample Analysis Requested ⁽⁵⁾ (Fill in the number of containers for each test)

Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: Miguel Britos Send Results To: Patrick Donahue

Sample ID <small>* For composite - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military (hhmm))	QC Code (3)	Field Filtered (1)	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Tritium (H3) Gamma Spec (GS) Strontium 90 (Sr90)	Comments Note: extra sample is required for sample specific QC
						Radioactive	TSCA Regulated			
MW-40-100-(016)	11/29/10	1212	N	N	GW	Y	N	1	1	2 Liter Poly
MW-40-127-(016)	11/29/10	1226	N	N	GW	Y	N	1	1	2 Liter Poly
MW-40-162-(014)	11/29/10	1245	N	N	GW	Y	N	1	1	2 Liter Poly
MW-40-27-(013)	11/29/10	1523	N	N	GW	Y	N	1	1	2 Liter Poly
MW-40-46-(014)	11/29/10	1636	N	N	GW	Y	N	1	1	2 Liter Poly
MW-40-81-(014)	11/29/10	1203	N	N	GW	Y	N	1	1	2 Liter Poly

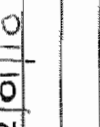
TAT Requested: Normal: Rush: _____ Specify: _____ Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Central Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures

Requested By (Signed)	Date	Time	Received by (signed)	Date	Time
	12/01/10	1135	ERIN TRENT	12/01/10	1135

Method of Shipment: FEDEX Date Shipped: _____

Airbill #: _____

Airbill #: _____

For Lab Receiving Use Only
Custody Seal Intact? YES / NO
Cooler Temp: _____ C

1) Chain of Custody Number = Client Determined
2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, FB = Field Duplicate, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
3) Field Filtered: For liquid matrices, indicate with a 'Y' - for yes, the sample was field filtered or - 'N' - for sample was not field filtered
4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Soil, SS=Sludge, SL=Sludge, O=Oil, F=Filter, P=Pipe, U=Urine, F=Fecal, N=Nasal
5) Sample Analysis Requested: Analytical method requested (ie: 8260B, 6010B, 8210B, 8230B, 8240B, 8250B, 8260B, 8270B, 8280B, 8290B, 8300B, 8310B, 8320B, 8330B, 8340B, 8350B, 8360B, 8370B, 8380B, 8390B, 8400B, 8410B, 8420B, 8430B, 8440B, 8450B, 8460B, 8470B, 8480B, 8490B, 8500B, 8510B, 8520B, 8530B, 8540B, 8550B, 8560B, 8570B, 8580B, 8590B, 8600B, 8610B, 8620B, 8630B, 8640B, 8650B, 8660B, 8670B, 8680B, 8690B, 8700B, 8710B, 8720B, 8730B, 8740B, 8750B, 8760B, 8770B, 8780B, 8790B, 8800B, 8810B, 8820B, 8830B, 8840B, 8850B, 8860B, 8870B, 8880B, 8890B, 8900B, 8910B, 8920B, 8930B, 8940B, 8950B, 8960B, 8970B, 8980B, 8990B, 9000B)
6) Preservative Type: BA = Phosphoric Acid, NI = Nitric Acid, SB = Sodium Borohydride, SA = Sulfuric Acid, AA = Acetic Acid, AX = Hexane, ST = Sodium Thiosulfate. If no preservative is added - leave field blank

WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT

GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC
2040 Savage Road
Charleston, SC 29407
Phone: (843) 556-8171
Fax: (843) 766-1178

Project #: Energy GW Mon Prog
GEL Quote #: _____
COC Number: 50013510
PO Number: _____

Client Name: Energy
Phone #: (914) 736-8405
Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center
Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: Miguel Britos
Send Results To: Patrick Donahue

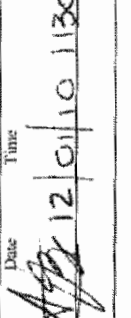
Sample ID
** For composites - indicate start and stop date/time*

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code (in)	Field Filtered (y)	Sample Matrix (y)	Should this sample be considered:		Total number of containers	Gamma Spec (GS)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
						Mercuric	TSCA Regulated					
MW-51-104-(015)	11/30/10	0955	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-51-135-(015)	11/30/10	0957	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-51-163-(015)	11/30/10	1002	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-51-189-(015)	11/30/10	0956	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-51-40-(017)	11/30/10	1254	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-51-79-(017)	11/30/10	1308	N	N	GW	Y	N	1	1	1		2 Liter Poly

TAT Requested: Normal: Rush: _____ Specify: _____ Subject to Surcharge: _____ Fax Results: Yes / No / No
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
 Sample Collection Time Zone: Eastern / Pacific / Other _____
 Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures

Received by (Signed)	Date	Time	Date	Time
	12/01/10	1130	12/01/10	1130

GEL PM: ERIN TRENT
 Method of Shipment: FEDEX
 Date Shipped: _____
 Airbill #: _____
 Airbill #: _____

For Lab Receiving Use Only

Custody Seal Intact? YES / NO
 Cooler Temp: _____ / C

1) Chain of Custody Number = Client Determined
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Deployable, EB = Equipment Blank, MS = Matrix Spike, MSD = Matrix Spike Duplicate Sample, C = Grab, C = Composite
 3) Field Filtered: For liquid matrices, indicate with a 'Y' for yes the sample was field filtered or a 'N' if a sample was not field filtered.
 4) Matrix Codes: BW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Milk, LD = Liquid, SD = Solid, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Wipe, U = Urine, F = Fecal, N = Nail
 5) Sample Analysis Requested: Analytical method requested (ie. 8260B, 6010B/7470A) and number of containers provided for each (ie. 8260B - 3, 6010B/7470A - 1)
 6) Preservative Type: MA = Hydrochloric Acid, M = Nitric Acid, SH = Sulfuric Acid, SA = Salicylic Acid, AA = Acetic Acid, AW = Ascorbic Acid, HA = Hexanoic Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY
YELLOW = FILE
PINK = CLIENT

GEL Laboratories, LLC
 2040 Savage Road
 Charleston, SC 29407
 Phone: (843) 536-8171
 Fax: (843) 766-1178

GEL Chain of Custody and Analytical Request

See www.gel.com for GEL's Sample Acceptance SOP

GEL Work Order Number:

Sample Analysis Requested⁽⁵⁾ (Fill in the number of containers for each test)

Page: <u>1</u> of <u>1</u> Project #: <u>Energy GW Mon Prog</u> GEL Quote #: _____ COC Number ⁽¹⁾ : <u>50013510</u> PO Number: _____			Client Name: Entergy Phone #: (914) 736-8405 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247 Address: 450 Broadway, Suite 3, Buchanan, NY 10511			Total number of containers considered: TSC A Regulated: _____ Radioactive: _____ Should this sample be considered: _____ <- Preservative Type (6)			
Collected by: <u>Miguel Britos</u> Send Results To: Patrick Donahue Sample ID * For composites - indicate start and stop date/time			*Date Collected (mm-dd-yy)	*Time Collected (Military) (hhmm)	QC Code ⁽²⁾	Field Filtered ⁽³⁾	Sample Matrix ⁽⁴⁾	Tritium (H3) Gamma Spec (GS) Strontium 90 (Sr90)	Comments Note: extra sample is required for sample specific QC 2 Liter Poly
MH-5-(013)			11/24/10	1110	N	N	GW	1 1 1	

LAI Requested: Normal: <input checked="" type="checkbox"/> Rush: _____ Specify: _____	(Subject to Surcharge)	Fax Results: Yes / No	Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4
Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards			
Chain of Custody Signatures			
Authorized By (Signed) _____ Date <u>10/24/10</u> Time <u>1200</u> Received By (Signed) _____ Date <u>10/24/10</u> Time <u>1200</u> <i>Miguel Britos</i> <i>SEKURED STORAGE</i>	Sample Shipping and Delivery Details GEL PM: ERIN TRENT Method of Shipment: FEDEX Date Shipped: _____ Airbill #: _____ Airbill #: _____		

Chain of Custody Signatures Authorized By (Signed) _____ Date _____ Time _____ Received By (Signed) _____ Date _____ Time _____	Sample Shipping and Delivery Details GEL PM: ERIN TRENT Method of Shipment: FEDEX Date Shipped: _____ Airbill #: _____ Airbill #: _____		
For Lab Receiving Use Only:			
Custody Seal Intact? YES / NO			
Cooler Temp: _____ C			

1.) Chain of Custody Number - Client Determined
 2.) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite
 3.) Field Filtered: For liquid matrices, indicate with a -Y- for yes the sample was field filtered or -N- for sample was not field filtered.
 4.) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, ML=Misc Liquid, SO=Soil, SD=Sediment, SL=Sludge, SS=Solid Waste, OS=Oil, F=Filter, P=Wipe, U=Urine, F=Faecal, N=Nasal
 5.) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B/7470A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7470A - 1).
 6.) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SA = Sulfuric Acid, AA = Ascrobic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank
WHITE = LABORATORY YELLOW = FILE PINK = CLIENT



APPENDIX D: 4TH QUARTER 2010 SAMPLING DATA SHEETS

WELL ID: MW 51-189

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50°

PROJECT NO: 01.0017869.92
 DATE: 11/30/10
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)
184.2 to 197.8

TOTAL VOLUME PURGED: 1.45 gal

SAMPLING PORT
189

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
819	0							5.6/5.6	42
829	0.1	11.95	1.505	1.97	6.67	-115.7	—	↓	↓
837	0.25	12.00	1.515	1.20	6.63	-126.0	—		
845	0.45	12.21	1.520	0.82	6.60	-153.1	2.53		
854	0.65	12.29	1.520	0.70	6.60	-176.2	1.09		
902	0.85	12.33	1.522	0.50	6.60	-219.0	1.00		
909	1.0	12.31	1.522	0.44	6.60	-232.2	0.54		
914	1.1	12.26	1.522	0.41	6.60	-246.1	0.51		
923	1.2	12.23	1.522	0.38	6.59	-250.0	0.57		
928	1.3	12.21	1.518	0.40	6.59	-244.6	0.61		
929		PUMP OFF							
930		START SAMPLE COLLECTION							
956		SAMPLE COMPLETED : 2 L IPEC							
956		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 51-163

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50°

PROJECT NO: 01.0017869.92
 DATE: 11/30/10
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)
154.7 to 166.2

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT
163 2

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
819	0		PUMP ON					5.6 5.6	42
829	0.05	11.47	2.089	0.57	6.49	-116.4	—	↓	↓
837	0.12	11.49	2.090	0.42	6.56	-112.5	—	↓	↓
845	0.30	11.65	2.103	0.27	6.67	-98.6	2.36	↓	44
854	0.40	11.74	2.111	0.23	6.71	-94.3	1.37	↓	↓
902	0.50	11.79	2.118	0.20	6.75	-80.1	0.80	↓	↓
909	0.60	11.82	2.120	0.20	6.76	-80.8	0.76	↓	↓
914	0.70	11.81	2.123	0.19	6.77	-78.9	0.74	↓	↓
915		PUMP OFF							
917		START SAMPLE COLLECTION							
1002		SAMPLE COMPLETED : 2 L ± PEC							
1002		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>2</u> 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW SL-135

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50°

PROJECT NO: 01.0017869.92
 DATE: 11/30/10
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)
130.2 to 143.7

TOTAL VOLUME PURGED: 1.75 gal

SAMPLING PORT
135 3

PURGE RATE: variable (gal/min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
819	0	PUMP ON						5.6/5.6	42
829	0.1	12.10	2.397	1.49	6.62	-111.4	—	↓	↓
837	0.3	12.28	2.428	0.89	6.72	-77.2	—		
845	0.55	12.39	2.444	0.61	6.81	-24.7	0.67		
854	0.75	12.39	2.445	0.55	6.83	-4.9	0.58		
902	1.0	12.43	2.444	0.49	6.83	+17.8	0.49		
909	1.2	12.44	2.443	0.46	6.83	23.8	0.59		
914	1.3	12.45	2.444	0.43	6.83	27.6	0.64		
923	1.4	12.44	2.436	0.43	6.82	28.5	0.67		
928	1.6	12.43	2.439	0.42	6.82	27.7	0.70		
929		PUMP OFF							
930		START SAMPLE COLLECTION							
957		SAMPLE COMPLETED : 2 L IPEC							
957		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 5L-104

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: cloudy 50°

PROJECT NO: 01.0017869.92
 DATE: 11/30/10
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)
130.2 to 143.7

TOTAL VOLUME PURGED: 3.65 gal

SAMPLING PORT
104 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	
819	0		PUMP ON					5.6/5.6	42	
829	0.1	12.51	2.672	2.40	6.96	57.7	—	↓	↓	
837	0.4	12.67	2.669	1.81	7.05	43.6	—			
845	1.0	12.69	2.680	1.67	7.06	28.4	0.00			44
854	1.4	12.64	2.679	1.58	7.06	19.3	0.01			
902	1.8	12.66	2.678	1.55	7.06	11.2	0.00			
909	2.1	12.64	2.681	1.50	7.06	9.1	0.0			
914	2.3	12.61	2.682	1.48	7.06	7.0	0.0			
923	2.5	12.62	2.678	1.47	7.05	6.5	0.0			
928	2.9	12.63	2.684	1.44	7.05	1.1	0.0			
937	3.3	12.64	2.687	1.46	7.06	0.7	0.0			
942	3.5	12.64	2.688	1.49	7.06	0.1	0.0			
943		PUMP OFF								
943		START SAMPLE COLLECTION								
955		SAMPLE COMPLETED : 2 L IPEC								
955		PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 51-79

SAMPLE ID: 017

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50°

PROJECT NO: 01.0017869.92
 DATE: 11/30/10
 SAMPLER(S): Miguel Britos

SAMPLING INTERVAL (depth in ft below top of casing)
63.2 to 81.2

TOTAL VOLUME PURGED: 1.55 gal

SAMPLING PORT
79 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1120	0	PUMP ON						6.5/8.4	2.4
1130	0.01	12.32	2.622	2.12	6.64	-83.4	-		
1135	0.08	12.29	2.619	1.80	6.58	-75.0	6.17		
1142	0.15	12.52	2.625	1.74	6.57	-59.8	6.04		
1149	0.30	12.63	2.621	1.74	6.57	-30.8	5.26		
1155	0.45	12.66	2.620	1.78	6.58	-16.1	6.49		
1200	0.55	12.71	2.618	1.75	6.58	+ 1.1	4.38		
1206	0.75	12.73	2.618	1.75	6.58	+ 7.2	6.15		
1214	0.95	12.76	2.616	1.81	6.58	19.3	5.90		
1219	1.05	12.77	2.616	1.73	6.58	26.5	5.79		
1229	1.20	12.74	2.614	1.70	6.58	33.9	5.83		
1234	1.30	12.74	2.614	1.68	6.58	35.1	5.76		
1239	1.40	12.73	2.613	1.65	6.58	36.0	5.80	↓	↓
1240		PUMP OFF							
1241		START SAMPLE COLLECTION							
1308		SAMPLE COMPLETED : 2 L IPEC							
1308		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 51-40

SAMPLE ID: 017

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Cloudy 50°

PROJECT NO: 01 0017969.92
DATE: 11/30/10
SAMPLER(S): Miguel Britos

SAMPLING INTERVAL (depth in ft below top of casing)
29.7 to 44.2

TOTAL VOLUME PURGED: 2.45 gal

SAMPLING PORT
40 7

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1120	0	PUMP ON						6.5 / 8.4	24
1130	0.05	12.61	2.624	4.20	6.83	-84.9			
1135	0.15	12.75	2.574	4.52	6.81	-71.6	0.01		
1142	0.30	13.00	2.547	5.00	6.81	-48.4	0.02		
1149	0.65	13.01	2.540	5.07	6.81	-17.1	0.03		
1155	0.80	13.03	2.539	5.00	6.80	-3.2	0.0		
1200	1.0	13.07	2.539	5.12	6.80	+5.9	0.0		
1206	1.2	13.08	2.540	5.14	6.79	+9.5	0.0		
1214	1.45	13.10	2.540	5.22	6.79	29.1	0.0		
1219	1.80	13.13	2.541	5.24	6.78	36.2	0.0		
1229	2.05	13.10	2.541	5.29	6.78	43.4	0.0		
1234	2.15	13.11	2.542	5.32	6.78	44.7	0.0		
1239	2.30	13.11	2.542	5.33	6.78	45.3	0.0	↓	↓
1240		PUMP OFF							
1241		START SAMPLE COLLECTION							
1254		SAMPLE COMPLETED : 2 L IPEC							
1254		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde	2
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 40.162

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
 DATE: 11/29/10
 SAMPLER(S): M.S

SAMPLING INTERVAL (depth in ft below top of casing)
158.7 to 190.3

TOTAL VOLUME PURGED: 0.60 gal

SAMPLING PORT
162

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1040	0	PUMP ON						6/9	44
1050	0.01	12.40	1.250	2.60	6.04	-127.7	—	↓	↓
1100	0.10	11.70	1.261	0.86	5.98	-117.5	—		
1110	0.20	11.97	1.254	0.66	5.92	-106.6	1.01		
1118	0.25	12.08	1.253	0.54	5.92	-102.5	0.82		
1124	0.30	12.10	1.253	0.49	6.09	-99.3	0.77		
1133	0.35	12.10	1.254	0.48	6.17	-94.5	0.39		
1139	0.40	12.12	1.255	0.48	6.19	-93.9	0.36		
1146	0.45	12.13	1.254	0.50	6.22	-91.4	0.34		
1147		PUMP OFF							
1148		START SAMPLE COLLECTION							
1245		SAMPLE COMPLETED : 2 L IPEC							
1245		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 3563 Sonde	1
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 40-127

SAMPLE ID: 016

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
DATE: 11/29/10
SAMPLER(S): M.B

SAMPLING INTERVAL (depth in ft below top of casing)
125.2 to 136.7

TOTAL VOLUME PURGED: 1.50 gal

SAMPLING PORT
127 2

PURGE RATE: variable (gal / min)
PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1040	0							619	44
1050	0.05	13.83	2.174	2.28	6.58	-105.9	—		
1100	0.30	13.89	2.189	0.92	6.81	-122.6	—		
1110	0.55	14.28	2.195	0.60	7.00	-134.1	2.85		
1118	0.75	14.03	2.199	0.47	7.05	-137.7	2.73		
1124	0.85	13.93	2.200	0.49	7.07	-140.4	1.37		
1133	0.95	13.89	2.206	0.45	7.08	-143.6	0.60		
1139	1.05	13.85	2.205	0.41	7.08	-145.1	0.57		
1146	1.15	13.98	2.207	0.41	7.09	-147.9	0.43		
1156	1.30	14.03	2.205	0.41	7.08	-150.0	0.47		
1201	1.35	13.96	2.207	0.40	7.09	-151.9	0.44		
1202		PUMP OFF							
1203		START SAMPLE COLLECTION							
1226		SAMPLE COMPLETED: 2 L IPEC							
1226		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200704243

NOTES AND OBSERVATIONS:

WELL ID: MW 40-100

SAMPLE ID: 016

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
 DATE: 11/29/10
 SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
93.2 to 106.7

TOTAL VOLUME PURGED: 3.05 gal

SAMPLING PORT
100

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

3

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1040	0	PUMP ON						6/9	44
1050	0.1	14.29	2.776	2.45	6.18	-74.6	—	↓	↓
1100	0.4	14.45	2.704	0.54	6.45	-79.8	—		
1110	0.9	14.53	2.687	0.40	6.60	-51.5	16.70		
1118	1.2	14.40	2.678	0.46	6.64	40.1	15.98		
1124	1.5	14.34	2.674	0.49	6.6	32.9	14.97		
1133	1.8	14.30	2.666	0.56	6.69	23.2	16.38		
1139	2.0	14.24	2.665	0.57	6.70	-19.1	17.08		
1146	2.5	14.23	2.660	0.59	6.70	-17.6	17.45		
1156	2.9	14.21	2.656	0.60	6.69	-16.8	16.96		
1157		PUMP OFF							
1158		START SAMPLE COLLECTION							
1212		SAMPLE COMPLETED				2 L IPEC			
1212		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 40.81

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
DATE: 11/29/10
SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
64.7 to 84.2

TOTAL VOLUME PURGED: 3.05 gal

SAMPLING PORT
81

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

4

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)		
1040	0	PUMP ON						6/9	44		
1050	0.1	15.11	5.370	5.07	6.13	-17.9	=	↓	↓		
1100	0.5	14.98	4.971	2.68	6.21	-14.5	=				
1110	1.1	14.88	4.927	2.26	6.29	-9.7	0.58				
1118	1.4	14.74	4.904	2.19	6.30	-7.0	0.51				
1124	1.7	14.62	4.882	2.12	6.31	-3.0	0.60				
1133	2.3	14.54	4.900	2.10	6.30	-2.4	0.61				
1139	2.5	14.56	4.897	2.07	6.30	-2.1	0.64				
1146	2.9	14.58	4.905	2.05	6.31	-2.8	0.60				
1147		PUMP OFF, START SAMPLE COLLECTION									
1203		SAMPLE COMPLETED									
1203		PUMP OFF									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 40.46

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
 DATE: 11/29/10
 SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
44.2 to 53.7

TOTAL VOLUME PURGED: 0.55 gal

SAMPLING PORT
46 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1339	0	PUMP ON						5/9	20
1348	0.05	14.19	5.522	0.81	6.56	-48.3		5/9	18
1353	0.10	14.10	5.527	0.52	6.50	-55.8	0.76		
1358	0.12	13.68	5.565	0.44	6.50	-56.6	0.74		
1406	0.16	12.96	5.549	0.36	6.54	-45.8	0.79		
1414	0.20	12.34	5.534	0.27	6.57	-34.5	0.82		
1424	0.25	12.49	5.537	0.22	6.60	-26.7	1.19		
1434	0.30	12.52	5.547	0.22	6.62	-14.0	1.32		
1444	0.35	12.45	5.556	0.20	6.62	-11.3	1.22		
1450	0.38	12.48	5.555	0.19	6.62	-10.8	1.25		
1455	0.40	12.51	5.555	0.19	6.62	-9.9	1.22		
1456		PUMP OFF							
1457		START SAMPLE COLLECTION							
1636		SAMPLE COMPLETED : 2 L IPEC							
1636		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>2</u>
turbidity meter	<u>200704293</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 40-27

SAMPLE ID: 013

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01 0017869.92
 DATE: 11/29/10
 SAMPLER(S): M.B

SAMPLING INTERVAL (depth in ft below top of casing)
18.2 to 35.2

TOTAL VOLUME PURGED: 1.50 gal

SAMPLING PORT
27 6

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1339	0	PUMP ON						5/9	20
1348	0.01	14.56	4.360	7.48	6.69	-54.7	—	5/9	18
1353	0.05	14.33	4.472	6.11	6.44	-14.1	3.56		
1358	0.10	14.33	4.462	5.40	6.36	+6.9	3.88		
1406	0.25	14.27	4.449	4.98	6.40	30.4	3.49		
1414	0.45	14.20	4.435	4.77	6.44	53.6	2.98		
1424	0.60	14.49	4.445	4.80	6.49	64.4	0.58		
1434	0.95	14.60	4.459	4.51	6.51	74.9	0.45		
1444	1.15	14.57	4.467	4.48	6.52	76.2	0.51		
1450	1.25	14.62	4.468	4.52	6.53	77.6	0.49		
1455	1.35	14.64	4.471	4.49	6.54	78.2	0.52	↓	↓
1456		PUMP OFF							
1457		START SAMPLE COLLECTION							
1523		SAMPLE COMPLETED : 2 L IPEC							
1523		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 54-190

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017369.92
 DATE: 11/23/10
 SAMPLER(S): M.B

SAMPLING INTERVAL (depth in ft below top of casing)
185.0 to 203.6

TOTAL VOLUME PURGED: 2.10 gal

SAMPLING PORT
190

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1059	0	PUMP ON						7.5/6.7	35
1109	0.05	21.23	2.084	1.69	5.85	-1.4	-		36
1119	0.15	21.48	2.077	0.36	5.99	-39.1	1.82		
1129	0.35	21.50	2.074	0.22	6.35	-35.6	0.05		
1139	0.70	21.12	2.072	0.09	6.72	-6.5	0.00		
1147	1.15	21.09	2.071	0.10	6.79	+1.9	0.0		
1153	1.45	21.06	2.071	0.10	6.83	+6.8	0.0		
1201	1.75	20.03	2.071	0.11	6.85	7.2	0.0		
1206	1.95	20.01	2.072	0.10	6.87	7.3	0.0	↓	↓
1207		PUMP OFF							
1208		START							
1222		SAMPLE COMPLETED			: 2	L IPEC			
1222		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW-54-173

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/23/10
 SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
170.5 to 182.0

TOTAL VOLUME PURGED: 2.65 gal

SAMPLING PORT
173

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

2

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1059	0							7.5/6.7	35
1109	0.05	21.38	1.846	1.96	5.96	-116.6	0.90	↓	36
1119	0.20	21.54	1.873	0.40	6.13	-118.0	0.21		
1129	0.50	21.33	1.877	0.30	6.42	-84.0	0.00		
1139	1.05	20.95	1.876	0.24	6.72	+19.9	0.00		
1147	1.35	20.90	1.876	0.24	6.79	+29.8	0.00		
1153	1.65	20.73	1.876	0.23	6.83	34.0	0.00		
1201	1.90	20.69	1.875	0.23	6.84	35.8	0.00		
1206	2.00	20.65	1.875	0.23	6.85	36.9	0.00		
1211	2.50	20.64	1.874	0.23	6.86	37.3	0.00		
1212		PUMP OFF							
1213		START SAMPLE COLLECTION							
1225		SAMPLE COMPLETED : 2 L IPEC							
1225		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW-54-144

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/23/10
 SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
135.0 to 155.5

TOTAL VOLUME PURGED: _____ gal

SAMPLING PORT
144 3

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1059	0	PUMP ON						7.5/6.7	35
1109	0.05	21.40	2.013	1.58	6.30	-36.7	—	↓	36
1119	0.25	21.63	1.970	0.53	6.45	-29.1	0.68		
1129	0.55	21.33	1.953	0.41	7.15	-12.5	0.11		
1139	1.30	20.92	1.957	0.34	7.23	+17.9	0.00		
1147	1.60	20.87	1.961	0.3	7.2	+29.8	0.00		
1153	2.00					39.5			
1201	2.50					46.9			
1206	2.70	20.63	1.968	0.30	7.26	48.7			
1211		20.62		0.29	7.26	49.8	0.00		
1216	3.25	20.60	1.968	0.30	7.27	50.4	0.00		
1217		PUMP OFF							
1218		START SAMPLE COLLECTION							
1230		SAMPLE COMPLETED : 2 L IPEC							
1230		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	200701254 ⁶

NOTES AND OBSERVATIONS:

WELL ID: MW 54-123

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: cloudy 50's

PROJECT NO: 01.0017869.92
DATE: 11/23/10
SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
116.0 to 126.0

TOTAL VOLUME PURGED: 0.95 gal

SAMPLING PORT
123

PURGE RATE: variable (gal / min)
PURGE METHOD: Double Valve Pump

4

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressu (psi)
1345	0	PUMP ON						6/4	20
1353	0.05	22.02	1.882	1.19	6.16	-71.9	—	↓	↓
1403	0.20	22.07	1.883	0.50	6.43	-85.3	0.13	↓	↓
1411	0.30	21.96	1.887	0.34	6.70	-96.3	0.00	↓	↓
1420	0.45	21.94	1.890	0.29	6.89	-101.6	0.00	↓	↓
1429	0.70	21.90	1.891	0.27	6.93	-102.2	0.00	↓	↓
1434	0.80	21.87	1.891	0.26	6.96	-103.8	0.00	↓	↓
1435		PUMP OFF							
1436		START							
1512		SAMPLE COMPLETED : 2 L IPEC							
1512		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 54-58

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/23/10
 SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
51.5 to 64.0

TOTAL VOLUME PURGED: 1.85 gal

SAMPLING PORT
58

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

5

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressu (psi)
1345	0	PUMP ON						6/4	20
1353	0.05	21.90	1.743	1.37	6.37	-104.1	—	↓	↓
1403	0.35	21.62	1.667	0.39	6.42	-95.7	0.00		
1411	0.60	21.51	1.664	0.33	6.54	-93.7	0.01		
1420	1.0	21.47	1.677	0.30	6.69	-89.8	0.0		
1429	1.3	21.42	1.693	0.31	6.73	-84.0	0.0		
1434	1.45	21.42	1.696	0.31	6.75	-82.2	0.0		
1439	1.70	21.41	1.702	0.32	6.78	-80.8	0.0		
1440		PUMP OFF							
1441		START SAMPLE COLLECTION							
1455		SAMPLE COMPLETED : 2 L IPEC							
1455		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 54-37

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: cloudy 50's

PROJECT NO: 01.0017869.92
DATE: 11/23/10
SAMPLER(S): MB

SAMPLING INTERVAL (depth in ft below top of casing)
29.0 to 42.0

TOTAL VOLUME PURGED: 2.35 gal

SAMPLING PORT
37

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1345	0							6/4	20
1353	0.05	21.86	1.898	6.60	7.00	-33.9	—	↓	↓
1403	0.4	21.65	1.864	5.63	7.10	+23.6	1.14	↓	↓
1411	0.8	21.58	1.864	5.58	7.12	33.1	1.05	↓	↓
1420	1.5	21.55	1.865	5.09	7.13	39.2	1.19	↓	↓
1429	2.0	21.53	1.867	5.06	7.14	40.7	1.23	↓	↓
1434	2.2	21.51	1.868	5.02	7.14	41.5	1.25	↓	↓
1435									
1436									
1447									
1447									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>200701254</u>

NOTES AND OBSERVATIONS:

WELL ID: LAF-002
 SAMPLE ID: 014

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY

PROJECT NO: 01.0017869.92
 DATE: 11/22/10
 SAMPLER(S): M.B
 PUMP DEPTH: _____ ft

WEATHER: Sun + clouds 60°F

WATER QUALITY: DTW = 74.40 Transducer Actual Depth _____

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Purged Notes H ₂ O (gal)
1040	74.40		PUMP	ON				5/28	48	
1050	74.45							5/30	48	0
1055	74.50	13.87	1.334	8.96	6.49	234.2	—	↓	↓	0.01
1101	74.55	13.89	2.534	5.64	6.21	230.6	2.26	↓	↓	0.20
1117	74.60	13.62	2.514	1.96	6.26	42.1	0.56	5/43	40	
1130	74.60	14.63	2.497	1.67	6.30	38.1	0.78	5/30	40	0.25
1136	74.61	15.01	2.500	1.65	6.31	37.5	0.72			
1141	74.62	15.30	2.497	1.58	6.31	38.1	0.79			
1146	74.62	15.59	2.494	1.56	6.32	32.1	0.78			0.30
1151	74.61	15.61	2.491	1.53	6.32	31.7	0.80			0.32
1156	74.61	15.64	2.491	1.54	6.32	33.0	0.77	↓	↓	
1157		START SAMPLE COLLECTION								
1441		SAMPLE COMPLETED: 2 L IPEC								
1441		PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.45 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: I-2
 SAMPLE ID: 002

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Showers, cloudy, windy 60's

PROJECT NO: 01.001786992
 DATE: 11/17/10
 SAMPLER(S): M B
 PUMP DEPTH: 38.28 ft

WATER QUALITY: DTW = 31.42 Transducer Actual Depth = 7.480 transd. read = 5074

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1153	7.481		PUMP	ON					
1240			Change sampling method to Modified traditional Purge.						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	
turbidity meter	

NOTES AND OBSERVATIONS: Total volume purged _____ gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: I-2
SAMPLE ID: 002

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Showers, cloudy, windy 60's

PROJECT NO: 01.0017869.92
DATE: 11/17/10
SAMPLER(S): MB

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{40.13}{DTB} - \frac{31.42}{DTW} = \frac{8.71}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 8.71 x 0.163 = 1.42 gal

Multiplier Well Volume

1.42 x 1.5 = 2.13 gal

Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = 31.42 Transducer Actual Depth = 7.480 Transd. read = 50.74

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1242	0	7.481		PUMP ON					
1253	0.3	7.092	16.00	1.113	8.30	6.56	58.1	-	
1303	0.5	6.827	15.64	1.096	9.33	6.58	65.0	-	
1312	0.75	6.756	15.46	1.103	9.57	6.63	68.3	-	
1319	1.05	6.709	15.88	1.118	9.19	6.69	70.7	-	
1327	1.25	6.586	15.61	1.126	9.29	6.70	70.8	-	
1332	1.40	6.544	15.69	1.130	8.79	6.73	70.9	-	
1337	1.55	6.402	15.75	1.135	8.25	6.75	71.1	-	
1345	1.80	6.374	15.83	1.139	7.64	6.77	71.2	-	
1350	2.0	6.342	15.80	1.136	7.01	6.78	71.4	-	
1355	2.15	6.324	15.77	1.131	6.61	6.80	71.6	-	
1356			START SAMPLE COLLECTION						
1425			SAMPLE COMPLETED : 2 L IPEC						
1425			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	-

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

Used two peristaltic pumps in line.

WELL ID: MW 39-195

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
193.0 to 198.6

TOTAL VOLUME PURGED: 0.65 gal

SAMPLING PORT
195 1

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1127	0							8/10	70
1140	0.05	16.42	1.281	1.70	6.50	-165.0	—	↓	↓
1150	0.10	16.34	1.275	1.04	6.57	-165.4	1.28		
1200	0.15	16.18	1.268	0.68	6.67	-166.9	0.99		
1207	0.20	16.03	1.258	0.55	6.67	-174.0	0.59		
1214	0.30	15.98	1.250	0.42	6.79	-184.4	0.51		
1222	0.40	15.80	1.244	0.36	6.90	-198.1	0.53		
1227	0.45	15.78	1.241	0.35	6.91	-202.0	0.54		
1232	0.50	15.77	1.238	0.34	6.93	-205.7	0.50		
1233		PUMP OFF							
1234		START SAMPLE COLLECTION							
1325		SAMPLE COMPLETED : 2 L IPEC							
1325		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-183

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, 50's

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
169.5 to 186.0

TOTAL VOLUME PURGED: 1.75 gal

SAMPLING PORT
183 2

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1149	0.05							8/10	70
1140	0.05	16.51	1.134	1.60	6.89	-91.0			
1150	0.20	16.37	1.143	0.97	7.03	-85.5	1.10		
1200	0.50	16.20	1.138	0.62	7.11	-69.6	0.91		
1207	0.70	16.13	1.129	0.50	7.12	-62.1	0.57		
1214	1.0	16.00	1.118	0.41	7.12	-59.6	0.62		
1222	1.25	15.86	1.111	0.39	7.12	-57.9	0.59		
1227	1.40	15.84	1.109	0.37	7.13	-57.1	0.61		
1232	1.60	15.80	1.105	0.36	7.13	-56.6	0.63	↓	↓
1233		PUMP OFF							
1234		START SAMPLE COLLECTION							
1253		SAMPLE COMPLETED				2 L	IPEC		
1253		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-124

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
1150 to 126.5

TOTAL VOLUME PURGED: 3.35 gal

SAMPLING PORT
124 3

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1127								8/10	70
1140	0.1	16.27	2.645	2.60	6.23	-173.6	—	↓	↓
1150	0.4	16.08	2.664	1.49	6.19	-224.1	16.21		
1200	0.9	15.86	2.653	0.90	6.24	-261.8	11.70		
1207	1.3	15.75	2.642	0.75	6.30	-267.2	7.85		
1214	2.0	15.70	2.570	1.58	6.37	-222.7	10.28		
1222	2.5	15.64	2.549	1.55	6.4	-209.0	7.49		
1227	2.8	15.61	2.548	1.55	6.4	-205.6	7.55		
1232	3.2	15.58	2.547	1.58	6.4	-200.9	7.48		
1233		PUMP OFF							
1234		START SAMPLE COLLECTION							
1246		SAMPLE COMPLETED			2	L IPEC			
1246		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-102

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
93.0 to 103.0

TOTAL VOLUME PURGED: 0.70 gal

SAMPLING PORT
102

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

4

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1359	0							6/14	32
1411	0.01	15.65	2.540	2.97	6.62	-137.5	-	6/16	34
1421	0.20	15.62	2.548	2.63	6.78	-142.1	1.63		
1431	0.22	15.46	2.549	2.55	6.92	-140.3	1.45		
1438	0.30	15.96	2.535	2.61	6.94	-139.4	1.63		
1448	0.35	16.13	2.543	2.66	6.99	-139.7	0.67		
1455	0.40	15.85	2.547	2.70	7.05	-130.2	0.59		
1505	0.45	15.83	2.537	2.81	7.11	-114.3	0.51		
1514	0.50	16.22	2.537	2.87	7.11	-112.7	0.49		
1519	0.53	16.26	2.537	2.86	7.11	-110.8	0.49		
1524	0.55	16.22	2.538	2.89	7.12	-109.2	0.52	↓	↓
1525		PUMP OFF							
1526		START SAMPLE COLLECTION							
1612		SAMPLE COMPLETED : 2 L IPEC							
1612		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-84

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
76.5 to 85.0

TOTAL VOLUME PURGED: 0.80 gal

SAMPLING PORT
84 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1359	0	PUMP ON						6/14	32
1411	0.01	15.74	2.243	6.47	6.54	-109.0	—	6/16	34
1421	0.1	15.70	2.256	3.52	6.51	-71.3	2.13	↓	↓
1431	0.15	15.59	2.255	3.31	6.51	-61.9	1.74		
1438	0.20	15.76	2.254	3.33	6.51	-54.3	1.83		
1448	0.25	16.09	2.253	3.23	6.57	-44.3	1.44		
1455	0.30	15.97	2.252	3.17	6.56	-36.2	1.48		
1505	0.35	15.88	2.247	3.15	6.58	-23.1	1.39		
1514	0.40	16.10	2.245	3.13	6.60	-17.1	1.45		
1519	0.45	16.19	2.248	3.16	6.62	-10.0	1.47		
1524	0.48	16.14	2.251	3.13	6.63	-4.1	1.43		
1529	0.50	16.09	2.252	3.10	6.62	-0.9	1.39		
1535	0.55	16.01	2.253	3.14	6.62	+1.0	1.40		
1541	0.60	15.98	2.253	3.16	6.62	+1.5	1.42		
1548	0.65	15.95	2.255	3.20	6.61	+1.9	1.45		
1549		PUMP OFF							
1550		START SAMPLE COLLECTION							
1638		SAMPLE COMPLETED : 2 L IPEC							
1638		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-67

SAMPLE ID: 010

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's

PROJECT NO: 01.0017369.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
65.0 to 70.5

TOTAL VOLUME PURGED: 1.40 gal

SAMPLING PORT
67 7

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1359	0	PUMP	ON					6/14	32
1411	0.01	15.86	1.893	9.42	7.27	-65.1	—	6/16	34
1421	0.25	15.87	1.921	10.15	7.40	-25.2	1.25		
1431	0.50	15.90	2.007	10.02	7.50	+18.9	1.10		
1438	0.70	16.10	2.006	9.50	7.47	28.1	1.34		
1448	0.80	16.34	2.027	8.87	7.38	37.2	1.49		
1455	0.90	16.17	2.044	8.36	7.25	40.0	1.42		
1505	1.0	16.22	2.057	7.41	7.17	42.1	1.49		
1514	1.05	16.26	2.060	6.99	7.14	42.4	1.47		
1519	1.08	16.22	2.066	6.83	7.11	43.2	1.39		
1524	1.10	16.24	2.069	6.76	7.11	43.9	1.37		
1529	1.15	16.19	2.080	5.20	7.08	45.4	1.42		
1535	1.20	16.06	2.092	5.16	7.07	47.4	1.45		
1541	1.25	16.03	2.099	5.13	7.06	47.5	1.49	↓	↓
1542		PUMP	OFF						
1543		START	SAMPLE COLLECTION						
1608		SAMPLE	COMPLETED : 2 L IPEC						
1628		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW-56-53

SAMPLE ID: 009

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: MOSTLY CLOUDY, SU

PROJECT NO: 01.0017869.92
 DATE: 11/15/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 47.42 Transducer Actual Depth

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes gal
1138	47.42	PUMP ON	DN					717.5	28	
1143	47.89	17.78	1.917	3.88	6.25	-74.0	—	↓		0.01
1150	48.13	17.49	1.535	2.75	6.55	-87.0	3.12	617		0.20
1200	48.12	17.38	1.770	1.91	6.81	-52.7	2.02	↓		0.40
1210	48.12	17.32	1.974	1.26	6.93	-19.9	1.58	↓		0.60
1215	48.12	17.41	2.054	1.12	6.97	-13.7	1.37	↓		0.70
1220	48.13	17.39	2.112	1.09	6.99	-11.8	1.28	↓		0.80
1225	48.13	17.40	2.154	1.10	7.02	-11.4	1.24	↓		0.90
1227	START SAMPLE COLLECTION									
1248	END SAMPLE COLLECTION: 2L IPEC									
	PUMP OFF									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

Total volume purged 1.15 gal

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-56-83
SAMPLE ID: 011

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: MOSTLY CLOUDY, 52'S

PROJECT NO: 01.0017869.92
DATE: 11/5/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{83}{\text{DTB}} - \frac{47.38}{\text{DTW}} = \frac{35.62}{\text{Water Column Height}}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 35.62 x $\frac{0.041}{\text{Multiplier}}$ = 1.46 gal

1.46 x 1.5 = 2.19 gal

TOTAL VOLUME PURGED: 2.40 gal

WATER QUALITY: DTW = 47.38 Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1343	0	---	PUMP ON						
1349	0.01	---	16.58	0.274	3.96	6.86	72.8	114.6	
1355	0.10	---	16.30	0.782	2.26	6.57	37.6	118.0	
1400	0.25	---	16.69	1.355	0.90	6.54	37.1	146.4	
1405	0.50	---	17.09	1.390	0.76	6.66	36.7	180.4	
1408	0.75	---	16.99	1.583	0.83	6.67	44.2	125.5	
1413	1.00	---	16.89	1.753	1.49	6.73	56.6	62.95	
1416	1.25	---	16.82	1.789	1.83	6.77	62.7	59.17	
1419	1.50	---	16.82	1.800	2.08	6.79	65.9	36.00	
1422	1.75	---	16.77	1.801	2.07	6.81	68.0	38.40	
1425	2.00	---	16.73	1.799	1.90	6.82	69.5	31.83	
1427	2.20	---	16.73	1.794	1.88	6.83	70.1	48.27	
1428	START	SAMPLE COLLECTION							
1437	END	SAMPLE COLLECTION: 2L IPEC							
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	2011701234

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-5150

SAMPLE ID: 023

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, 40%

PROJECT NO: 010017869.92
 DATE: 11/21/10
 SAMPLER(S): EPS
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 8.30 Transducer Actual Depth 32.735

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (%l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1042	32.738	PUMP ON							
1102	32.730	20.47	2.534	2.43	6.96	200.1	0.72		0.07
1110	32.730	21.21	2.633	1.30	7.14	199.4	0.62		0.25
1115	32.741	21.83	2.675	0.86	7.25	180.9	0.56		0.30
1120	32.750	22.20	2.674	0.64	7.34	172.3	0.61		0.40
1125	32.755	22.31	2.702	0.60	7.38	157.0	0.55		0.50
1130	32.761	22.42	2.704	0.56	7.44	141.4	0.54		0.60
1135	32.766	22.49	2.707	0.50	7.47	131.2	0.52		0.70
1140	32.777	22.50	2.708	0.49	7.49	132.4	0.51		0.75
1144	START SAMPLE COLLECTION								
1210	END SAMPLE COLLECTION 12:15 P.M.								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	1
turbidity meter	200101254

NOTES AND OBSERVATIONS: Total volume purged 0.90 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: WV-50.66
 SAMPLE ID: 028

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny, 40s

PROJECT NO: 01 0017869.92
 DATE: 11/2/10
 SAMPLER(S): CB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 10.59 Transducer Actual Depth 89.240

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1042	88.197	Pump	0.0						gal
1107	88.197	20.76	2.221	1.30	7.19	140.6	1.23		0.05
1110	87.603	21.20	2.221	0.63	7.22	103.7	1.05		0.20
1115	87.760	21.58	2.221	0.49	7.25	73.4	1.12		0.30
1120	87.122	21.76	2.221	0.49	7.26	40.9	0.90		0.38
1125	88.000	21.74	2.220	0.61	7.28	31.7	0.93		0.42
1130	88.140	21.66	2.220	0.64	7.28	22.4	0.90		0.48
1135	88.140	21.61	2.221	0.68	7.28	18.8	0.86		0.54
1140	88.155	21.61	2.222	0.72	7.28	16.8	0.89		0.60
1145	START SAMPLE COLLECTION								
1230	END SAMPLE COLLECTION - IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	4
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.80 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msf

WELL ID: MW-49-2W
 SAMPLE ID: 022

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SWANNY, 40S

PROJECT NO: 01 0017869.92
 DATE: 11/1/10
 SAMPLER(S): COMB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 12.13 Transducer Actual Depth 12.622 Transducer read = 2.111

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1020	12.13								
1150	12.15								PUMP ON
1218	11.95	13.69	2.645	2.20	7.02	188.7	---		0.10
1230	10.82	14.98	2.649	1.02	7.11	122.9	0.63		0.50
1240	10.62	15.52	2.648	0.98	7.14	118.4	0.61		0.60
1250	10.58	15.70	2.647	0.70	7.15	114.8	0.58		0.75
1256	10.44	15.84	2.645	0.77	7.16	115.9	0.68		0.85
1302	10.33	15.07	2.653	0.70	7.17	114.3	0.62		0.85
1312	10.21	13.69	2.692	0.67	7.17	123.1	0.55		0.90
1318	10.15	12.95	2.652	0.62	7.16	120.8	0.60		1.00
1328	10.06	13.87	2.643	0.65	7.18	113.8	0.62		1.05
1336	9.97	13.90	2.639	0.68	7.17	112.9	0.65		1.10
1342	9.91	13.87	2.635	0.68	7.18	112.0	0.67		1.20
1344	START SAMPLE COLLECTION								
1423	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
Flow meter	3
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 1.35 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-49-42
 SAMPLE ID: 022

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny, 40's

PROJECT NO: 01 0017869.92
 DATE: 11/10
 SAMPLER(S): 551M3
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 11.71 Transducer Actual Depth 15.864 Transducer = 2.713

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1104	15.864								
1156	16.090								PUMP ON
1218	16.553	12.37	2.570	4.18	6.46	215.8	—		0.105
1230	16.780	13.07	2.542	2.36	6.45	159.0	0.82		0.120
1240	16.880	13.92	2.552	2.06	6.47	141.0	0.86		0.130
1250	16.989	14.00	2.567	1.61	6.51	125.1	0.93		0.140
1256	17.071	14.01	2.579	1.57	6.53	117.7	0.93		0.145
1302	17.222	13.93	2.585	1.26	6.55	111.5	0.80		0.150
1312	17.263	13.87	2.590	1.26	6.57	104.1	0.82		0.160
1318	17.329	13.86	2.591	1.25	6.59	107.3	0.81		0.170
1327	START	SAMPLE	COLLECTION						
1413	END	SAMPLE	COLLECTION: 21						IPEC
									PUMP OFF

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	2
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.85 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl

WELL ID: M60-49-105
 SAMPLE ID: 022

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, 40'S

PROJECT NO: 01.0017869.92
 DATE: 11/11/10
 SAMPLER(S): CB, MPS
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 11.94 Transducer Actual Depth = 13.923 Transducer read = 2399

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1033	13.923								
1150	14.577								
			PUMP ON						
1218	14.891	11.74	2.309	3.98	7.24	237.2	—		0.105
1230	14.921	11.93	2.423	2.21	7.31	202.5	1.13		0.10
1240	15.102	12.07	2.446	1.75	7.31	189.8	1.02		0.20
1250	15.228	12.22	2.462	1.53	7.32	172.9	1.08		0.25
1256	15.305	12.30	2.471	1.36	7.32	165.4	1.02		0.30
1302	15.393	12.35	2.478	1.24	7.32	155.9	0.97		0.35
1312	15.417	12.41	2.482	1.20	7.33	143.3	1.06		0.40
1318	15.510	14.08	2.494	0.91	7.33	133.4	0.93		0.50
1328	15.630	14.09	2.496	1.29	7.34	127.7	0.93		0.60
1336	15.684	14.18	2.501	1.31	7.34	125.6	0.93		0.65
1340	START SAMPLE COLLECTION								
1418	END SAMPLE COLLECTION								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	4
turbidity meter	2007012-24

NOTES AND OBSERVATIONS: Total volume purged 0.75 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 58-26
 SAMPLE ID: 011

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny, windy 40's

PROJECT NO: 01 (X)17869.92
 DATE: 11/11/10
 SAMPLER(S): CG, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 7.43 Transducer Actual Depth = 17.808 transd read = 6.838

Time	DTW Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1149	7.40	PUMP ON							
1207	7.50	12.53	1.074	1.52	7.70	-267	—	0.4	
1212	7.50	12.40	1.079	1.27	7.74	-37.7	4.59		
1220	7.50	11.88	1.090	2.26	7.74	-69.3	4.42		0.06
1230	7.50	11.27	1.097	0.99	7.75	-78.8	3.77		0.1
1239	7.50	11.81	1.095	0.77	7.73	-77.4	3.21		0.15
1249	7.50	11.95	1.097	0.87	7.71	-89.9	3.10		0.20
1259	7.50	11.97	1.099	0.89	7.71	-95.1	3.15		0.25
1305	7.50	11.98	1.105	0.90	7.69	-93.9	3.09	✓	0.30
1307		START SAMPLE COLLECTION							
1512		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	5
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.45 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-58-65
 SAMPLE ID: 011

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny, windy 40's

PROJECT NO: 01 (X)17869.92
 DATE: 11/11/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 7.21 Transducer Actual Depth = 62.675 ^{transd.} read = 7.614

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1149	62.663		PUMP	ON					
1207	62.576	12.91	0.908	1.27	6.36	-77.9	—	0.8	0.10
1212	62.591	13.13	0.905	0.64	6.44	-77.0			0.15
1220	62.652	12.60	0.903	1.05	6.61	-98.7	1.10		0.30
1230	62.631	11.88	0.901	0.60	6.74	-100.4	0.90		0.40
1239	62.670	12.99	0.898	0.45	6.88	-112.0	0.80		0.50
1249	62.705	13.40	0.895	0.50	6.98	-114.0	0.55		0.65
1259	62.733	13.47	0.891	0.48	6.99	-113.3	0.49		0.80
1309	62.760	13.49	0.890	0.46	7.01	-112.9	0.53	↓	0.90
1307	START SAMPLE C								
1353	SAMPLE COMPLETED		: 2 L IPEC						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 1.05 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-06-21

SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, WINDY, 40-5

PROJECT NO: 01 0017869.92
 DATE: 11/10/10
 SAMPLER(S): CR, MPS
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 12.67 Transducer Actual Depth 8.088

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1027	8.160	PUMP ON							
1106	8.210	15.84	1.217	2.48	7.06	143.8	13.15		0.05
1115	8.407	15.96	1.190	0.98	7.16	-154.8	10.18		0.20
1125	8.584	15.14	1.153	0.42	7.17	-159.0	4.87		0.55
1135	8.960	14.91	1.144	0.40	7.19	-157.4	5.90		0.50
1140	8.993	15.18	1.129	0.32	7.22	-159.9	4.45		0.60
1145	9.025	16.00	1.122	0.28	7.24	-151.9	6.01		0.70
1150	9.110	16.64	1.116	0.22	7.26	-153.8	4.84		0.80
1155	9.185	16.60	1.113	0.20	7.27	-177.6	5.10		0.90
1200	9.245	16.44	1.111	0.24	7.25	-177.0	5.80		0.95
1205	9.241	16.42	1.108	0.24	7.24	-176.9	5.58		1.05
1210	9.295	16.40	1.103	0.24	7.26	-175.8	5.71		1.10
1213	START SAMPLE COLLECTION								
1513	END SAMPLE COLLECTION - 2.6 IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	3
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 1.30 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msf.

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WELL ID: MW-61-36
SAMPLE ID: 014

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, WINDY, 40s

PROJECT NO: 01 (0)17869.92
DATE: 11/10/10
SAMPLER(S): CB, MS
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 12.05 Transducer Actual Depth 12.413

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1027	12.535	PUMP ON							
1106	12.744	13.46	2.300	2.14	6.54	-98.0	1.70		0.05
1115	12.826	13.50	2.427	1.19	6.73	-97.8	1.71		0.10
1125	12.874	13.93	2.483	0.83	6.76	-94.1	1.22		0.25
1135	12.949	14.43	2.519	0.78	6.81	-85.4	0.80		0.40
1140	12.947	14.67	2.558	0.69	6.83	-78.7	0.84		0.50
1145	13.057	15.23	2.549	0.53	6.84	-80.1	0.81		0.60
1150	13.082	15.68	2.560	0.49	6.88	-85.9	0.82		0.70
1155	13.137	15.72	2.556	0.41	6.90	-90.1	0.81		0.80
1159	START SAMPLE COLLECTION								
1233	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	4
turbidity meter	200704245

NOTES AND OBSERVATIONS: Total volume purged 0.907 gal
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msf.

WELL ID: MW 67-340

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/10/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
335.3 to 347.9

TOTAL VOLUME PURGED: 1.65 gal

SAMPLING PORT
340

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1233	0	PUMP ON						6/6	45
1241	0.1	16.47	0.731	1.49	6.67	-90.4	—	6/6	45
1246	0.2	16.37	0.731	0.74	6.78	-107.9	1.58	6/6	50
1254	0.4	15.89	0.728	0.41	6.98	-171.4	1.27	↓	↓
1301	0.6	15.58	0.724	0.30	7.02	-178.4	0.93		
1308	0.75	15.51	0.723	0.28	7.03	-186.7	1.05		
1315	1.0	15.52	0.725	0.23	7.04	-203.5	1.01		
1320	1.3	15.53	0.726	0.22	7.03	-211.6	0.98		
1328	1.5	15.55	0.728	0.21	7.05	-215.9	1.04		
1329		PUMP OFF							
1330		START SAMPLE COLLECTION							
1353		SAMPLE COMPLETED : 2 L IPEC							
1353		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 67-323

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/10/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
317.8 to 328.3

TOTAL VOLUME PURGED: 2.30 gal

SAMPLING PORT
323 2

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1233	0							6/6	45
1241	0.05	16.39	0.876	1.70	6.72	-117.0	—	6/6	45
1246	0.1	16.27	0.870	0.80	6.82	-124.5	2.01	6/6	50
1254	0.25	16.03	0.868	0.09	6.95	-167.8	1.90		
1301	0.50	16.28	0.860	—	6.88	-188.6	1.32		
1308	0.65	18.41	0.780	—	6.88	-198.2	0.98		
1315	0.85	24.91	0.593	—	6.88	-206.2	1.07		
1320	1.0	33.75	0.411	—	6.86	-240.2	0.98		
1330		REPLACED YSI #6 with YSI #2					1.07		
		and continue readings							
1343	1.40	16.39	0.850	0.22	7.01	253.5	—		
1353	1.60	16.00	0.843	0.10	6.98	-279.5	1.01		
1359	1.85	15.69	0.826	0.08	6.97	-286.0	0.98		
1406	2.00	15.72	0.824	0.07	6.98	-283.2	0.94		
1411	2.15	15.76	0.821	0.07	6.98	-281.9	0.99	↓	↓
1412		PUMP OFF							
1413		START SAMPLE COLLECTION							
1435		SAMPLE COMPLETED 7 2 L IPEC							
1435		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	
turbidity meter	<u>6</u> 200701294

NOTES AND OBSERVATIONS:

WELL ID: MW 67-276

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
DATE: 11/10/10
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
250.8 to 281.3

TOTAL VOLUME PURGED: 3.05 gal

SAMPLING PORT
276 3

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1233	0							6/6	45
1241	0.15	16.84	0.935	0.71	6.42	-63.4	-	6/6	45
1246	0.25	16.63	0.936	0.43	6.56	-78.0	0.93	6/6	50
1254	0.60	16.27	0.932	0.20	6.69	-63.7	0.88		
1301	0.90	15.97	0.928	0.16	6.72	-50.8	0.87		
1308	1.10	15.87	0.924	0.17	6.73	-44.5	0.70		
1315	1.40	15.87	0.922	0.30	6.74	-42.4	0.72		
1320	1.70	16.70	0.919	0.28	6.73	-40.2	0.74		
1343	2.50	16.78	0.924	0.11	6.76	-39.5	1.00		
1353	2.70	16.74	0.927	0.09	6.73	-38.8	1.02		
1359	2.90	16.72	0.927	0.08	6.74	-38.0	1.05		
1400		PUMP OFF							
1401		START	SAMPLE COLLECTION						
1416		SAMPLE COMPLETED			: 2 L IPEC				
1416		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>3</u> <u>200701254</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 67-219

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
DATE: 11/10/10
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
209 to 229.8

TOTAL VOLUME PURGED: 2.25 gal

SAMPLING PORT
219 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1233	0							6/6	45
1241	0.2	17.00	1.144	1.09	6.54	-123.5	-	6/6	45
1246	0.35	16.64	1.151	0.71	6.62	-122.7	0.95	6/6	50
1254	0.65	16.32	1.152	0.40	6.59	-110.3	0.85		
1301	0.00	16.02	1.150	0.32	6.57	-109.9	0.89	↓	↓
1308	1.50	16.01	1.149	0.28	6.58	-107.5	0.74	↓	↓
1315	1.75	16.02	1.148	0.23	6.62	-104.0	0.85	↓	↓
1320	2.10	16.04	1.148	0.21	6.59	-102.7	0.75	↓	↓
1321		PUMP OFF							
1322		START SAMPLE COLLECTION							
1340		SAMPLE COMPLETED : 2 L IPEC							
1340		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>5</u> 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 67-173

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy, 40's

PROJECT NO: 01.0017869.92
 DATE: 11/10/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
164.8 to 188.3

TOTAL VOLUME PURGED: 1.25 gal

SAMPLING PORT
173 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1028	0	PUMP						8/8	20
1040	0.2	14.71	1.211	0.81	6.51	-14.3	—		
1047	0.25	14.62	1.208	0.60	6.55	-54.6	6.27		
1052	0.30	14.65	1.197	0.47	6.60	-95.1	2.82		
1102	0.50	14.79	1.177	0.28	6.66	-152.8	2.82		
1114	0.70	14.80	1.170	0.25	6.67	-168.3	2.71		
1119	0.80	14.93	1.164	0.25	6.68	-177.3	2.66		
1126	0.90	14.91	1.157	0.21	6.70	-202.4	2.60		
1131	1.00	14.91	1.151	0.21	6.71	-210.9	2.58		
1136	1.10	14.90	1.149	0.20	6.72	-217.8	2.53	↓	↓
1137		PUMP OFF							
1138		START SAMPLE COLLECTION							
1204		SAMPLE COMPLETED : 2 L IPEC							
1204		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 67-105

SAMPLE ID: 014

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/10/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
90.3 to 110.8

TOTAL VOLUME PURGED: 1.15 gal

SAMPLING PORT
105 6

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1028	0	PUMP ON						8 / 8	20
1040	0.2	14.38	1.517	0.81	6.44	-132.4			
1047	0.3	14.32	1.509	0.63	6.50	-138.2			
1052	0.4	14.36	1.506	0.50	6.56	-141.2	2.14		
1102	0.6	14.42	1.506	0.39	6.64	-142.9	1.71		
1107	0.75	14.53	1.508	0.36	6.67	-145.1	1.71		
1114	0.90	14.56	1.506	0.35	6.71	-147.6	1.68		
1119	1.00	14.60	1.502	0.35	6.72	-148.2	1.65		
1120		PUMP OFF							
1121		START SAMPLE COLLECTION							
1142		SAMPLE COMPLETED : 2 L IPEC							
1142		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 67 - 39

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/10/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
28.8 to 54.3

TOTAL VOLUME PURGED: 2.45 gal

SAMPLING PORT
39 7

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1028	0	PUMP ON						8/8	20
1040	0.3	15.01	3.504	1.54	5.78	-116.8	—		
1047	0.45	15.06	3.595	0.98	5.92	-139.0			
1052	0.60	15.20	3.623	0.75	6.07	-166.0	1.24		
1102	1.00	15.22	3.682	0.56	6.27	-179.5	1.17		
1107	1.20	15.33	3.678	0.49	6.33	-195.0	1.08		
1114	1.50	15.40	3.680	0.50	6.45	-200.6	1.05		
1119	1.70	15.42	3.681	0.49	6.49	-197.7	1.00		
1126	1.85	PUMP OFF	3.701	0.44	6.57	-206.2	1.00		
1131	2.15	15.55	3.704	0.42	6.61	-210.0	1.01		
1136	2.30	15.56	3.705	0.40	6.63	-207.6	0.98	↓	↓
1137		PUMP OFF							
1137		START SAMPLE COLLECTION							
1149		SAMPLE COMPLETED 1.2 L IPEC							
1149		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW-62-18
 SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: WINDY, P. CLOUDY, 40

PROJECT NO: 01 0017869.92
 DATE: 11/09/15
 SAMPLER(S): CB, MPS
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 12.71 Transducer Actual Depth 3.728

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1000	4.115	PLUM	PUM						
1015	4.275	13.05	1.936	2.90	7.44	197.9	2.13		0.01
1025	4.380	11.86	2.117	3.03	7.41	161.1	1.50		0.1
1035	4.504	10.17	2.242	3.49	7.42	115.7	1.00		0.2
1045	4.618	10.27	2.244	3.44	7.42	55.6	0.65		0.25
1050	4.667	10.24	2.585	3.25	7.44	27.4	0.45		0.3
1055	4.720	10.87	3.712	2.81	7.45	61.5	0.39		0.32
1100	4.787	10.85	3.710	2.20	7.41	-19.7	0.37		0.36
1105	4.842	10.82	3.715	2.01	7.44	-25.1	0.35		0.40
1110	4.906	10.80	3.719	1.98	7.44	-29.8	0.34		0.44
1111	START SAMPLE COLLECTION								
1157	END SAMPLE COLLECTION 7:15 PM								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
Flow meter	2
turbidity meter	2000 701754

NOTES AND OBSERVATIONS: Total volume purged 0.55 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WELL ID: MW-62-37
SAMPLE ID: 015

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: WINDY, P. CLOUDY, 40

PROJECT NO: 010017869.92
DATE: 11/04/10
SAMPLER(S): CR, MPS
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 11.9' Transducer Actual Depth 10.63'

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1000	10.725	PUMP	P ON						#1
1015	10.872	10.73	1.513	1.80	7.33	-84.16	1.74		0.07
1025	10.923	10.71	1.507	1.21	7.37	-92.4	0.83		0.07
1035	11.065	10.42	1.505	1.01	7.45	-103.1	0.72		0.15
1045	11.064	10.30	1.504	1.01	7.46	-103.2	0.70		0.22
1050	11.096	10.41	1.507	0.85	7.47	-104.5	0.69		0.25
1055	11.134	10.43	1.504	0.87	7.48	-106.8	0.67		0.32
1100	11.182	10.46	1.505	0.89	7.49	-108.7	0.66		0.35
1108	START SAMPLE COLLECTION								
1156	END SAMPLE COLLECTION. 2L IPEC.								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	4
turbidity meter	20070127-1

NOTES AND OBSERVATIONS: Total volume purged 0.150 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 62-182

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/9/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
177.6 to 198.7

TOTAL VOLUME PURGED: 1.45 gal

SAMPLING PORT
182

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1310	0	PUMP ON						6/4	30
1318	0.01	16.29	1.250	1.87	6.61	-92.9	-	↓	↓
1323	0.1	16.25	1.238	0.94	6.70	-103.7	1.27		
1328	0.2	16.37	1.225	0.67	6.82	-90.7	0.92		
1335	0.35	16.14	1.226	0.32	6.93	-81.6	1.01		
1340	0.50	15.96	1.225	0.27	7.00	-57.5	0.77		
1350	0.60	15.87	1.224	0.21	7.08	-43.5	0.56		
1358	0.80	15.91	1.224	0.23	7.10	-40.0	0.49		
1405	1.0	15.88	1.224	0.21	7.10	-38.2	0.42		
1410	1.15	15.88	1.224	0.21	7.11	-37.4	0.40		
1416	1.30	15.88	1.225	0.21	7.12	-36.5	0.43		
1417		PUMP OFF							
1417		START SAMPLE COLLECTION							
1443		SAMPLE COMPLETED 1.2 L IPEC							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 62-138

SAMPLE ID: 015

**GZA GeoEnvironmental of New York
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/9/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
126.1 to 143.6

TOTAL VOLUME PURGED: 1.65 gal

SAMPLING PORT
138 3

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1310	0							6/4	30
1318	0.05	16.55	1.565	1.60	6.83	1.9	-		
1323	0.20	16.53	1.588	0.90	7.02	-6.3	0.93		
1328	0.35	16.65	1.609	0.63	7.23	-6.3	0.36		
1335	0.50	16.29	1.629	0.45	7.32	-4.5	0.72		
1340	0.60	15.99	1.631	0.38	7.34	-2.9	0.80		
1350	0.80	16.25	1.631	0.33	7.37	-2.0	0.54		
1358	1.0	16.30	1.633	0.30	7.38	-1.7	0.39		
1505	1.3	16.34	1.632	0.29	7.38	-1.4	0.36		
1410	1.5	16.36	1.631	0.28	7.38	-1.1	0.39	↓	↓
1411		PUMP OFF							
1412		START							
1431		SAMPLE COMPLETED							
1431		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 62 - 53

SAMPLE ID: 014

**GZA GeoEnvironmental of New York
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
 DATE: 11/9/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
49.6 to 54.1

TOTAL VOLUME PURGED: 0.70 gal

SAMPLING PORT
53 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	
1043	0		PUMP ON					5 6	25	
1050	0.05	14.95	1.431	1.74	6.14	-91.2	—			
1058	0.10	13.60	1.440	0.94	6.28	-58.7	4.08			
1105	0.20	12.73	1.398	0.58	6.84	-43.2	5.67			
1113	0.25	12.17	1.393	0.46	6.88	-8.1	4.81			
1121	0.30	11.78	1.387	0.39	6.93	20.7	4.68			
1128	0.35	11.80	1.385	0.33	6.99	25.5	4.41			
1137	0.40	11.81	1.384	0.31	7.03	33.7	4.22			
1142	0.45	11.83	1.382	0.30	7.03	37.9	4.07			
1147	0.50	11.82	1.381	0.29	7.04	39.1	4.00			
1152	0.55	11.81	1.380	0.29	7.05	40.4	3.96	↓	↓	
1153			PUMP OFF							
1154			START SAMPLE COLLECTION							
1249			SAMPLE COMPLETED: 2 L IPEC							
1249			PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 62 - 71

SAMPLE ID: 015

GZA GeoEnvironmental of New York
Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Cloudy, windy 40's

PROJECT NO: 01.0017869.92
DATE: 11/9/10
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
61.1 to 82.6

TOTAL VOLUME PURGED: 1.45 gal

SAMPLING PORT
71 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1043	0		PUMP ON					5/6	25
1050	0.01	14.15	1.337	2.00	6.72	59.0	-		
1058	0.20	14.42	1.318	0.69	7.07	-10.6	0.51		
1105	0.35	14.45	1.416	0.69	7.29	-48.2	0.70		
1113	0.55	14.43	1.415	0.48	7.36	-65.4	0.78		
1121	0.75	14.29	1.413	0.39	7.4	-72.2	0.77		
1128	1.0	14.33	1.411	0.36	7.42	-77.9	0.79		
1137	1.20	14.32	1.410	0.34	7.43	-79.4	0.80		
1142	1.30	14.31	1.408	0.34	7.44	-80.2	0.78		
1143			PUMP OFF						
1144			START SAMPLE COLLECTION						
1102			SAMPLE COMPLETED: 2 L IPEC						
1102			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 62-92

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Cloudy, Windy 40's

PROJECT NO: 01.0017869.92
DATE: 11/9/10
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
88.6 to 99.1

TOTAL VOLUME PURGED: 1.35 gal

SAMPLING PORT
92 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1043	0							5 6	25
1050	0.01	13.48	1.405	2.23	7.11	-113.3			
1058	0.20	13.96	1.376	1.01	6.99	-129.2	0.53		
1105	0.25	13.80	1.323	0.70	6.42	-114.3	1.23		
1113	0.40	13.61	1.324	0.50	6.46	-103.7	1.05		
1121	0.60	13.64	1.319	0.43	6.49	-95.1	0.60		
1128	0.80	13.55	1.320	0.40	6.53	-106.1	0.50		
1137	1.00	13.91	1.319	0.37	6.56	-97.1	0.57		
1142	1.10	13.97	1.318	0.36	6.58	-97.3	0.54		
1147	1.20	14.00	1.321	0.35	6.59	-96.6	0.53	↓	↓
1148		PUMP OFF							
1149		START SAMPLE COLLECTION							
1115		SAMPLE COMPLETED: 2 L IPEC							
1115		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>5</u> <u>200704293</u>

NOTES AND OBSERVATIONS:

WELL ID: U1-CSS
 SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Rain, Wind, Low 40's

PROJECT NO: 01 0017869 92
 DATE: 11/08/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 5.87 Transducer Actual Depth 8.515

Time	DTW or (Actual Depth)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1204	8.514	PUMP ON							
1235	8.086	19.19	1.747	6.64	7.37	174.2	4.43	21	0.01
1240	8.094	19.30	1.733	6.15	7.47	171.1	4.12	1	0.004
1245	8.132	19.39	1.723	5.96	7.53	171.0	3.43		0.07
1250	8.157	19.41	1.722	5.98	7.58	170.3	2.59		0.10
1255	8.182	19.47	1.717	6.26	7.61	169.3	2.98		0.12
1300	8.191	19.50	1.715	6.09	7.65	167.7	1.74		0.14
1305	8.204	19.57	1.711	6.56	7.67	166.9	1.94		0.16
1310	8.220	19.57	1.709	6.57	7.69	165.8	1.89		0.18
1315	8.238	19.57	1.707	6.58	7.71	164.7	1.84		0.20
1316	START SAMPLE COLLECTION								
1456	END SAMPLE COLLECTION, 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
Flow meter	4
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.35 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 30-69(036)

SAMPLE ID: 036

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Showers, 53°F

PROJECT NO: 01.0017869.92
 DATE: 11/05/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
67.3 to 71.3

TOTAL VOLUME PURGED: 0.80 gal

SAMPLING PORT
69

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1050	0	PUMP ON						6 12	40
1054	0.01	23.25	1.228	8.48	8.01	95.2	---		
1059	0.10	23.94	1.222	8.70	8.15	88.7	---		
1105	0.25	24.33	1.203	8.63	8.17	76.0	---		
1110	0.35	24.46	1.190	8.76	8.18	62.1	---		
1115	0.45	24.45	1.205	8.82	8.17	60.2	---		
1120	0.55	24.47	1.206	8.74	8.17	57.5	---		
1125	0.65	24.44	1.208	8.80	8.17	55.2	---		
1127	START SAMPLE COLLECTION								
1156	END SAMPLE COLLECTION: 2L IPEC 0.5L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	1

NOTES AND OBSERVATIONS:

WELL ID: MW 30-84

SAMPLE ID: 027

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Showers, 53°F

PROJECT NO: 01.0017869.92
 DATE: 11/05/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
77.3 to 85.4

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT
84

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1050	0	PUMP ON	DN					6/12	40
1059	0.01	22.14	1.717	3.93	6.73	-16.5	—		
1105	0.07	22.11	1.731	3.91	6.81	-20.5	—		
1110	0.12	22.09	1.732	3.74	6.86	-17.2	—		
1115	0.15	21.84	1.737	3.70	6.90	-75.1	—		
1120	0.18	21.51	1.741	3.64	6.93	-10.3	—		
1125	0.20	21.10	1.744	3.63	6.95	-6.9	—		
1130	0.22	20.77	1.745	3.42	6.97	-5.9	—		
1135	0.25	20.42	1.745	3.70	6.98	-6.7	—		
1140	0.40	23.08	1.78	9.19	7.31	-16.4	—		44
1145	0.50	23.39	1.730	9.04	7.77	-13.6	—		
1150	0.60	23.44	1.730	9.05	7.81	-12.1	—		
1155	0.70	23.45	1.735	9.66	7.80	-11.5	—		
1155	START SAMPLE COLLECTION								
1235	END SAMPLE COLLECTION (DN) 2 IPEC DISLIFE								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2

NOTES AND OBSERVATIONS:

WELL ID: MW-36-24
 SAMPLE ID: 020

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Rain 40's

PROJECT NO: 01 0017869.92
 DATE: 11/4/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 4.72 Transducer Actual Depth 59.241 Transd read = 6.868

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (µl)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Nuts (gal)
1455	59.283								
1501	59.283	29.73	5.500	4.60	7.24	19.2	3.31		
1506	59.285	28.61	5.531	1.96	7.23	26.1	1.40		
1516	59.287	28.53	5.521	0.70	7.21	37.6	1.14		0.15
1522	59.281	27.90	5.515	0.57	7.29	34.5			0.25
1530	59.278	27.99	5.494	0.24	7.30	32.6			0.45
1537	59.274	28.46	5.485	0.34	7.36	32.9			0.75
1546	59.277	28.49	5.482	0.33	7.38	33.1			0.85
1552	59.273	28.51	5.483	0.32	7.41	34.0			0.95
1553		START SAMPLE COLLECTION							
1615		SAMPLE COMPLETED 2 L IPEC							
1615		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	2
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged _____ gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-36-41
SAMPLE ID: 014

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Rain 40's

PROJECT NO: 01.0017869.92
DATE: 11/4/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{41}{\text{DTB}} \cdot \frac{4.97}{\text{DTW}} = \frac{36.03}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } \underline{36.03} \times \frac{\underline{0.041}}{\text{Multiplier}} = \underline{1.48} \text{ gal}$$

$$\underline{1.48} \times 1.5 = \underline{2.22} \text{ gal}$$

Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1455	0	—	PUMP ON						
1501	0.1	—	24.70	4.502	0.70	8.07	-156.0	3.36	
1506	0.4	—	24.91	4.208	1.14	7.94	-143.5	2.23	
1516	0.9	—	25.31	3.719	1.25	7.81	-120.2	1.86	
1522	1.2	—	25.64	3.184	1.11	7.72	-111.5	1.75	
1530	1.4	—	25.91	2.866	1.20	7.63	-103.2	1.59	
1537	1.65	—	26.11	2.816	1.27	7.61	-96.4	2.19	
1546	1.80	—	26.27	2.792	1.32	7.59	-90.2	2.95	
1558	1.95	—	26.14	2.837	1.51	7.56	-85.9	3.76	
1605	2.15	—	26.24	2.861	1.62	7.55	-82.7	4.99	
1606			START SAMPLE COLLECTION						
1655			SAMPLE COMPLETED: 2 L IPEC						
1655			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-36-52
SAMPLE ID: 019

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Rain 40's

PROJECT NO: 01.0017869.92
DATE: 11/4/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{52}{\text{DTB}} \cdot \frac{5.36}{\text{DTW}} = \frac{46.640}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 46.640 x 0.041 = 1.912 gal

Multiplier Well Volume

1.912 x 1.5 = 2.87 gal

Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = 5.36 Transducer Actual Depth 46.217 Transd read = 6.353

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1455	0	46.217	PUMP ON						
1501	0.25	44.521	23.92	1.923	0.34	7.09	-78.1	3.09	
1506	0.55	41.386	23.62	1.917	0.29	7.09	-73.5	1.21	
1516	1.0	38.191	23.93	1.822	0.29	7.08	-80.4	1.49	
1522	1.50	35.428	23.86	1.763	0.21	7.07	-80.4	1.36	
1530	1.90	32.811	23.63	1.696	0.25	7.07	-81.5	1.49	
1537	2.35	29.585	23.47	1.716	0.20	7.06	-75.7	1.44	
1545	2.75	27.586	23.28	1.728	0.19	7.06	-76.9	1.49	
1546		START SAMPLE COLLECTION							
1555		SAMPLE COMPLETED: 2 L IPEC							
1555		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-37-22
 SAMPLE ID: 020

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: RAIN, 40's

PROJECT NO: 01 0017869.92
 DATE: 11/04/10
 SAMPLER(S): CBMB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 9.79 Transducer Actual Depth 12.131

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1052	12.144	Pump	ON						
1135	12.105	25.26	4.350	2.32	7.29	-29.3	1.40		0.01
1140	12.132	25.35	4.363	2.28	7.29	-40.5	1.27		0.05
1145	12.146	25.12	4.379	2.15	7.29	-43.0	1.30		0.08
1150	12.144	24.83	4.388	1.97	7.29	-43.0	1.31		0.10
1155	12.119	24.91	4.379	1.90	7.28	-48.5	1.16		0.12
1200	12.136	24.99	4.380	1.95	7.29	-50.1	1.00		0.14
1205	12.088	25.07	4.381	2.00	7.29	-51.8	1.02		0.16
1210	12.090	25.02	4.385	1.97	7.29	-51.9	1.01		0.18
1215	START SAMPLE COLLECTION								
1428	END SAMPLE COLLECTION: 21 IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
Flow meter	1
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.32 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-31-32
 SAMPLE ID: 020

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: RAIN, 40'S

PROJECT NO: 01 0017869.92
 DATE: 11/04/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 9.70 Transducer Actual Depth 14.846

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (u/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1052	14.859	Pump Down							gal
1140	14.829	25.14	3.101	1.33	7.18	213.4	0.57		0.01
1145	14.830	25.07	3.086	1.18	7.17	206.9	0.23		0.05
1150	14.821	25.01	3.095	1.07	7.18	197.1	0.22		0.10
1155	14.840	25.19	3.088	0.96	7.21	195.0	0.33		0.15
1200	14.842	25.36	3.079	0.77	7.23	191.9	0.06		0.20
1205	14.798	25.39	3.072	0.75	7.25	187.5	0.01		0.25
1210	14.845	25.73	3.073	0.72	7.28	181.4	0.00		0.30
1215	14.831	25.86	3.075	0.70	7.28	181.3	0.00		0.35
1220	14.821	25.96	3.076	0.66	7.28	179.7	0.00		0.40
1225	14.811	25.93	3.078	0.64	7.29	177.4	0.00		0.45
1226	START SAMPLE COLLECTION								
1314	END SAMPLE COLLECTION: 2 IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	4
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged: 0.55 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-37-40
SAMPLE ID: 020

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Rain 40's

PROJECT NO: 01.0017869.92
DATE: 11/4/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{40}{\text{DTB}} \cdot \frac{8.63}{\text{DTW}} = \frac{31.37}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } 31.37 \times \frac{0.041}{\text{Multiplier}} = \frac{1.29}{\text{Well Volume}} \text{ gal}$$

$$\frac{1.29}{\text{Designed Purge Volume}} \times 1.5 = \frac{1.93}{\text{Well Volume}} \text{ gal}$$

TOTAL VOLUME PURGED: 2.10 gal

WATER QUALITY: DTW = 8.63 Transducer Actual Depth 31,231

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Purged Notes H ₂ O (gal)
1123	0	PUMP ON							
1126	0.05	—	25.98	1.945	0.99	7.14	-142.3	—	
1130	0.15	—	26.17	1.931	0.48	7.23	-201.4	9.50	
1135	0.50	—	26.10	1.908	0.27	7.27	-235.9	978.1	
1140	0.90	—	25.90	1.902	0.14	7.26	-245.9	106.7	
1145	1.15	—	25.70	1.898	0.12	7.26	-239.2	519.2	
1150	1.50	—	25.76	1.895	0.14	7.27	-222.8	1011	
1155	1.80	—	25.75	1.892	0.20	7.28	-204.2	1035	
1157	1.95	—	25.74	1.892	0.22	7.28	-201.9	21100	
1158		START SAMPLE COLLECTION							
1206		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

*Continue purging after sampling to de-silt well.
Turbidity > 1100 ntu. Very silty level.*

WELL ID: MW-37-57
 SAMPLE ID: 020

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: RAIN, 40%

PROJECT NO: 010017869.92
 DATE: 11/04/10
 SAMPLER(S): CLMB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 8.45 Transducer Actual Depth 42.247

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1052	42.235	PUMP	ON						
1130	41.241	24.17	1.943	3.24	6.72	151.7	—		
1135	41.111	24.33	1.937	3.16	6.73	140.4	0.86		0.05
1140	41.343	24.39	1.935	2.91	6.75	134.4	0.87		0.07
1145	41.337	24.16	1.937	2.63	6.77	127.9	0.80		0.09
1150	41.332	23.80	1.929	2.47	6.78	123.2	0.82		0.11
1155	41.309	23.96	1.927	2.39	6.79	118.3	0.51		0.13
1200	41.315	24.16	1.918	2.29	6.82	117.3	0.59		0.15
1205	41.330	24.32	1.907	2.31	6.84	116.8	0.42		0.17
1210	42.141	24.44	1.900	2.48	6.86	117.0	0.42		0.19
1215	42.182	24.38	1.896	2.37	6.87	116.8	0.42		0.21
1219	START SAMPLE COLLECTION								
1349	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	3
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.35 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 31-49

SAMPLE ID: 028

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, 40°C

PROJECT NO: 01.0017869.92
 DATE: 11/03/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
34.8 to 49.3

TOTAL VOLUME PURGED: 3.90 gal

SAMPLING PORT
49

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1050	0	PUMP	0.0					1017	29
1055	0.1	18.29	1.648	9.33	6.47	128.3			
1058	0.25	18.47	1.651	10.22	6.42	121.4	2.17		
1100	0.50	18.53	1.682	10.63	6.40	116.5	3.09		
1105	1.00	18.56	1.660	10.79	6.42	108.7	2.24		
1110	1.25	18.57	1.641	10.33	6.46	106.6	1.67		
1115	1.50	18.56	1.603	11.11	6.50	100.4	2.14		
1120	2.00	18.52	1.583	11.02	6.53	97.7	3.43		
1125	2.50	18.46	1.559	10.70	6.57	95.6	1.73		
1130	2.75	18.52	1.940	10.83	6.59	94.5	2.18		
1135	3.00	18.51	1.520	10.88	6.62	93.5	1.32		
1140	3.50	18.49	1.511	10.90	6.64	93.0	1.25		
1145	3.75	18.43	1.505	10.93	6.67	92.3	1.29		
1146	START	SAMPLE	COLLECTION						
1155	ENDS	SAMPLE	COLLECTION	0.5L	IPEC				
					IPEC				

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 31-63

SAMPLE ID: 028

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, 40S

PROJECT NO: 01.0017869.92
 DATE: 11/03/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
55.8 to 63.8

TOTAL VOLUME PURGED: 0.55 gal

SAMPLING PORT
63

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1050	0	PUMP	DN					6/7	29
1100	0.05	15.47	1.218	0.99	7.00	-35.4	2.02		
1105	0.10	15.72	1.169	1.34	7.08	-47.3	1.46		
1110	0.15	15.94	1.139	1.63	7.12	-44.8	1.79		
1115	0.20	16.16	1.108	1.90	7.16	-38.1	0.81		
1120	0.25	16.31	1.092	2.23	7.18	-32.2	0.93		
1125	0.30	16.34	1.086	2.48	7.19	-21.8	0.54		
1130	0.35	16.33	1.082	2.50	7.20	-16.4	0.52		
1135	0.40	16.40	1.088	2.52	7.20	-11.9	0.50		
1138	START SAMPLE COLLECTION								
1200	END SAMPLE COLLECTION								
1232	0.5 L IPEC								
	0.5 L IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	700704293

NOTES AND OBSERVATIONS:

WELL ID: MW 31-85

SAMPLE ID: 028

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, 40S

PROJECT NO: 01.0017869.92
 DATE: 11/03/10
 SAMPLER(S): CHMB

SAMPLING INTERVAL (depth in ft below top of casing)
109.8 to 85.4

TOTAL VOLUME PURGED: 1.00 gal

SAMPLING PORT
85'

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1050	0	PUMP ON						617	29
1058	0.1	16.29	1.597	1.74	6.63	-65.2	0.73		
1100	0.15	16.67	1.602	2.25	6.66	-70.7	0.41		
1105	0.20	17.05	1.639	3.12	6.71	-58.8	0.30		
1110	0.25	17.17	1.658	3.32	6.74	-51.6	0.27		
1115	0.30	17.31	1.690	3.49	6.77	-48.6	0.27		
1120	0.35	17.32	1.707	3.52	6.79	-42.7	0.27		
1125	0.40	17.31	1.713	3.51	6.78	-40.3	0.27		
1129	START	SAMPLE	COLLECTION						
1200	ENDS	SAMPLE	COLLECTION	1.20 IPEC					
				0.51 IPEC					

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 700704293

NOTES AND OBSERVATIONS:

WELL ID: MW 32-85

SAMPLE ID: 025

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 50°F

PROJECT NO: 01.0017869.92
 DATE: 11/3/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
79.3 to 92.8

TOTAL VOLUME PURGED: 0.75 gal

SAMPLING PORT
85

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

5

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1053	0	PUMP ON						8/11	40
1103	0.01	16.66	1.606	1.28	6.64	-114.2	—		
1111	0.05	15.21	1.624	1.20	6.69	-97.8	2.29		
1120	0.15	14.37	1.608	0.85	6.63	-75.7	2.17		
1125	0.20	13.84	1.606	0.83	6.72	-60.6	1.97		
1131	0.25	14.39	1.590	0.78	6.75	-54.7	1.32		
1138	0.30	14.77	1.585	0.65	6.79	-48.4	0.74		
1146	0.40	14.89	1.591	0.57	6.81	-42.0	0.80		
1151	0.44	14.95	1.583	0.56	6.81	-36.0	0.79		
1156	0.48	15.06	1.579	0.55	6.83	-34.7	0.64		
1201	0.54	15.09	1.587	0.52	6.84	-32.9	0.62		
1206	0.60	15.11	1.585	0.52	6.85	-31.6	0.60	↓	↓
1207		PUMP OFF							
1207		START SAMPLE COLLECTION							
1245		SAMPLE COMPLETED ; 2 L IPEC							
1245		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32-59

SAMPLE ID: 022

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 50°F

PROJECT NO: 01.0017869.92
 DATE: 11/3/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
28.3 to 61.3

TOTAL VOLUME PURGED: 2.65 gal

SAMPLING PORT
59 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	
								8/11	40	
1103	0.05	17.19	0.460	5.89	6.75	163.2	—	↓	↓	
1111	0.15	17.48	0.422	5.32	6.85	150.4	1.71			
1120	0.55	18.79	0.370	5.17	7.67	141.2	1.38			
1125	0.90	18.79	0.367	5.25	7.83	139.4	1.10			
1131	1.20	18.80	0.366	5.24	7.94	137.2	1.03			
1138	1.50	18.86	0.360	5.26	8.03	134.0	1.12			
1146	2.0	18.87	0.335	5.02	8.15	129.6	0.75			
1151	2.25	18.91	0.333	5.02	8.16	127.9	0.80			
1156	2.50	18.95	0.334	5.08	8.17	127.2	0.77			
1156		PUMP OFF								
1157		START	SAMPLE COLLECTION							
1208		SAMPLE COMPLETED				2 L	IPEC			
1208		PUMP OFF			0.5 L	IPEC				

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32-190

SAMPLE ID: 024

**GZA GeoEnvironmental of New York
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 50° F

PROJECT NO: 01.0017869.92
 DATE: 11/3/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
180.3 to 193.9

TOTAL VOLUME PURGED: 1.05 gal

SAMPLING PORT
190

PURGE RATE: variable (gal / min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1356	0	PUMP ON						10 12	58
1420	0.05	16.70	1.797	1.02	6.68	-134.9	—		
1430	0.15	16.34	1.797	0.89	6.84	-143.4	0.80		
1436	0.20	16.46	1.787	0.78	6.92	-150.5	0.58		
1442	0.30	16.55	1.785	0.53	7.01	-148.6	0.26		
1456	0.50	16.61	1.790	0.34	7.09	-133.9	0.14		
1502	0.60	16.57	1.790	0.32	7.10	-131.7	0.13		
1511	0.80	16.67	1.783	0.26	7.10	-128.0	0.12		
1520	0.90	16.65	1.786	0.25	7.11	-124.0	0.11		
1525	START SAMPLE COLLECTION								
1607	END SAMPLE COLLECTION: 2L IPEC 0.5L IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32-173

SAMPLE ID: 020

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 50°F

PROJECT NO: 01.0017869.92
 DATE: 11/3/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
165.8 to 174.3

TOTAL VOLUME PURGED: 1.20 gal

SAMPLING PORT
173

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

2

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1356	0	PUMP ON						10/12	58
1420	0.10	16.97	1.992	0.83	6.59	-158.3	—		
1430	0.30	17.01	2.010	0.42	6.61	-150.4	1.85		
1436	0.40	17.10	2.028	0.30	6.57	-135.4	1.31		
1442	0.50	17.18	2.036	0.28	6.73	-128.2	0.98		
1456	0.80	17.12	2.043	0.18	6.89	-107.8	0.85		
1502	0.40	17.05	2.044	0.17	6.91	-109.1	0.81		
1511	1.00	17.09	2.046	0.15	6.90	-104.4	0.78		
1519	START SAMPLE COLLECTION								
1553	END SAMPLE COLLECTION								
				0.5L TPEC					
				0.5L TPEC					

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32-149

SAMPLE ID: 022

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sunny 50°F

PROJECT NO: 01.0017869.92
DATE: 11/3/10
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
147.3 to 156.8

TOTAL VOLUME PURGED: 1.10 gal

SAMPLING PORT
149

PURGE RATE: variable (gal/min)
PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1356	0	PUMP ON						10/12	58
1420	0.10	15.59	2.099	2.08	6.50	-122.3	—		
1430	0.15	16.12	2.125	0.64	6.59	-139.0	1.67		
1436	0.18	16.23	2.153	0.42	6.67	-143.3	1.43		
1442	0.20	16.41	2.173	0.29	6.76	-139.6	0.61		
1456	0.45	16.54	2.212	0.22	6.87	-130.3	0.44		
1502	0.55	16.48	2.215	0.19	6.89	-125.2	0.41		
1511	0.70	16.54	2.225	0.20	6.90	-117.4	0.39		
1520	0.85	16.63	2.224	0.19	6.91	-112.3	0.38		
1528	0.95	16.63	2.224	0.21	6.93	-109.3	0.37		
1532	START SAMPLE COLLECTION								
11009	END SAMPLE COLLECTION! 2L IPEC 0.5L IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW-63-18
SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MID 40's

PROJECT NO: 01 0017869.92
DATE: 11/02/10
SAMPLER(S): CB, MB
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 11.13 Transducer Actual Depth 6.231

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
10:22	6.077	PUMP ON	0.0						gal
11:24	5.889	16.31	1.917	3.68	6.85	-106.0	16.62		0.01
11:34	5.889	16.49	2.759	1.05	6.82	-132.6	16.96		0.08
11:42	5.889	16.92	2.220	0.91	6.84	-127.7	10.85		0.11

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	1
turbidity meter	200-254

NOTES AND OBSERVATIONS: Total volume purged _____ gal
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet asl.

PURGING AS SLOW AS POSSIBLE, THOUGH WATER LEVEL KEEPS DRIPPING GREATER THAN 0.3'. SWITCHED PURGE METHOD TO MODIFIED TRADITIONAL AT 11:58

2 of 2

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-6378
SAMPLE ID: 015

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MID 40'S

PROJECT NO: 01.0017869.92
DATE: 11/2/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{18}{\text{DTB}} - \frac{11.13}{\text{DTW}} = \frac{6.87}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } \frac{6.87}{\text{Multiplier}} \times \frac{0.041}{\text{Well Volume}} = \frac{0.28}{\text{gal}}$$

$$\frac{0.28}{\text{Designed Purge Volume}} \times 1.5 = \frac{0.42}{\text{gal}}$$

TOTAL VOLUME PURGED: 0.75 gal

WATER QUALITY: DTW = Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1202	0.22	5.264	17.34	2.097	0.96	6.85	-122.6	8.13	
1208	0.30	5.131	18.17	2.060	0.66	6.88	-134.8	5.22	
1212	0.45	5.108	18.90	1.975	0.65	6.91	-129.0	4.58	
1215	START	SAMPLE COLLECTION							
1222	END	SAMPLE COLLECTION - 2L FILL							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>3</u>
turbidity meter	<u>2802701254</u>

NOTES AND OBSERVATIONS:
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-63-34
SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MD-40's

PROJECT NO: 01.0017869.92
DATE: 11/02/10
SAMPLER(S): CB, MB
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 11.14 Transducer Actual Depth 13.554

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1032	13.481	PUMP ON							
1124	13.057	16.38	1.361	7.67	7.30	10.10	6.52		0.01
1134	12.990	16.36	1.355	5.78	7.28	-4.0	4.76		0.02
1142	12.929	16.30	1.361	5.27	7.30	-4.3	5.20		0.60

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	3
turbidity meter	2007 01254

NOTES AND OBSERVATIONS: Total volume purged _____ gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.
 PURGING AS SLOW AS POSSIBLE, THOUGH WATER LEVEL KEEPS DRIPPING
 GREATER THAN 0.3'. SWITCHED PURGE METHOD TO MODIFIED TRADITIONAL AT 11:58

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-63-34
SAMPLE ID: 015

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MID -40'S

PROJECT NO: 01.0017869.92
DATE: 1/6/10
SAMPLER(S): CB114B

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{34}{\text{DTB}} - \frac{11.14}{\text{DTW}} = \frac{22.86}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } \underline{22.86} \times \frac{\underline{0.041}}{\text{Multiplier}} = \underline{0.937} \text{ gal}$$

$$\underline{0.937} \times 1.5 = \underline{1.41} \text{ gal}$$

TOTAL VOLUME PURGED: 1.50 gal

WATER QUALITY: DTW = Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1202	12.76	12.768	17.33	1.359	5.59	7.30	2.0	5.56	
1208	0.12	12.715	17.16	1.356	4.37	7.30	-14.5	5.76	
1212	0.14	12.688	17.31	1.352	3.80	7.29	-45.0	—	
1229	0.30	12.492	17.44	1.353	2.90	7.32	-75.9	1.06	
1236	0.70	12.430	17.01	1.360	0.61	7.37	-121.2	1.03	
1241	0.85	12.395	17.44	1.356	0.35	7.39	-142.6	0.23	
1244	1.0	12.369	17.37	1.358	0.28	7.40	-147.3	0.27	
1247	1.2	12.345	17.44	1.360	0.23	7.41	-150.4	0.15	
1250	1.35	12.319	17.46	1.358	0.22	7.42	-152.5	0.12	
1252		START SAMPLE COLLECTION							
1304		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>B</u>
turbidity meter	<u>200701254</u>

NOTES AND OBSERVATIONS:
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 63-174

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01 0017869.92
 DATE: 11/2/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
168.0 to 191.1

TOTAL VOLUME PURGED: 2.25 gal

SAMPLING PORT
174

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1024	0		PUMP ON					8/8.2	35
1031	0.05	16.46	0.997	1.07	5.79	-119.1	-	↓	↓
1036	0.20	16.38	0.999	0.76	5.76	-119.9			
1043	0.40	16.43	0.996	0.48	5.84	-103.6	1.51		
1050	0.60	16.32	1.000	0.40	6.07	-88.1			
1100	1.10	16.09	1.002	0.32	6.39	-75.9	0.61		
1110	1.50	16.29	1.000	0.28	6.44	-78.6	0.40		
1118	1.70	16.31	1.001	0.27	6.47	-79.9	0.25		
1123	1.80	16.33	1.000	0.25	6.49	-81.8	0.23		
1129	2.1	16.38	1.002	0.23	6.54	-83.2	0.22		
1130			PUMP OFF, START SAMPLE COLLECTION						
1150			SAMPLE COMPLETED : 2 L IPEC						
1150			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 63-163

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
 DATE: 11/2/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
150.5 to 165

TOTAL VOLUME PURGED: 2.15 gal

SAMPLING PORT
163 2

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1024	0	PUMP ON						8/8.2	35
1031	0.1	16.45	0.992	0.85	6.56	-164.9	—	↓	↓
1036	0.25	16.30	0.982	0.72	6.79	-150.1			
1043	0.45	16.32	0.969	0.53	7.04	-142.7	0.38		
1050	0.65	16.13	0.966	0.45	6.95	-131.4	0.44		
1100	1.10	15.97	0.970	0.31	6.96	-113.7	0.80		
1110	1.40	16.20	0.973	0.28	7.01	-110.5	0.45		
1118	1.60	16.29	0.976	0.25	7.04	-108.7	0.		
1123	1.80	16.35	0.976	0.23	7.04	-106.5			
1129	2.0	16.39	0.974	0.22	7.04	-103.2			
1131		PUMP OFF, START SAMPLE COLLECTION							
1149		SAMPLE COMPLETED : 2 L IPEC							
1149		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 63-121

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Sunny 40's

PROJECT NO: 01.0017869.92
 DATE: 11/2/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
118 to 127.5

TOTAL VOLUME PURGED: 2.70 gal

SAMPLING PORT
121 3

PURGE RATE: variable (gal/min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1024	0		PUMP	ON				8/8.2	35
1031	0.1	16.44	1.441	0.75	7.26	-68.3	-		
1036	0.3	16.30	1.433	0.60	7.34	-73.6			
1043	0.55	16.41	1.427	0.43	7.38	-70.4	0.68		
1050	0.80	16.17	1.429	0.41	7.39	-67.2			
1100	1.40	16.35	1.415	0.37	7.39	-67.4	0.57		
1110	2.0	16.24	1.418	0.41	7.39	-70.9	0.29		
1118	2.2	16.19	1.414	0.38	7.39	-72.3	0.35		
1123	2.4	16.24	1.409	0.37	7.39	-74.7	0.33		
1129	2.55	16.26	1.410	0.36	7.39	-76.7	0.37	↓	↓
1132			PUMP OFF, START SAMPLE COLLECTION						
1146			SAMPLE COMPLETED : 2 L IPEC						
1146			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> <u>200704293</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 63-112

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MID-40's

PROJECT NO: 01.0017869.92
DATE: 11/02/10
SAMPLER(S): CB, MPS

SAMPLING INTERVAL (depth in ft below top of casing)
106.5 to 112.0

TOTAL VOLUME PURGED: 1.05 gal

SAMPLING PORT
112 4

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1348	0	PUMP	DN					7/7.4	20
1356	0.02	17.52	1.327	0.77	7.17	-105.9	0.72		
1403	0.20	17.01	1.281	0.50	7.32	-104.4	0.44		
1410	0.30	16.90	1.300	0.40	7.35	-95.9	0.19		
1415	0.40	17.02	1.310	0.36	7.36	-89.9	0.32		
1420	0.56	17.13	1.311	0.31	7.37	-83.9	0.31		
1425	0.60	17.03	1.313	0.29	7.38	-77.9	0.36		
1430	0.70	17.08	1.310	0.26	7.38	-73.6	0.35		
1435	0.80	17.05	1.310	0.27	7.38	-69.9	0.34		
1439	START SAMPLE COLLECTION								
1505	END SAMPLE COLLECTION: ZL IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200707293

NOTES AND OBSERVATIONS:

WELL ID: MW 63-93

SAMPLE ID: 016

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: SUNNY, MID 40's

PROJECT NO: 01.0017869.92
 DATE: 11/02/10
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)
81.5 to 100.5

TOTAL VOLUME PURGED: 1.10 gal

SAMPLING PORT
5D 5

PURGE RATE: variable (gal/min)
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1348	0							717.4	20
1356	0.02	17.37	0.949	1.43	6.00	-83.6	0.69		
1405	0.10	16.88	1.011	0.55	5.92	-97.2	0.43		
1412	0.20	16.73	1.020	0.43	5.95	-95.2	0.42		
1415	0.40	16.81	1.023	0.36	6.06	-75.1	0.58		
1420	0.50	16.85	1.019	0.31	6.11	-61.0	0.46		
1425	0.60	16.83	0.993	0.29	6.19	-52.9	0.36		
1430	0.70	16.83	0.961	0.27	6.26	-47.4	0.26		
1435	0.80	16.80	0.928	0.26	6.34	-48.8	0.24		
1440	0.90	16.83	0.904	0.24	6.35	-46.6	0.22	↓	↓
1445	START SAMPLE COLLECTION								
1508	END SAMPLE COLLECTION 2L PPE								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	2182764293

NOTES AND OBSERVATIONS:

WELL ID: MW 63.50

SAMPLE ID: 015

GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: SUNNY, MID 40s

PROJECT NO: 01 0017869.92
DATE: 11/02/10
SAMPLER(S): CB, JMB

SAMPLING INTERVAL (depth in ft below top of casing)
41.5 to 58.0

TOTAL VOLUME PURGED: 2.40 gal

SAMPLING PORT
5D 7

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1348	0							7/7.4	2.0
1352	0.05	17.00	1.1103	8.41	6.90	-7.18	—		
1356	0.10	16.94	1.157	3.31	6.99	-8.58	1.23		
1405	0.20	16.80	1.155	1.62	7.12	-20.10	0.89		
1410	0.30	16.78	1.158	1.28	7.16	-18.1	0.83		
1415	0.45	16.85	1.161	1.08	7.19	-20.2	0.61		
1420	1.00	16.84	1.163	1.02	7.22	-22.1	0.39		
1425	1.25	16.84	1.165	1.00	7.23	-25.3	0.65		
1430	1.50	16.81	1.167	0.96	7.25	-27.2	0.51		
1435	1.75	16.80	1.170	0.99	7.26	-30.6	0.16		
1440	2.00	16.70	1.174	1.05	7.28	-28.1	0.36		
1445	2.15	16.72	1.179	0.99	7.28	-28.16	0.39		
1450	2.30	16.71	1.181	0.97	7.29	-28.9	0.37		
1452	START SAMPLE COLLECTION								
1507	END SAMPLE COLLECTION: 2L IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 55-24

SAMPLE ID: 016

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: WINDY, SUNNY, 40's

PROJECT NO: 010017869.92
 DATE: 11/6/10
 SAMPLER(S): CAS, MPS
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 10.50 Transducer Actual Depth 5.305

Time	DTW or <u>Actual Depth</u>	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
11:11	5.350	PUMP ON							
11:30	5.263	10.44	0.516	3.17	7.74	-69.3	---		0.01
11:40	5.234	10.03	0.529	3.17	7.76	-78.1	1.45		0.05
11:50	5.151	10.18	0.541	2.22	7.79	-82.0	0.99		0.07
12:00	5.211	10.40	0.531	1.83	7.82	-107.0	0.81		0.10
12:05	5.191	10.44	0.531	1.78	7.82	-99.4	0.48		0.15
12:10	5.240	10.45	0.533	1.82	7.83	-94.6	0.39		0.20
12:15	5.255	10.42	0.540	1.71	7.83	-91.2	0.26		0.25
12:20	5.255	10.39	0.542	1.68	7.83	-91.6	0.13		0.30
12:25	5.255	10.34	0.541	1.63	7.84	-85.2	0.10		0.40
12:30	5.255	10.32	0.540	1.60	7.84	-84.2	0.12		0.50
12:34	START SAMPLE COLLECTION								
14:10	END SAMPLE COLLECTION: 2L JPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	2
turbidity meter	200104293

NOTES AND OBSERVATIONS: Total volume purged 0.60 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-55-35
 SAMPLE ID: 015

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: WINDY, SUNNY, 40's

PROJECT NO: 010017869.92
 DATE: 11/01/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 10.8' Transducer Actual Depth 21.0'

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
11:11	21.091	PUMP	P ON						
11:50	20.960	11.23	0.576	2.41	6.93	-110.9	4.18		0.01
12:00	20.978	11.88	0.566	1.39	7.10	-127.1	2.07		0.05
12:05	20.952	12.13	0.562	1.40	7.18	-138.7	2.24		0.07
12:10	21.001	12.15	0.558	0.93	7.23	-150.3	1.81		0.10
12:15	20.964	12.14	0.554	0.91	7.30	-141.0	1.12		0.25
12:20	20.961	12.28	0.551	0.86	7.38	-141.2	1.05		0.35
12:25	20.964	12.35	0.549	0.86	7.42	-151.3	0.71		0.45
12:30	20.966	12.45	0.551	0.81	7.48	-157.4	0.61		0.50
12:35	20.975	12.58	0.554	0.76	7.49	-157.7	0.66		0.55
12:40	20.971	12.69	0.558	0.70	7.51	-157.3	0.68		0.60
12:45	20.969	12.75	0.560	0.68	7.52	-158.0	0.65		0.65
12:50	20.958	12.78	0.562	0.66	7.53	-158.7	0.62		0.70
12:54	START SAMPLE COLLECTION								
14:26	SAMPLE COMPLETED : 2 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	1
turbidity meter	20104293

NOTES AND OBSERVATIONS: Total volume purged 0.75 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-55-54

SAMPLE ID: 016

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: WINDY, SUNNY, 40's

PROJECT NO: 010017869.92
DATE: 11/01/10
SAMPLER(S): CB, MPS
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 10.65 Transducer Actual Depth 38.771

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
11:11	10.65	PUMP DOWN							
11:30	10.69	9.70	1.795	5.26	6.08	248.0	—		0.05
11:40	10.69	9.88	1.795	4.64	6.07	240.3	0.56		0.09
11:50	10.69	10.13	1.7910	4.32	6.14	241.4	0.51		0.15
12:00	10.70	10.30	1.788	4.12	6.21	231.2	0.58		0.25
12:05	10.70	10.49	1.786	4.01	6.24	225.8	0.70		0.30
12:10	10.70	10.63	1.786	3.87	6.28	220.4	0.05		0.40
12:15	10.71	10.42	1.790	3.88	6.33	213.4	0.00		0.52
12:20	10.71	10.36	1.788	3.87	6.35	208.9	0.00		0.60
12:25	10.71	10.34	1.787	3.85	6.37	205.1	0.00		0.70
12:32	START SAMPLE COLLECTION								
13:30	END SAMPLE COLLECTION IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde	3
flow meter	4
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.70 gal
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msL.

WELL ID: MW-111
 SAMPLE ID: 035

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: M. Sunny 40's

PROJECT NO: 010017869.92
 DATE: 11/1/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 9.18 Transducer Actual Depth - 6.556 ^{Transd.} read - 9.465

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Notes H ₂ O (gal)
1143	6.544		0	PUMP	ON				
1200	6.404	8.88	0.357	11.63	6.88	-58.2	-	0.35	
1209	6.359	10.08	0.811	3.93	6.82	-39.7	0.91		
1219	6.376	11.38	0.808	2.71	6.82	-32.8	1.16		0.10
1230	6.450	11.70	0.812	2.59	6.98	-14.7	1.45		0.15
1237	6.456	12.11	0.819	2.31	6.99	-13.4	1.50		0.18
1246	6.464	11.97	0.819	2.31	6.93	-8.9	1.40		0.20
1252	6.501	12.51	0.825	2.21	6.99	-8.8	1.51		
1257	6.495	12.48	0.824	1.99	6.99	-8.0	1.42		
1305	6.474	12.56	0.825	2.06	7.02	-7.8	1.47		0.25
1310	6.463	12.49	0.829	2.02	6.96	-8.0	1.50		0.28
1312		START SAMPLE COLLECTION							
1455		SAMPLE COMPLETED : 2 L IPEC							
1455		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	4
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.4 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: U3-4S
 SAMPLE ID: 002

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: Cloudy 50's windy

PROJECT NO: 01 0017869.92
 DATE: 10/29/10
 SAMPLER(S): MB, CB
 PUMP DEPTH: 15.0 ft

WATER QUALITY: DTW = 10.18 Transducer Actual Depth - NO TRANSDUCER.

Time	<u>DTW</u> or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Notes H ₂ O (gal)
0928	<u>10.18</u>								
0938	10.18	13.76	0.672	4.78	7.06	137.8	—	0.5	0.01
0945	10.18	13.96	1.276	3.26	7.02	45.5	—		0.02
0950	10.18	13.96	1.281	2.20	7.08	90.3	12.47		0.03
0955	10.18	14.39	1.281	1.92	7.14	36.8	12.18		0.07
1003	10.18	14.28	1.285	2.00	7.21	45.0	12.30		0.12
1013	10.18	13.30	1.292	1.35	7.23	43.7	12.43		0.20
1018	10.18	13.20	1.290	1.31	7.25	43.1	12.37		0.25
1023	10.18	13.18	1.292	1.30	7.25	44.5	12.33		0.30
1028	10.18	13.14	1.293	1.29	7.25	46.2	12.40	↓	0.34
1029		start sample collection							
1140		Sample completed: 2 L IPEC 0.5 L IPEC							
1140		Pump off							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	3
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged _____ gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: U3-71
 SAMPLE ID: 030

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: OVERCAST, 50's

PROJECT NO: 01 0017869 92
 DATE: 10/29/10
 SAMPLER(S): CB, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1450	2.348	PUMP	ON						
1507	2.356	20.52	0.989	4.79	7.62	192.8	0.32		0.01
1515	2.359	20.91	0.988	2.80	7.73	184.2	0.32		0.15
1520	2.362	21.14	0.987	2.29	7.75	179.7	0.32		0.25
1525	2.364	21.24	0.987	1.83	7.76	175.1	0.32		0.35
1530	2.366	21.27	0.987	1.80	7.77	171.7	0.21		0.45
1535	2.368	21.28	0.987	1.79	7.77	167.9	0.20		0.55
1536	START	SAMPLE COLLECTION							
1604	END	SAMPLE COLLECTION: 2L IPEC 0.5 L IPEC							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	1
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.70 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: U3-72

SAMPLE ID: 035

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: OVERCAST, SDS

PROJECT NO: 01.0017869.92
DATE: 10/29/10
SAMPLER(S): CB, MB
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 4.65 Transducer Actual Depth 2.149

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (wt)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
0913	2.138	PUMP ON							
0934	2.119	23.75	1.450	4.03	7.73	92.0	3.24	<1.0	0.01
0944	2.121	24.27	1.452	4.52	7.74	-72.8	2.74		0.09
0954	2.121	24.57	1.446	3.14	7.76	-89.9	3.20		0.15
1000	2.121	24.60	1.448	3.09	7.76	-89.8	3.15		0.20
1005	2.119	24.59	1.448	3.02	7.76	-99.6	3.22		0.25
1010	2.117	24.61	1.447	2.73	7.76	-108.2	3.15		0.30
1015	2.118	24.67	1.446	2.55	7.76	-102.1	3.45		0.35
1020	2.115	24.67	1.446	2.52	7.76	-90.8	3.44		0.40
1025	2.116	24.67	1.446	2.49	7.76	-88.0	3.43		0.45
1030	2.117	24.67	1.446	2.47	7.76	-85.5	3.42		0.50
1031	START SAMPLE COLLECTION								
1127	END SAMPLE COLLECTION: 2L IPEC								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	1
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.65 gal
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: U3-4D
SAMPLE ID: 026

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sun + clouds 70°F

PROJECT NO: 01.0017869.92
DATE: 10/28/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 4 in

$$\frac{27.25}{\text{DTB}} - \frac{10.72}{\text{DTW}} = \frac{16.53}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } \underline{16.53} \times \frac{\underline{0.653}}{\text{Multiplier}} = \underline{10.79} \text{ gal}$$

$$\underline{10.79} \times 1.5 = \underline{16.19} \text{ gal}$$

Designed Purge Volume

TOTAL VOLUME PURGED: 8.85 gal

WATER QUALITY: DTW = 10.72 Transducer Actual Depth = 50.288 ^{Transd.} _{read.} = 3.789

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1149	0		PUMP ON						
1156	0.7+0.5	47.943	33.77	1.620	1.70	8.08	96.7	—	
1205	1.5+1.2	45.574	33.93	1.537	2.51	8.55	33.4	0.79	
1210	1.9+1.6	44.296	33.48	1.514	2.93	8.63	9.9	0.71	
1217	2.3+2.0	42.570	33.29	1.504	3.11	8.69	-8.7	0.63	
1225	2.7+2.6	40.609	33.20	1.500	3.31	8.71	-20.3	0.76	
1232	3.2+3.0	38.896	33.05	1.496	3.45	8.72	-25.8	0.74	
1235	3.5+3.2	38.375	33.02	1.496	3.44	8.72	-26.3	0.72	
1244	3.9+3.7	36.189	32.48	1.501	3.43	8.71	-28.2	0.50	
1247	4.0+3.8	35.771	32.53	1.503	3.20	8.70	-28.4		
1254	4.0+4.2	34.701	32.71	1.502	3.45	8.71	-29.7	0.72	
1301	4.0+4.7	34.182	PUMP OFF			Well dry - let well recharge.			
1341		START SAMPLE COLLECTION							
1404		SAMPLE COMPLETED : .2 L IPEC							
		0.5 L IPEC in house analysis							
1404		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	
turbidity meter	<u>2</u> <u>200704293</u>

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-46
SAMPLE ID: 022

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sunny, 70's

PROJECT NO: 01.0017869.92
DATE: 10/28/10
SAMPLER(S): CB

WATER COLUMN HEIGHT (ft) Well Diameter: 4 in

$$\frac{29.7}{DTB} - \frac{4.07}{DTW} = \frac{25.63}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 25.63 x 0.653 Multiplier = 16.74 gal Well Volume
16.74 x 1.5 = 25.10 gal Designed Purge Volume
TOTAL VOLUME PURGED: 2515 gal

WATER QUALITY: DTW = 4.07 Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1112	0	23.777	PUMP	0N					
1124	2.5	20.710	21.10	0.754	0.36	7.50	-74.0	20.39	
1134	5.25	18.647	21.20	0.740	0.37	7.51	-54.4	30.50	
1145	8.0	15.636	21.19	0.653	0.41	7.55	-42.3	39.13	
1200	12.5	9.910	21.25	0.532	0.64	7.63	-64.2	34.31	
1212	15.0	7.308	21.23	0.767	2.03	7.65	-64.1	27.82	
1225	18.25	7.308	21.17	1.003	3.71	7.68	-86.7	20.73	
1233	20.0	1.976	21.12	1.084	4.49	7.70	-85.4	15.19	
1258	23.0	1.975	21.10	1.271	5.54	7.69	-95.6	6.65	
1315	25.0	2.440	21.10	1.305	5.55	7.67	-94.0	10.97	
1316	START	SAMPLE COLLECTION							
1325	END	SAMPLE COLLECTION: 2L IPEC 0.5L IPEC							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WELL ID: MW-42-49
SAMPLE ID: 023

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: RAIN, MID-60S

PROJECT NO: 01.0017869.92
DATE: 10/27/10
SAMPLER(S): CB, MPS
PUMP DEPTH: _____ ft

WATER QUALITY: DTW = ~~30~~ 34.81 Transducer Actual Depth 13.584

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
1125	13.591	Pump on						5/10	25	gal
1130	13.082	18.11	1.362	7.21	6.48	152.4	2.00			0.01
1140	12.725	18.03	1.400	6.02	6.39	128.7	0.93			0.75
1145	12.768	18.15	1.392	5.87	6.46	119.1	0.59		22	1.00
1150	12.810	18.26	1.388	5.77	6.54	109.7	0.21			1.25
1155	12.811	18.20	1.378	5.78	6.62	101.9	0.20			1.50
1200	12.824	18.24	1.356	5.84	6.67	96.7	0.20			1.75
1205	12.828	18.28	1.336	5.83	6.73	91.0	0.20			1.85
1208	START SAMPLE COLLECTION									
1223	END SAMPLE COLLECTION: 2L IPEC 0.5 L IPEC									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 2.0 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-42-78
SAMPLE ID: 018

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: RAIN, MID-60'S

PROJECT NO: 01.0017869.92
DATE: 10/27/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 4.00 in

$\frac{78}{\text{DTB}} \cdot \frac{33.87}{\text{DTW}} = \frac{44.13}{\text{Water Column Height}}$ ft

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 44.13 x $\frac{0.041}{\text{Multiplier}}$ = 1.81 gal

1.81 x 1.5 = 2.71 gal

TOTAL VOLUME PURGED: 3.0 gal

WATER QUALITY: DTW = 33.87 Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1325		—	Pump on						
1330	0.01	—	18.93	1.957	8.99	6.86	204.2	40.88	
1334	0.40	—	17.90	1.983	6.91	6.47	191.2	410.8	
1337	0.80	—	17.59	1.975	5.99	6.36	184.0	438.7	
1340	1.20	—	17.58	1.966	5.35	6.34	176.4	373.0	
1343	1.60	—	17.44	1.959	4.93	6.35	169.0	308.4	
1346	2.00	—	17.41	1.954	4.55	6.36	162.4	240.8	
1349	2.40	—	17.43	1.947	4.28	6.39	155.2	200.7	
1351	2.70	—	17.41	1.946	4.17	6.41	150.8	170.5	
1352		START SAMPLE COLLECTION							
1356		END SAMPLE COLLECTION: 2L IPEC							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-53-82

SAMPLE ID: 017

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC

SITE: Buchanan, NY

WEATHER: Showers 70°F

PROJECT NO: 01.0017869.92

DATE: 10/27/10

SAMPLER(S): CB, MB

PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 60.25 Transducer Actual Depth 21.587 ^{transd. read} - 9.951

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	H ₂ O purged Notes (gal)
1001	21.587									
1039	21.499		PUMP	ON				5/16	40	
1045	21.317	19.35	1.863	2.69	6.09	155.3	—	5/20	38	0.01
1050	21.355	19.50	1.740	4.15	6.50	181.0	56.14			
1055	21.361	19.60	1.643	5.30	6.75	176.5	26.88			
1100	21.397	19.62	1.614	5.65	7.04	176.1	19.29			0.20
1105	21.415	19.68	1.598	5.74	7.25	175.2	18.49			0.30
1112	21.381	19.61	1.608	5.91	7.50	175.1	12.26			0.45
1119	21.395	19.55	1.635	5.90	7.66	175.0	10.46			0.55
1128	21.384	19.61	1.670	5.90	7.71	175.2	6.20			0.70
1134	21.388	19.64	1.689	5.91	7.74	175.5	5.97			0.85
1139	21.366	19.62	1.705	5.86	7.77	175.7	5.89			0.95
1141		START SAMPLE COLLECTION								
1207		SAMPLE COMPLETED : 2 L IPEC								
1207		PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	4
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Total volume purged _____ gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-53-120
SAMPLE ID: 021

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Showers 70°F

PROJECT NO: 01.0017869.92
DATE: 10/27/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{120}{\text{DTB}} \cdot \frac{6087}{\text{DTW}} = \frac{59.13}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 59.13 x 0.041 = 2.42 gal
Multiplier Well Volume

2.42 x 15 = 3.64 gal
Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1207	0		PUMP ON						
1212	0.01	—	18.99	1.441	6.84	—	192.1	30.19	
1215	0.20	—	18.52	1.448	4.85	—	196.0	60.38	
1220	0.75	—	18.38	1.519	4.01	—	199.1	143.3	
1226	1.50	—	18.30	1.572	3.53	—	200.2	148.7	
1230	2.00	—	18.19	1.585	3.74	—	201.3	126.1	
1234	2.50	—	18.10	1.593	3.36	—	201.3	114.5	
1238	3.00	—	18.10	1.597	2.31	—	201.5	93.09	
1241	3.50	—	18.11	1.596	2.48	—	202.1	93.10	
1243	3.75	—	18.09	1.596	2.24	—	202.0	93.06	
1243			START SAMPLE COLLECTION						
1248			SAMPLE COMPLETED: 2 L IPEC						
1248			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	4
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-44-66
SAMPLE ID: 018

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: M. sunny 70's

PROJECT NO: 01.0017869.92
DATE: 10/26/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) 66 DTB = 59.44 DTW = 6.56 Water Column Height
Well Diameter: _____ in

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 6.56 x 0.163 Multiplier = 1.069 gal Well Volume
1.069 x 1.5 = 1.61 gal Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
0941	0	5.228		PUMP	ON				10/15	88	
0943	0.1	4.466	18.30	1.648	2.89	6.82	53.9	—	10/15	38	
0947	0.2	3.988	18.16	1.615	4.24	6.91	39.9	50.09			
0952	0.4	2.955	17.75	1.595	5.61	7.06	34.2	42.97			
0955	0.5	2.596	17.67	1.589	5.96	7.10	34.8	38.31			
0958	0.65	2.108	17.70	1.586	6.36	7.15	36.7	52.01			
1000	0.80	1.790	17.64	1.588	6.58	7.19	40.0	47.89			
1004	1.0	1.792	17.96	1.591	6.43	7.24	44.7	49.61			
1010	1.2	1.792	18.22	1.600	6.17	7.25	45.4	51.06			
1014	1.35	1.790	18.74	1.602	5.82	7.27	44.5	53.10			
1018	1.40	1.790	18.92	1.606	5.65	7.27	43.7	48.29			
1025	1.45	1.790	19.17	1.610	5.54	7.27	43.2	47.49			
1027		Well dry. Let recharge before sampling									
1420		START SAMPLE COLLECTION									
1440		END SAMPLE COLLECTION. 2L IPEC 0.5L IPEC									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 <u>200701254</u>

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-44-102
SAMPLE ID: 019

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: M. Sunny 70's

PROJECT NO: 01.0017869.92
DATE: 10/26/10
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 0.041 in

$$\frac{93.09}{\text{DTB}} - 102 - \frac{68.16}{\text{DTW}} = \frac{24.93}{\text{Water Column Height}} = 33.84 \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 33.84 x $\frac{0.041}{\text{Multiplier}}$ = 1.387 gal

1.387 x 1.5 = 2.08 gal
Designed Purge Volume

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = 68.16 Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (µl)	pH (SU)	ORP	Turbidity (NTU)	Notes
1312	0	68.16	Pump	ON					
1315	0.25	—	19.78	1.257	9.50	7.63	116.9	978.4	
1320	0.75	—	18.97	1.313	6.36	7.43	98.5	1100.0	TURB > 1100, SUCTY
1323	1.25	—	18.44	1.294	6.41	7.41	85.1	—	
1325	1.50	—	18.07	1.293	6.72	7.40	84.6	—	
1326	1.75	—	18.38	1.293	7.27	7.40	83.0	—	
1328	2.00	—	18.20	1.302	7.27	7.56	101.3	—	
1329	START	SAMPLE COLLECTION							
1332	END	SAMPLE COLLECTION: 2L IPEC 0.5L IPEC							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	2007 04293

NOTES AND OBSERVATIONS:
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York

Low-Flow Sampling Data Sheet

WELL ID: Mw-11-40

SAMPLE ID: 018

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: PARTLY CLOUDY, 60'S

PROJECT NO: 01.0017869.92
 DATE: 10/25/10
 SAMPLER(S): CG, MB
 PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 23.11 Transducer Actual Depth 51.230

Time	DTW or <u>Actual Depth</u> (ft)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1325	51.230	Pump ON							
1345	51.025	20.73	2.602	4.30	7.00	114.5	1.89		0.05
1355	51.062	20.71	2.574	4.25	7.06	111.4	1.27		0.10
1400	51.064	20.70	2.563	4.21	7.08	111.2	0.96		0.13
1405	51.071	20.68	2.553	4.22	7.10	110.8	1.32		0.18
1410	51.060	20.64	2.545	4.18	7.10	111.0	1.23		0.22
1415	51.060	20.70	2.530	4.28	7.11	110.6	0.98		0.26
1420	51.055	20.83	2.525	4.14	7.12	110.2	0.86		0.30
1425	51.051	20.92	2.522	4.21	7.12	110.1	0.72		0.34
1430	51.047	21.02	2.520	4.16	7.13	110.2	0.68		0.38
1435	51.047	21.01	5.320	4.18	7.13	110.4	0.67		0.42
1438	START SAMPLE COLLECTION								
1606	END SAMPLE COLLECTION								
					2 LIPEC				
					0.5 LIPEC				

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.55 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-41-63
SAMPLE ID: 017

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: Sun + clouds 70°F

PROJECT NO: 01.0017869.92
DATE: 10/25/10
SAMPLER(S): _____

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{63}{\text{DTB}} - \frac{26.25}{\text{DTW}} = \frac{36.75}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 36.75 x 0.041 Multiplier = 1.51 Well Volume gal

1.51 x 1.5 = 2.26 gal

Designed Purge Volume

TOTAL VOLUME PURGED: 2.50 gal

WATER QUALITY: DTW = 26.25 Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1120	0	26.25	PUMP	ON					
1125	0.05	-	19.57	2.249	7.50	6.63	124.3	-	
1130	0.25	-	18.98	2.266	6.36	6.75	117.3	32.27	
1136	0.50	-	18.72	2.197	5.86	6.84	110.5	42.59	
1142	0.75	-	18.65	2.149	5.19	6.89	106.9	39.44	
1148	1.10	-	18.60	2.127	4.77	6.93	103.9	25.95	
1155	1.50	-	18.52	2.121	4.45	6.95	101.4	18.45	
1200	1.75	-	18.56	2.124	4.28	6.97	99.4	19.23	
1205	2.20	-	18.47	2.120	4.19	6.96	98.1	22.61	
1206			START SAMPLE COLLECTION						
1210			SAMPLE COMPLETED : 2 L IPEC						
1210			PUMP OFF 0.5 L IPEC						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200704293

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-4328

SAMPLE ID: 017

**GZA GeoEnvironmental of New York
Low-Flow Sampling Data Sheet**

CLIENT: Entergy - IPEC

SITE: Buchanan, NY

WEATHER: PARTLY CLOUDY, 60's

PROJECT NO: 01.0017869.92

DATE: 10/25/10

SAMPLER(S): CB, MB

PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 15.44 Transducer Actual Depth 24.392

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
0952	24.395	PUMP ON	DN					5.5/22	10	0
1000	24.155	18.08	4.570	3.93	5.90	242.0	4.42			0.01
1010	23.963	18.24	4.524	1.40	5.94	219.3	2.13			0.20
1020	23.704	18.42	4.401	0.87	5.98	185.4	1.44			0.40
1025	23.613	18.48	4.380	0.74	6.00	170.4	1.15			0.50
1030	23.542	18.38	4.345	0.74	6.09	158.3	0.80			0.60
1035	23.468	18.44	4.336	0.65	6.12	150.4	0.71			0.70
1040	23.387	18.57	4.339	0.65	6.10	148.1	0.69			0.80
1045	23.345	18.61	4.343	0.65	6.13	140.9	0.58			0.90
1050	23.293	18.67	4.347	0.65	6.14	138.7	0.57			1.00
1054	START SAMPLE COLLECTION									
1129	END SAMPLE COLLECTION									
										500 ml IPEC

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 1.15 gal
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-43-02

SAMPLE ID: 017

GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC

PROJECT NO: 01.0017869.92

SITE: Buchanan, NY

DATE: 10/25/10

WEATHER: PARTLY CLOUDY, 60's

SAMPLER(S): CB, MR

PUMP DEPTH: _____ ft

WATER QUALITY: DTW = 17.11 Transducer Actual Depth 35.008

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes gal
0952	35.011	PUMP	DN					6/6	32	
1000	34.511	17.25	2.782	2.28	7.09	88.5	5.11		30	0.05
1010	34.554	17.38	2.798	2.25	7.05	86.9	7.30			0.20
1020	34.518	17.65	2.837	2.22	7.05	91.6	5.84			0.35
1025	34.417	17.75	2.848	2.30	7.05	94.0	5.83			0.35
1030	34.378	17.63	2.857	2.22	7.04	96.5	6.24			0.45
1035	34.288	17.55	2.860	2.19	7.03	98.7	5.54			0.65
1040	34.181	17.48	2.861	2.17	7.04	100.4	5.79			0.75
1045	33.974	17.41	2.862	2.15	7.05	102.3	5.64			0.85
1052	START SAMPLE COLLECTION									
1106	END SAMPLE COLLECTION									
					2 IPEC					
					0.5 IPEC					

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	4
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Total volume purged 1.00 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-45-4
SAMPLE ID: 022

CLIENT: Entergy - IPEC
SITE: Buchanan, NY
WEATHER: M. Sunny 50's windy

PROJECT NO: 01.0017869.92
DATE: 10/22/10
SAMPLER(S): M. BRITOS

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

42 DTB 23.97 DTW = 18.03 Water Column Height ft

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 18.03 x 0.163 Multiplier = 2.94 Well Volume gal

2.94 x 1.5 = 4.41 gal
Designed Purge Volume

TOTAL VOLUME PURGED: gal 3.45

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
0930	0	17.089	PUMP ON						5.5/7	28	
0935	0.2	15.721	17.20	1.606	3.18	7.11	244.4	—		26	
0940	0.35	14.481	17.80	1.546	1.28	7.40	244.8	2.65			
0945	0.50	13.672	17.67	1.505	0.84	7.50	244.9	1.20			
0952	0.60	13.706	17.88	1.349	0.66	7.65	243.4	0.81			
1000	1.0	12.451	18.23	1.140	0.57	7.81	240.8	0.62			
1009	1.3	11.407	18.16	1.020	0.48	8.03	237.5	1.28			
1021	1.6	10.111	18.13	0.926	0.78	8.43	231.5	16.74			
1030	2.0	8.589	18.12	0.918	0.93	8.45	228.4	23.00			
1040	2.5	6.807	18.51	1.000	0.80	8.23	226.4	20.68			
1050	3.0	5.112	18.24	1.177	0.62	7.96	225.3	15.38			
1100	3.3	3.448	17.80	1.351	0.56	7.78	222.8	12.99			
1102	3.45	3.395		Well dry. Let recharge before sample.							
1459		START SAMPLE COLLECTION									
1510		SAMPLE COMPLETED :									
1510		PUMP OFF				0.5	L	IPEC			

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
Groundwater Elevation measurements are given in feet msl.

GZA GeoEnvironmental of New York

Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-45-61
 SAMPLE ID: 022

CLIENT: Entergy - IPEC
 SITE: Buchanan, NY
 WEATHER: M. Sunny windy 50's

PROJECT NO: 01.0017869.92
 DATE: 10/22/10
 SAMPLER(S): M. BRITOS

WATER COLUMN HEIGHT (ft) Well Diameter: _____ in

$$\frac{61}{\text{DTB}} - \frac{24.95}{\text{DTW}} = \frac{36.05}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

$$\text{Water Column Height } 36.05 \times \frac{0.041}{\text{Multiplier}} = \frac{1.48}{\text{Well Volume}} \text{ gal}$$

$$\frac{1.48}{\text{Well Volume}} \times 15 = \frac{2.22}{\text{Designed Purge Volume}} \text{ gal}$$

TOTAL VOLUME PURGED: _____ gal

WATER QUALITY: DTW = _____ Transducer Actual Depth _____

Time	Volume Purged (gal)	(DTW) or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
10:25		24.95							
11:19	0	—	PUMP ON						
11:21	0.1	—	17.62	0.226	7.45	7.72	298.8	68.30	
11:24	0.25	—	17.80	0.901	4.85	7.34	300.6	77.21	
11:28	0.60	—	17.92	0.969	4.14	7.29	299.6	99.78	
11:32	0.95	—	17.78	1.060	3.79	7.28	297.1	111.5	
11:37	1.40	—	17.70	1.158	3.43	7.27	293.6	154.9	
11:42	1.80	—	17.55	1.201	3.29	7.27	291.4	155.4	
11:46	2.10	—	17.59	1.230	3.24	7.28	289.2	132.0	
11:48	2.25	—	17.60	1.237	3.23	7.26	288.5	126.9	
11:48		STOP PUMP and START SAMPLE COLLECTION							
11:54		SAMPLE COMPLETED : 2 L IPEC							
		0.5 L IPEC							
11:54		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.
 Groundwater Elevation measurements are given in feet msl.



APPENDIX E: POST-Q4 2010 MID-QUARTER SAMPLING DATA SHEETS

NO POST QUARTER 4-2010 SAMPLES COLLECTED



APPENDIX F: DOSE CALCULATIONS



Facility Groundwater Flux Calculation

Site Indian Point
Job No. 17869.02

Prepared By: JAS
Reviewed By: mb

Parameter Values:

year
2010

Totals						
Total Catchment Zone (ft ²)		Total Improved Zone (ft ²)		Recharge (ft/yr)	Precipitation (ft/yr)	
3,969,765		1,432,972		0.61	3.10	
Surface Area						
Northern Clean Zone Improved (ft ²)	Unit 2 North Improved Zone (ft ²)	Unit 1/2 Improved Zone (ft ²)	Unit 3 North Improved Zone (ft ²)	Unit 3 South Improved Zone (ft ²)	Southern Clean Improved Zone (ft ²)	
0	148,214	433,904	316,210	321,290	213,354	
Northern Clean Unimproved Zone (ft ²)	Unit 2 North Unimproved Zone (ft ²)	Unit 1/2 Unimproved Zone (ft ²)	Unit 3 North Unimproved Zone (ft ²)	Unit 3 South Unimproved Zone (ft ²)	Southern Clean Zone Unimproved (ft ²)	
106,429	204,317	438,221	323,116	268,862	585,600	
Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	
50,265	0	291,166	106,718	17,730	144,347	
Northern Clean Zone Catchment (ft ²)	Unit 2 North Catchment Zone (ft ²)	Unit 1/2 Catchment Zone (ft ²)	Unit 3 North Catchment Zone (ft ²)	Unit 3 South Zone (ft ²)	Southern Clean Zone (ft ²)	
156,694	352,531	1,163,311	746,044	607,882	943,302	
Activity (pCi/L)						
Groundwater						
Upper Zone Before Canal	Northern Clean Zone Catchment	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South Zone	Southern Clean Zone
	150	337	4,139	445	741	169
Lower Zone Before Canal	150	239	3,530	1,286	564	220
Upper Zone After Canal	150	256	3,286	303	741	169
Lower Zone After Canal	150	502	899	476	564	220
Stormwater Discharging to Canal (pCi/L)						
Storm Water for Northern Clean Zone	Storm Water for Unit 2 North	Storm Water for Unit 1/2	Storm Water for Unit 3 North	Storm Water for Unit 3 South	Storm Water for Southern Clean Zone	
NA	2,165	NA	0	1,558	283	
	Avg MH-4a		Avg CB-14 and CB-34	Avg U3-CB-B8	Avg D1, C3, E6, & E10	
Stormwater Discharging to River (pCi/L)						
Storm Water for Northern Clean Zone	Storm Water for Unit 2 North	Storm Water for Unit 1/2	Storm Water for Unit 3 North	Storm Water for Unit 3 South	Storm Water for Southern Clean Zone	
NA	129	0	0	NA	201	
	Avg MH-1 and MH-12	Avg MH-14	Avg CB-15		Avg E13, CB-C2	

Potential Water Received by Storm Drain System

= (Improved Area) x Precipitation

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
0	459,463	1,345,103	980,252	995,993	661,399	ft ³ /yr
0	1,259	3,685	2,686	2,729	1,293	ft ³ /day
0.00	6.54	19.14	13.95	14.18	9.41	GPM
0	13,010,545	38,089,071	27,757,643	28,203,511	18,728,730	L/Yr

The total amount of water available to be received by the storm system is computed as the combined area of buildings and paved areas in the catchment multiplied by the annual precipitation rate. Note this conservatively assumes that the amount of water lost to the atmosphere or other sinks after precipitation has fallen on paved or built up surfaces is zero.

Water Directly Recharged to Aquifer from Precipitation

= Unimproved Area x Recharge

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
85,782	164,680	353,206	260,431	216,703	471,994	ft ³ /yr
235	451	968	714	594	1,293	ft ³ /day
1.22	2.34	5.03	3.71	3.08	6.72	GPM
2,429,073	4,663,211	10,001,688	7,374,588	6,136,349	13,365,375	L/Yr

Note that this calculation reflects recharge to the aquifer in non-paved areas. The Recharge value listed above and used in this calculation reflects only that portion of precipitation that actually recharges the aquifer.



Facility Groundwater Flux Calculation

Site Indian Point
Job No. 17869.02

Prepared By: JAS
Reviewed By: mib

Water Recharged to Aquifer (Direct Recharge Plus Storm Water Leakage Minus Building Drain Removal)

= (Direct Recharge + X% Water Received by Storm System) - (Y% x Water Removed by Building Drains)

Total Water Discharged to Aquifer

Upper and Lower Zone	[Northern Clean Area Catchment + (0% Storm Drain Water)] ¹	[Unit 2 North + (50% Storm Drain Water)]-[5gpm]	[Unit 1/2 Area Catchment + (30% Storm Drain Water)]-[7.5 gpm]	[Unit 3 North Area Catchment + (60% Storm Drain Water)]-[7.5gpm]	[Unit 3 South Area + (10% Storm Drain Water)]	[Southern Clean Zone Area + (40% Storm Drain Water)]	Units
		85,782	43,099	229,768	321,614	316,303	736,553
	235	118	630	881	867	2,018	ft ³ /day
	1.22	0.61	3.27	4.58	4.50	10.48	GPM
	2,429,073	1,220,421	6,506,317	9,107,080	8,956,700	20,356,867	L/Yr

¹ There are no improved surfaces in Northern Clean Zone.

Groundwater Discharged to Canal

=Water Recharged to Aquifer x X% flowing to Canal

Upper and Lower Zone	Northern Clean Area Catchment x 0%	Unit 2 North x 15.2%	Unit 1/2 Area Catchment 24.2%	Unit 3 North Area Catchment x 22.9%	Unit 3 South Area x68.4%	Southern Clean Zone Area x 0%	Units
		0	6,551	55,604	73,649	216,351	0
	0	18	152	202	593	0	ft ³ /day
	0.00	0.09	0.79	1.05	3.08	0.00	GPM
	0	185,504	1,574,529	2,085,521	6,126,383	0	L/Yr

Groundwater Discharged to River

=Water Recharged to Aquifer x X% flowing to River x Y% Flowing in Appropriate Vertical Zone

Upper Zone	Northern Clean Area Catchment x 100% x 59.3%	Unit 2 North x 84.8% x 15.1%	Unit 1/2 Area Catchment x 75.8% x 11.7%	Unit 3 North Area Catchment x 77.1% x 47.9%	Unit 3 South Area x 31.6% x 31.3%	Southern Clean Zone Area x 100% x 55.2%	Units
		50,869	5,519	20,377	118,775	31,285	406,577
	139	15	56	325	86	1,114	ft ³ /day
	0.72	0.08	0.29	1.69	0.45	5.79	GPM
	1,440,440	156,273	577,019	3,363,327	885,889	11,512,991	L/Yr
Lower Zone	Northern Clean Area Catchment x 100% x 40.7%	Unit 2 North x 84.8% x 84.9%	Unit 1/2 Area Catchment 75.8% x 88.3%	Unit 3 North Area Catchment x 77.1% x 52.1%	Unit 3 South Area x 31.6% x 68.7%	Southern Clean Zone Area x 100% x 44.8%	Units
		34,913	31,029	153,787	129,189	68,667	329,976
	96	85	421	354	188	904	ft ³ /day
	0.50	0.44	2.19	1.84	0.96	4.70	GPM
	988,633	878,645	4,354,769	3,658,232	1,944,428	9,343,877	L/Yr

Water Remaining in Storm Drains and Discharged to Canal

=Storm Drain Water x X% Not Leaking to Groundwater and Not Discharging to River

Northern Clean Area Catchment (0% Storm Drain Water)	Unit 2 North (45% Unit 2 North and 30% of Unit 1/2 Storm Drain Water). Plus 5 gpm (351k cf/yr) from U2 footing drain.	Unit 1/2 Area Catchment (0% Storm Drain Water)	Unit 3 North Area Catchment (3% Unit 3 North Storm Drain Water)	Unit 3 South Area (3% Unit 3 North and 42% Unit 3 South Storm Drain Water)	Southern Clean Zone Area (30% Unit 1/2, 27% Unit 3 North, 43% Unit 3 South, and 55% Southern Clean Zone Storm Drain Water)	Units
0	961,289	0	29,408	447,727	1,460,247	ft ³ /yr
0	2,634	0	81	1,227	4,001	ft ³ /day
0	13.68	0.00	0.42	6.37	20.78	GPM
0	27,221,998	0	832,729	12,678,204	41,349,597	L/Yr

Water Remaining in Storm Drains and Discharged to River

Northern Clean Area Catchment (0% Storm Drain Water)	Unit 2 North (5% Storm Drain Water)	Unit 1/2 Area Catchment (10% Storm Drain Water)	Unit 3 North Area Catchment (7% Storm Drain Water)	Unit 3 South Area (5% Storm Drain Water)	Southern Clean Zone Area (5% Storm Drain Water)	Units
0	22,973	134,510	68,618	49,800	33,070	ft ³ /yr
0	63	369	188	136	91	ft ³ /day
0	0.33	1.91	0.98	0.71	0.47	GPM
0	650,527	3,808,907	1,943,035	1,410,176	936,437	L/Yr



Facility Groundwater Flux Calculation

Site Indian Point
Job No. 17869.02

Prepared By: JAS
Reviewed By: mb

Flux Calculations

Conceptual Model: Migration Pathway Summary

	Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone
GW	100% Upper and Lower Zone To River	84.8% Upper Zone and Lower Zone Flow To River. 15.2% Upper Zone and Lower Zone Flow to Canal	75.8% Upper Zone and Lower Zone To River. 24.2% Upper Zone and Lower Zone to Canal	77.1% Upper Zone and Lower Zone To River. 22.9% Upper Zone and Lower Zone to Canal	31.8% Upper Zone and Lower Zone To River. 68.4% Upper Zone and Lower Zone to Canal	100% Upper and Lower Zone To River
SW	NA	To Canal (Storm Water Considered Clean; Estimated at 5.5 GPM) and To River (5% Storm Water)	To Canal (60% Storm Water) and To River (10% Storm Water)	To Canal (33% Storm Water) and To River (7% Storm Water)	To Canal (85% Storm Water) and To River (5% Storm Water)	To Canal (55% Storm Water) and To River (5% Storm Water)

Flux (pCi/Yr)

	North Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	South Clean Zone	Total
GW to River-Upper Zone	2.16E+08	4.00E+07	1.90E+09	1.02E+09	6.56E+08	1.95E+09	5.78E+09
GW to River-Lower Zone	1.48E+08	4.41E+08	3.92E+09	1.75E+09	1.10E+09	2.06E+09	9.41E+09
GW to Canal	0.00E+00	6.25E+07	6.52E+09	9.29E+08	4.54E+09	0.00E+00	1.20E+10
SW to Canal	NA	5.90E+10	0.00E+00	0.00E+00	1.97E+10	1.17E+10	9.04E+10
SW to River	NA	8.40E+07	0.00E+00	0.00E+00	0.00E+00	1.89E+08	2.73E+08

Curies/Yr ==> 0.12

Notes:

The recharge rate used herein, 28% of precipitation (~10 in/yr), is within the range of values discussed in the USGS modeling report! The reported recharge ranged from 3.6 inches/year to 7.5 inches/year for a till to 20 inches per year for coarse grained glacially stratified deposits. A yearly rolling average precipitation value measured at the Facility meteorological station is also used in the computations. The catchment area was defined using an AutoCAD topo map for the Site and surrounding area. The catchment was defined by starting at the area marked "line of water grant" and tracking east, away from the River, to define portions of the land surface contributing water to the selected discharge zone. Calculations assume that run-off or overland flow in unimproved areas of the Site is negligible, there are no changes in storage and the Hudson River is a gaining stream.

1. USGS. Water Use, Ground-Water Recharge and Availability, and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002



APPENDIX G: UNIT 2 TRITIUM PLUME TREND ANALYSES

**TABLE G1
MANN-KENDALL TREND EVALUATION SUMMARY
TRITIUM IN GROUNDWATER NEAR UNIT 2
INDIAN POINT ENERGY CENTER
BUCHANAN, NY**

Well ID	Number of Data Points	Number of Times below MDC	Minimum Tritium Activity (pCi/L)	Maximum Tritium Activity (pCi/L)	Mann-Kendall Statistic (S)	Normalized Test Statistic (Z)	Probability	Trend at 95% Level of Significance
MW-30-69	40	0	7.36E+04	6.01E+05	-164	-1.90	0.971	decreasing
MW-30-84	27	0	3.78E+03	1.25E+04	116	2.40	0.992	increasing
MW-31-49	39	0	2.98E+02	1.04E+05	91	1.09	0.862	no trend
MW-31-63	27	0	5.00E+03	7.35E+04	128	2.65	0.996	increasing
MW-31-85	27	0	3.17E+02	2.25E+04	139	2.88	0.998	increasing
MW-32-59	26	0	4.13E+02	1.55E+05	56	1.21	0.887	no trend
MW-32-85	25	0	5.42E+03	1.49E+04	117	2.71	0.997	increasing
MW-32-149	22	0	1.99E+02	1.05E+04	3	0.06	0.522	no trend
MW-32-173	20	0	4.31E+02	5.89E+03	-8	-0.23	0.590	no trend
MW-32-190	24	0	1.53E+03	1.13E+04	-197	-4.86	1.000	decreasing
MW-33	26	0	3.69E+03	2.64E+05	-167	-3.66	1.000	decreasing
MW-35	20	0	1.04E+03	1.19E+05	-88	-2.82	0.998	decreasing
MW-36-24	18	2	1.54E+02	3.42E+04	25	0.91	0.818	no trend
MW-36-41	13	0	6.11E+03	5.52E+04	-35	-2.07	0.981	decreasing
MW-36-52	18	0	5.97E+03	2.68E+04	-103	-3.86	1.000	decreasing
MW-37-22	20	0	2.26E+03	3.49E+04	-60	-1.91	0.972	decreasing
MW-37-32	20	0	2.49E+03	3.01E+04	-58	-1.85	0.968	decreasing
MW-37-40	19	0	4.22E+03	1.70E+04	-89	-3.08	0.999	decreasing
MW-37-57	20	0	4.05E+03	4.48E+04	-82	-2.63	0.996	decreasing
MW-42-49	20	0	1.12E+03	7.22E+04	-59	-1.88	0.970	decreasing
MW-42-78	15	0	3.46E+02	1.28E+03	-11	-0.49	0.690	no trend
MW-49-26	22	0	2.59E+03	1.54E+04	-195	-5.47	1.000	decreasing
MW-49-42	22	0	2.20E+03	1.13E+04	-179	-5.02	1.000	decreasing
MW-49-65	22	0	1.26E+03	5.76E+03	-162	-4.54	1.000	decreasing
MW-50-42	23	4	1.01E+02	9.75E+03	-51	-1.32	0.907	no trend
MW-50-66	27	0	2.08E+03	1.08E+04	-199	-4.13	1.000	decreasing
MW-53-82	17	0	4.54E+02	1.32E+04	2	0.04	0.516	no trend
MW-53-120	20	0	3.81E+03	9.61E+03	-128	-4.12	1.000	decreasing
MW-55-24	16	0	7.82E+02	3.08E+03	-19	-0.81	0.791	no trend
MW-55-35	15	0	8.53E+02	9.04E+03	-47	-2.28	0.989	decreasing
MW-55-54	16	0	5.47E+03	1.31E+04	-23	-0.99	0.839	no trend
MW-111	36	0	6.81E+03	5.78E+05	-285	-3.87	1.000	decreasing
DOWNGRADIENT WELLS								
MW-66-21	15	2	8.28E+01	3.57E+03	-19	-0.89	0.813	no trend
MW-66-36	14	0	3.05E+03	9.10E+03	-71	-3.83	1.000	decreasing
MW-67-39	13	0	2.55E+03	5.07E+03	-36	-2.14	0.984	decreasing
MW-67-105	14	0	1.14E+03	2.93E+03	-59	-3.18	0.999	decreasing
MW-67-173	14	0	6.25E+02	1.05E+03	-54	-2.90	0.998	decreasing
MW-67-219	13	0	9.22E+02	1.44E+03	-6	-0.31	0.620	no trend
MW-67-276	13	0	6.79E+02	1.18E+03	-11	-0.61	0.729	no trend
MW-67-323	13	1	3.13E+02	1.29E+03	16	0.92	0.820	no trend
MW-67-340	13	0	3.69E+02	6.69E+02	32	1.89	0.971	increasing

Notes: Calculations based on Mann-Kendall trend evaluations as presented in U.S. EPA Practical Methods for Data Analysis, U.S. EPA QA/G-9 QA00 UPDATE, July 2000, Section 4.3.4

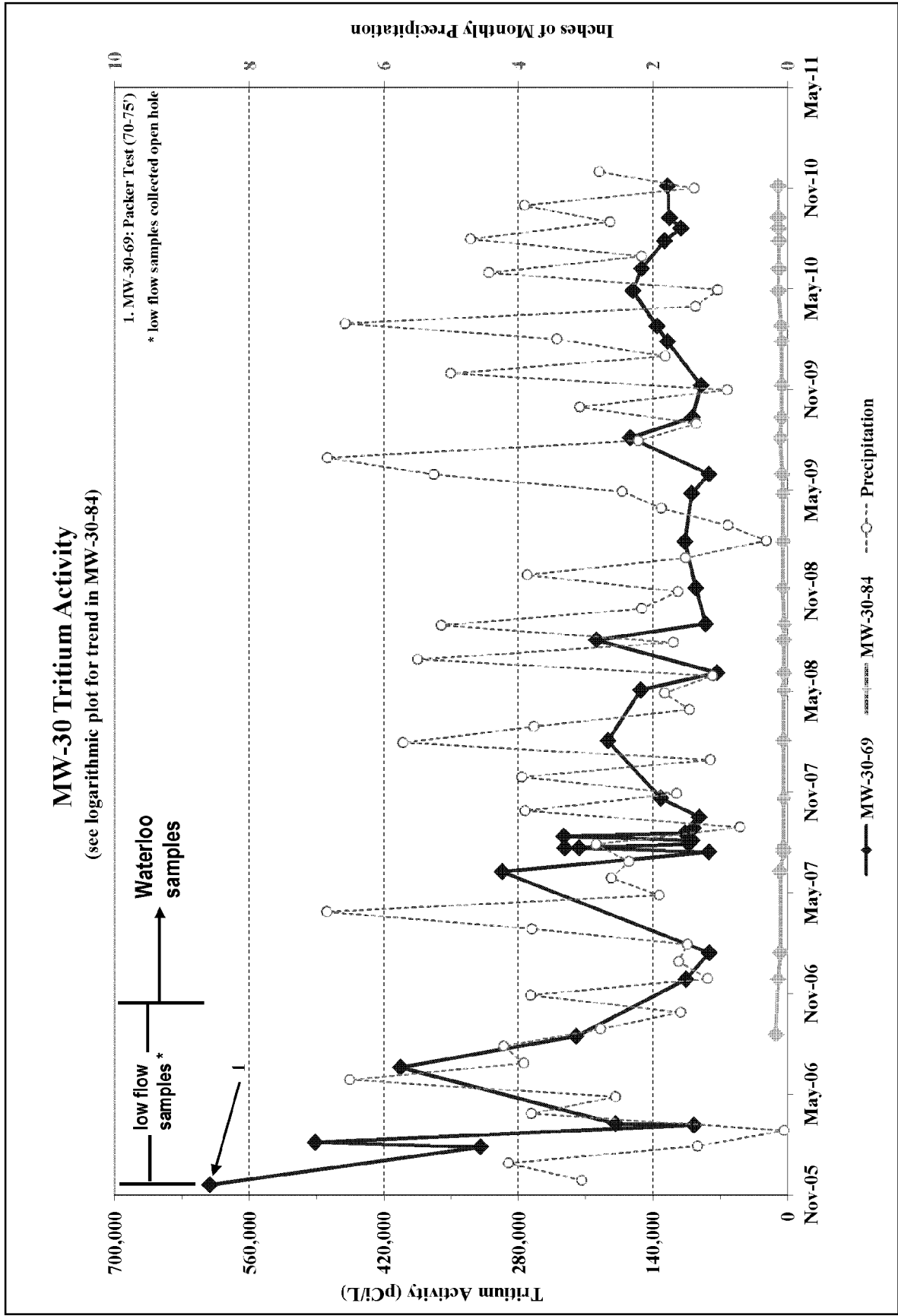


FIGURE G1

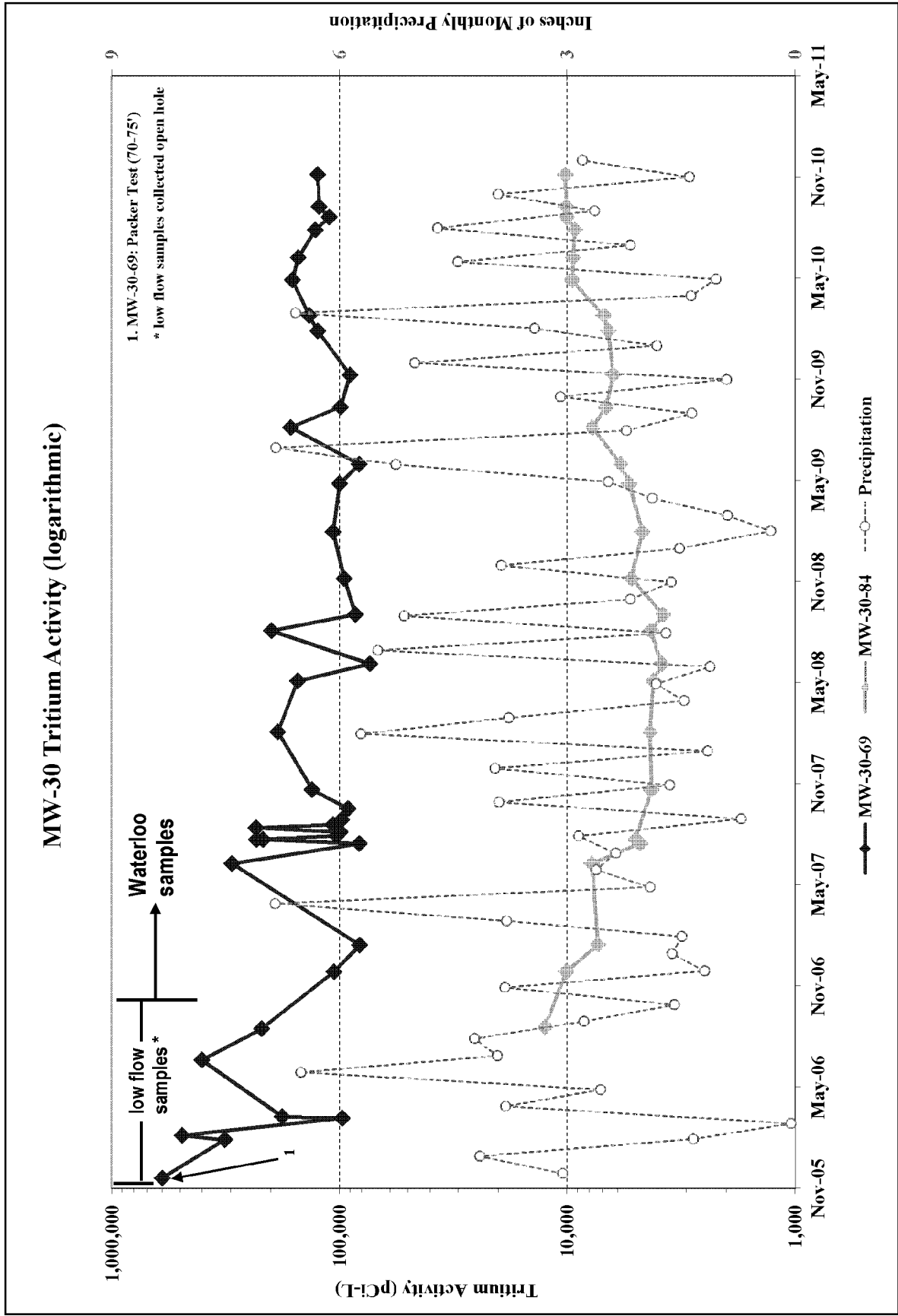


FIGURE G1a

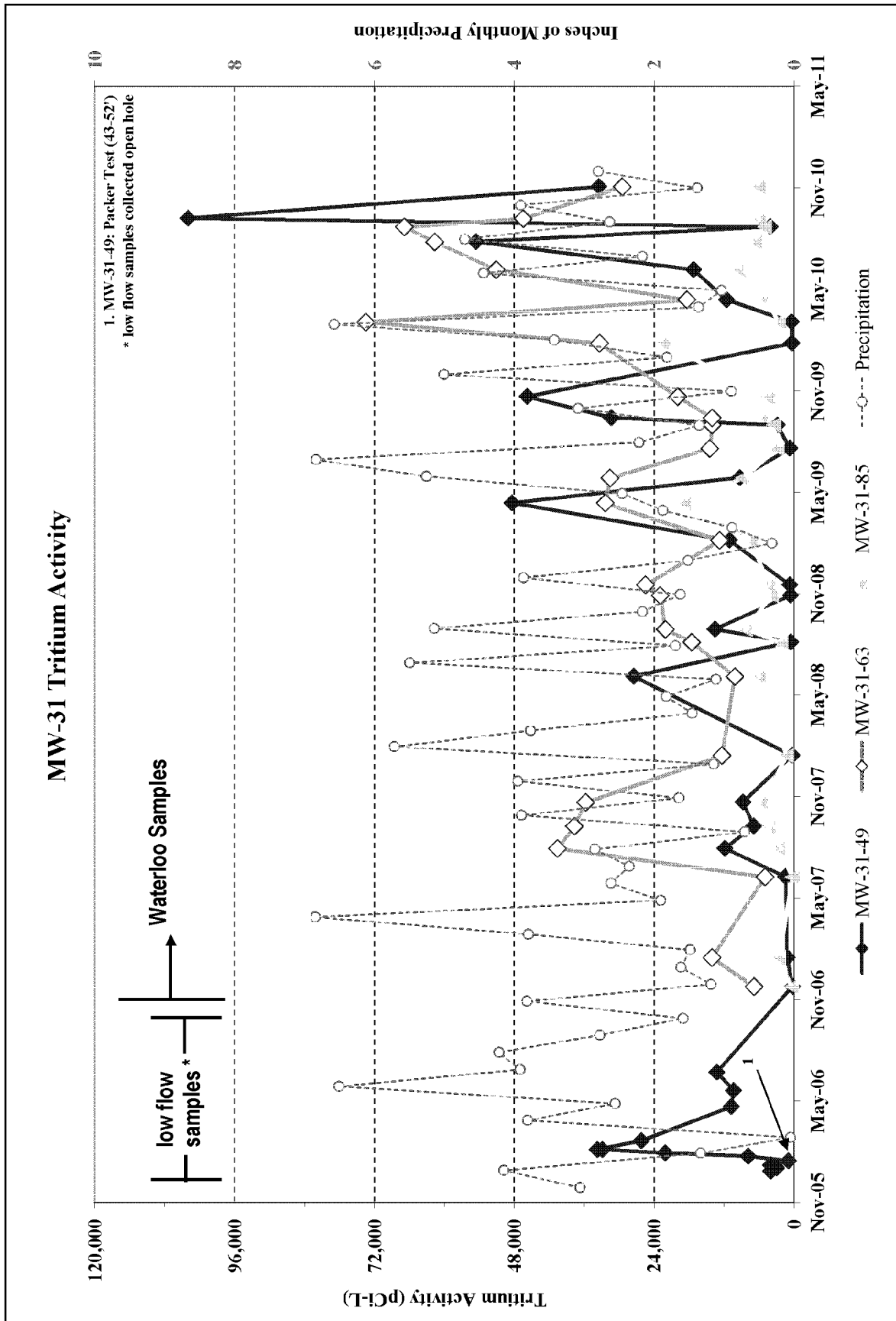


FIGURE G2

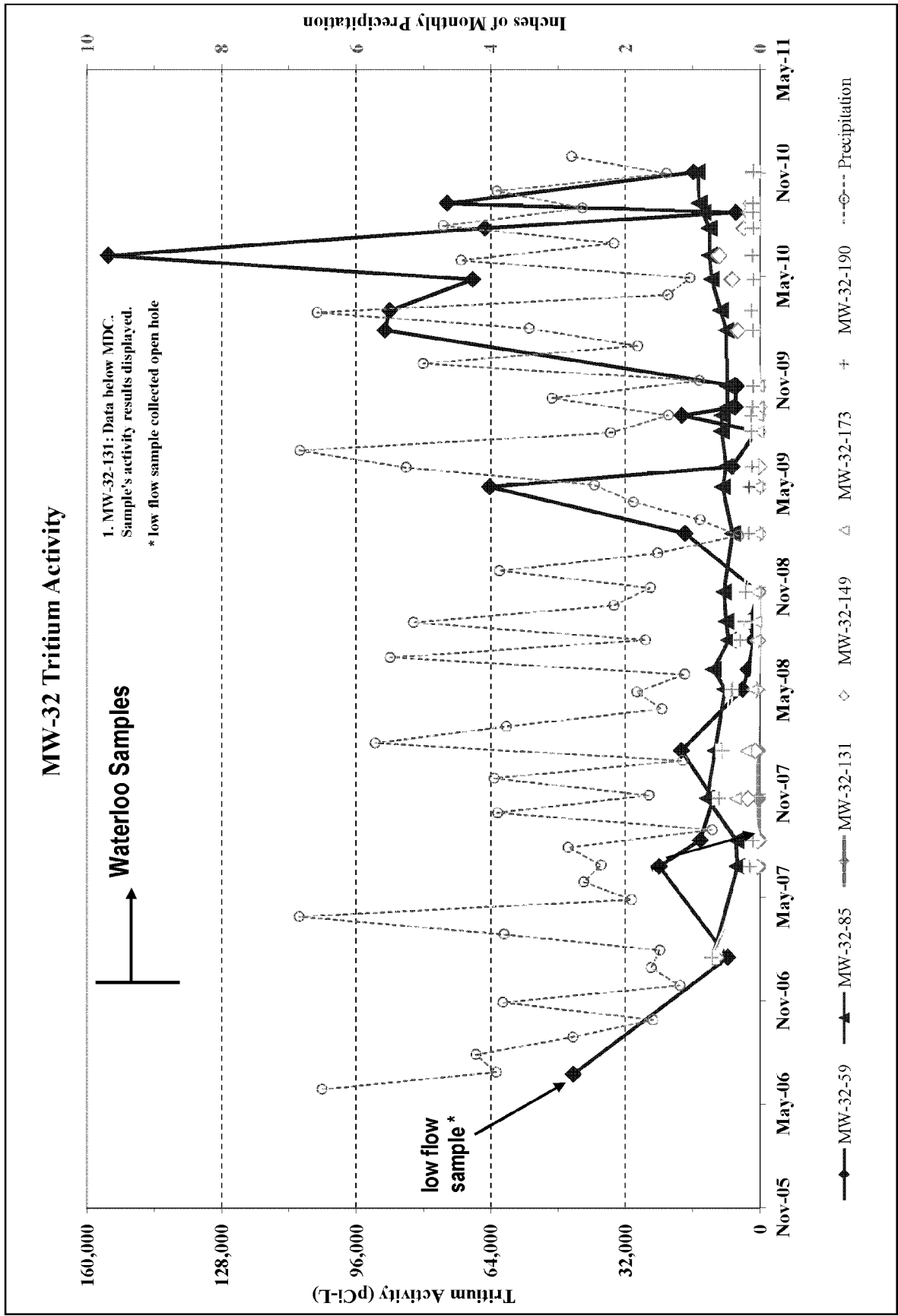


FIGURE G3

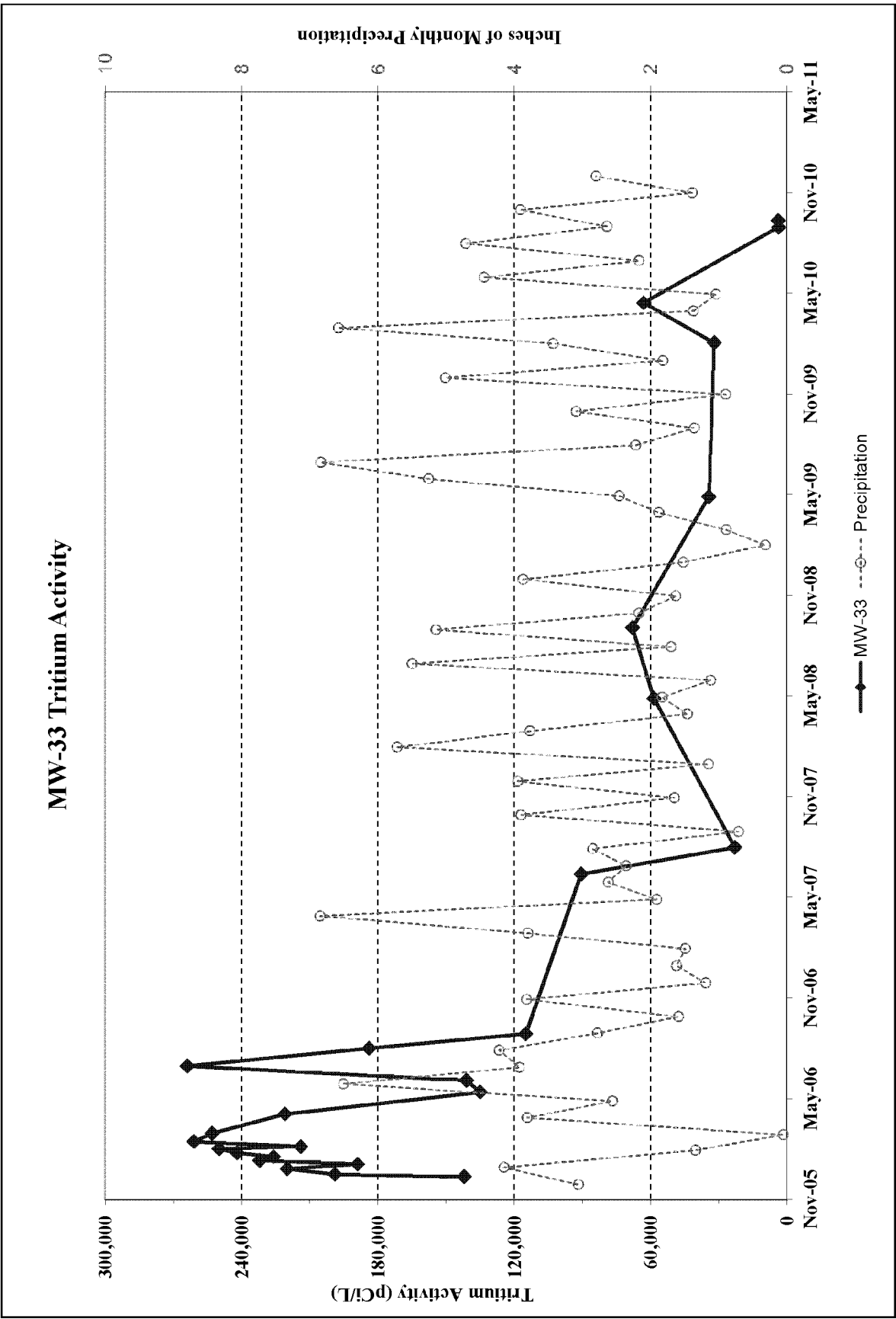


FIGURE G4

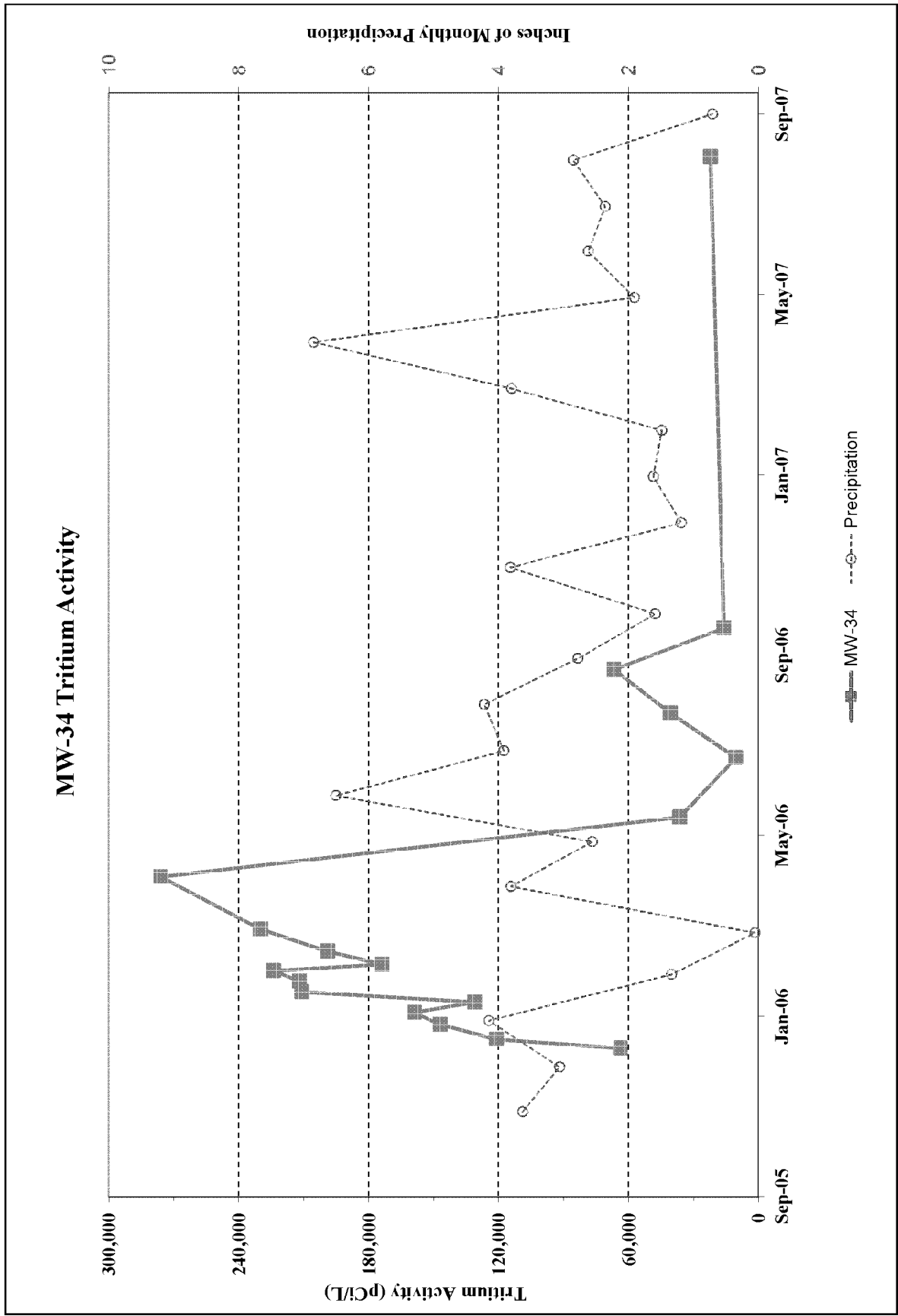


FIGURE G5

MW-35 Tritium Activity

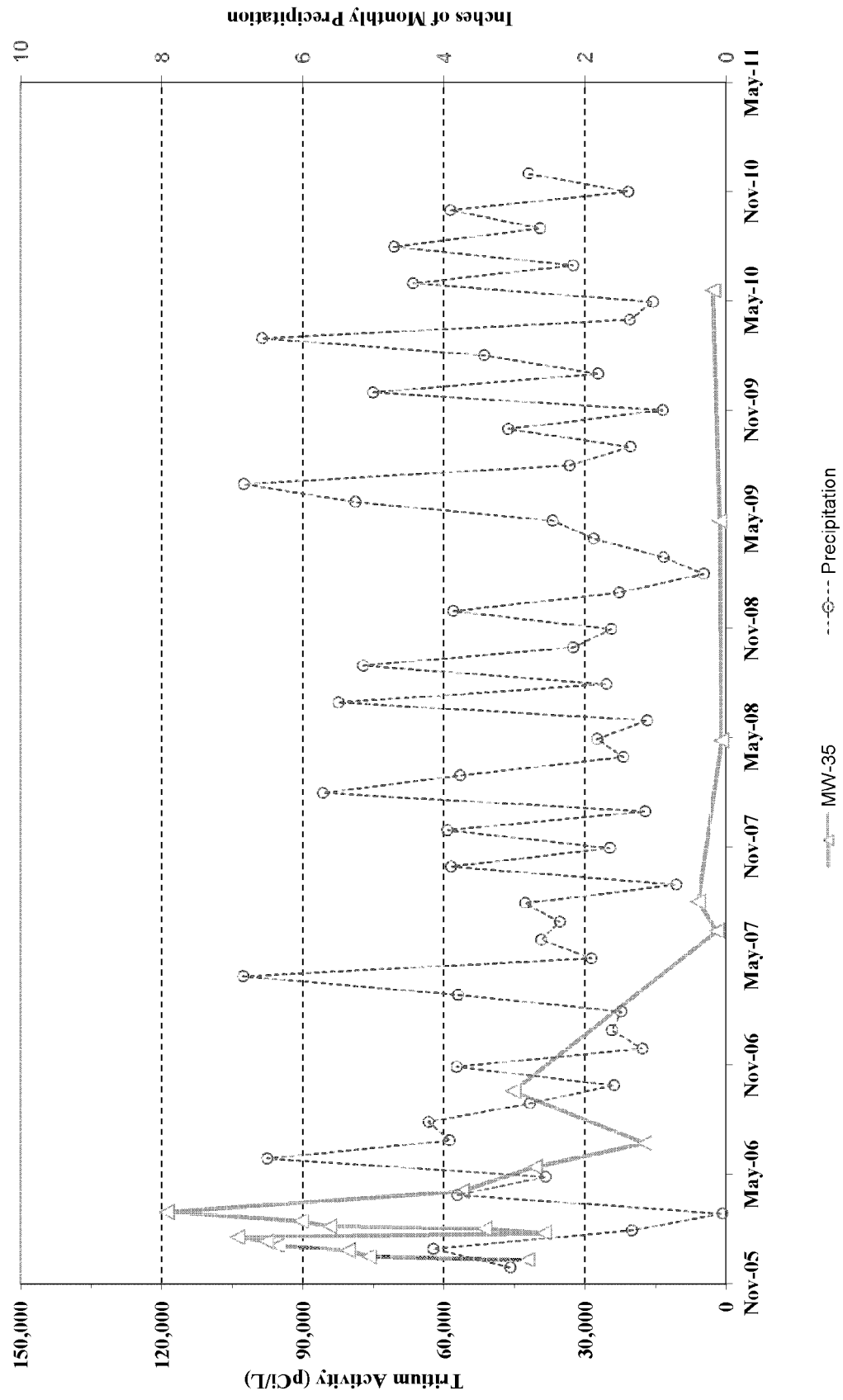


FIGURE G6

MW-36 Tritium Activity

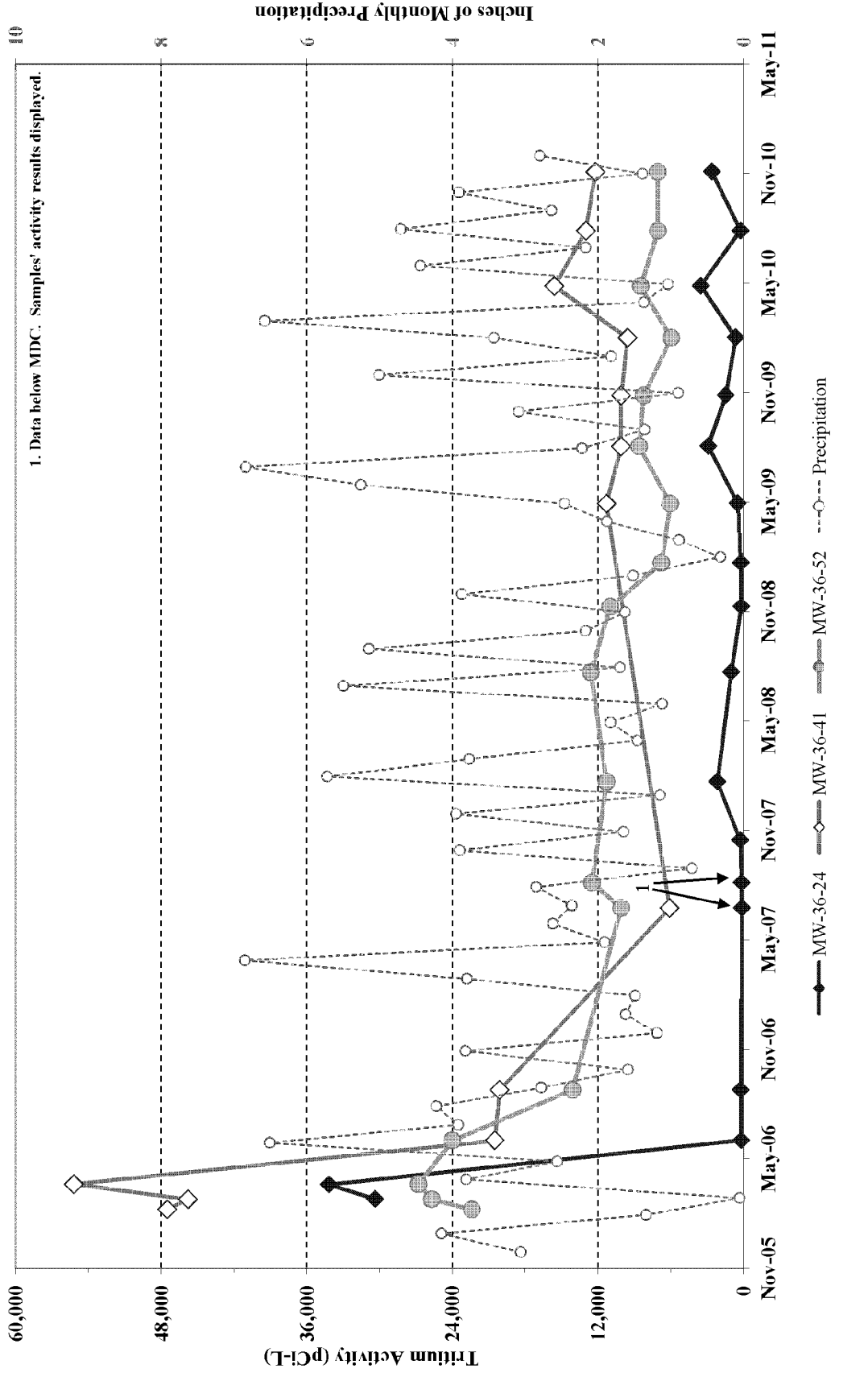


FIGURE G7

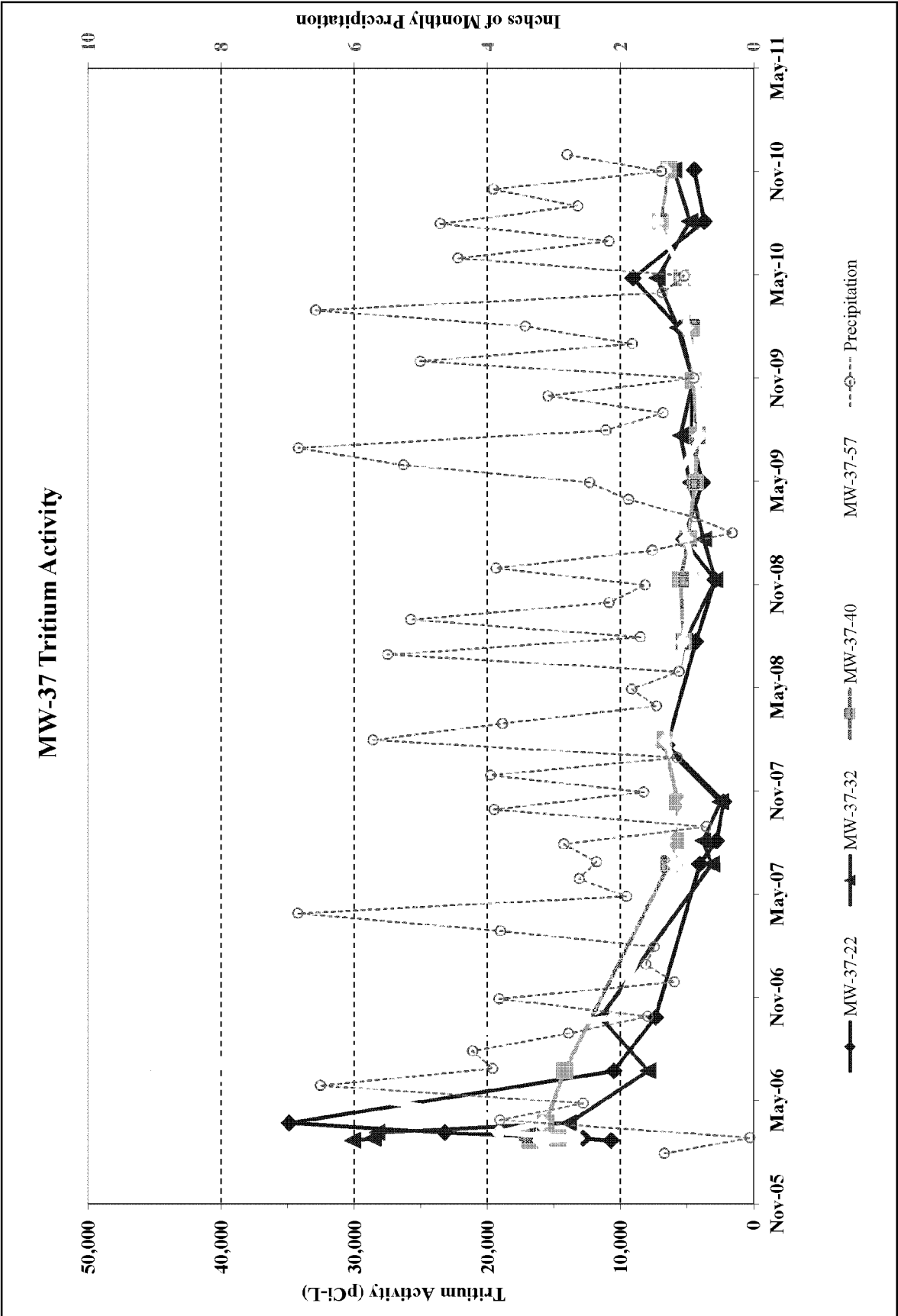


FIGURE G8

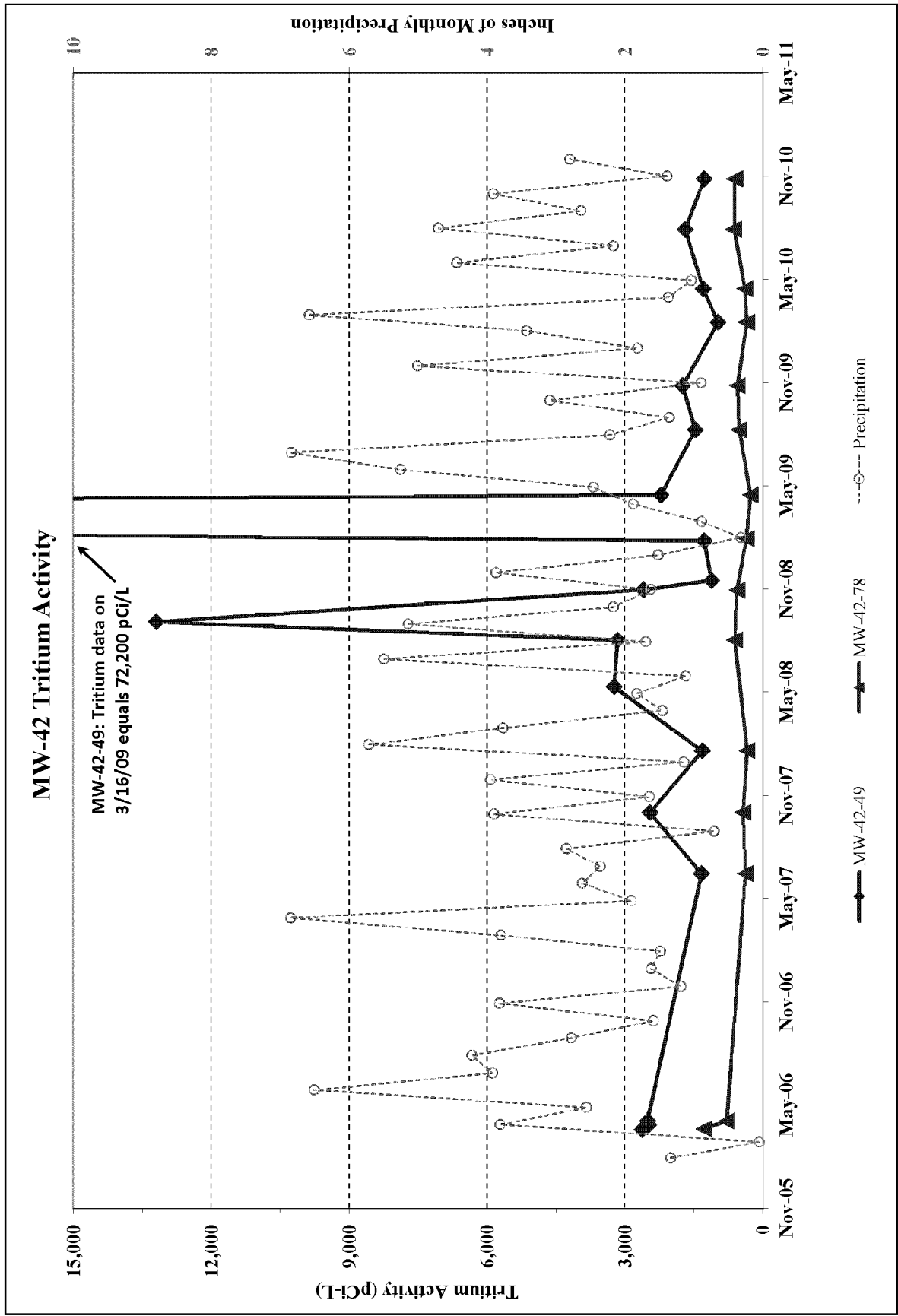


FIGURE G9

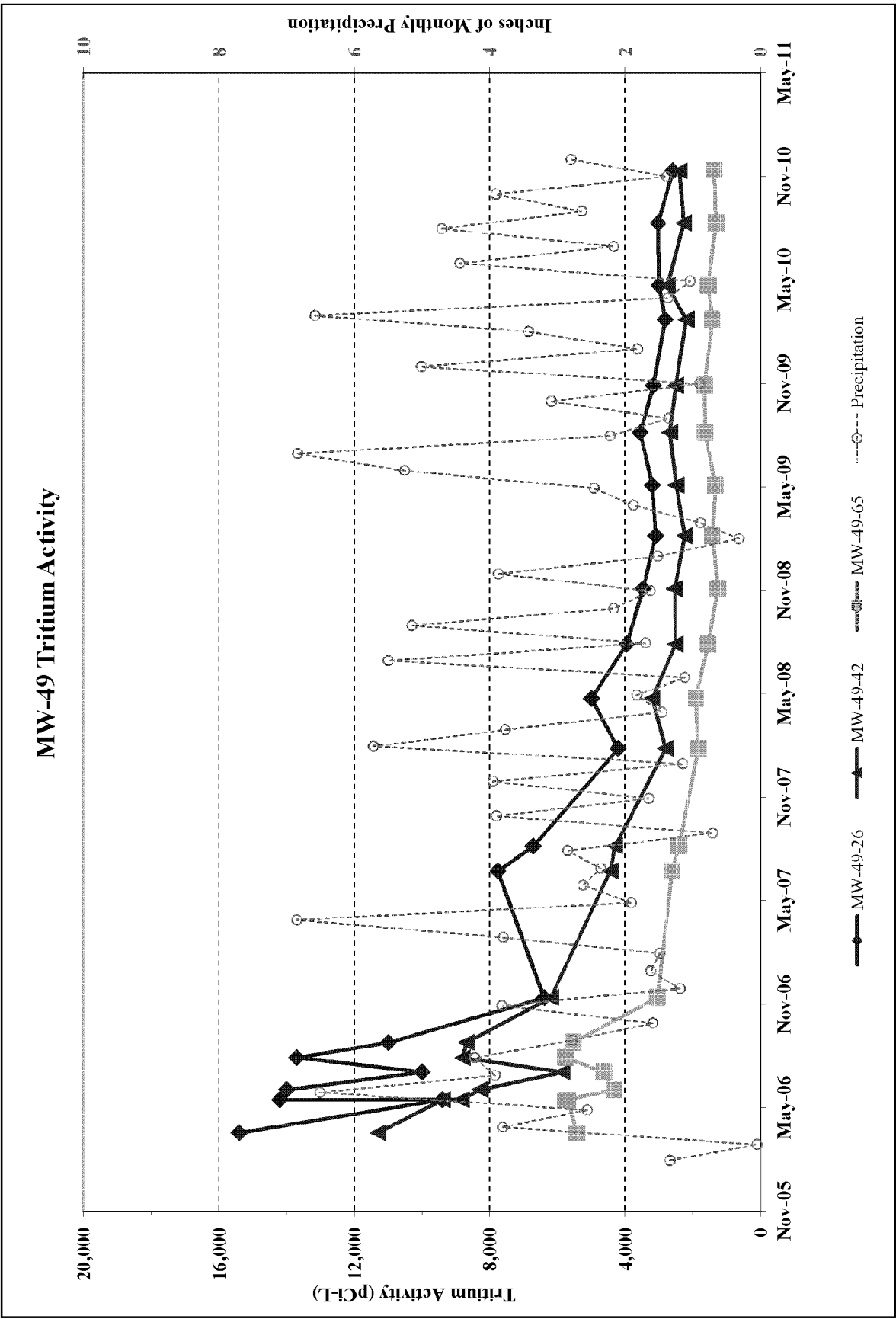


FIGURE G10

MW-50 Tritium Activity

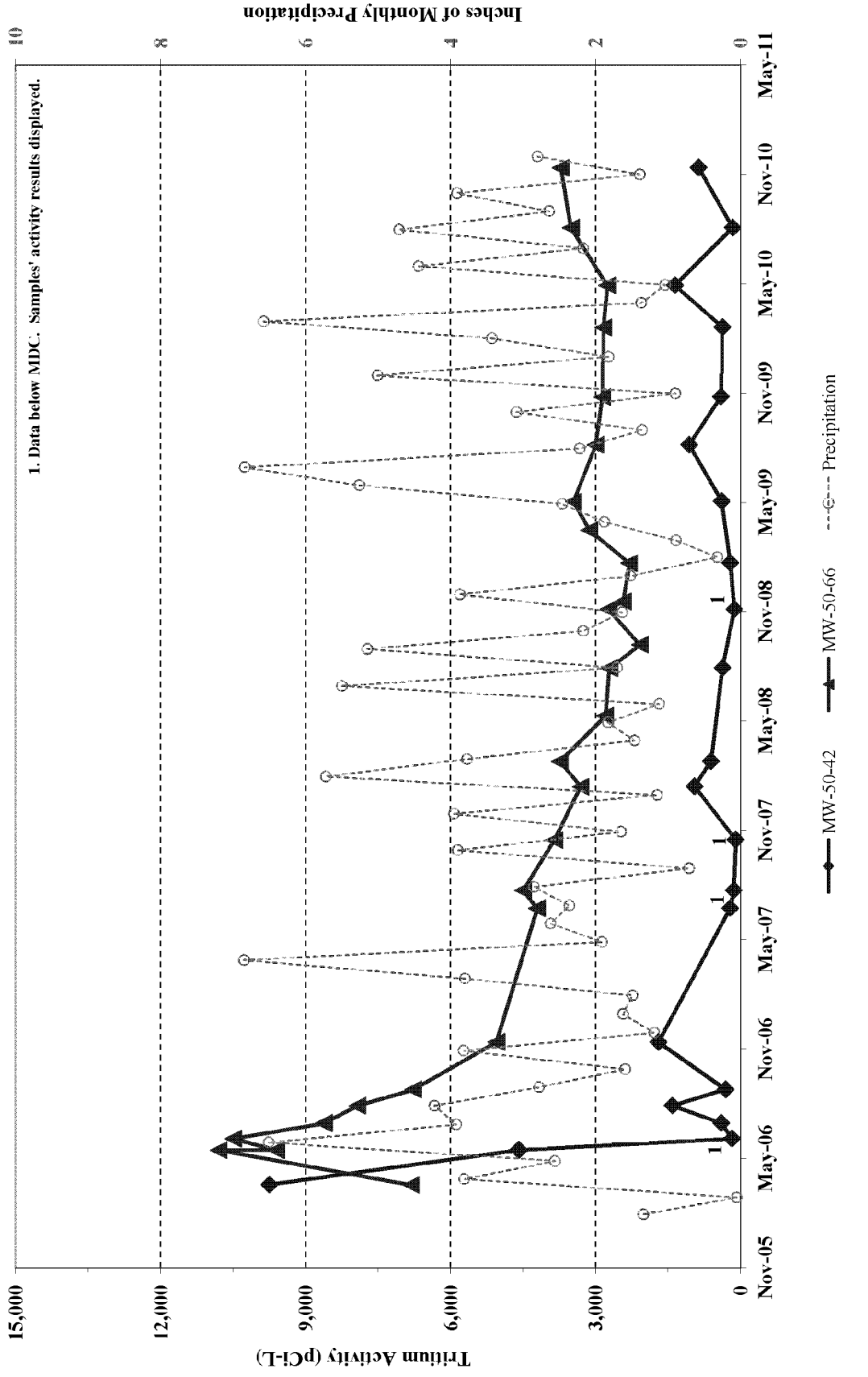


FIGURE G11

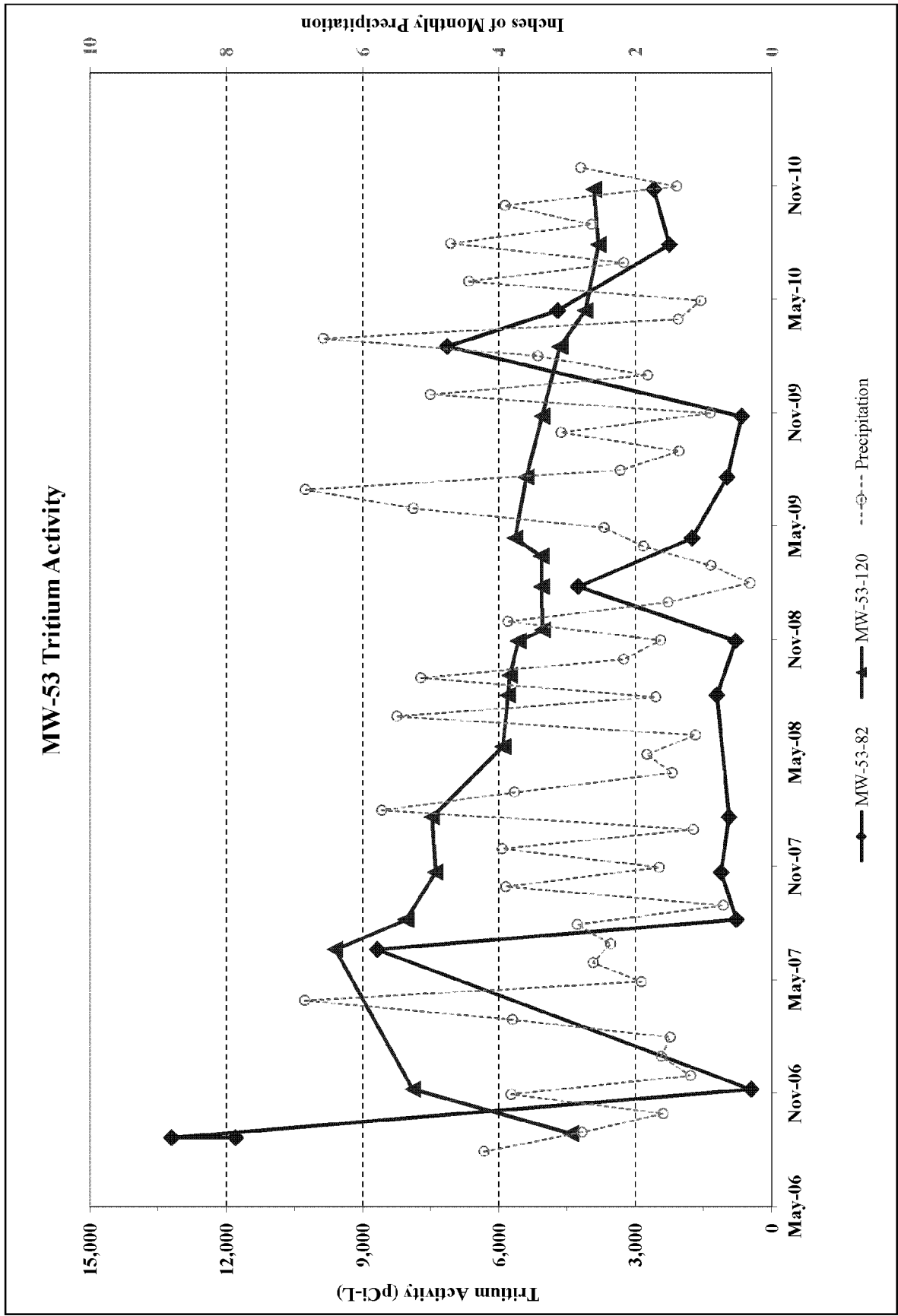


FIGURE G12

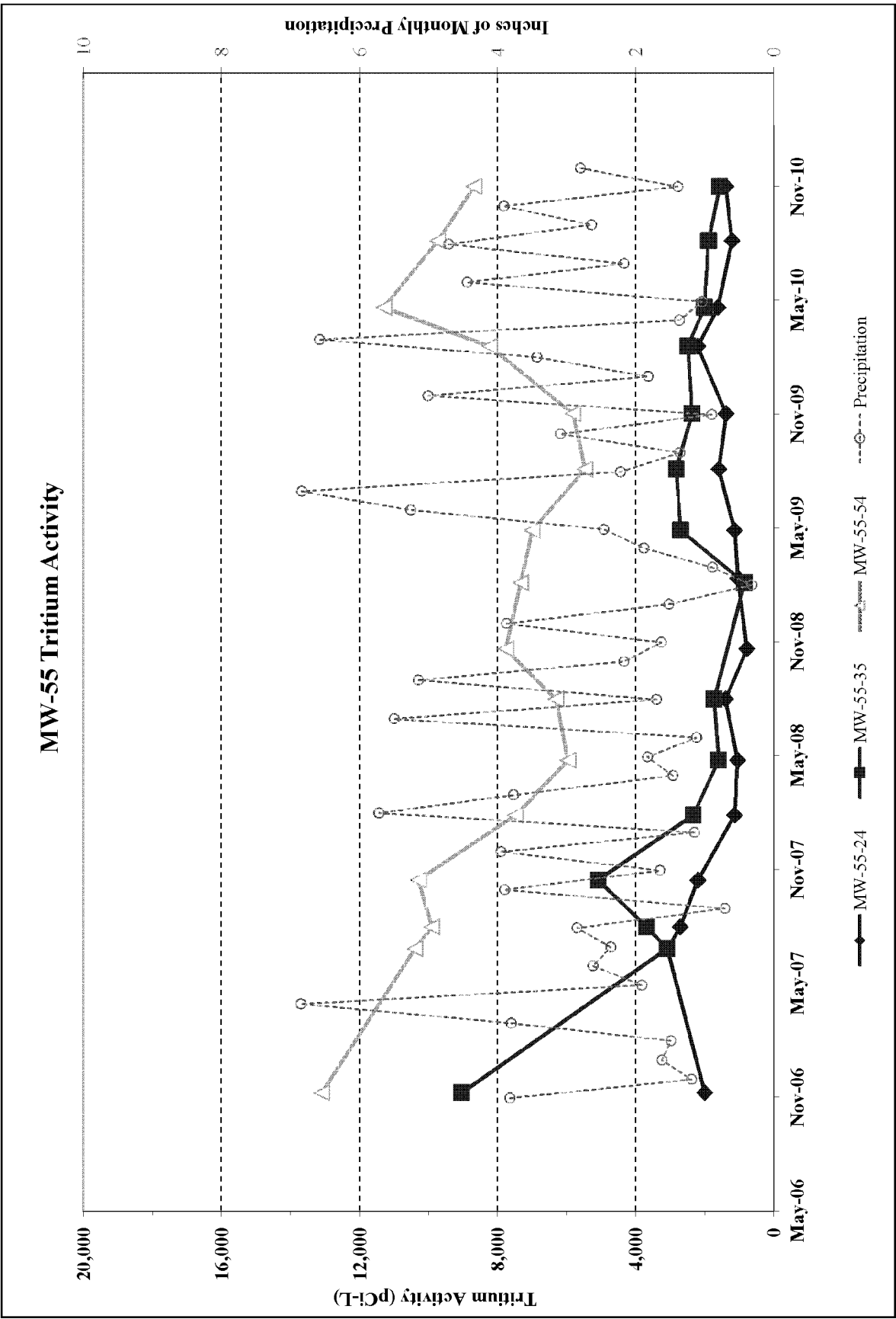


FIGURE G13

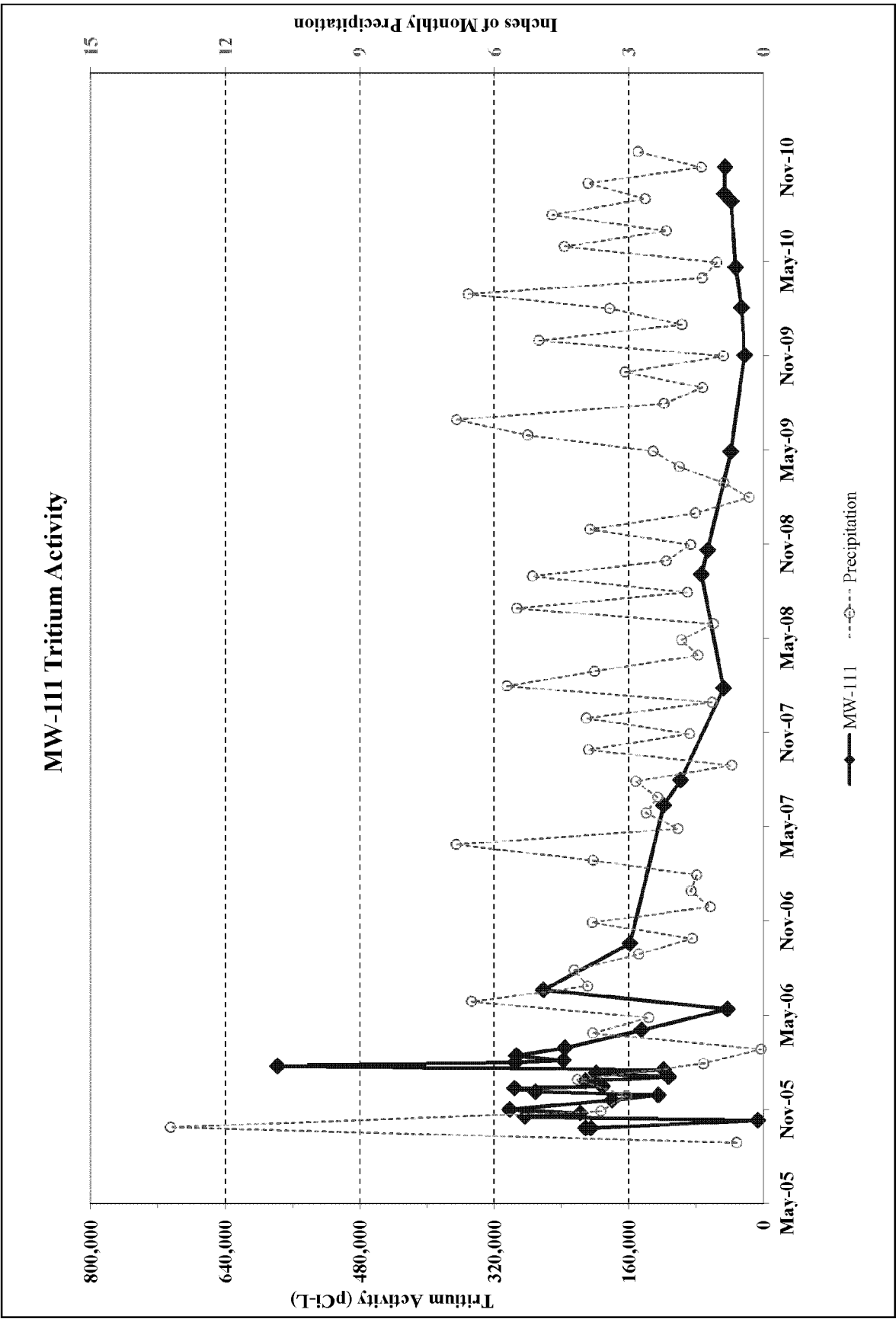


FIGURE G14

MW-66 Tritium Activity

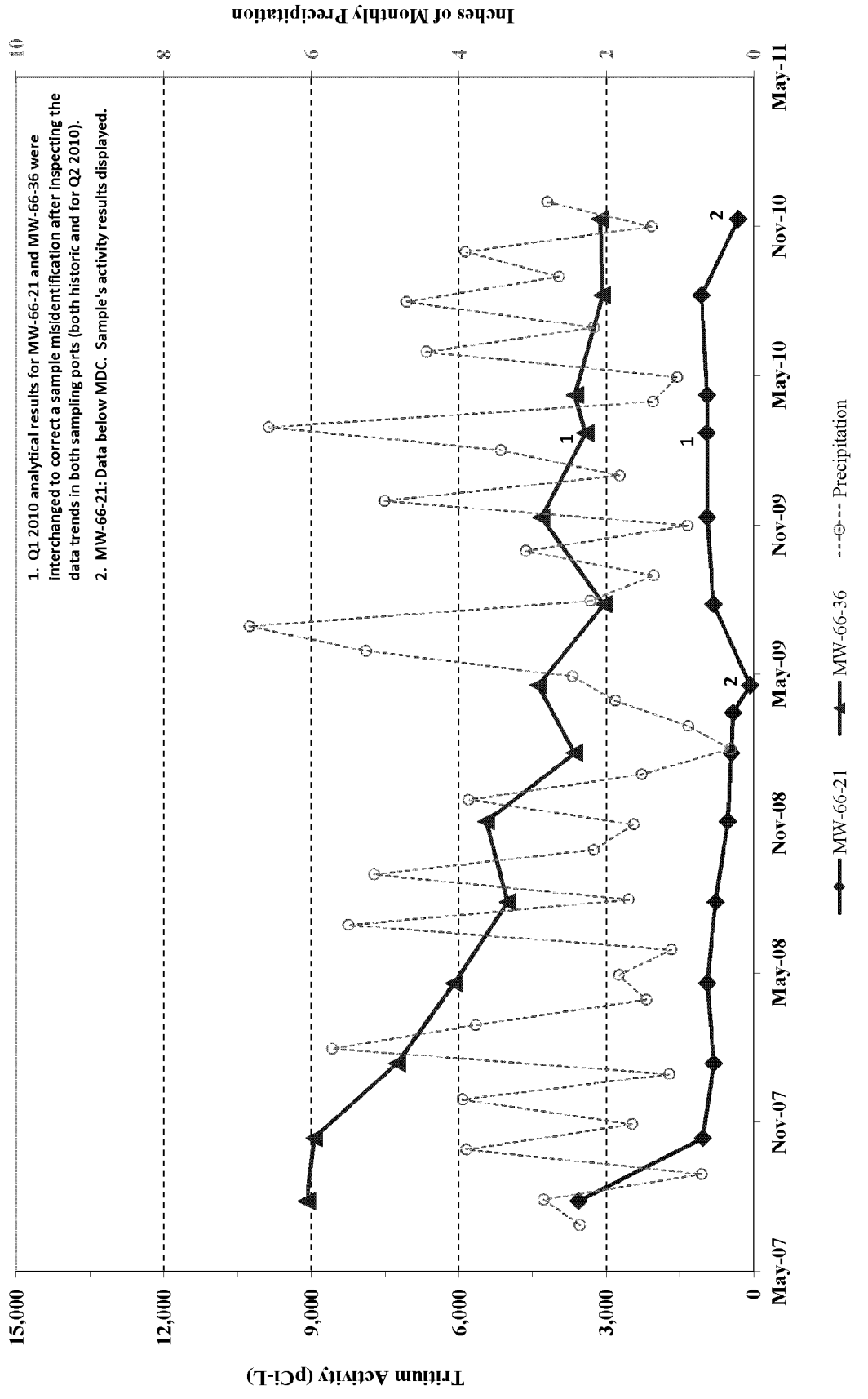


FIGURE G15

MW-67 Tritium Activity

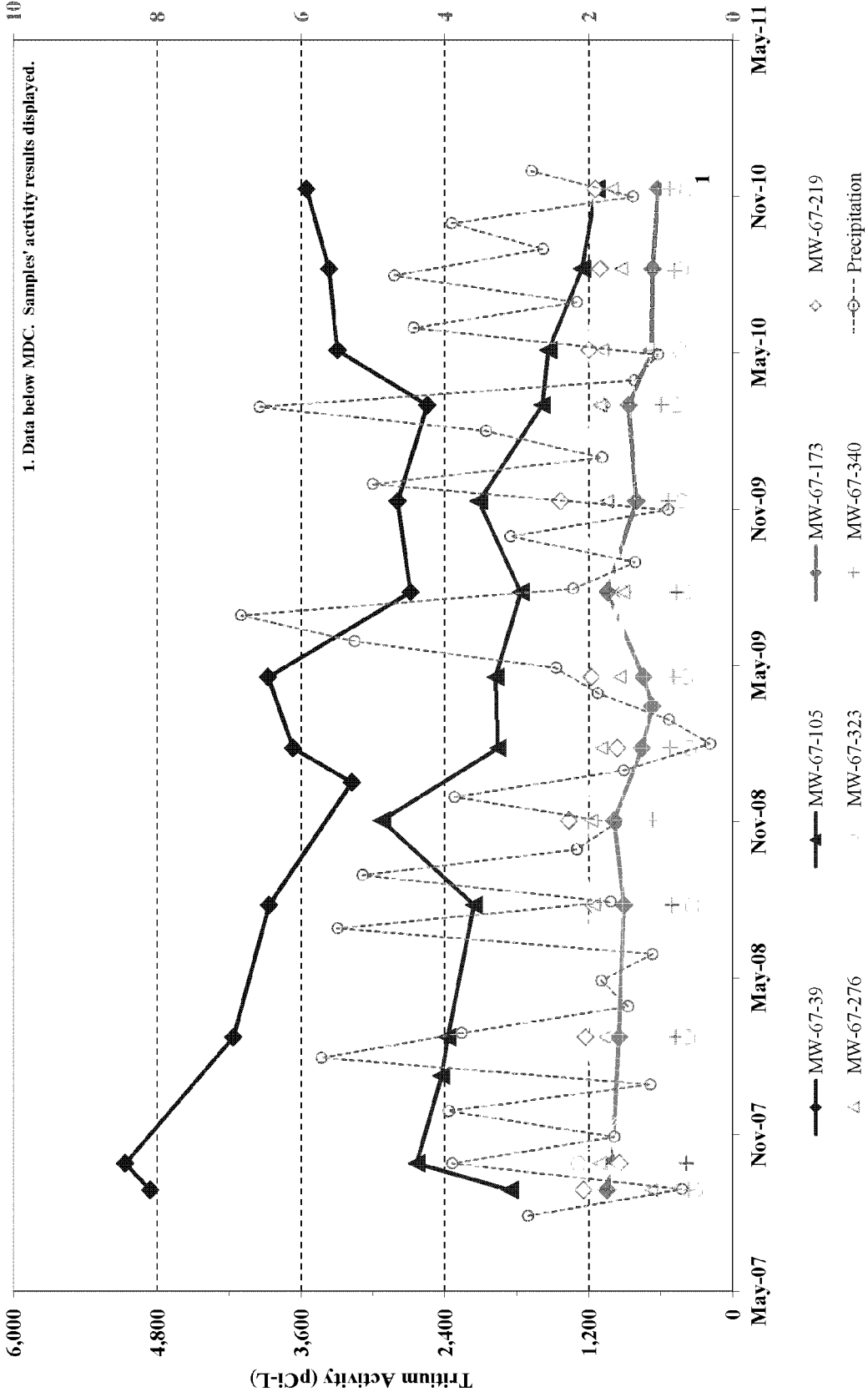
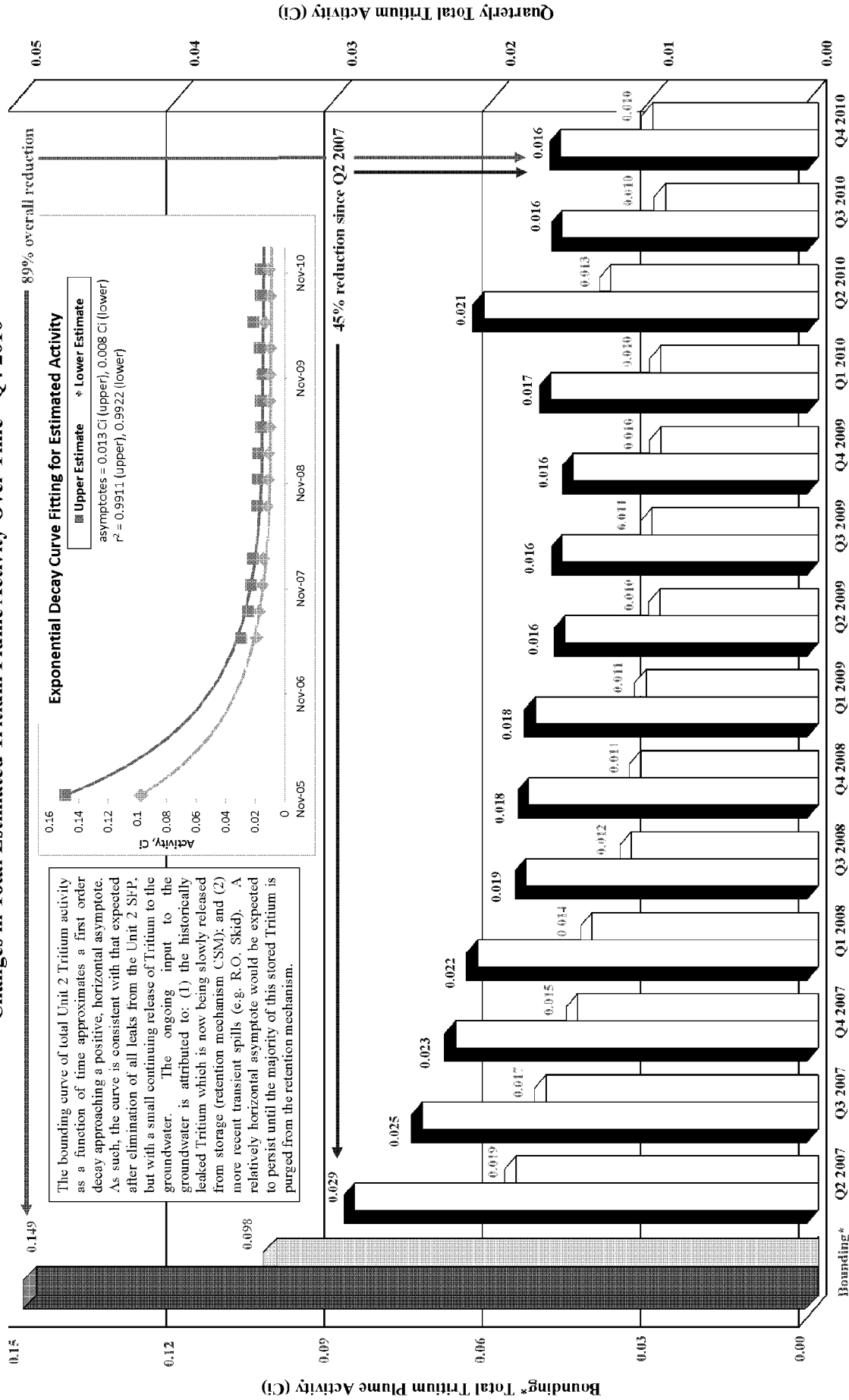


FIGURE G16

Changes in Total Estimated Tritium Plume Activity Over Time - Q4 2010



The bounding curve of total Unit 2 Tritium activity as a function of time approximates a first order decay approaching a positive, horizontal asymptote. As such, the curve is consistent with that expected after elimination of all leaks from the Unit 2 SFP, but with a small continuing release of Tritium to the groundwater. The ongoing input to the groundwater is attributed to: (1) the historically leaked Tritium which is now being slowly released from storage (retention mechanism CSM); and (2) more recent transient spills (e.g. R.O. Skid). A relatively horizontal asymptote would be expected to persist until the majority of this stored Tritium is purged from the retention mechanism.

Note: Lower estimate is based on a porosity of 0.003 which was derived from a pumping test conducted in 2006. Upper estimate is based on a porosity of 0.003 derived from an tracer test conducted in 2007. The Q2 2007 to Q4 2010 Tritium plume activity estimates are each based on Tritium levels measured in the groundwater monitoring installations at individual quarterly "snapshots" in time. *The bounding activity estimate, however, encompasses a longer period of time, and is based on the Tritium levels existing during the earliest portions of the groundwater investigation. During this period of time, before termination of all the identified SFP leaks, Tritium concentrations were at their highest levels, but the network of monitoring installations was still being installed. Therefore, measurements made at a multiple times were required to capture early data covering the full extent of the Tritium plume, primarily over the period from Nov 2005 through Nov 2006 (a smaller percentage of the Tritium levels required inclusion of measurements through Sept 2007). For the bounding Tritium plume activity estimate, the highest value recorded for each monitoring location during this time period was used in the analysis. For further discussion see Sections 6.0, 7.0 and 8.0 of the Final Hydrogeologic Site Investigation Report, prepared by GZA and dated January 7, 2008.

Figure G-17



APPENDIX H: SOUTHERN BOUNDARY WELLS

TEMPORAL TRITIUM TRENDS IN SOUTHERN BOUNDARY WELLS

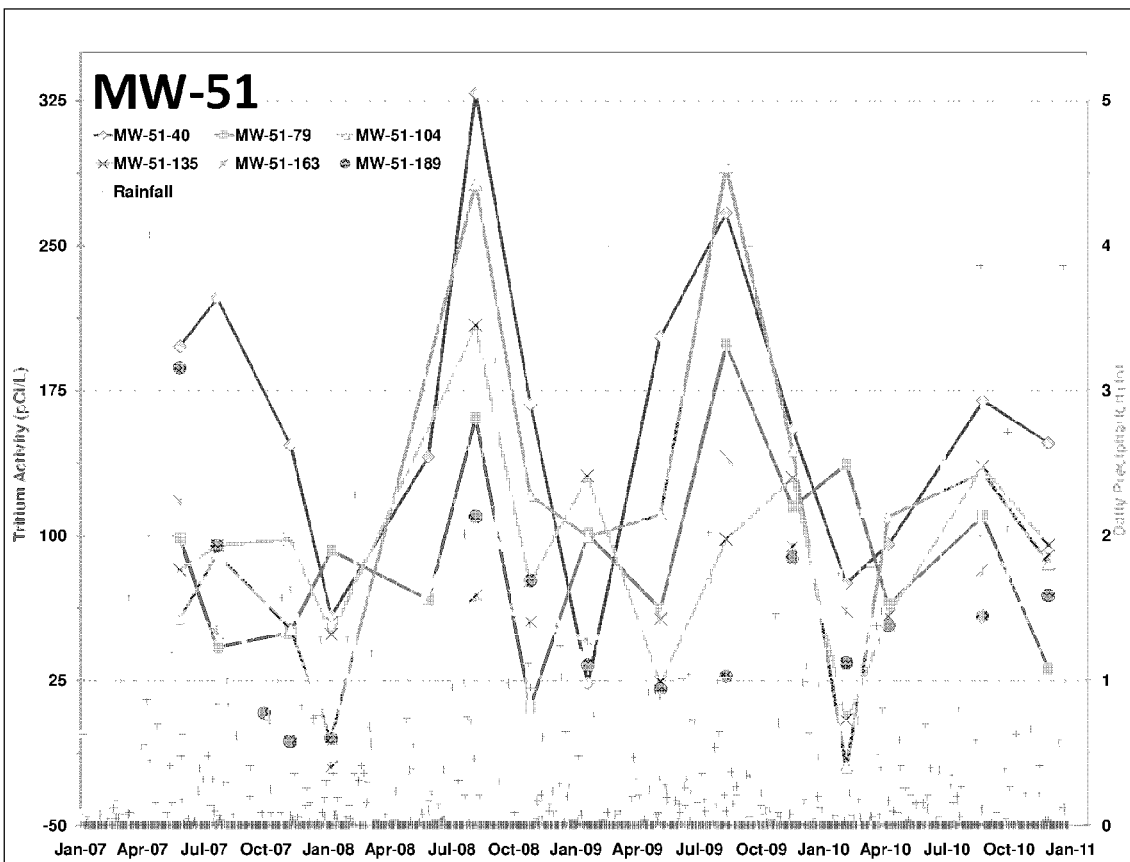
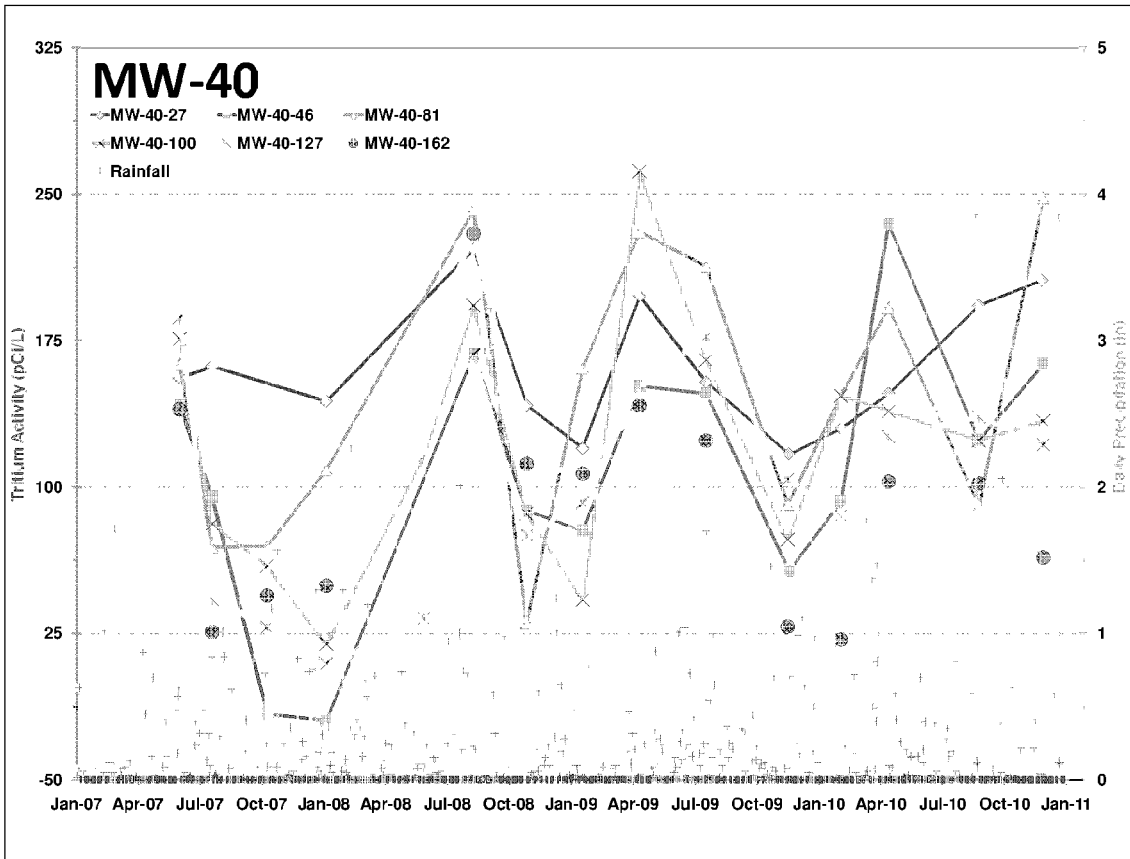


FIGURE H1